UNCLASSIFIED

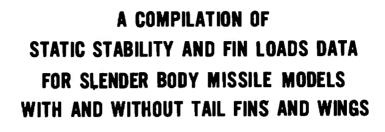
AD NUMBER ADB010054 LIMITATION CHANGES TO: Approved for public release; distribution is unlimited. FROM: Distribution authorized to U.S. Gov't. agencies only; Test and Evaluation; MAR 1976. Other requests shall be referred to Air Force Armament Laboratory, ATTN: AFATL/DLMA), Egling AFB, FL 32543. **AUTHORITY** USADTC ltr dtd 10 Dec 1979

AEDC-TR-75-125 AFATL-TR-76-23

ARCHIVE COPY

cy.

axaaxaa



VOLUME II

(APPENDIXES A THROUGH E)
(TESTS NUMBER 1 THROUGH 5)

PROPULSION WIND TUNNEL FACILITY
ARNOLD ENGINEERING DEVELOPMENT CENTER
AIR FORCE SYSTEMS COMMAND
ARNOLD AF STATION, TENNESSEE 37389

March 1976

Final Report for Period March 1968 - March 1973

Distribution limited to U.S. Government agencies only; this report contains information on test and evaluation of military hardware; March 1976; other requests for this document must be referred to Air Force Armament Laboratory (AFATL/DLMA), Eglin Air Force Base, Florida 32543.

Property of L. S. Mar Force ADDC CHRIST F40000-70-0-0001

Prepared for

AIR FORCE ARMAMENT LABORATORY (AFATL/DLMA)
EGLIN AIR FORCE BASE, FLORIDA 32543



NOTICES

When U. S. Government drawings specifications, or other data are used for any purpose other than a definitely related Government procurement operation, the Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise, or in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

Qualified users may obtain copies of this report from the Defense Documentation Center.

References to named commercial products in this report are not to be considered in any sense as an endorsement of the product by the United States Air Force or the Government.

APPROVAL STATEMENT

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

hu & Taylor

JOHN R. TAYLOR

Analysis & Evaluation

Division

Directorate of Test

CRAIG E. MAHAFFY

raig & Madaffy

Colonel, USAF

Director of Test

UNCLASSIFIED

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AEDC-TR-75-125 AFATL-TR-76-23	SION NO. 3 RECIPIENT'S CATALOG NUMBER
4 TITLE (and Subtitle) A COMPILATION OF STATIC ST BILITY AND FIN LOADS DATA FOR SLENDER MISSILE MODELS WITH AND WITHOUT TAIL I	BODY Final Report - March
AND WINGS - VOLUME II (APPENDIXES A (Continued)	6. PERFORMING ORG. REPORT NUMBER
G. R. Gomillion, ARO, Inc.	8 CONTRACT OR GRANT NUMBER(a)
PERFORMING ORGANIZATION NAME AND AODRESS Arnold Engineering Development Center	10. PROGRAM ELEMENT PROJECT, TASK AREA & WORK UNIT NUMBERS
Air Force Systems Command Arnold Air Force Station, Tennessee 37	Program Element 62201F
11. CONTROLLING OFFICE NAME AND ADDRESS	12. REPORT DATE
Air Force Armament Laboratory (AFATL/I Eglin Air Force Base, Florida 32543	OLMA) March 1976 13. NUMBER OF PAGES 618
14 MON'TORING AGENCY NAME & ADDRESS(II dillerent from Controlling	Office) 15 SECURITY CLASS. (of this report)
	UNCLASSIFIED
	15. OECLASSIFICATION DOWNGRADING SCHEDULE N/A
tion of military hardware; March 1976 document must be referred to Air Force DLMA), Eglin Air Force Base, Florida 17 DISTRIBUTION STATEMENT (of the ebatract entered in Block 20, 11 de	e Armament Laboratory (AFATL/ 32543.
18 SUPPLEMENTARY NOTES	
Available in DDC; complete report cons	
19 KEY WORDS (Continue on reverse elde il necessary and identity by blo Martin Generalized Research Model si	ck number) Lender bodies
tables (data) si	tatic stability
8	ins
	erodynamic loading ontrol surfaces (Cont'd)
20 ABSTRACT (Continue on reverse side it necessary and identify by bloc This document contains a compilation of Martin Generalized Research Model, wh:	k number) of aerodynamic data for the

presented in tabulated and plotted form for a Mach number range

UNCLASSIFIED

4. TITLE (Continued)

THROUGH E) (TESTS NUMBER 1 THROUGH 5)

19. KEY WORDS (Continued)

deflection transonic flow supersonic flow wind tunnel tests

20. ABSTRACT (Continued)

from 0.20 to 4.63 over an angle-of-attack range from -6 to 60 deg and a sideslip angle range from -20 to 20 deg for the body-alone configurations, body-wing configurations, and the body-wing-tail fin configurations. In addition, the tail fin configurations were tested using the reflection plane technique, and the resulting fin loads data are presented for a Mach number range of 0.80 to 2.16 over an angle-of-attack range from 0 to 210 deg. Volume II contains the tabulated data obtained during Tests Number 1 and 2 at AEDC and Tests Number 3, 4, and 5 at NASA Langley Research Center.

AFSC Arno 4 AFS Tenn

PREFACE

The data presented herein were compiled by the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC), under the sponsorship of the Air Force Armament Laboratory (AFATL), Eglin Air Force Base, Florida. Seven different tests were conducted by three organizations: ARO, Inc. (a subsidiary of Sverdrup & Parcel and Associates, Inc.), contract operator of the AEDC, AFSC, Arnold Air Force Station, Tennessee; Naval Ship Research and Development Center (NSRDC), Bethesda, Maryland; and Langley Research Center (LRC), National Aeronautics and Space Administration (NASA), Langley Air Force Base, Virginia. The data were compiled under ARO Project No. P34A-37A. The author of this report was G. R. Gomillion, ARO, Inc. The manuscript (ARO Control No. ARO-PWT-TR-75-88) was submitted for publication on June 20, 1975.

This volume contains the tabulated data that were obtained during (1) Tests Number 1 and 2 that were conducted in the Aerodynamic Wind Tunnel (4T) at AEDC during December 1970 and May 1972, respectively, and (2) Tests Number 3, 4, and 5 that were conducted in the Unitary Plan Wind Tunnel (UPWT) at NASA Langley Research Center during March 1968, April 1970, and July 1971, respectively. As an aid in the use of these data, tables that list the part numbers for the tabulated data from Tests Number 1 through 5 and the general list of nomenclature are repeated from Volume I at the end of this volume.

APPENDIX A TEST 1

ĕΕ	ENGINEE 1 OF 1 1 OF 1		LOPHENT			ROPULSION MARTIN MI	HIND TUN	NEL FACILIT	IY(PWT) _ DATA -	AER		1NO TUNNEL (4 <u>T)</u>
	TEST	PART MAC	P.10-6	PHI 0.0	CONF Made 12 0	L DEL	DEL2	DEL3 DEL .	TRANSITI	DN	:	
INT"	ÄLPHA	OF TA	CN	CLM	CA	CLN	CLL	CA	CAB	CAF	ACP .	
1	-0.00				-0.0792	0.0919	0.0003	0.2532	0.0970		-2.8852	
5	1.99			-0.7170		0.0862	-0.0015	0.2604	6.0987	0.1617	-2.2637	•
3 .	3.44		0.6359	-1,4537		0.0439	-0.0015	0.2655	0.1057	0.1597	-Z.2660	
6	5.97 7.98		0.9856 1.3572	-3.1644		0.0861	-0.0032	0.2013 0.2981	0.1124 0.1154	0.1669	-2.30 69 -2.3440	•
6	9.98		1.7206			0.0600	-0.00R5	0.3192	0.1283		-2.3421	
7	11.96		2.1170	-4.6762		0.0596	-0.0066	0.3286	0.1461		-2.3128	•
8	13.96		2.5000	-5.6443		0.0768	-0.0065	0.3348	0.1578	0.1770	-2.2570	
9	15.90	-0.0u	CLHA.S	-0.2580	-G.01-1	0.0954	-0.0049	0.3365	0.1651	0-1714	-2.1702	
10	17.04		3.0276	-6.2964	-0.6152	0.1006	-0.9952	0.3325	0.1605	0.1640	-Z.0797	
11	18.00	-	3.2007	-6.5009		0.0736	-0.0129	0.3430	0.1753	0.1678	-2.0510	
15	19.03		3.4277	-		0.0805	-0.0131	0.3501	0.1849		-2.0295	
13	20.02		3.6427	-7-2512		0.0431	-0-0191	0.3530	0.1906	0.1623	-1.9906	
16	21.05		3.63.9	-7.5622		0.0363	-0.0250 -0.0140	0.3522 0.3575	0.2015 0.2092	0.1507	-1.9561	
15 16	23.00		4.3725	-A.1643		0.0000	-0.0037	0.3554	0.5505	0.1484	-1.9292	
17	20.11			-8.2636		0.0104	0.0123	0.3535	0.2256	0.1200	-1.8475	
18	25.16			-8.1462		-0.0253	0.0-0-	0.3522	0.2438	0.1084	-1.7948	
14	26.10			-4.3984		-0.0640	0.0899	0.3536	0.2587	0.0949	-1.7477	
20	27.18		5.0284	-H.5453			C-1-01	0.3590	0.2760	0.0811	-1.6994	
21	28.17	0.01		-0.023-			0.1451	0.3586	0.2960	0.0626	-1.6736	
22	29.15	0.01.		-4.0646			0.1477	0.3497	0.3102		-1.6386	
23	29.16			-9.0457		-0.5310	0.1570	0.3447	0.3316		-1.6488	
24	30.21	0.05	567514	-9.2423	0.3173	-0.6633	0.1623	0.3295	0.3315	-0.0020	-1.6070	
											····	
		,										
										h		
										-		
							 ,					
												

	TEST		CH RX10-		CONF	L. DEL	1 DELS	DEL3 DEL4	TRANSIT			
		- BETA-			·	CFM	-	cā	CAB		KCP	
		-0.00		-0.1083		0.0840		0.2514	0.0890		-7.4762	
	1.99	-0.00		-0.7600		U.0803	-0.0063	0.2566	0.0991	0.1574	-2.2541	
•	3.96	-0.0u		-1.6764		0.0406	-0.0076	0.2614	0.1075	0.1539	7504-5-	
	5.98	-0.00		-2.6632		0.0816	-0.0091	0.2742	0.1195	0.1547	-2.4737	
_		-0.00		-3.7503		0.0646	-0.0059	0.3018	0.1262		-7,5178	
		-0.00		-3.7e37	-0.0119	0.0737	-0.0120	0.3035	0.1244		-2.5377	
	9.98	-0.31.			-0.0042	0.0742	-0.01B4	0.3349	0.1386		-2.5073	
	1.93	-0.01			-0.0043	0.0743	-0.0233	0.3470	0.1581	0.1886	-2.4594	
	3.96	-0.01	2.7311		-0.0006	0.0326	-0.0233	0.3469	0.1635		-5-3067	
		-0.01		-7.2062	-0.0037	0.130A	-0.0096	0.3494	0.1682		-2.3103	
		0.01_		-7.4029	-0.0312	0.2579	0.0143	0.3548	0.1722		-2.2350	
		-0.01		-7.5056 -7.6643	0.0160	0.2090 0.0835	-0.0113	0.3581 0.3628	0.1916	0.1461	-2.1661 -2.0989	
	20.05	-0.01		-7.4666	0.0127	0.0192	-0.0337	0.3723	0.2313	0.1410	-2.0472	
		-0.01		-6-1461	0.0180	0.0172	-0.025	0.3858	0.2430	0.1428	-5.0065	
		-0.01		-8.2823	0.0095	0.0554	-0.0143	0.3601	0.2612	0.1189	-1.9462	
		-0.01		-6.3776	0.0057	0.0837	-0.0096	0.3860	0.2761		-1.8799	
		-0.01	4.4418	-8.4436	0.0008	0.0986	-0.0017	0.3693	0.2903	0.0990		
		-0.01		-6.4900	-0-0064	0.1736	-0.0055	0.3846	0.3656		-1.7476	
	26.20	-0.01	. 5.0646		-0.0202	0.1767		0.3752	0.3217		-1.6925	
		-0.01	5.3600		0.0561	0.0391	0.0421	0.3614	0.3316	0.0296	-1.5985	
		-0.0i		-9.4536	0.0661	0.0171	0.0359	0.3429	0.3353		-1.5011	 -
		-0-01		-8.4045	0.1111		0.0587	_ 0.3312	0.3499		-1.4153	
	30.36	-0.01	6.1796	-8.4184	0.0816	0.0034	0.0448	0.3114	0.3551	-0.0438	-1.3623	
_												
				•								
_		· · · · · · · · · · · · · · · · · · ·			•							
			-									•

1E		4CM RX10- 64 2.3		CONF CONF CONF CONF CONF		O O	DEL3 DEL4 0 0			· · ··	
INT " ALPH	META	CN	CLH	CY	CLN		CA	CAR	CAF	XCP	
	0.00		-0.1351			-0.0190	0.7656	0.1054		-2.5959	
5 5-0		4545.0	-0.6554		0.10-9	-0.0206	0.2711	0.1045	0-1667		
33.9 4. 5.9			-1.6448	-0.0235		-0.0204	0.2686 0.2848	0.1104 0.1100		-2.3476 -2.4503	
5 7.9			-3.7095		0.1013	-0.0200	0.3085	0.1363		-2.4951	
	5 -0.01		-4.1-12		0.1016	-0.0276	0.3355	0.1518		-2.4992	
7 11.9		2.3180	-5.7034	-0.0135	0.1056	-0.0339	0.3541	0.1640	0.1901	-2.4605	
	5 -0.01	2.7495			0.1064	-0.0339	0.3549	0.1769	0.1781	-2.3934	
9 15.9	7 -0.01	3.1593	-7.2954	-0.0010	0.1479	-0.0240	0.3608	0.1683		-2.3093	
	0.01		-7.6671	-0.0023	0.1386	-0.0209	0.3696	8065.0		-2.2658	· . — - ·
	9 -0.01	_	-7.617.	-0.0081	0.1635	0.0050	0.3737	0.2156		-2.2084	
	1 -0.01		-7.4442	-	0-1491	-0.02+8	0.3743	0.2407		-2.1323	
	-0.01		-A.0263	0.0071	0.0747	-0.0438	0.3899	0.2455		-5-0555	
	6 -0.01		-8.3924		0.0634	-0.0-11	0.3966	0.2795		-2.0037	
	8 -0.01 2 -0.01		-6.4452	C.0157	0.0552	-0.0333 -0.0290	0.4050	0.2792		-1.9423	
	7 -0.01	4.7627			0.1130		0.3483	0.3042	0.0941		
	9 -0.01	4.9900	-6.4651		0.1223	-0.0255	0.3921	0.3172		-1.6964	
	3 -0.01		-6.4361	0.0022		-0.0135	0.3807	0.3317		-1.6095	
20 27.		5.5334	-0.4011	0.0527	0.0204	0.0143	0.3659	0.3407		-1.5143	
21 28.3	6 -0.01	5.8931	-6.3060	0.1091	-0.0945	0.0309	0.3557	0.3393	0.0165	-1.4098	
	≥ -0.0u		-8.2792	0.1752	-0.2415		0.3368			-1.3366	
	7 -0.00		-6.2783		-0.2765	0.0463	0.3181	0.3629		-1.2756	
24 0.0	0 -0.01	0.0716	-0.1511	-0.0306	0.1284	-0.0396	0.3017	0.1122	0.1895	-2.1109	
											
				· · · ——							
	<u> </u>		_								

6E	1 OF 1					MARTIN M	ISSILE TA	NEL FACILI	DATA			0 TUNNEL (<u>47)</u>	
	TEST		ACH RX10-6		CONF		1 DEL2	DEL3 DEL4	TRANSIT				
Olnt	ALPHA -	BETA	CN T	ËLM	CY -	CLNT.	CLL	CA	CAB .	CAF	. XCO		
1	0.00	-0.01	• • • •		-0.0316	0.1798		0.3011	0.1137		-2.0566		
2	2.06	-0.01		-0.8966	-0.0269	0.1203	-0.0426	0.2984	0-1200	0.1784	-2.3128		
3	3.94	-0.01	0.7375	-1.7660	-0.0202	0.1125	-0.0439	0.3044	0.1163	0.1861	-2.3947		
4	5.90	-0.01	1.0812	-2.0447	-0.0205	0.1098	-0.0434	0.3125	0.1278	0.1847	-2.4461		
5	7.97	-0.01	1.4768	-3.6280	-0.0166	0.1062	-0.0465	0.3323	0.1425	0.1897	-2.4534		
6	9.95	-0.01		-4:620Y	-U.013A	0.1102	-0.0529	0.3589	0.1535	0.2054	-2.4508		
7	11.95	-0.01		-5.6200	-0.0096	0.1067	-0.0560	0.3450	0.1621	0.2229	-2,4275		
8	13.96	-0.01		-6.5037	-0.0045		-0.0559	0.3853	0.1848	0.2005	-2.3676		
9	15.97	-0-01		-7.2090	0.0047	0.1051	-0.0546	0.3498	0.2054	0.1944	-2.2947	·	
10		-0.01		-7.6015	0.0039		-0.0528	0.4116	0.2132		-2.2436		
11	14.00	-0.01		-7.952,1	0.0096		-0.0516	0.4198	0.2361	0.1837	-5.5033		
15	18.99	-0.01		-8.1854	0.0005		-0.0326	0-4117	0.2590	0.1528	-2.1511		
13		-0.01		-8.2708	0.0706		-0.0610	0.4079	6.2665		-2.0797		
14	21.09	-0.01	4.2127	-6.3446	0.0151		-0.0615	8954.0	0.2637	0.1651	-1.9938		
15 _	22.10	-0-01		-8.4201	0.0025		-0.0603	0.4245	0.2838	0.1407	-1.9156		
16	23.13			-8.5361	-0.0130		-0.0626	0.4157	0.2927	0.1530	-1.8367		
17 18		-0.01	-	-8.5627	0.0266	_	-0.0429	0.4100	0.3028		-1-7581		
19	25.23 26.27	-0.01 -0.01	5.1777 5.0273	-8.5368	0.0519 0.0855		-0.0262 8E00.0	0.4156 0.3980	0.3066	0.0741	-1.64 88 -1.5519		
20	27.32	-0.00		-8.3430	0.1377				0.3403	0.0430	-1.4593		
51	28.42	-0.00	_		0.1134		0.0245		0.3461	0.0166	-1 -3652		
22		-0.01		-8.2585		-0.1255	0.0226		0.3499	0.0067			·
23		-0.02		-8.2319		0.0144			0.3577		-1.2251		
										- 			
						······································							
													
													

`

1 OF 1				•	MARTI- MI	SSILE T	WEL FACILITAL EFFECTS	TY (Put) DATA	AER	ODÁNTHIC TIMB TAMEF (TÍ)
				CONF					D44	
1	14 (-	•	54#0F12	0.9		0 0	- UNKNOWN		
ALPHA .	"BET	CN .	CLM	. CA .	CLN	"CLL"	CA	SAR	CAF	ACP
-0.00		0.0469	-0-1117		0.0836	0-0017	0.3384	0.1433	0-1951	-5.3626
_										-2.3925
										-2.4205
_										-2,4538 -2,4544
										-2.4364
11.96					0.0757	-0.0022				-2,3030
13.96					0.0771	0-0026	0.4360	0.2176	4055.0	-2.3269
15.96						0.0024	0.4466	0-2420		-2.2637
16.99								0.2511	0.2175	-2.1992
										-2-1516
										-2.1073
										-2.0363 -1.9916
	_									-1.8926
										-1.7946
24.20										-1.6999
25.24	-0.0	0 5.3296	-8.5042	0.0390	0.0021	0-0254	0.4300	0.3387		-1.6069
27.36	-0.0	0 5.9702	-8.4652	0.1144	-0.1525	0.0522	0.3934	0.3426	0.0507	-1.4179
29.44									0.0278	
_										
	_									-1.5146
-	_									-1.6929
5.97										-2.4710
1.99	-0.0	0.3815	-0.4160							
-0.00	-0.0	0.0553	-0.1354	-0.0295	0.0956	0.0143	0.3388	0.1366	0.2021	
-0.00	-0.0	0.0553	-0.1354	-0.0295	0.0956	0.0143	0.3386	0.1366	0.2021	-2.4486
	TEST 1 ALPMA -0.00 1.99 3.99 5.99 7.98 9.96 11.96 13.96 15.90 18.01 19.02 20.05 21.08 22.12 23.14 24.20 25.24 27.36 29.44 29.49 30.55 26.30 27.09 18.01	TEST PART 1 14 6 ALPMA BET4 -0.00 -0.01 1.99 -0.00 3.99 -0.00 5.99 -0.00 1.96 -0.00 13.96 -0.00 15.96 -0.00 15.91 -0.0 20.05 -0.0 21.08 -0.0 22.12 -0.0 23.14 -0.0 24.20 -0.0 25.24 -0.0 25.24 -0.0 25.25 -0.0 25.26 -0.0 27.36 -0.0 25.27 -0.0 27.36 -0.0 27.36 -0.0 27.36 -0.0 27.36 -0.0 27.36 -0.0 27.37 -0.0 27.38 -0.0 27.39 -0.0 27.39 -0.0 27.39 -0.0	TEST PART MACH RX10-1 1 14 0.40 2.3 ALPMA BETA CN -0.00 -0.00 0.0469 1.99 -0.00 0.7261 5.99 -0.00 1.0853 7.98 -0.00 1.0853 1.96 -0.00 2.7060 15.96 -0.00 3.1271 16.99 -0.01 3.3500 18.01 -0.01 3.5759 19.02 -0.01 3.8193 20.05 -0.00 4.3011 22.12 -0.00 4.3011 22.12 -0.00 4.5505 23.14 -0.01 4.7444 24.20 -0.00 5.9762 25.24 -0.00 5.9762 29.49 0.00 6.5386 30.55 -0.00 6.8655 26.30 -0.00 5.9762 29.49 0.00 6.5386 27.09 -0.00 4.5434 18.01 -0.00 3.5869 13.96 -0.00 3.5869 13.96 -0.00 1.8723 5.97 -0.00 1.8723 5.97 -0.00 1.8723	TEST PART MACH RX10-6 1 14 0.90 2.3 0.0 6 ALPMA BETA CN CLM -0.00 -0.00 0.0469 -0.1117 1.99 -0.00 0.3697 -0.8845 3.99 -0.00 0.7261 -1.7633 5.99 -0.00 1.0853 -2.6622 7.98 -0.00 1.0853 -2.6622 9.90 -0.00 1.0853 -2.6622 13.90 -0.00 2.7060 -6.3066 15.96 -0.00 2.7060 -6.3066 15.96 -0.00 3.1271 -7.0787 16.99 -0.01 3.3500 -7.3674 18.01 -0.01 3.4759 -7.6939 19.02 -0.01 3.6193 -6.043 20.05 -0.00 4.3011 -8.5670 22.12 -0.00 4.3011 -8.5670 22.12 -0.00 4.5505 -8.6134 23.14 -0.01 4.7444 -8.5240 23.14 -0.01 5.9702 -8.6622 23.14 -0.01 5.9702 -8.5642 27.36 -0.00 5.3296 -8.2595 25.24 -0.00 5.3296 -8.2595 25.24 -0.00 5.3296 -8.2595 26.30 -0.00 5.6618 -8.2595 26.30 -0.00 5.6618 -8.2595 27.30 -0.00 5.6618 -8.2595 27.30 -0.00 5.6618 -8.2595 27.09 -0.00 4.5434 -6.6001 13.90 -0.00 3.5869 -7.7401 13.90 -0.00 1.0905 -2.6946 5.97 -0.00 1.0905 -2.6946	TEST PART MACM RX10-6 1 14 U-VD 2.3 0.0 6440F12 ALPMA BETA CN CLM CY -0.00 -0.00 0.0469 -0.1117 -0.0222 1.99 -0.00 0.3647 -0.8645 -0.0249 3.99 -0.00 1.0853 -2.6622 -0.0265 7.98 -0.00 1.4640 -3.5932 -0.0202 9.90 -0.00 1.8531 -4.5149 -0.0144 11.96 -0.00 2.7080 -6.3066 -0.0129 15.96 -0.00 2.7080 -6.3066 -0.0129 15.96 -0.00 3.1271 -7.0787 -0.0071 16.90 -0.01 3.3500 -7.3674 -0.0024 18.01 -0.01 3.5759 -7.6939 0.0023 19.02 -0.01 3.8193 -6.0463 0.0046 20.05 -0.00 4.3011 -8.5670 -0.0117 22.12 -0.00 4.5505 -8.6134 0.0257 23.14 -0.01 4.7444 -8.5240 0.0326 25.24 -0.00 5.3296 -8.5080 0.0390 25.25 -0.00 5.3296 -8.5080 0.0390 27.36 -0.00 5.3296 -8.5080 0.0390 27.36 -0.00 5.59702 -8.6622 0.1144 28.44 -0.00 6.5336 -8.2595 0.1601 27.09 -0.00 6.5336 -8.2595 0.1601 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5595 0.1601 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0908 27.09 -0.00 5.6618 -8.5750 0.0080	TEST PART MACH RX10-6 PM1 CONF L DEL1 1 14 U.VD 2.3 0.0 8400F12 0.0 0 ALPMA BETA CN CLM CY CLM -0.00 -0.00 0.0469 -0.1117 -0.0222 0.0836 1.99 -0.00 0.3697 -0.8865 -0.0249 0.0637 3.99 -0.00 0.7261 -1.7633 -0.0215 0.0737 5.99 -0.00 1.0853 -2.6622 -0.0205 0.0797 7.98 -0.00 1.4640 -3.5932 -0.0202 0.0692 9.96 -0.00 2.7060 -6.3066 -0.0129 0.0771 13.96 -0.00 2.7060 -6.3066 -0.0129 0.0771 15.96 -0.00 3.1271 -7.0787 -0.0071 0.0729 16.99 -0.01 3.5500 -7.3674 -0.0024 0.0644 15.01 -0.01 3.5759 -7.6939 0.0023 0.0604 19.02 -0.01 3.8193 -d.0463 0.0046 0.0560 20.05 -0.00 4.0509 -8.2569 -0.0017 0.072 21.08 -0.00 4.3011 -8.5670 -0.0117 0.0874 22.12 -0.00 4.5505 -8.6134 0.0257 0.0072 23.14 -0.01 4.7444 -6.5240 0.0326 0.0231 24.20 -0.00 5.3296 -8.5642 0.0390 0.0021 27.36 -0.00 5.3296 -8.5642 0.0390 0.0021 27.36 -0.00 5.3296 -8.5642 0.1144 -0.1525 29.49 0.00 6.5386 -8.2595 0.1641 -0.2690 30.55 -0.00 6.6655 -8.2425 0.104 -0.2690 30.55 -0.00 5.66616 -8.5754 0.0908 -0.1122 27.09 -0.00 5.6655 -8.2425 0.105 -0.2263 26.30 -0.00 5.66616 -8.5754 0.0908 -0.1122 27.09 -0.00 4.5834 -8.6601 0.0213 0.0114 13.96 -0.00 2.7184 -6.3561 -0.0102 0.0779 5.97 -0.00 1.0905 -2.6946 -0.0226 0.0851 1.99 -0.00 0.3815 -0.9160 -0.0256 0.0935	TEST PART MACH RX10-6 PM1 CONF L DEL1 DEL2 1 14 U.90 2.3 0.0 8480F12 0.0 0 0 ALPMA BETA CM CLM CY CLM CVLOP63 0.0017 1.99 -0.00 0.3647 -0.8845 -0.0222 0.0836 0.0017 3.99 -0.00 0.7261 -1.7633 -0.0215 0.0837 0.0052 5.99 -0.00 1.0853 -2.6622 -0.0205 0.0790 0.0054 7.98 -0.00 1.4640 -3.5932 -0.0205 0.0790 0.0054 7.98 -0.00 1.8531 -0.5149 -0.0144 0.0673 0.0059 11.96 -0.00 2.7264 -5.4294 -0.0144 0.0673 0.0099 11.96 -0.00 2.7264 -5.4294 -0.0169 0.0757 -0.0022 13.90 -0.00 3.1271 -7.0787 -0.0071 0.0729 0.0024 15.98 -0.00 3.1271 -7.0787 -0.0071 0.0729 0.0024 16.99 -0.01 3.3500 -7.3674 -0.0024 0.0644 -0.0264 18.01 -0.01 3.5759 -7.6939 0.0023 0.0604 -0.0029 19.02 -0.01 3.8193 -6.0483 0.0046 0.0560 -0.0016 20.05 -0.00 4.0549 -8.2569 -0.0117 0.0874 0.0010 22.12 -0.00 4.5505 -8.6134 0.0257 0.0072 0.0060 23.14 -0.01 4.7444 -8.55240 0.0326 0.0731 0.0167 24.20 -0.00 5.3296 -8.6134 0.0257 0.0072 0.0060 27.36 -0.00 5.3296 -8.5542 0.0390 0.0021 0.0254 27.36 -0.00 5.3296 -8.5542 0.1391 -0.2150 0.0552 27.36 -0.00 5.8702 -8.8522 0.1144 -0.1525 0.0522 25.44 -0.00 5.3246 -8.5545 0.1681 -0.2650 0.0792 20.05 -0.00 5.86618 -8.5754 0.0002 0.0071 0.0055 27.36 -0.00 5.8569 -8.6618 -8.2754 0.0000 0.0711 0.0072 27.36 -0.00 5.8569 -8.6618 -8.2555 0.1681 -0.2650 0.0753 27.99 -0.00 1.8723 -4.5844 -0.0162 0.0711 0.0055 27.09 -0.00 1.8723 -4.5844 -0.0185 0.0749 0.0153 9.97 -0.00 1.8723 -4.5844 -0.0185 0.0749 0.0128 1.99 -0.00 0.3815 -0.9160 -0.0256 0.0855 0.0138	TEST PART MACH RX10-6 PM1 CONF L DEL1 DEL2 DEL3 DEL4 1 14 U. VO 2.3 0.0 84 WOF12 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEST PART MALM RX10-6 PM1 COMF L DEL1 DEL2 DEL3 DEL4 TRAMSITION L	TEST PART MACM RX10-6 PM1 CONF L DEL1 DEL2 DEL3 DEL4 TRANSITION 1 14 0.50 2.3 0.0 8440F12 0.0 0 0 0 0 0 UMAROCON ALPMA BETA CN CLM CY CLM CLL CA CAR CAF -0.00 -0.00 0.0469 -0.1117 -0.0222 0.0836 0.0017 0.3384 0.1333 0.1951 1.99 -0.00 0.7501 -1.7633 -0.0215 0.0837 0.0050 0.3325 0.1332 0.1991 3.99 -0.00 0.7261 -1.7633 -0.0215 0.0837 0.0050 0.3325 0.1352 0.2073 5.99 -0.00 1.0853 -2.6022 -0.0205 0.0790 0.0050 0.3484 0.1529 0.1955 7.98 -0.00 1.6453 -2.6022 -0.0205 0.0790 0.0050 0.3486 0.1529 0.2227 9.90 -0.00 1.6453 -2.6022 -0.0144 0.0673 0.0009 0.3976 0.1878 0.2298 11.96 -0.00 2.7744 -5.4294 -0.0144 0.0673 0.0009 0.3976 0.1878 0.2298 11.96 -0.00 2.7040 -6.3060 -0.0129 0.0771 0.0022 0.4271 0.2044 0.2224 15.96 -0.00 3.1271 -7.0787 -0.0071 0.0729 0.0020 0.4360 0.2176 0.2224 15.96 -0.00 3.1271 -7.0787 -0.0071 0.0729 0.0024 0.4666 0.2220 0.2046 16.99 -0.01 3.3500 -7.3674 -0.0023 0.0664 -0.0026 0.4666 0.2220 0.2046 19.02 -0.01 3.5759 -7.6939 0.0023 0.0664 -0.0026 0.4667 0.22511 0.2175 19.01 -0.01 3.6759 -8.6134 0.0023 0.0664 -0.0029 0.4715 0.2881 0.1904 22.15 -0.00 4.5505 -8.6134 0.0027 0.0072 0.0000 0.5668 0.2917 0.1627 22.15 -0.00 4.5505 -8.6134 0.0257 0.0072 0.0000 0.5668 0.2921 0.2046 23.14 -0.01 4.7444 -6.5240 0.0017 0.0072 0.0000 0.5668 0.2921 0.1642 23.14 -0.01 4.7444 -6.5240 0.0025 0.0072 0.0000 0.5668 0.2921 0.1642 23.14 -0.01 4.7444 -6.5240 0.0032 0.0072 0.0000 0.5668 0.2921 0.1642 25.24 -0.00 5.276 -8.5084 0.0057 0.0072 0.0000 0.5668 0.2921 0.1645 25.24 -0.00 5.276 -8.5084 0.0057 0.0072 0.0000 0.3669 0.3378 0.3037 0.0913 27.36 -0.00 4.5618 -8.5754 0.0000 0.0072 0.0000 0.3778 0.3509 0.0072 28.44 -0.00 6.5286 -8.2255 0.1605 -0.2263 0.0052 0.3338 0.3169 0.1194 25.24 -0.00 5.500 8.6585 -8.2255 0.1605 -0.2263 0.0052 0.3338 0.3559 0.0053 26.43 -0.00 6.5286 -8.2255 0.1605 -0.2263 0.0052 0.3338 0.3559 0.0064 26.30 -0.00 5.6618 -8.5754 0.0000 0.0000 0.0000 0.3778 0.3509 0.0072 27.38 -0.00 6.5569 -8.618 -8.5754 0.0000 0.0000 0.0000 0.0000 0.3778 0.3509 0.0078 29.99 0.00 6.5564 -8.5255 0.1605 -0.0000 0.0000 0.3338 0.35

MA BETA 00 -0.01 99 -0.01 99 -0.01	0.0085 0.3478 0.6795	-0.027-	-0.0467	CLN	CLL -	CA	CAB	CAF.	
90 -0.01 90 -0.01	0.0045	-0.027-	-0.0467					CAP	ACP
99 -0.01		-0.837u		0.61.03	0.0124	0.5259	0.2148	-	-3,2133
	A 4746		-0.0441	0.2019	0.01-2	0-5277	0.5500	0.3077	-2.4065
44 -0°A;		-1.6067	-0.0454	0.1827	0.0127	0.5242	0.2291	0.2951	
99 -0.01	1.0609	-2.5414	-0.0346	0.1673	0.0143	0.5339 0.5484	0.2239 0.2452	0.3100	-2.3955 -2.32 85
98 -0.01	1.7854	-4.0847	-0-0243	0.1766	0.0125	0.5661	0.2476	0.3185	-2.2873
	2.1740	-4.6000	-0.0278	0.1296	0.0109	0.5746	0.2532	0.3214	
	2.1075	-4.4051	-0.0268	0.1248	0.0124	3.5694	6.2626	0.3067	-2.2149
02 -0.01	2.5731	-5.4368	-0.025t	0.1257	0.0120	0.5780	0.2640	0.3139	-2-1129
		-6.0203				0.5844		0.3138	-2.0163
									-1.9665
									-1.7827
									-1.6248
									-1.5496
			0.0574	-0.0316	0.0131	0.5369	0.3135		-1.4622
37 -0.00	5.4645	-7.5543	0.0045	-0.0654	0.0187	0.5242	0.3145	0.2097	-1.3824
_	5.7940	-7.5631	0.0616	-0.0651		0.5146			-1.3086
									-1.2551
	3.9456			0.1245					-1.7708
				0.1473			0.2429		-3.9148
	00 -0.01 00 -0.01 02 -0.01 04 -0.01 07 -6.61 13 -0.01 15 -6.01 21 -0.01 22 -0.01 337 -0.00 44 -0.00 45 -0.01 54 -0.00 55 -0.00 55 -0.00 55 -0.00	00 -0.01 2.1740 00 -0.01 2.1740 00 -0.01 2.1740 02 -0.01 2.5731 04 -0.01 3.2243 13 -0.01 3.9654 16 -0.01 4.2419 21 -0.01 4.5356 20 -0.01 4.8273 32 -0.01 5.1402 337 -0.00 5.4645 44 -0.00 5.7940 45 0.01 6.0846 54 0.00 6.4500 55 -0.00 7.5667	00 -0.01	00 -0.01 2.1740 -4.6040 -0.0278 00 -0.01 2.1645 -4.6050 -0.0208 02 -0.01 2.5731 -5.4368 -0.0256 04 -0.01 2.9828 -6.0203 -0.0223 07 -0.01 3.2243 -6.3505 -0.0136 13 -0.01 3.9659 -7.0700 -0.0052 16 -0.01 4.2419 -7.2247 0.0006 17 -0.01 4.5356 -7.3699 0.013 18 -0.01 5.1462 -7.5248 0.0574 18 -0.01 5.1462 -7.5543 0.0645 18 -0.00 5.7940 -7.5632 0.1670 19 -0.00 6.4600 -7.7103 0.1327 19 -0.00 6.4600 -7.8420 0.1201 19 -0.00 6.7566 -7.8420 0.1201 10 -0.01 3.9456 -6.9809 -0.0112	00 -0.01 2.1740 -4.8040 -0.0778 . 0.1276 00 -0.01 2.1675 -4.8051 -0.0268 0.1278 02 -0.01 2.5731 -5.4368 -5.0256 0.1257 04 -0.01 2.9828 -6.0203 -0.0223 0.1250 07 -0.01 3.2243 -6.3505 -0.0136 0.1144 13 -0.01 3.9659 -7.0700 -0.0052 0.1051 16 -0.01 4.2419 -7.2277 0.0006 0.1057 21 -0.01 4.5356 -7.3699 0.0113 0.0701 22 -0.01 4.8273 -7.4612 0.0332 0.0155 32 -0.01 5.1462 -7.5248 0.0574 -0.0316 33 -0.00 5.4665 -7.5543 0.0645 -0.0654 44 -0.00 5.7940 -7.5632 0.1670 -0.3469 54 0.01 6.0896 -7.6632 0.1670 -0.3469 55 0.00 6.4600 -7.7103 0.1327 -0.2464 55 -0.00 6.7566 -7.8420 0.1201 -0.2464 55 -0.00 6.7566 -7.8420 0.1201 -0.2464 55 -0.00 7.0647 -7.9263 0.1920 -0.3575	00 -0.01 2.1740 -4.6000 -0.0278 0.1246 0.0109 00 -0.01 2.1740 -4.8051 -0.0268 0.1248 0.0124 02 -0.01 2.5731 -5.368 -0.0256 0.1257 0.0120 04 -0.01 2.9828 -6.0203 -0.0223 0.1250 0.0086 07 -0.01 3.2243 -6.3505 -0.0136 0.1151 0.0053 13 -0.01 3.9654 -7.0700 -0.0052 0.1051 0.0055 16 -0.01 4.2419 -7.2247 0.0006 0.1047 0.0049 21 -0.01 4.5356 -7.3699 0.013 0.0701 0.0054 25 -0.01 4.8273 -7.4612 0.0332 0.0155 0.0131 37 -0.01 5.1462 -7.5248 0.0574 -0.0316 0.0131 37 -0.01 5.4645 -7.5543 0.0616 -0.0654 0.0172 44 </th <th>00 -0.01 2.1740 -4.5040 -0.0278 0.1276 0.0109 0.5746 00 -0.01 2.1045 -4.7051 -0.0268 0.1278 0.0124 3.5694 02 -0.01 2.5731 -5.368 -3.0256 0.1257 0.0120 0.5780 04 -0.01 2.9828 -6.0203 -0.0223 0.1250 0.0086 0.5844 07 -0.01 3.2273 -6.3505 -0.0136 0.1144 0.0053 0.5908 13 -0.01 3.9657 -7.0700 -0.0052 0.1051 0.0055 0.5617 16 -0.01 4.2419 -7.2277 0.0000 0.1057 0.0049 0.5736 21 -0.01 4.5356 -7.3697 0.0113 0.0701 0.0054 0.5519 22 -0.01 4.8273 -7.4612 0.0332 0.0155 0.0101 0.5501 32 -0.01 5.1462 -7.5248 0.0574 -0.0316 0.0131 0.5369 33 -0.00 5.4645 -7.5543 0.0645 -0.0654 0.0187 0.5242 44 -0.00 5.7948 -7.5631 0.0616 -0.0651 0.0172 0.5146 45 0.01 6.0876 -7.6632 0.1670 -0.3469 0.0536 0.5083 54 0.00 6.4600 -7.7103 0.1320 -0.2464 0.0245 0.4975 55 -0.00 6.7566 -7.8428 0.1670 -0.3469 0.0577 0.4919 55 -0.00 7.0647 -7.4263 0.1920 -0.3575 0.0273 0.4822</th> <th>00 -0.01 2.1740 -4.8000 -0.0770 0.1276 0.0109 0.5746 0.2537 00 -0.01 2.1677 -4.8051 -0.0268 0.1278 0.0124 0.5694 0.2626 02 -0.01 2.5731 -5.368 -0.0256 0.127 0.0120 0.5780 0.2640 04 -0.01 2.9820 -6.0203 -0.0223 0.1250 0.0006 0.5844 0.2706 07 -6.61 3.2243 -6.3505 -0.0136 0.1144 0.0053 0.5908 0.2785 13 -0.01 3.9659 -7.0700 -0.0052 0.1051 0.0055 0.5917 0.3062 16 -6.01 4.2419 -7.2297 0.0006 0.107 0.0049 0.5736 0.3046 21 -9.01 4.5356 -7.3699 0.013 0.0701 0.0054 0.5019 0.3099 26 -0.01 4.6273 -7.4612 0.0332 0.0155 0.0101 0.5501<th>00 -0.01 2.1740 -4.8000 -0.0770 0.1276 0.0109 0.5746 0.2537 0.3214 00 -0.01 2.1677 -4.8051 -0.0260 0.1278 0.0124 0.5694 0.2626 0.3067 02 -0.01 2.5731 -5.368 -5.0256 0.127 0.0120 0.5780 0.2640 0.3139 04 -0.01 2.9820 -6.0203 -0.0223 0.1250 0.0086 0.5844 0.2706 0.3138 07 -6.61 3.2243 -6.3505 -0.0136 0.1144 0.0053 0.5908 0.2785 0.3128 13 -0.01 3.9657 -7.0700 -0.0052 0.1051 0.0055 0.5917 0.3062 0.2755 16 -6.01 4.2419 -7.2277 0.0006 0.1047 0.0049 0.5736 0.3046 0.2690 21 -0.01 4.5356 -7.3699 0.013 0.0701 0.0054 0.5019 0.3099 0.2520</th></th>	00 -0.01 2.1740 -4.5040 -0.0278 0.1276 0.0109 0.5746 00 -0.01 2.1045 -4.7051 -0.0268 0.1278 0.0124 3.5694 02 -0.01 2.5731 -5.368 -3.0256 0.1257 0.0120 0.5780 04 -0.01 2.9828 -6.0203 -0.0223 0.1250 0.0086 0.5844 07 -0.01 3.2273 -6.3505 -0.0136 0.1144 0.0053 0.5908 13 -0.01 3.9657 -7.0700 -0.0052 0.1051 0.0055 0.5617 16 -0.01 4.2419 -7.2277 0.0000 0.1057 0.0049 0.5736 21 -0.01 4.5356 -7.3697 0.0113 0.0701 0.0054 0.5519 22 -0.01 4.8273 -7.4612 0.0332 0.0155 0.0101 0.5501 32 -0.01 5.1462 -7.5248 0.0574 -0.0316 0.0131 0.5369 33 -0.00 5.4645 -7.5543 0.0645 -0.0654 0.0187 0.5242 44 -0.00 5.7948 -7.5631 0.0616 -0.0651 0.0172 0.5146 45 0.01 6.0876 -7.6632 0.1670 -0.3469 0.0536 0.5083 54 0.00 6.4600 -7.7103 0.1320 -0.2464 0.0245 0.4975 55 -0.00 6.7566 -7.8428 0.1670 -0.3469 0.0577 0.4919 55 -0.00 7.0647 -7.4263 0.1920 -0.3575 0.0273 0.4822	00 -0.01 2.1740 -4.8000 -0.0770 0.1276 0.0109 0.5746 0.2537 00 -0.01 2.1677 -4.8051 -0.0268 0.1278 0.0124 0.5694 0.2626 02 -0.01 2.5731 -5.368 -0.0256 0.127 0.0120 0.5780 0.2640 04 -0.01 2.9820 -6.0203 -0.0223 0.1250 0.0006 0.5844 0.2706 07 -6.61 3.2243 -6.3505 -0.0136 0.1144 0.0053 0.5908 0.2785 13 -0.01 3.9659 -7.0700 -0.0052 0.1051 0.0055 0.5917 0.3062 16 -6.01 4.2419 -7.2297 0.0006 0.107 0.0049 0.5736 0.3046 21 -9.01 4.5356 -7.3699 0.013 0.0701 0.0054 0.5019 0.3099 26 -0.01 4.6273 -7.4612 0.0332 0.0155 0.0101 0.5501 <th>00 -0.01 2.1740 -4.8000 -0.0770 0.1276 0.0109 0.5746 0.2537 0.3214 00 -0.01 2.1677 -4.8051 -0.0260 0.1278 0.0124 0.5694 0.2626 0.3067 02 -0.01 2.5731 -5.368 -5.0256 0.127 0.0120 0.5780 0.2640 0.3139 04 -0.01 2.9820 -6.0203 -0.0223 0.1250 0.0086 0.5844 0.2706 0.3138 07 -6.61 3.2243 -6.3505 -0.0136 0.1144 0.0053 0.5908 0.2785 0.3128 13 -0.01 3.9657 -7.0700 -0.0052 0.1051 0.0055 0.5917 0.3062 0.2755 16 -6.01 4.2419 -7.2277 0.0006 0.1047 0.0049 0.5736 0.3046 0.2690 21 -0.01 4.5356 -7.3699 0.013 0.0701 0.0054 0.5019 0.3099 0.2520</th>	00 -0.01 2.1740 -4.8000 -0.0770 0.1276 0.0109 0.5746 0.2537 0.3214 00 -0.01 2.1677 -4.8051 -0.0260 0.1278 0.0124 0.5694 0.2626 0.3067 02 -0.01 2.5731 -5.368 -5.0256 0.127 0.0120 0.5780 0.2640 0.3139 04 -0.01 2.9820 -6.0203 -0.0223 0.1250 0.0086 0.5844 0.2706 0.3138 07 -6.61 3.2243 -6.3505 -0.0136 0.1144 0.0053 0.5908 0.2785 0.3128 13 -0.01 3.9657 -7.0700 -0.0052 0.1051 0.0055 0.5917 0.3062 0.2755 16 -6.01 4.2419 -7.2277 0.0006 0.1047 0.0049 0.5736 0.3046 0.2690 21 -0.01 4.5356 -7.3699 0.013 0.0701 0.0054 0.5019 0.3099 0.2520

	TEST		ACH RE10-6		CONF	L 0EL1		DEL3 DEL4	TRANSITIO	<u> </u>		
	_ •											
INT	ALPHA	BETA	CN	CLM	CÅ	CLN	CLL	CA	CAB	CAF	ACP	
-	0.00	-0.00	-0.0137	0.0544	-0.0213		0.0124	0.5157	0.1A39_		-3,9891	
	2.00	-0.00	0.3135	-0.6603	-0-0126		0.0125	0.5155	0.1943	0.3711	-5-1065	
	6.00	-0.00	0.9907	-2.2042	-6.0128		0.0140	0.5214	0.2048	0.3166	-2.2151	
i	8.00	-0.00	1.3594	-2.4805	-0.0025		0.0140	0.5365	0.2069		-2.1923	
·	10.00	-0.00	1.7339	-3./106	-0.0062		0.0124	0.5472	0.2129		-2.1400	
	12.01	-0.00	2.1119	3523	-0.0010	-	0.0092	0.5579	0.2178	C.3401	-2.0608	
	16.06	-0.00	2.9243	-5.4115	0.0000		0.0001	0.5622	0.2368	0.3234	-1.6476	
)	17.11	-0.00	3.16/5	-5.6612	0.0099		0.0048	0.5656	0.2443	0.3213	-1.7673	
•	18.14	-0.00	3.4204	-5.6697	0.0124		0.0057	0.5652	0.2546	0.3107	-1.7161	
?	19.18	-0.00	3.6992	-6.0527	0.0140	0.0174	0.0051	0.5626	0.2610	0.3017	-1.6362	
1	20.22	-0.00	3.9864	-6.1680	0.0206	0.0057	0.0057	0.5568	0.2665	4095.0	-1.5525	
	21.27	-0.00	4.2496	-6.321-	0.0224		0.0050	0.5511	0.2721	0.2790	-1.4737	
)	22.33	-0.00	4.5921	-6.3480	0.0245		0.0051	0.5424	0.2728	0.2696	-1.3934	
•	23.37	-0.00	4.4913	-6.4712	. u . 0323		0.0065	_	0.2773	0.2574	-1.3230	
•	25.49	0.00	5.5405	-6-5900	0.1072		0.0279	0.5232	0.2911	0.2351	-1.1905	
•	26.54	0.00	5.27-4	-0.6563	0.1281		0.0344	0.5214	0.2948	0.2266	-1.1331	
)	27.61	0.00		-6.7480	0.1500		0.0371	0.51A0	0.2986	0.2194	-1.0676	
2	29.69	0.00	6.5366	-6.881e	0.1632		0.0327	0.5144	0.3023	0.2123	-1.0526	
3	30.75		7.2465	-7-2705			0.0265	0.5104 0.5037	0.3155	0.2045	-1.0280 -1.0041	
;—		-0.00	3.9455				0.0071	0.5568	0.2811	0.2757		
5		-0.00		-3.7003					0.2589		-2.1496	
<u>-</u>		-0.00	-0.0259				0.0136		0.2091		-3.0664	
												
									<u> </u>			
_					 -			<u> </u>				
	···											

ARNOLD ENGINEERING DEVELOPMENT CENTER(AEDC) PAGE 1 OF 1	PROPULSION WIND TUNNEL FACILITY(PWT)	AERODYNAMIC SIND TUNNEL (4T)
SHEET 1 OF 1		

TEST 1		ACH RX10-6 3u 2.3		CONF Bou OF 12	· · · · · · · · · · · · · · · · · · ·	O O	DEL3 DE	4 TRANSITI		
ALPHA	BFTA	CN.	CLA	CY	CLN	CLE	CA" .	CAB	CAF	ACP
-0.00	-0.00	0.0069	-0.6401	0.0240	0.077	0.0119	0.4809	0.1756	0.3053	-5.0152
2.00	-0.00	0.2419	-0.55/3	-0.0205	6.077	0.0205	0.4893	0.1855	0.3037	-1.9773
. 4.01	-0.00	0.5995	-1.2245	-0.02le	0.083	0.0141	0.4900	0.1937	0.2962	-2.0424
6.02	-0.00	0.9240	-1.9044	-0.0195	0.090	0.0191	0.5030	0.1952	0.3076	-2.0500
8.03	-0.01		-5.5645	-0-0117	0.082	0.0176			0.3143	-2.0175
10.03		1.6328	-3.1930	-0.0144	0.081	0.0159	0.5215	0.2058	0.3157	-1.9555
14.11	-0.06	2.4056	-4.2346	-0.004	0.050	3 0.0175	0.5309	0.2287	0.3022	-1.7601
15.10	-0.00	2.6548	-4.6770	-0.001	0.041	0.0152	0.5373	0.2327	0.3046	-1.6356
	-0.00	3.1097	-4.4650	-0.0004	0.047	7 . 0.0161	0.5366	0.2387	0.2960	-1.5646
	-0.00	3.3887	-5.623>					0.2440	0.2916	-1.4824
	-0.00		-5.1632	0.005	0.041	3 0.0172	0.5325	0.2501	0.2824	-1.4037
20.30	-0.00	3.9606	-5.2410	0.016	0.014	7 0.0174	0.5293	0.2557	0.2736	-1.3290
21.36	-0.00	4.7645	-5.3605		0.00-	3 0.0186				-1.2500
						1 0.0168				-1.1835
						5 0.0176	0.5163			-1.1220
										-1.0618
	-0.00	5.5211	-5.5422							-1.8129
	-0.00				-0.117					-0.9726
27.69	-0.00	6.5141	-5.8748						0.2313	-0.9454
						0.0199				-0.9107
										-0.6938
26.65	-0.00	5.8741	-5.6119			7 0.0330	0.5212	0.3163	0.2049	-0.9554
	-0.00	4.5895	-5-3691	0.025	50.001	2 _ 0.0215	0.5264	0.3150	0.2106	-1.1699
18.21	-0.00	3.3896	-5.0423						0.5500	-1.4875
14.21	-0.00	3.3966	-5.0454							-1,4863
14.06	-0.00	2.4061								
10.03	-0.0u	1.6345	-3-1914		1 0.040				0.2527	1.9525
6.02	-0-00	0.9380							0.2429	-2.0545
2.00	-0.00	0.2859	-0.5442	-0.023	9 0.075	4 0.0254	0.4944	0-2417	0.2527	-1.9636
0.00	-0.00	-0.0113	0.0756	-0.021	5 0.064	3 0.0236	0.4930	0.2260	0.2670	-6.6698
	1 ALPHA -0.00 2.00 4.01 6.02 8.03 10.03 14.11 15.10 17.17 18.22 19.27 20.30 21.35 22.41 23.47 24.59 26.60 27.69 29.80 10.86 26.65 22.42 18.21 14.21 10.03 6.02	1 16 1. ALPMA BFTA -0.00 -0.00 2.0u -0.00 4.01 -0.0v 6.02 -0.0u 8.03 -0.01 10.03 -0.00 14.11 -0.0v 17.17 -0.00 19.27 -0.0v 20.30 -0.00 21.36 -0.00 22.41 -0.00 23.47 -0.00 24.54 -0.00 25.59 -0.00 26.64 -0.00 27.69 -0.0v 29.80 -0.0v 29.80 -0.0v 29.80 -0.0v 21.80 -0.0v 21	1 16 1.30 2.3 ALPMA BFTA CN -0.00 -0.00 0.0069 2.00 -0.00 0.2419 4.01 -0.00 0.5495 6.02 -0.00 0.9240 8.03 -0.01 1.2735 10.03 -0.00 1.6328 14.11 -0.00 2.6548 17.17 -0.00 3.1097 19.27 -0.00 3.4763 20.30 -0.00 4.2645 22.41 -0.00 4.5616 23.47 -0.00 4.5616 23.47 -0.00 5.211 26.66 -0.00 5.211 26.66 -0.00 5.211 26.66 -0.00 5.211 26.66 -0.00 5.211 27.69 -0.00 6.2141 29.80 -0.00 6.2141 29.80 -0.00 6.2141 29.80 -0.00 6.2141 22.42 -0.00 4.5695 18.21 -0.00 3.3896 18.21 -0.00 3.3896 18.21 -0.00 3.3906	1 16 1.30 2.3 0.0 6 ALPMA BFTA CN CLM -0.00 -0.00 0.0064 -0.6401 2.00 -0.00 0.2419 -0.573 4.01 -0.00 0.5495 -1.2245 6.02 -0.00 0.9240 -1.9040 8.03 -0.01 1.2735 -2.5692 10.03 -0.00 1.6328 -3.1430 14.11 -0.00 2.6548 -4.2366 15.10 -0.00 3.007 -4.6650 17.17 -0.00 3.1097 -4.6650 19.27 -0.00 3.4783 -5.1632 20.30 -0.00 3.9800 -5.2436 21.36 -0.00 4.7645 -5.3605 22.41 -0.00 4.7645 -5.3605 22.41 -0.00 4.7645 -5.3605 23.47 -0.00 4.7645 -5.3605 23.47 -0.00 5.7101 -5.5710 25.59 -0.00 5.7101 -5.5710 25.59 -0.00 5.7101 -5.5710 27.69 -0.00 6.7141 -5.6119 29.90 -0.00 6.7141 -5.6119 29.90 -0.00 6.7141 -5.6119 22.42 -0.00 4.5895 -5.3691 18.21 -0.00 3.3896 -5.0423 18.21 -0.00 3.3896 -5.0423 18.21 -0.00 3.3896 -5.0423 18.21 -0.00 3.3896 -5.0423 18.21 -0.00 3.3896 -5.0423	1 16 1.30 2.3	1 16 1.30 2.3	1 16 1-30 2-3	1 18 1-3U 2-3	ALPMA BFTA CN CLM CY CLN CLL CA CAB -0.00 -0.00 0.0069 -0.0401 -0.0240 0.0770 0.0119 0.4809 0.1756 2.00 -0.00 0.7419 -0.55/3 -0.0205 0.0778 0.0205 0.4893 0.1855 4.01 -0.00 0.5995 -1.2245 -0.0216 0.0839 0.0191 0.4900 0.1937 6.02 -0.00 0.9290 -1.9044 -0.0195 0.0904 0.0191 0.5030 0.1952 8.03 -0.01 1.2735 -2.5692 -0.0117 0.0821 0.0176 0.5141 0.1998 10.03 -0.00 1.6328 -3.1930 -0.0144 0.00159 0.5215 0.2058 14.11 -0.00 2.6598 -4.2346 -0.0045 0.0563 0.0175 0.5309 0.2287 17.17 -0.00 3.1097 -4.4656 -0.0004 0.0477 0.0161 0.5336 0.2327 17.17 -0.00 3.1097 -4.4656 -0.0004 0.0477 0.0161 0.5366 0.2387 18.22 -0.00 3.4673 -5.1632 0.0059 0.0413 0.0172 0.5325 0.2501 19.27 -0.00 3.4763 -5.1632 0.0059 0.0413 0.0174 0.5293 0.2557 20.30 -0.00 3.9600 -5.2936 0.0169 0.0177 0.0174 0.5293 0.2557 21.38 -0.00 4.5816 -5.4225 0.0059 0.013 0.0174 0.5293 0.2557 22.41 -0.00 4.5816 -5.4225 0.0293 0.0065 0.0176 0.5163 0.2572 23.47 -0.00 5.5211 -5.5310 0.0243 0.0065 0.0176 0.5163 0.2572 23.47 -0.00 5.5211 -5.5310 0.0243 0.0065 0.0176 0.5163 0.2575 24.59 -0.00 5.5211 -5.5310 0.0243 0.0065 0.0176 0.5163 0.2575 25.59 -0.00 5.5211 -5.5310 0.0243 0.0065 0.0176 0.5163 0.2675 26.60 -0.00 5.6705 -5.7105 0.0011 -0.1174 0.00305 0.5172 0.2728 27.40 -0.00 6.7431 -5.5174 0.0243 0.0065 0.0176 0.5163 0.2676 28.60 -0.00 5.6705 -5.7105 0.0011 -0.1174 0.00305 0.5172 0.2728 29.80 -0.00 6.7431 -5.5194 0.0703 -0.0867 0.0199 0.5277 0.03188 30.680 -0.00 7.3357 -6.5567 0.1086 -0.1011 0.0188 0.5209 0.5222 0.2708 29.80 -0.00 5.6705 -5.7105 0.0011 -0.1174 0.0305 0.5172 0.2728 18.21 -0.00 3.3884 -5.0425 0.0094 -0.1518 0.0199 0.5277 0.3188 30.680 -0.00 7.3357 -6.5567 0.1086 -0.1017 0.0185 0.5242 0.3163 22.42 -0.00 3.3886 -5.0425 0.0094 0.0012 0.0199 0.5277 0.330 0.5212 0.3163 30.680 -0.00 7.3357 -6.5567 0.1086 -0.1017 0.0185 0.5264 0.3163 30.680 -0.00 3.3886 -5.0425 0.0094 0.0012 0.0395 0.0296 0.5222 0.2708 30.680 -0.00 3.3886 -5.0425 0.0094 0.0012 0.0396 0.5056 0.5057 0.3191 30.680 -0.00 3.3886 -5.0425 0.0094 0.0012 0.0396 0.5056 0.5057 0.3191 30.600 -0.00 3.3886 -5.0425 0.00	ALPMA BFTA CN CLM CV CLM CLL CA CAB CAF -0.00 -0.00 0.0069 -0.0001 -0.0200 0.0770 0.0119 0.0809 0.1756 0.3053 2.00 -0.00 0.7419 -0.5573 -0.0705 0.0778 0.0225 0.0809 0.1756 0.3053 2.00 -0.00 0.5995 -1.2245 -0.0216 0.0899 0.0191 0.5903 0.1855 0.3037 4.01 -0.00 0.5995 -1.2245 -0.0216 0.0899 0.0191 0.5903 0.1855 0.3037 6.02 -0.00 0.9290 -1.9000 -0.0195 0.0900 0.0191 0.5030 0.1952 0.3078 8.03 -0.01 1.2735 -2.5592 -0.0117 0.0821 0.0176 0.5161 0.1998 0.3163 10.03 -0.00 1.6328 -3.1930 -0.0104 0.0159 0.5215 0.2556 0.3157 10.11 -0.00 2.6558 -4.2306 -0.0055 0.0553 0.0175 0.5309 0.2287 0.3022 15.16 -0.00 2.6558 -4.2306 -0.0010 0.015 0.0152 0.5373 0.2327 0.3046 17.17 -0.00 3.1097 -4.6650 -0.0010 0.0015 0.0152 0.5373 0.2327 0.3046 19.22 -0.00 3.3887 -5.0235 0.0021 0.0416 0.0168 0.5356 0.2867 0.2960 19.22 -0.00 3.6763 -5.1632 0.0059 0.0176 0.5366 0.2387 0.2960 19.22 -0.00 3.66763 -5.1632 0.0059 0.0197 0.0174 0.5293 0.2557 0.2736 20.30 -0.00 3.9800 -5.2490 0.0105 0.0174 0.5293 0.2557 0.2501 0.2824 20.30 -0.00 4.5816 -5.225 0.0059 0.013 0.0172 0.5325 0.2501 0.2824 22.41 -0.00 4.8797 -5.5749 0.0224 0.0061 0.0188 0.5209 0.2623 0.2556 23.47 -0.00 4.8797 -5.5749 0.0224 0.0062 0.0161 0.5163 0.2675 0.2508 24.50 -0.00 5.2101 -5.5319 0.0277 0.0062 0.0161 0.5179 0.2722 0.2546 23.47 -0.00 4.8797 -5.5749 0.0224 0.0062 0.0161 0.5179 0.2722 0.2546 23.47 -0.00 4.8797 -5.5749 0.0224 0.0062 0.0161 0.5179 0.2722 0.2546 24.50 -0.00 5.8705 -5.1105 0.0011 0.0110 0.0190 0.5209 0.5222 0.2909 0.2313 29.80 -0.00 5.8705 -5.1105 0.0011 0.0110 0.0190 0.5209 0.5222 0.2909 0.2313 29.80 -0.00 5.8755 -5.519 0.0050 0.0050 0.0175 0.5060 0.5060 0.2768 0.2386 26.60 -0.00 5.8755 -5.519 0.0050 0.0050 0.0062 0.0062 0.5269 0.5222 0.2909 0.2313 29.80 -0.00 6.5471 -5.5190 0.0011 0.0180 0.0070 0.0070 0.5212 0.3168 0.2065 18.21 -0.00 3.3880 -5.0423 0.0029 0.0029 0.00296 0.5222 0.2909 0.2313 29.80 -0.00 5.8751 -5.5619 0.0850 -0.1507 0.0330 0.5212 0.3168 0.2066 18.21 -0.00 3.3880 -5.0424 0.0010 0.00397 0.0236 0.5407 0.3168 0.2066 18.21 -0.00 3.3880 -5.0424 0.0010 0.00397

Ð
ö
×
Y.
꾸
7
٧ı
7

E :	l OF I		VEL OPMENT	CENTER (A	EDC1 . P	ROPULSIGN (SSILE TAI	EL FACILI L EFFECTS	DATA	. AER		MMEP (#I)
	TEST	PART M	ACH PX10-	6 PHI		L_ DEL)						
•	1	19 0.	94 2.3	0.0 8	4=0f12 0		45	0 0	UNKNOW	N		
INT -	ALPHA	BETA	CM.	CLM	<u></u>	CLN	CLL .	- CĂ	CAB	CAF	KCP	
2	1.99	-6.00	D.303H	-0.7290	-0.0764	0.0991	0.0265	0.2731	0.0992	0.1739	-2.3993	
3	1.99	-0.0u	0.3047	-0.7407	-0.0307	0-1036	0.0280	0.2756	0.1009	0-17-7	-2.4310	
•	3.99	-0.0u	0.6400	-1-5605	-0.0267	0-09-9	0.0283	0.2692	0-1158	0.1535	-2.4361	
5	5.97	-0.00	1.0191		-0.0264	0-10-2	0-0271	0-5844	0.1155	0.1694	-2.5134	
6 .	7.96	0.00	1.4447	-3-6454		0.0958	0.0258	0-3071	0.1320	0.1751	-2.5491	
7		-0.00	1.4643	-4.7274.		0.0956	0.0228	0.3295	0.1467	0.1827	-7.5358	
<u> </u>	11.95	-0.60	2.2829	-5.6547	-0.0165	0.0899	0.0179	0.3530	0.1548	0,1983	-2.4792	
1		-0.01	2.6947 3.3532	-6.4984	-0.0211	0.0940	0.0212	0.3673	0.2166	0.1831 0.1506	-2.4115 -2.2759	
ż	10.01		3.5119	-7.7254	-0.0238	0.1660	0.0390	0.3660	0.2242	0.1438	-2.1998	— · —— — -
3.	19.03			-7.7664	-0-0145	0-1-13	0.0237	0.3743	0.2397	0.1346	-2.1273	
•		-0.00		-7.4554	-0.0050	0.0733	0.0196	0.3949	8005.0	0.1441	-2.0578	 -
5		-0.00	0.08n2	-R-1876	-0.0015	0.0793	0.0158	0.3990	0.2569		-2.0027	
	22.00	-0.00	4.2833	-6.2991	0.0104	0.06>9	0.0299	0.3984	0.2749	0.1235	-1.9375	
7	23.12	-0.00	4.4802	-8.3034	0.0032	0.0965	L.0554	0.4063	0.2639	0.1224	-1.8534	
8	24.15	-0.01	4.6690	-8.2656	0.0151	0.1229	0.0762	0.4006	0.2985	0.1021	-1.7703	
9	24.15	0.00	4.6825	-8.3154	0.0062	0.1301	0.0796	0.4053	0.3137	0.0916	-1.7759	
6		-0.00		-4.5881	0.0213	0.0752	0.0751	0.3952	0.3274	0.0678	-1.6930	
1		-0.60		-8.3454	0.0461	0-0565	0.0757	0.3858	0.3480	0.0378		
5	27.26	-0.00		-6.2759	0.0707	-0.0077	0.0841	0.3676	0.3531	0.0145	-1.5209	
3	_28,35_			·-A.2799	0.0077	-0.0614	0.0933	0.3529	0-3511		-1-4176	
•		-0.00		-8.2228	0.0073	-0.0517	0.0838	0-3348	0.3562	-0.0214	-1.3402	
5		0.00_		-8-1009	0.1350	-0.132F 0.0370	0.0725	0.3233	0.3632	-0.0399	-1 .2561	
7	54.53	-0.00		-8.7575	0.006R	0.0747	0.0283	0.3904 0.3984	0.3651	0.0253	-1.6091	
9	13.04	-0.00		-6.5657		0.0922	0.0197	0.3327	0.3446	0.1122	-1,9408 -2,4180	
0	9.96	-0.00		-4.7697	-0.0178	0.0934	0.0195	0.3160	0.1911		-2.5305	
ī	-5.97			-2.6035	-0.0251	0.1059	0.0223	0.2649	0-1747		-5.2551	·
2		-0.00		-0.7429		0.1010	0.0232	0.2715	0.1263		-2.4305	
3	-0.00	-0.00		-0-0583		0.1019	0.0248	0.7677	0.1207		-36,8062	

		·									
	TES1 1	SS D'AR		-	CONF B4d0f13 0		0 0	DEL3 DEL4 0 0	TRANSITI		
INT A		BETA	CN	CLH	CA	CĽN "	CLL	CA .	CAB	CAF	ACP
	-01	-0.00			-0-0540	0.0A49		0.2528	0.1077		-4.0236
	0.01	-0.00	0.0623	-0.2286	-0.0265	0.0476	-0.0088	0.2540	0.1053	0-1467	-3.6686
	0.01	-0.00 -0.00	0.0645	-0.7266		0.0859 0.0907	-0.0069		0.1086		-3,5155 -3,5166
	0.01	-0.00	0.0623	-0.4202		6.0933	-0.0069		0.1030		-3.5323
	.98	-0.00	0.3516	-0.9713		0.0951	-0.0086		0.1039		-2.5440
	.96	-0.00	0.7434	-1-0707		0.0976	-0.0102		0.1059	0.1260	-2.5162
	96	-0.0u	1.1225	-5.4400	-0.0295	0.1096	-0.0132	0.2356	0.1163	0.1192	-2.5799
	7.90	-0.00	1,4701	-3.7722		0.1051	-0.0149	0.2582	0.1298		-2.5640
	96	-0.00	1.8396	-4.3495		0.1145	-0.0148		0.1449		-2.4731
	. 48	-0.01	2.1439	-5-1437		0.1357	-0.0130		0.1573		-5.3665
_	.00	-0.00	2.3445	-5.1703		0.11.9	0.0007		0.1798		-2.2053
	6.03 7.05	-0.01 -0.01	2,5285	-5.0398		0.1312	-0.0074		10.2263		-1.9932
	R. 00	-0.0u	2.6445	-5.0427		0.1059	-0.0153 -0.0198		0.2761 0.3091	0.0925	-1.9069 -1.8137
_	9.16	-0.00	2.8761	-4.8526			-0.0387		0.3375		-1.6672
	9.10	0.00	2.6255	-4.7.95		-0.1351	-0.0479		0.3306		-1.6811
·· ż	0.12	0.00	2.9477	-4.0634			-0.0512		0.3632		-1.5820
	1.16	-0.01	3.0686	-4.556		0.0616	-0.0220		0.3876		-1.4050
2	2.16	-0.00	3.2769	-4.0305	-0.0135		-0.0225		0.4066	0.1113	-1.4741
2	3.10	-0.01	3.4437	-4.4512	-0.0175	0.0916	-0.0227	0.5258	0.4184	0.1074	-1.4377
	4-50	-0.01	3.6423	-5.153-			-0.0231		0.4329		-1.4149
	2.51	-0.01	3.6643	-5.36/1			0.0237		0.4503		-1.3669
	6.23	-0.01	4.0565	-5.5672			-0.0205		0.4606		-1.3724
	7 . 25	-0.01	4.3013	-5.6733			-0.0049		0-4717		-1.3655
	9.29	-0.01 -0.00	4.8394	-6.1943			-0.0046		0.4746		-1.3601
	0.30	0.00	5.1034	-6.856]		-0.3660	0.0434		0.4848		-1.3626 -1.3434
	0.30	0.00	301034	-0.0301	0.2344	-0.4363	0.0434	0.4013	0.4460	-0.0003	-1.3434

	- TES1	PART MA	CH PX10-0		CONF B4m0F13	L DE	DEL2	0EL3 DEL4	TRANSITI UNKNOWN	•		
)IN	ALPHA		CN		ĊŸ		CLL		CAB	CAF	XCP	
2-	1-99	-0.00	0.0376 0.3520		-0-6315		-0.0084 -0.0083		0.1049		-5.2057 -2.6174	
	1.99	-0.00	0.3611		-0.0277		-0.0100		0.1058	0.1347	-2.5869	
- 📜	1.99	-0.00	0.3676		-6.0276		-0.0100		0.1255	0.1166	-2.5635	
5	3.48	-0.00	0.7235		-0.02m7				0.1108		-9 6467	
6	5.96	-0.00	1.1240	-2.4552	-0.0267	0.0956	-0.0042	0.2372	0.1152		-2.6292	
7		-0.00	1.4718	-3.8367	-0-6555	0.0899	-0.0107	0.2579	0.1182	0.1397	-2,5864	
8	9.95		1.8107	-4.3895					0.1327	0.1435	-7.5347	
9		0.00	2.1234	-5.1349					0.1488		-2.4182	
10		-0.00	2.3884		-0.3125				0.1728		-5.2566	
11		0.00_		-5.4207					0.2099		-2.2645	
15		-0.00	2.5770	-5.269					0.2415	_	-2.0450	
13	17.05	-0.00		-5.2500	-0.0100				0.2826		-1.9430 -1.9458	
15_		-0.00		-5.1647					0.3046			
16	- 19.11				0.0585				0.3276		-1.6672	
17	20.14	0.00			0.0364				0.3488			
18	21.16				-0.0116				0.3787		-1.5035	
19	22.17	-0.01	3.2455	-4./585	-0.0162	C.103	-0.0144		0.4052		-1.4572	
50	22.17	-0.01	3.2596	-4.7670				0.5264	0.4057		-1.4625	
21		0.01	-4901	-4.9945					0.4192		-1.4310	
22		-0.01		-5.2011			5 -0.022		0.4310	0.1003	-1.4065	
53	25.23		3.9183	-5.4454		0.015			0.4347	0.0954	1.3897	
24		-0.61	_	-5.6779		-0.034			0.4511		-1.3716	
25	27.27		4.4071	-6.0007		-0-556			0.4654		-1.3616	· · · · · · · · · · · · · · · · · · ·
27	28.29		4.6656	-6.3433		-6.492	3 0.026 (8 0.091		0.4618		-1.3596	
28	29.30	-0.00			0.411		5 0.103	2 0.4926 3 0.4849	0.4809	_ 0.0120	<u>1.3553</u>	
												
				 -								

NT AL				440 0	4#0F13 0	. 0	0 0	0 0	UNKNOWN	1	
	PMA	BETA .	CN	CLM .	CY	CLY	CLL	CÁ	CAB	CAF	XCP
-	1	-0.00		-0.1545	-0.0290		-0.0000	0.2926	0.1004	0.1923	-5,4637
-0	-01	-0.00	0.0330	-0-1613	-0.0290	0.0910	-0.0080	0.2914	0.1041	0.1873	-4.8927
. 2	.00	-0.00	0.3124	-0.7361	-0.0235	0.0406	-0.0148	0.2849	0.1063	0.1786	-2.3628
		-0.00	0.6806	-1.6791	-0.0245	0.0925	-0.0077	0.2800	0.1053	0.1747	-2.4649
5	. 97	-0.00	1.0623	-2.7060	-0.0245	0.0947	-0.0023	0.2795	0.1200	0.1596	-2,5492
	-	-0.00	1.5021	-3.9327	-0.0154	0.0587	-0.0071	0.3000	0.1141	0.1809	
	.94	-0.00	1.6703	-4.8431	-0.0109	0.0504	-0-0102	0.3234	0.1391	0.1843	-2,5895
	.96	-0.00	2.1472	-5.300H	-0-00>4	0.0529	-0.0154	0.3458	0.1565	0.1891	-2.4667
	. 95	0.61	2.4745	-5.1757	0.0050	0.0552	-0.0157	0.3660	0.1830	0.1630	-2.3341
	.99	-0.01	2.7652	-6.0496	0.0216	0.0345	-0.0164	0.3921	0.2148	0.1773	-2.1878
	F0.	-0.01	2.8460	-5.4451	0.0004	0.0418	-9.0067	0.4114	0.5469	0.1645	-2-0889
	. 07	-0.00	7.9347	-5.1248	0.0099	0.0176	-0.0214	0.4454	0.2693		-1.9507
	.06	-0-00_	3.0081	-5,4641	0.0465	-0-0916	-0-034B	0.4824	0.2921	0,1903	-1.8165
	.10	-0.00	3.1046	-5.2680	0.0584	-0.1424	-0.0394	0.5127	0.3311	0.1915	-1.7033
	.14	-0.00	3.3632	-5.3788_	0.0350	-0.0941	-0.0296	0.5271	0.3453	0.1818	-1.6204
		-0.00	3.4612	-5.5436	0-0568	-0.0076	-0.0188	0.5392	0.3617	0.1775	-1.6016
	.20	-0.01	3.7000		0.0085	Q. 0759	-0.01/3	0.5483	0.3793		-1.5209
	.22	-0.01	3.6139	-5.8+05	0.0098	0.0626	-0.0193	0.5568	0.4015		
	. 25	-0.01	4.54-9	-5.8245	0.0275	0.0438	-0.0103	0-5520	0.4235	0.1785	-1,4234
	.25	-0.01	4.3427		0.0644	-0.0297	0.0003	0.5530	0.4373		
		-0.01	4.6355	-6.1572	0.1576	-0.1090	0.0330	0.5467	0.4523	0.0944	
		-0.00	4,9000	-5.4465	0.1594	-0.2314	0.0421	0.5404	0.4534		-1.2218
		-0.00	5.1679	-4-1016	0.2443	-0.3998	0.0527	0.5321	0.4922		1.1607
		-0.00	5.5233	-6.0634	0.5055	-0.3235	0.0432		0.5100		-1.0978
	. 4 /	-0.00	5.5206	-5,4753	0.2151	-0.3200	5840.0	0.5216	0.4951	0.0265	-1,0624

11 15.97 -0.0U	E	1 OF 1		FONNERI			MARTIN M	ISSILE TA	MEL FACILI	DATA	AER	DOYNAMIC <u>LIND</u> TUNN	·
	_	TEST					L OEL						
1 -0.01 -0.00 0.0278 -0.1673 -0.0273 0.0914 0.0003 0.3144 0.1092 0.2051 -6.0258 2 1.79 -0.00 0.3661 -0.0770 -0.0274 0.0014 0.0038 0.3022 0.1122 0.1900 -2.6786 3 3.98 -0.00 0.7455 -2.0050 -0.0231 0.0824 0.0061 0.3022 0.1211 0.1811 -2.6787 0.7455 -7.0050 -0.0231 0.0824 0.0061 0.3022 0.1217 0.176 -2.6787 0.776 -7.006 0.1539 0.0155 0.0825 0.0061 0.3022 0.1217 0.176 -2.6788 0.0061 0.3022 0.1217 0.176 -2.6788 0.0061 0.3022 0.1217 0.176 -2.6788 0.0061 0.3022 0.1217 0.176 -2.6788 0.0061 0.3022 0.1217 0.176 -2.7788 0.0061 0.3025 0.1354 0.1911 -2.7888 0.0061 0.3025 0.1354 0.1911 -2.7888 0.0061 0.3025 0.1354 0.1911 -2.7888 0.0061 0.3025 0.1354 0.1911 -2.7888 0.0061 0.3025 0.1354 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1364 0.1911 -2.7888 0.0061 0.3025 0.1367 0.1387 0.1941 -2.7888 0.0061 0.3025 0.1497 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1497 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1497 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1497 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1497 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1497 0.1091 0.2053 -2.6275 0.1191 0.1900 -2.6180 0.0061 0.3025 0.1491 0.1716 -2.4214 0.0061 0.0061 0.3025 0.1907 0.1716 0.1900 -2.6180 0.0061 0.0061 0.3006 0.1900 0.2050 0.1900 0.1900 0.2050 0.1900 0.1900 0.2050 0.1900 0.		•				•		5 050	4.1	- Calleranes			
2 1.49 -0.00	DINT												
3 3.98 - 0.00													
5.95 -0.00 1,163 -3.1266 -0.0197 0.0626 0.0061 0.3062 0.1287 0.1776 -2.7288 5.703 -0.00 1.6013 -0.6161 -0.0146 0.0065 0.0066 0.3265 0.1354 0.1911 -2.7488 6. 7.03 -0.00 1.6013 -0.4161 -0.0146 0.0465 0.0066 0.3267 0.1387 0.1941 -2.7578 7. 9.06 -0.00 1.6773 -4.9167 -0.0115 0.0367 -0.0003 0.3327 0.1387 0.1941 -2.7578 8. 9.3 -0.00 1.6013 -0.0115 0.0169 0.0517 0.0015 0.3550 0.1497 0.2053 -2.6275 9. 11.96 -0.00 7.2177 -5.5756 -0.0141 0.0460 0.0045 0.3706 0.1717 0.1990 -2.5118 10. 13.05 -0.00 2.5756 -6.2386 -0.0065 0.0507 0.0012 0.3906 0.2191 0.1716 -2.4214 11. 5.97 -0.00 2.6460 -6.081 0.0178 -0.0000 -0.0081 0.4098 0.2655 0.1643 -2.2508 12. 17.00 -0.00 2.9666 -6.2326 -0.0006 -0.0006 -0.0008 0.4270 0.2755 0.1515 -2.1651 13. 16.06 -0.01 3.0651 -6.2121 0.0226 -0.0008 -0.0081 0.4503 0.2248 0.1515 -2.1651 14. 19.06 -0.00 3.1656 -5.9683 0.0266 -0.0085 -0.0183 0.6816 0.3145 0.1670 -1.6791 15. 20.11 -0.00 3.1520 -5.6200 0.0030 -0.0820 -0.0236 0.5225 0.3339 0.1786 -1.7195 16. 20.10 -0.00 3.2066 -5.6687 0.0068 -0.0826 -0.0236 0.5225 0.3339 0.1786 -1.7195 17. 21.13 C.00 3.3865 -5.6832 0.0283 -0.0823 -0.0237 0.5111 0.3536 0.1565 -1.7635 18. 22.16 -0.00 3.5430 -5.6632 0.0283 -0.0823 -0.0237 0.5111 0.3536 0.1565 -1.7635 19. 23.20 -0.00 3.6016 -5.6632 0.0283 -0.0826 -0.0073 0.5550 0.3894 0.1551 -1.6041 22. 25.27 -0.01 4.2616 -5.9926 0.0628 0.0073 0.0555 0.0498 0.1622 -1.5352 23. 24. 25. 0.00 4.8202 -5.9955 0.1755 -0.2679 0.0245 0.5550 0.4795 0.00757 -1.2438 24. 27. 36 -0.00 5.8930 -5.6636 0.0871 -0.2997 0.0545 0.5561 0.4002 0.0679 -1.4778 25. 28.41 -0.00 5.9360 -5.0716 0.1735 -0.2667 0.0545 0.5561 0.4053 0.0508 -1.4796 0.0977	3	3.94											
5 7.93 -0.00 1.5941 -4.3624 -0.0135 0.0454 0.0081 0.3265 0.1354 0.1011 -2.7576 6 7.93 -0.00 1.4013 -4.4101 -0.0144 0.0465 0.0084 0.3327 0.1387 0.1387 0.1941 -2.7576 7 9.94 -0.00 1.4073 -4.4107 -0.0115 0.0367 -0.0003 0.3327 0.1387 0.1387 0.2461 -2.5176 8 9.93 -0.00 1.9000 -5.1515 -0.0169 0.0517 0.0015 0.3550 0.1497 0.2053 -2.6275 9 11.94 -0.00 7.2177 -5.5754 -6.2386 0.0045 0.0045 0.3706 0.1717 0.1990 -2.5118 10 13.95 -0.00 7.7574 -6.2386 -0.0065 0.0507 0.0012 0.3906 0.2191 0.1716 -2.4214 11 15.97 -0.00 7.4400 -0.0081 0.0178 -0.0004 0.0012 0.3906 0.2191 0.1716 -2.4214 11 15.97 -0.00 7.4400 -0.0081 0.0178 -0.0004 0.00081 0.4098 0.2455 0.1643 -2.2508 12 17.00 -0.00 7.4400 -0.0081 0.0028 -0.0000 0.4098 0.2455 0.1643 -2.2508 13 18.04 -0.01 3.0051 -6.2121 0.0224 0.0139 -0.0091 0.4093 0.2488 0.1515 -2.1631 15 19.06 -0.00 3.1856 -5.4083 0.0264 -0.0085 -0.0103 0.4916 0.3145 0.1670 -1.6791 15 20.11 -0.00 3.1520 -5.4093 0.0264 -0.0085 -0.0103 0.4916 0.3145 0.1670 -1.6791 15 20.11 -0.00 3.1856 -5.4083 0.0264 -0.0085 -0.0133 0.5225 0.3339 0.1786 -1.7795 16 20.10 -0.00 3.8855 -5.8832 0.0283 -0.0283 -0.0237 0.5311 0.3689 0.1622 -1.6792 18 22.16 -0.00 3.5865 -5.8832 0.0283 -0.0823 -0.0284 0.5101 0.3536 0.1665 -1.7795 18 22.26 -0.00 3.7611 -5.7739 -0.0048 0.0529 0.0073 0.5525 0.3894 0.1522 -1.6792 20 24.22 -0.00 3.7611 -5.7739 -0.0048 0.0080 0.0073 0.5550 0.4198 0.1622 -1.6792 21 23.20 -0.00 3.7611 -5.7739 -0.0048 0.0080 0.0073 0.5550 0.4198 0.1652 -1.4728 22 25.27 -0.01 4.2616 -5.4920 0.0082 0.0073 0.5550 0.4198 0.1652 -1.4728 22 25.27 -0.00 4.2616 -5.4920 0.0082 0.0073 0.5550 0.4198 0.1652 -1.4728 22 25.27 -0.00 4.2616 -5.4920 0.0082 0.0073 0.5550 0.4198 0.1652 -1.4728 23 26.30 -0.00 4.202 -5.9955 0.1713 -0.2047 0.0545 0.5540 0.4085 0.0069 -1.3352 24 27 -0.00 5.8591 -5.47798 0.2163 -0.0373 0.0785 0.5489 0.5700 0.0069 -1.3352 25 28.41 -0.00 5.8591 -5.47798 0.2163 -0.0373 0.0786 0.5540 0.5050 0.0073 0.0569 -1.0531 27 30.45 -0.00 5.8591 -5.47798 0.2163 -0.0373 0.0786 0.5040 0.5040 0	-	5.95											
6 7.93 -0.00 1.6013 -0.0146 0.0485 0.0068 0.3327 0.1387 0.1941 -2.7578 7 9.94 -0.00 1.6773 -0.9167 -0.0115 0.0367 -0.0003 0.3397 0.1571 0.1820 -2.6198 1.94 -0.00 1.94 -0.0115 0.0367 -0.0003 0.3397 0.1571 0.1820 -2.6198 1.94 -0.00 2.053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1497 0.2053 -2.6275 0.1515 0.1497 0.2053 -2.6275 0.1515 0.1497 0.2053 0.2061 0.1717 0.1990 -2.5118 0.1395 -0.00 2.7640 0.0012 0.3006 0.2191 0.1716 -2.4214 0.1597 -0.00 2.7640 0.0012 0.3006 0.2091 0.4099 0.2455 0.1643 -2.2508 0.1211 0.1716 -2.4214 0.0128 0.0002 0.0012 0.3006 0.2055 0.1643 -2.2508 0.1211 0.1716 0.2053 0.2053 0.1643 -2.2508 0.1211 0.1716 0.2053 0.2053 0.1643 -2.2508 0.1211 0.1716 0.1916 0.1716 0.1916 0.2053 0.2055 0.1643 -2.2508 0.1211 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916 0.1716 0.1916	5												
7	6												
9 11.94 -0.00	7	9.94	-0.00	1.6773	-4.9167	-0.0119	0.0367	-0.0003	0.3397	0.1571	0,1820	-2,6190	
13.95	Ð				-5.1515	-0.0169	0.0517	0.0015	0.3550	0.1497	0.2053	-2.6275	
11	9												
17.00 -0.00 2.9645 -6.4232 0.0049 0.0228 -0.0002 0.4270 0.2755 0.1515 -2.1631 18.04 -0.01 3.0651 -6.2121 0.0224 0.0139 -0.0091 0.4503 0.2488 0.1515 -2.0267 14 19.06 -0.00 3.1856 -5.4803 0.0266 -0.0085 -0.0139 0.4916 0.3145 0.1670 -1.6791 15 20.11 -0.00 3.1520 -5.4200 0.0430 -0.0820 -0.0234 0.5225 0.3439 0.1786 -1.7795 16 20.10 -0.00 3.2086 -5.6587 0.0430 -0.0826 -0.0246 0.5101 0.3536 0.1565 -1.7635 17 21.13 0.00 3.3865 -5.6832 0.0263 -0.0823 -0.0237 3.5311 0.3689 0.1622 -1.6792 18 22.16 -0.00 3.5430 -5.6832 0.0263 -0.0823 -0.0237 3.5311 0.3689 0.1622 -1.6792 19 23.20 -0.00 3.7611 -5.7739 -0.0048 0.0596 0.0073 0.5582 0.3960 0.1622 -1.5352 20 24.22 -0.00 4.0014 -5.0400 -0.0081 0.0826 0.0073 0.5582 0.3960 0.1622 -1.5352 22 25.27 -0.01 4.2616 -5.4924 0.0428 0.0079 0.0217 0.5648 0.6035 0.1013 -1.4061 23 26.30 -0.00 4.4948 -0.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.00 4.6202 -5.4955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1291 -5.8868 0.1871 -0.2997 0.0585 0.5681 0.4002 0.0679 -1.1477 26 29.46 0.60 5.4831 -5.7798 0.2163 -0.3737 0.0748 0.5524 0.4055 0.0569 -1.0531 27 30.55 -0.00 5.4831 -5.47798 0.2163 -0.3737 0.0748 0.5544 0.4055 0.0569 -1.0531 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4533 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2698 0.0508 -1.7994	10												
13 16.00 -0.01 3.0051 -0.2121 0.0220 0.0139 -0.0091 0.0503 0.2488 0.1515 -2.0267 14 19.00 -0.00 3.1856 -5.7883 0.0260 -0.0085 -0.0183 0.0816 0.3145 0.1670 -1.6791 15 20.11 -0.00 3.1520 -5.0200 0.0030 -0.0820 -0.0234 0.5225 0.3439 0.1786 -1.7195 16 20.10 -0.00 3.2066 -5.6567 0.0003 -0.0845 -0.0206 0.5101 0.3536 0.1565 -1.7635 17 21.13 0.00 3.3865 -5.6832 0.0263 -0.0833 -0.0237 0.5311 0.3689 0.1622 -1.6792 18 22.16 -0.00 3.5030 -5.6832 0.0263 -0.0833 -0.0237 0.5311 0.3689 0.1622 -1.6792 18 23.20 -0.00 3.7611 -5.7739 -0.0048 0.0596 0.0073 0.5582 0.3960 0.1622 -1.5352 20 24.22 -0.00 4.0016 -5.0000 -0.0011 0.0826 0.0073 0.5582 0.3960 0.1622 -1.5352 22 25.27 -0.01 4.2616 -5.4926 0.0026 0.0079 0.0217 0.5650 0.4198 0.1652 -1.4728 23 26.30 -0.00 4.4998 -6.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.00 4.6908 -6.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 25 28.41 -0.00 5.1271 -5.8868 0.1871 -0.2997 0.0585 0.5481 0.4802 0.0679 -1.1477 26 29.46 0.60 5.4691 -5.7798 0.2163 -0.3737 0.0708 0.5520 0.4855 0.0569 -1.0531 27 30.55 -0.00 3.2587 -5.8636 0.0573 -0.2667 0.0545 0.5349 0.5533 0.0508 -1.7994 28 20.10 0.00 3.2587 -5.8636 0.0519 -0.0046 0.0080 0.3455 0.2498 0.0957 -2.6446	11												
14 19.06 -0.00 3.1896 -5.9483 0.0266 -0.0085 -0.0183 0.4816 0.3145 0.1670 -1.6791 15 20.11 -0.00 3.1520 -5.6200 0.0430 -0.0820 -0.0234 0.5225 0.3439 0.1786 -1.7195 16 20.10 -0.00 3.2086 -5.6567 0.0403 -0.0845 -0.0246 0.5101 0.3536 0.1565 -1.7635 17 21.13 0.00 3.3865 -5.6832 0.0283 -0.0823 -0.0237 0.5311 0.3689 0.1622 -1.6792 18 22.16 -0.00 3.5430 -5.6832 0.0096 -0.0219 -0.0140 0.545 0.3894 0.1551 -1.6041 19 23.20 -0.00 3.7611 -5.7739 -0.0048 0.0596 0.0073 0.5582 0.3960 0.1622 -1.5352 20 24.22 -0.00 4.0014 -5.6900 -0.0081 0.0826 0.0084 0.5650 0.4198 0.1452 -1.4728 22 25.27 -0.01 4.2616 -5.4924 0.0428 0.0079 0.0217 0.5648 0.4035 0.1013 -1.4061 23 26.30 -0.00 4.4948 -0.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.00 4.6202 -5.9955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1271 -5.8868 0.1871 -0.2997 0.0585 0.5481 0.4802 0.0679 -1.1477 26 29.46 0.00 5.4891 -547798 0.2163 -0.3737 0.0748 0.5474 0.4855 0.0569 -1.0531 27 30.55 -0.00 5.9308 -5.0716 0.1735 -0.2607 0.0545 0.5349 0.5706 0.0143 -0.9727 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4633 0.00957 -2.6448					-								
15													
16													
17 21.13 G.OU 3.3865 -5.0832 0.0263 -0.0823 -0.0237 0.5311 0.3689 0.1622 -1.6792 18 22.16 -0.04 3.5430 -5.6832 0.0696 -0.0219 -0.0140 0.5445 0.3894 0.1551 -1.6041 19 23.20 -0.04 3.7611 -5.7739 -0.0048 0.0596 0.0073 0.5882 0.3960 0.1622 -1.5352 20 24.22 -0.06 4.0014 -5.0000 -0.0011 0.0826 0.0074 0.5650 0.4198 0.1452 -1.4720 22 25.27 -0.41 4.2616 -5.4924 0.0428 0.0079 0.0217 0.5648 0.4535 0.1013 -1.4061 23 26.30 -0.00 4.4998 -6.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.06 4.8202 -5.9955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1271 -5.8868 0.1871 -0.2997 0.0585 0.5481 0.402 0.0679 -1.1477 26 29.46 0.40 5.4821 -5.47798 0.2163 -0.3737 0.0748 0.5424 0.4055 0.0569 -1.0531 27 30.55 -0.00 5.9300 -5.0716 0.1735 -0.2647 0.0545 0.5349 0.5050 0.0143 -0.9727 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4533 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448													
18	17												
19 23.20 -0.00 3.7611 -5.7739 -0.0048 0.0596 0.073 0.5582 0.3960 0.1622 -1.5352 20 24.22 -0.00 4.0014 -5.04000 -0.0081 0.0826 0.0084 0.5650 0.4198 0.1452 -1.4728 22 25.27 -0.01 4.2616 -5.4924 0.0428 0.0079 0.0217 0.5648 0.4635 0.1013 -1.4061 23 26.30 -0.00 4.4948 -6.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.00 4.8202 -5.9955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1271 -5.8868 0.1871 -0.2997 0.0585 0.5481 0.4802 0.0679 -1.1477 26 29.46 0.60 5.4891 -5.7798 0.2163 -0.3737 0.0748 0.5424 0.4855 0.0569 -1.0531 27 30.55 -0.00 5.9308 -5.0718 0.1735 -0.2647 0.0545 0.5349 0.5206 0.0143 -0.9727 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4633 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448	18		_		_								
22 25.27 -0.01 4.2616 -5.4924 0.0428 0.079 0.0217 0.5648 0.4635 0.1013 -1.4061 23 26.30 -0.00 4.4948 -6.0081 0.1011 -0.1100 0.0392 0.5584 0.4715 0.0869 -1.3352 24 27.36 -0.00 4.8202 -5.4955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1271 -5.8668 0.1871 -0.2997 0.0585 0.5481 0.4802 0.0679 -1.1477 26 29.46 0.60 5.4831 -5.47798 0.2163 -0.3737 0.0748 0.5424 0.4802 0.0669 -1.0531 27 30.45 -0.00 5.9300 -5.0716 0.1735 -0.2647 0.0545 0.5349 0.5206 0.0143 -0.9727 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4533 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448	19		-0-00	3.7611	-5.7739	-0.004							
23	20	24.22	-0.00	4.0014	-5-0400	-0.006	1 0.0826	0.0074	0.5650	0.4198			
27.36 -0.00 4.8202 -5.9955 0.1745 -0.2679 0.0624 0.5553 0.4795 0.0757 -1.2438 25 28.41 -0.00 5.1291 -5.8868 0.1871 -0.2997 0.0585 0.5481 0.4802 0.0679 -1.1477 26 29.46 0.60 5.4891 -547798 0.2163 -0.3737 0.0748 0.5474 0.4855 0.0569 -1.0531 27 30.45 -0.00 5.9300 -5.0716 0.1735 -0.2647 0.0545 0.5349 0.5206 0.0143 -0.9727 28 20.10 0.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4533 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448	25						6 0.0079						
25	23												
26	74												
27 30.45 -0.00 5.9304 -5.0716 0.1735 -0.2607 0.0545 0.5349 0.5206 0.0143 -0.9727 28 20.10 9.00 3.2587 -5.8636 0.0573 -0.1698 -0.0316 0.5041 0.4533 0.0508 -1.7994 29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448	25		_								1111 -		
28	56												
29 9.93 -0.00 1.9072 -5.0441 -0.0119 0.0446 0.0080 0.3455 0.2498 0.0957 -2.6448													
													·
24 -0001 -00025 -001230 -001251 000000 000101 001101 001150 -000100	_												
•	34		-0000	0.0354	-0.01436	-0.032	10.0770	0.0101	043104	0.1401	0.1.54	-2014	
	_												

								IL EFFECTS			
	TEST	PART MA 32 0.9	CH RX10-6	PHI 0.0'	CONF Senof 13	L DEL1	DELZ	DEL3 DEL4	TRANSITI UNKNOWN	ON	
INT"	ALPHA	BF TA	CN.	CLM	CA	CLM	CLL	CA	CAB	CAF"	ACP
<u> </u>	-0.01	-0.00			-0.0301		0.0116	0.3492	0.1091		-7,3662
2	1.98	-0.00	0.3744	-1.0886			0.0151	0.3424	0.1232	0.2191	-2.8692
1	1.98	-0.00		-1-115#			0.0150	0.3434	0.1228		-2.8861
	3.96				-0.0233		0.0122	0.3405	0.1276		-2.8175
	5.94	-0.00	1.1953 1.62u5	-3.3630			0.0127	0.3469	0.1452	0.2017	-2.8302
	9.91	-0.00		-5.5618			0.0098	0.3652 0.3826	0.1541 0.1572	0.2111 0.2154	-2.80 66 -2.75 68
	11.94	-0.00	2.3126	-5.9502			0.0112	0.3876	0.1982	0.1994	-2.5729
	11.94	-0.00	2.3201	-6.0036			0.0112	0.3963	0.1954		-2.5877
	13.94	-0.00		-6.5271			0.0077	0.4094	0.2232		-2.4699
	13.94	-0.00		-6.6368			0.0077	0.4166	0.2470		-2.4778
	15.97	-0.00	2.9699	-6.9131	-0.0027		0.0220	0.4324	0.2675		-2.3121
	16.96	-0.00	3.1016	-6.9045	0.0115		0.0081	0.4359	0.2791		-2.2261
	18.00	-0.00	3.2960	-7.1439			0.0013	0.4524	0.2787	0.1737	-2.1674
	19.04	-0.00		-7.0624			0.0007		0.2918		-2.0657
i i	20.06	0.00		-6.6201			-0.0423		0.3128		-1.9149
	21.15	0.01		-4.4346			-0.0542		0.3271		-1.7663
	22.10	0.00		-6.0510			-0.0147		0.3549		-1.6315
	22.16	0.00		-6.1459			-0.0266	0.5330	0.4035		-1.6473
	23.20	-0.00	3.8940	-5.4872			0.0133		0.4058		-1.5375
		-0.00		-6.0162			0.0362		0.4261		-1.4541 -1.4415
	25.28			-6.0706			0.0522		0.4351		-1.3616
-	26.33	-0.00		-6-0539			0.0522		0.4582		-1.2903
	26.33	-0.00	4.7032	-6.0586			0.0715		0.4629		-1.2903
_	27.40	0.00	5.0575	-5.9370			0.0845		0.4678		-1.1636
		-0.00		-5.8194			0.0650		0.4737		-1.0777
	29.54	0.00		-5.7153			0.0766		0.4765		-0.9922
		-0.00		-5.6189			0.0556		0.4972	0.0503	
_	20.07	0.00	3.4930	-6.7567	0.053	0 -0.1573	-0.0276		0.3641		-1.9344
	9.91	-0.00	2.0458	-5.6271	-0.013	7 0.0635	0.0230	0.3826	0.2676		-2.7505
		-0.00		-0.3321			0.0179		0.1756	0.2095	-3.5977
	-0.01	0.0c	0.0230	-0.1767	-0.033	7 0.0980	0.0164	0.3425	0.1580	0.1845	-7."458

	_		ACH #X10-		CONF			DEL3 DEL4				
	1	23 0.	94 2.3	0.0	34#0F13 0		0	0 0	UNKNOWN			
OINT	ALPHA	BETA	- CN	CLM	ČŸ	CLN	CLL	CA.	CAR	CAF	KCP	
1	-0.01	-0.0u	0.0430	-0.2484	-0.0427	0.1274	0.0179	0.3939	0.1395	0.2544	-5,7860	
5	1.98	-0.00	0.4016	-1.1644	-0.0330	0.1061	0.0195	0.3770	0.1-86	5855.0		
3	3.96	-0.00	0.80%	-2.7623		0.0761	0.0185	0.3688	0.1586		Z.7951	
•	3.96	-0.00	0.7928	-2.2351		0.0788	0.0167	0.3838	0.1464		-5.6100	
	5.94	-0.00	. 1.2171	-3.4175	-0.0185	0.0689	0.0157	0.3799	0.1739		-5-9091	
	5.94	-0.03	1.2190	-3.4264	-0.020-	0.0752	0.0157	0.3896	0.1743	0.2155	-2.6109	
7 -	7.92	-0.00	1.6314	-4.3604	-0.0198	0.0548	0.0144	0.3974	0.1885	0.2090		
9	11.90	-0.0v	2.0516	-5.6663	-0.0169 -0.0175	0.0516	0.0195	0.4217 0.4375	0.1994	0.2223	-2.7485 -2.67 34	
10	13.93	0.00	2.7046	-6.7495	-0.0163	0.0450	0.0271	0.4323	0.2264	0.2059	-2.5057	
ii	13.93	0.00	2.7582	-6.9127	-0.0186	0.0575	0.0334	0.4441	0.2293	0.2148	-2.5062	
12	15.94	-0.00	3.0675	-7.3173	-0.0030	0.0287	0.0184	0.4591	0.2487	0.2104	-2.3700	
13	16.98	-0.00	3.2181	-7.3142	0.0001	0.0300	0.0196	0.4564	0.2730	0.1834		
14	16.97	-0.00	3.2833	-7.5350	0.0056	0.0153	0.0132	U.4708	0.2764	0.1943	-2,2949	
15	18.01	-0.00	3.4280	~7.5555	0.0058	0.0361	0.0225	0.4729	0.2855	0-1875	-2.2041	
16	19.03	-0.00	3.5957	-7.6266	0.0018	0-03-0	0.0252	0.4688	0.2958	0.1730	-5.1510	
17	20.04	-0.00	3.7706	-7.6927		0.0178	0.0196	0.4815	0.2916		2.0402	
16	21.08	0.00	3.9678	-7.6825		-0.0771	-0.0138	0.4792	0.3131		-1.9265	
19	25.15	0.00	4.1184	-7.3932	0.0731	-0-5018	-0.0349		0.3266		-1.7927	
50	23.16	0.01	4.2267	-0.8970	0.1244	-0.3A62	-0.0490		0.3415		-1.6310	
55 51	23.18	- 0.01	1605.0	-7.0255 -6.4123	0.102d 0.0559	-0.4296	-0.0550 0.0307		0.3512		-1.6538 -1.4659	
53		-0.00	4.3743 4.6512	-6.354e		-0.0357	0.0532		0.3667 0.4014		-1.3663	
54 —	26.35	-0.00	4.9345	-6.2412		-0.1155	0.0828		0.4284		-1.2646	
25	26.35	-0.00	4.9705	-6.28.0			0.0873		0.4372		-1.2642	
26	27.45	0.00	5.2575	-6.0767		-0.2037	0.0895		0.4577	0.1161	-1.1463	
27	27.44	0.00	5.3136	-6.0752		-0.1954	0.0924		0.4626		-1.1433	
28	28.52	0.00	5.6990	-5.4314		-0.2763	0.0817		0.4621	0.1064		
29	29.58	0.00	6.0482	-5.9224	0.1619	-0.3087	0.0871	0.5616	0.4755		-0.9793	
30	30.65	0.00	6.4095	-5.0026	0.1001	-0.2191	0.0557	0.5525	0.4799		-0.9178	-
31	20.05	-0.00	3.9365	-8. COH4	0.0015	0.0206	0.0208	0.5057	0.3920	0.1132	-2.0344	
35	20.04	-0.00		-7.d303		0.0437	0.0292	0.4806	0.3717	0-1089	-2.0376	
33	_ 9.90		_	-5.6720			0.0226		0.2719		2.7563	
34	-0.01	-0.00	0.0541	-0.2682	-0.0380	0.1297	0.0211	0.3987	0.1778	0.2209	-4.9623	

	1 OF 1					IN AITHAN	551LE T	ANEL FACILIY	DATA		DÖLMVATC	utho_tunnel_(41)_
	TEST 1		BLH RX10-6		CONF SAUDF13 (L 0EL1			TRANSITI			
POINT	ALPHA -	RETA	CN	CLH	CA _	CLN	CLL	CA "	CAR	CAF	ACP	
1	-0.01				-0.0475	0.1631	0.0189	0.5442	0.1533		-7.5104	
2	-0.01	-0.01		-0.1827		0.1611	0.0141	0.5471	0.1804		-7-7217	
3	-0.01	-0.01	0.0711	-C-1767		0.1605	0.0173	0.5477	Ne05.0		-8.3710	
•	-0.01	-0.01		-0.1884		0.1596	0.0167	0.5487	0.2085		-6.3500	
2	1.98	-0.01		-1.1216		0.1334	0.0188	0.5475	0.2024		-2.0697	
•		-0.01			-0.0405	0.1471	0.0205	0.5413	0.2091		-2.9065	
	3,96	-0.01			-0.0334	6.1309	0.0194	0.5280	0.2162		-5-8548	
•	5.95	-0.01		-3.4657			0.0169		0.2216		-2.0104	
		-0.01		-3.4314			0.0182	0.5408	0.2151	0.3258	-2-0014	
0		-0.00		-4.5717		0.1023	0.0185	0.5529	0.2281		-2.7681	
11 12	7.91 9.91	-0.00	1.6368	-4.5485	-0.0325 -0.0277	0.1056	0.0185	0.5507	0.2311		-2.7755	
13	11.91	0.00		-6.3710		0.0818 C.0649	0.0199	0.5778	G.2398 G.2483		-2.6894	
14	13.92	0.00	2.4507	-7.1844			0.0272		0.2586		-2,597 <u>7</u> -2,504 5	
15	15.96	-0.00		-7.54A6			0.0252		0.2673		-2,3434	
16	16.97	-0.00		-7.750e			0.0231	0.6008	0.2740		-2.2665	
17	18.00	-0.00		-7.7564			0.0273		0.2813	0.3226	-5.1965	
18	19.02	-0.00	3.8377	-6.1334		0.0101	0.0253		0.2944	0.3099	-2.1193	
19	20.05	-0.00		-6.2632			0.0278		0.3045		-2.0349	
50	21.09	-0.00		-8.3800			0.0271		0.3125		-1.9357	
21	22.15	-0.00		-6.4177			0.0169		0.3148		-1.0233	•
55	23.16	-0.00		-8.3542			0.0127		0.3153		-1.7117	
23		-0.00		-A.275A			0.0179		0.3270		-1-6028	
2=-	25.30	0.00		-8.2534			0.0376		0.3400		-1.5e72	
25	26.39	0.01	5	-8.1636	-		0.0772		0.3536		-1.4069	
26	26.37	0.01	5.7988	-H-1734			0.0742		0.3583		-1.4095	
27	27.44	0.01	6.1533	-8.0673			0.0837		0-3663		-1.3111	-
28	28.50	0.01	6.4547	-7.9347			0.0879		0.3784		-1.2293	
29	29.56	0.01	6.7622	-7.8565	0.1625	-0.3566	0.0697	0.5565	0.3012		-1.1616	
30	30.63	0.00	7.0083	-7.6740	0.1282	-0.2334	0.0506		0.3687		-1.0957	
11	20.05	0.00	4.0447	-A.231e	0.0119	-0.0061	0.0309		0.3882		-2.0352	
32	9.91	-0.00	2.0360	-5-5073	-0.0c6d	0.08>2	0.0230	0.5744	0.3081		-2.7050	-
22	-0.01	-0.01	0.0275	-0.2066	-0.0459	0.1635	0.0202	0.5513	0.2503		-7.5185	

TEST PAPT MACH RX10-6 PHI COMF L ULLI OFL2 DEL3 DEL4 TRANSITION 1 ALPHA 8Ffs CN CLM CV CLM CX CLL CA CAR CAPT MCP -0.01 -0.01 0.0222 -0.1498 -0.0466 0.1810 0.0215 0.5783 0.2076 0.3707 -4.7339 1.99 -0.01 0.4085 -1.1733 -0.0549 0.2169 0.0222 0.5737 0.1946 0.3751 -2.0721 1.99 -0.01 0.4085 -1.1733 -0.0549 0.2169 0.0222 0.5737 0.1946 0.3751 -2.0721 3.96 -0.01 0.7093 -1.0466 -0.0202 0.1718 0.0218 0.5705 0.2211 0.1494 -2.0211 3.96 -0.01 0.7012 -2.1523 -0.0475 0.1959 0.0225 0.5646 0.2047 0.3558 -2.0826 3.96 -0.01 1.1946 -3.2535 -0.0327 0.1040 0.0208 0.5641 0.2256 0.3355 -2.7355 5.96 -0.01 1.1946 -3.2535 -0.0327 0.1404 0.0208 0.5641 0.2256 0.3345 -2.7235 5.96 -0.01 1.9950 -4.2700 -0.0328 0.1737 0.0221 0.5016 0.2291 0.3267 2.2298 11.94 -0.00 7.3717 -0.001 1.0909 -5.2409 -0.0312 0.1137 0.0224 0.5767 0.2291 0.3267 2.2291 0.3267 2.2208 11.94 -0.00 7.3717 -0.0505 -0.0275 0.0999 0.0253 0.5961 0.2250 0.3365 -2.02266 11.94 -0.00 7.3717 -0.0110 0.0017 0.0260 0.6040 0.2511 0.3562 -2.0218 13.95 -0.06 7.4061 -6.7962 -0.0739 0.0899 0.0254 0.6006 0.2513 3.5567 -2.3222 16.97 -0.00 3.4744 -7.1172 -0.0066 0.0620 0.0728 0.6100 0.2591 0.3597 -2.0229 19.00 -0.00 3.9575 -7.6780 -0.0036 0.0620 0.0728 0.6100 0.2591 0.3509 -2.2499 19.00 -0.00 3.9575 -7.6780 -0.0017 0.0451 0.0027 0.5960 0.2261 0.3313 -7.21823 19.00 -0.00 3.8500 -7.0859 0.0017 0.0451 0.0260 0.5043 0.2813 3.5567 -2.2322 27.15 -0.00 4.0505 -0.0060 0.0101 0.0463 0.0241 0.0516 0.5968 0.2780 0.2781 0.3599 -2.2499 11.00 -0.00 3.8570 -7.6859 0.0017 0.0451 0.0007 0.5551 0.5969 0.2781 0.3599 -2.2499 27.15 -0.00 4.0510 -0.0505 0.0007 0.0451 0.0007 0.0510 0.0513 3.5567 -2.2616 27.15 -0.00 4.0510 -0.0510 0.0007 0	T	enginee 1 Of 1 1 Of 1	PING UEVE	LOPMENT	CENTERIA	EDC) P	ROPULSION (SSILE TA	MEL FACILI'	TY(P=T) DATA	AER	ODYNAMIC WIND TUNNEL (4)
-0.01 -0.01 0.0222 -0.149A -0.0486 0.1810 0.0215 0.5783 0.2076 0.3767 -A.7339 1.49 -0.01 0.4045 -1.1733 -0.0549 0.2167 0.0226 0.5737 0.1986 0.3751 -2.8721 1.98 -0.01 0.3403 -1.0364 -0.0420 0.1718 0.0218 0.5705 0.2211 0.3649 -2.8101 3.96 -0.01 0.7612 -2.4703 -0.0475 0.1959 0.0225 0.5646 0.2047 0.3598 -2.8288 3.96 -0.01 0.7612 -2.1523 -0.0421 0.1637 0.0221 0.5616 0.2260 0.3355 -2.7351 5.96 -0.01 1.1966 -3.2535 -0.0327 0.1604 0.0208 0.5661 0.2256 0.3385 -2.7351 7.94 -0.00 1.5995 -4.7900 -0.0328 0.1761 0.0224 0.5767 0.2291 0.3676 -2.6887 9.92 -0.00 1.9994 -5.2609 -0.0312 0.1137 0.0240 0.5886 0.2350 0.3536 -2.6286 11.94 -0.00 7.3573 -5.0565 -0.0275 0.0999 0.0253 0.5941 0.2400 0.3554 -2.5656 11.94 -0.00 7.3673 -5.065 -0.0275 0.0999 0.0253 0.5941 0.2400 0.3561 -2.5656 11.95 -0.00 3.2400 -7.5379 -0.0110 0.0617 0.0260 0.6026 0.2445 0.3582 -2.4219 15.95 -0.00 3.2400 -7.5379 -0.0110 0.0617 0.0260 0.6026 0.2531 3.5567 -2.3222 16.97 -0.00 3.5975 -7.6760 -0.0036 0.0555 0.0282 0.5998 0.2288 0.3313 -2.1363 19.04 -0.00 3.5975 -7.6760 -0.0036 0.0555 0.0282 0.5998 0.2288 0.3313 -2.1363 20.06 -0.00 4.0554 -8.2786 0.0017 0.0451 0.0507 0.5760 0.2721 0.3239 -2.085 21.11 -0.06 4.3597 -8.1497 0.0136 0.0411 0.0220 0.5843 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 -0.0047 0.0655 0.0282 0.5988 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 0.0010 0.0411 0.0220 0.5843 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 0.00247 0.0555 0.0144 0.5698 0.2998 0.2708 -1.68676 23.21 -0.01 4.6630 -8.2770 0.0468 -0.0167 0.0251 0.5843 0.3087 0.3966 -1.8993 24.26 -0.01 5.2591 -6.3097 0.0241 0.0455 0.0440 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1576 0.0465 0.0563 0.3999 0.2503 -1.6676 27.40 -0.00 4.7199 -8.2299 0.1166 -0.1579 0.0466 0.5530 0.3999 0.3514 0.1680 -1.2646 29.59 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0250 0.0466 0.5530 0.3999 0.3514							.0 0	0	DEL3 DEL4	TRANSITI	04	
-0.01 -0.01 0.0222 -0.149A -0.0486 0.1810 0.0215 0.5783 0.2076 0.3767 -A.7339 1.49 -0.01 0.4045 -1.1733 -0.0549 0.2167 0.0226 0.5737 0.1986 0.3751 -2.8721 1.98 -0.01 0.3403 -1.0364 -0.0420 0.1718 0.0218 0.5705 0.2211 0.3649 -2.8101 3.96 -0.01 0.7612 -2.4703 -0.0475 0.1959 0.0225 0.5646 0.2047 0.3598 -2.8288 3.96 -0.01 0.7612 -2.1523 -0.0421 0.1637 0.0221 0.5616 0.2260 0.3355 -2.7351 5.96 -0.01 1.1966 -3.2535 -0.0327 0.1604 0.0208 0.5661 0.2256 0.3385 -2.7351 7.94 -0.00 1.5995 -4.7900 -0.0328 0.1761 0.0224 0.5767 0.2291 0.3676 -2.6887 9.92 -0.00 1.9994 -5.2609 -0.0312 0.1137 0.0240 0.5886 0.2350 0.3536 -2.6286 11.94 -0.00 7.3573 -5.0565 -0.0275 0.0999 0.0253 0.5941 0.2400 0.3554 -2.5656 11.94 -0.00 7.3673 -5.065 -0.0275 0.0999 0.0253 0.5941 0.2400 0.3561 -2.5656 11.95 -0.00 3.2400 -7.5379 -0.0110 0.0617 0.0260 0.6026 0.2445 0.3582 -2.4219 15.95 -0.00 3.2400 -7.5379 -0.0110 0.0617 0.0260 0.6026 0.2531 3.5567 -2.3222 16.97 -0.00 3.5975 -7.6760 -0.0036 0.0555 0.0282 0.5998 0.2288 0.3313 -2.1363 19.04 -0.00 3.5975 -7.6760 -0.0036 0.0555 0.0282 0.5998 0.2288 0.3313 -2.1363 20.06 -0.00 4.0554 -8.2786 0.0017 0.0451 0.0507 0.5760 0.2721 0.3239 -2.085 21.11 -0.06 4.3597 -8.1497 0.0136 0.0411 0.0220 0.5843 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 -0.0047 0.0655 0.0282 0.5988 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 0.0010 0.0411 0.0220 0.5843 0.2897 0.2866 -1.8893 22.15 -0.00 4.6521 -6.2786 0.00247 0.0555 0.0144 0.5698 0.2998 0.2708 -1.68676 23.21 -0.01 4.6630 -8.2770 0.0468 -0.0167 0.0251 0.5843 0.3087 0.3966 -1.8993 24.26 -0.01 5.2591 -6.3097 0.0241 0.0455 0.0440 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1576 0.0465 0.0563 0.3999 0.2503 -1.6676 27.40 -0.00 4.7199 -8.2299 0.1166 -0.1579 0.0466 0.5530 0.3999 0.3514 0.1680 -1.2646 29.59 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0250 0.0466 0.5530 0.3999 0.3514	LNT.	ALPHA	BFTA	CN	CĻ=	CA	CLN	CLL	CA	CAB	CAF	XCP
1.98 -0.01 0.3403 -1.0964 -0.0020 0.1716 0.0216 0.5705 0.2211 0.3494 -2.8101 3.96 -0.01 0.7612 -2.1523 -0.421 0.1637 0.0221 0.5646 0.2047 0.3598 -2.8206 3.96 -0.01 1.1946 -3.2535 -0.0327 0.1040 0.0220 0.5646 0.2260 0.3385 -2.7235 5.96 -0.01 1.1946 -3.2535 -0.0327 0.1040 0.0220 0.5641 0.2256 0.3385 -2.7235 7.94 -0.00 1.5994 -5.2409 -0.0324 0.1761 0.0224 0.5767 0.2291 0.3676 -2.6867 9.92 -0.00 1.9994 -5.2409 -0.0312 0.1137 0.0220 0.5886 0.2350 0.3536 -2.6206 11.94 -0.00 7.3673 -5.0565 -0.0275 0.0989 0.0253 0.5941 0.2600 0.3561 -2.5265 13.95 -0.00 7.0061 -6.7962 -0.00739 0.0889 0.0253 0.5941 0.2600 0.3561 -2.5265 13.95 -0.00 3.2460 -7.5379 -0.0110 0.0617 0.0260 0.6080 0.2513 0.3567 -2.3222 14.97 -0.00 3.5975 -7.6760 -0.0066 0.0620 0.0728 0.6100 0.2513 0.3567 -2.3222 14.90 -0.00 3.5975 -7.6760 -0.0036 0.0655 0.0282 0.5998 0.2684 0.3313 -2.1343 19.00 -0.00 3.5975 -7.6760 -0.0036 0.0655 0.0282 0.5998 0.2684 0.3313 -2.1343 20.06 -0.00 4.0854 -8.0065 0.0101 0.0463 0.0221 0.5944 0.2628 0.3087 -1.9598 21.11 -0.00 4.3597 -8.1497 0.0136 0.0461 0.0220 0.5843 0.2897 0.2806 -1.6893 22.15 -0.00 4.6521 -6.2766 -0.0036 0.0655 0.0282 0.5948 0.2684 0.3313 -2.1343 22.17 -0.01 4.6630 -0.1630 0.0103 0.0779 0.0139 0.5785 0.3292 0.2838 -1.7849 22.17 -0.01 4.6630 -0.1630 0.0103 0.0779 0.0139 0.5785 0.3292 0.2838 -1.7849 22.17 -0.01 5.2591 -5.3397 0.0287 0.0455 0.0144 0.5696 0.2998 0.2708 -1.6893 23.21 -0.01 5.9659 -6.3760 0.0281 0.0455 0.0144 0.5696 0.2998 0.2709 -1.6676 24.26 -0.01 5.2591 -5.3397 0.0287 0.0455 0.0144 0.5696 0.3998 0.2709 -1.6676 24.26 -0.01 5.9629 -6.3601 0.1006 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1006 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1006 -0.1526 0.0421 0.5519 0.3310 0.3499 0.2011 -1.4954 27.54 0.00 6.6355 -8.6674 0.1316 -0.2203 0.0599 0.5560 0.3399 0.2011 -1.4954 27.55 0.00 6.6795 -5.4472 0.1701 -0.0527 0.0712 0.5525 0.3573 0.1852 -1.1436 27.59 0.00 7.00 6.3555 -8.6674 0.1316 0.0159 0.0207 0.5569 0.0567 0.3550 0.2562 -1.4068 20.00 -0.00 7.19	<u> </u>						0.1810	0.0215				-4.7339
3.96 -0.01	2											
3.46 -0.01	•											
5.96 -0.01 1.1946 -3.2535 -0.0327												
7.90 -0.00 1.5996 -0.7900 -0.0328 0.1761 0.0224 0.5767 0.2291 0.3076 -2.6887 9.92 -0.00 1.9999 -5.7209 -0.0312 0.1137 0.0220 0.5886 0.2350 0.3536 -2.6206 11.94 -0.00 7.3373 -5.0565 -0.0675 0.0959 0.0253 0.5941 0.2400 0.3541 -2.5265 13.95 -0.00 7.601 -6.7962 -0.0739 0.0869 0.0264 0.6026 0.2465 0.3502 -2.4219 15.95 -0.00 3.2450 -7.5379 -0.0110 0.0017 0.0260 0.6000 0.2513 0.3567 -2.3222 -2.4219 16.97 -0.00 3.4744 -7.6127 -0.0666 0.0620 0.0728 0.6100 0.2591 0.3509 -2.2499 18.00 -0.00 3.5975 -7.6760 -0.0036 0.0655 0.0262 0.5948 0.2684 0.3313 -2.1343 19.04 -0.00 3.8500 -7.6559 0.0017 0.0551 0.0307 0.5960 0.2721 0.3239 -2.0485 20.08 -0.00 4.0854 -8.0065 0.0101 0.0663 0.0220 0.5843 0.2897 0.2946 -1.8693 21.11 -0.06 4.3597 -8.1497 0.0136 0.0441 0.0220 0.5843 0.2897 0.2946 -1.8693 27.15 -0.00 4.6321 -6.2766 -0.0048 0.0665 0.0274 0.5785 0.3022 0.2783 -1.7782 27.17 -0.01 4.6640 -8.1830 0.0103 0.0779 0.0139 0.5758 0.2920 0.2838 -1.7549 23.21 -0.01 4.9665 -8.2786 0.0241 0.0455 0.0144 0.5696 0.2998 0.2708 -1.6676 24.26 -0.01 5.2591 -6.3097 0.0247 0.0485 0.0144 0.5696 0.2998 0.2708 -1.6676 25.33 -0.00 5.6016 -8.2770 0.0468 -0.0167 0.0220 0.5643 0.3065 0.2577 -1.5801 26.39 -0.00 5.9777 -8.3665 0.1030 -0.0157 0.0391 0.5489 0.3076 0.2271 -1.3946 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5560 0.3037 0.2523 -1.4778 26.39 -0.00 5.9777 -8.3665 0.1030 -0.1526 0.0441 0.5512 0.3311 0.2201 -1.3946 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 27.47 0.00 6.6795 -5.4072 0.1701 -0.3062 0.0723 0.5394 0.3514 0.1806 -1.2046 27.48 0.00 6.7991 -8.4186 0.1579 -0.22837 0.0370 0.5536 0.3525 0.1852 -1.1396 27.59 0.00 6.7970 -8.2299 0.1166 -0.1599 0.0172 0.5525 0.3573 0.1852 -1.1436 27.00 0.00 6.799 -8.2295 0.1166 -0.1599 0.0172 0.5586 0.3525 0.3899 0.25974 -2.46241												
9.92 -0.00	7											
11.94 -0.00	8											
15.95 -0.00	9 .			•	-							
16.97 -0.00 3.6746 -7.6172 -0.0066 0.0620 0.0728 0.6100 0.2591 0.3509 -2.2499 18.00 -0.00 3.5975 -7.6780 -0.0036 0.0655 0.0282 0.5998 0.2688 0.3313 -2.1343 19.00 -0.00 3.67300 -7.6657 0.0017 0.0651 0.0307 0.5960 0.2721 0.3239 -2.0485 20.06 -0.00 4.0854 -8.0065 0.0101 0.0463 0.0241 0.5914 0.2628 0.3087 -1.9598 21.11 -0.00 4.3597 -8.1497 0.0136 0.0441 0.0220 0.5843 0.2897 0.2996 -1.8493 22.15 -0.00 4.6321 -6.2786 -0.004 0.0695 0.0774 0.5785 0.3022 0.2763 -1.7872 22.17 -0.01 4.6640 -6.1830 0.0103 0.0779 0.0139 0.5758 0.2920 0.2838 -1.7549 23.21 -0.01 4.9665 -8.2786 0.0241 0.0455 0.0144 0.5696 0.2998 0.2708 -1.6676 24.26 -0.01 5.2591 -6.3397 0.0247 0.0475 0.0249 0.5643 0.3065 0.2577 -1.5801 25.33 -0.00 5.6016 -8.2770 0.0068 -0.0167 0.0208 0.5560 0.3037 0.2523 +1.4776 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5499 0.3076 0.2012 -1.3908 27.46 0.00 6.3555 -8.6674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 27.59 0.00 6.3555 -5.4672 0.1701 -0.3052 0.0723 0.5386 0.3525 0.1800 -1.2666 29.59 0.00 6.9781 -2.4180 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1800 -1.2666 30.64 -0.00 7.1999 -8.2299 0.1166 -0.1692 0.0712 0.5425 0.3573 0.1800 -1.2666 30.64 -0.00 7.1999 -8.2299 0.1166 -0.1692 0.0712 0.5869 0.2896 0.2896 -1.9468	0			2.5061	-6.7962	-0.0734	0.0859	0.0264	0.6026	0.2445		
18.00 -0.00 3.5975 -7.6780 -0.0036 0.0655 0.0282 0.5998 0.2686 0.3313 -2.1343 19.04 -0.00 3.8300 -7.6659 0.0017 0.0451 0.0307 0.5960 0.2721 0.3239 -2.0485 20.08 -0.00 4.0854 -8.0665 0.0101 0.0463 0.0241 0.5914 0.2628 0.3087 -1.9598 21.11 -0.00 4.3597 -8.1997 0.0136 0.0441 0.0220 0.5843 0.2897 0.2946 -1.8693 22.15 -0.00 4.6321 -6.2786 -0.0048 0.0685 0.0774 0.5785 0.3022 0.2763 -1.7872 22.17 -0.01 4.6630 -8.1630 0.0103 0.0779 0.0139 0.5758 0.2290 0.2838 -1.7549 23.21 -0.01 4.9665 -8.2786 0.0241 0.0455 0.0144 0.5696 0.2998 0.2708 -1.6676 24.20 -0.01 5.2591 -6.3097 0.0247 0.0475 0.0208 0.5560 0.3037 0.2523 -1.4776 25.33 -0.00 5.6016 -8.2770 0.0468 -0.0147 0.0208 0.5560 0.3037 0.2523 -1.4776 26.40 -0.00 6.067 -8.3769 0.1034 -0.1510 0.0391 0.5489 0.4076 0.2412 -1.3946 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1566 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9029 -8.301 0.1006 -0.1569 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.4072 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1080 -1.2448 29.59 0.00 6.799 -8.2299 0.1166 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 20.08 -0.00 7.1999 -8.2299 0.1166 -0.1579 -0.2837 0.0370 0.5386 0.3525 0.3573 0.1852 -1.1439 20.08 -0.00 4.1014 -7.9945 0.0104 0.0515 0.0284 0.5967 0.3405 0.2594 -2.6241	1_											
19.00 -0.00 3.8300 -7.6657 0.0017 0.0651 0.0307 0.5960 0.2721 0.3239 -2.0485 20.06 -0.00 4.0854 -8.0665 0.0101 0.0463 0.0241 0.5914 0.2628 0.3087 -1.9598 21.11 -0.00 4.3597 -8.1697 0.0136 0.0441 0.0220 0.5843 0.2897 0.2946 -1.8493 22.15 -0.00 4.6321 -6.2766 -0.0048 0.0685 0.0774 0.5785 0.3022 0.2763 -1.7872 22.17 -0.01 4.6630 -8.1830 0.0103 0.0779 0.0139 0.5758 0.2920 0.2838 -1.7549 23.21 -0.01 4.9665 -8.2786 0.0241 0.0455 0.0144 0.5696 0.2948 0.2700 -1.6676 24.20 -0.01 5.2591 -6.3097 0.0247 0.0455 0.0144 0.5696 0.2948 0.2700 -1.6676 25.33 -0.00 5.6016 -8.2770 0.0468 -0.0167 0.0208 0.5560 0.3037 0.2523 -1.4776 26.30 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5489 0.3076 0.2412 -1.3946 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1086 -0.1539 0.0446 0.5530 0.3499 0.2011 -1.3993 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 27.55 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 27.55 0.00 6.9781 -6.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1860 -1.2046 27.59 0.00 6.9781 -6.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1860 -1.2046 27.59 0.00 6.9781 -6.4186 0.1579 -0.2837 0.0370 0.5425 0.3573 0.1652 -1.1438 27.00 6.00 7.1999 -8.2495 0.0104 0.0515 0.0545 0.5967 0.3405 0.2594 -2.6241	5											
20.06 -0.00	3											
21.11 -0.00	•					-						
27.15 -0.00	5											
27.17 -0.01 4.6630 -0.1030 0.0103 0.0779 0.0139 0.5758 0.2920 0.2038 -1.7549 23.21 -0.01 4.9645 -8.2786 0.0241 0.0455 0.0144 0.5696 0.2998 0.2700 -1.6676 24.26 -0.01 5.2591 -6.3097 0.0247 0.0275 0.0209 0.5643 0.3065 0.2577 -1.5801 25.33 -0.00 5.6016 -0.2770 0.046 -0.0147 0.0208 0.5560 0.3037 0.2523 -1.4776 26.40 -0.00 6.0067 -8.3769 0.1034 -0.1510 0.0391 0.5489 0.3076 0.2412 -1.3946 26.39 -0.00 5.9777 -4.3645 0.1030 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3943 26.39 -0.00 5.9629 -0.3601 0.1086 -0.1539 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.472 0.1701 -0.3082 0.0723 0.5394 0.3514 0.1880 -1.2446 29.59 0.00 6.9781 -2.4180 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1880 -1.2446 30.44 -0.00 7.1999 -8.2299 0.1166 -0.1692 0.0172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	6 7						-					
23.21 -0.01	6											
74.26 -0.01 5.2591 -6.3097 0.0287 0.0289 0.5643 0.3065 0.2577 -1.5801 25.33 -0.00 5.6016 -8.2770 0.0468 -0.0157 0.0288 0.5560 0.3037 0.2523 -1.4776 26.40 -0.00 6.0067 -8.3769 0.1034 -0.1510 0.0391 0.5489 0.3076 0.2012 -1.3946 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1086 -0.1589 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.4672 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1880 -1.2646 29.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1880 -1.2646 30.64 -0.00 7.1999 -8.2249 0.1166 -0.1692 0.0172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 4.0164 -7.4845 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468	ĕ											
26.00 -0.00 6.0067 -8.3767 0.1034 -0.1510 0.0391 0.5489 0.3076 0.2412 -1.3946 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1086 -0.1589 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.4672 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1880 -1.2448 29.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1880 -1.2648 30.64 -0.00 7.1999 -8.2299 0.1166 -0.1692 0.0172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 4.1014 -7.9845 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	0										0.2577	-1.5801
26.00 -0.00 6.0067 -8.3767 0.1034 -0.1510 0.0391 0.5489 0.3076 0.2412 -1.3946 26.39 -0.00 5.9777 -8.3645 0.1030 -0.1526 0.0421 0.5512 0.3311 0.2201 -1.3993 26.39 -0.00 5.9629 -8.3601 0.1086 -0.1589 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.4672 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1880 -1.2448 29.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1880 -1.2648 30.64 -0.00 7.1999 -8.2299 0.1166 -0.1692 0.0172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 4.1014 -7.9845 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	1	25.33	-0.00	5.6016	-8.277ū	0.0-68	-0.0167	0.0208	0.5560	0.3037	0.2523	-1-4776
26.39 "-0.00 5.9629 -6.3601 0.1086 -0.1589 0.0446 0.5530 0.3499 0.2031 -1.4054 27.46 0.00 6.3555 -8.4674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.4472 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1880 -1.2646 29.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1860 -1.2646 30.44 -0.00 7.1999 -8.2249 0.1166 -0.1592 0.0172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 4.1014 -7.4045 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	2	26.40	-0.00			0.1034	-0.1510	0.0391	0.5489		0.5415	-1.3946
27.00 0.00 6.3555 -8.0674 0.1316 -0.2403 0.0599 0.5470 0.3530 0.1939 -1.3324 28.53 0.00 6.6795 -5.0072 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1800 -1.2606 29.59 0.00 6.9781 -2.4180 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1800 -1.2066 30.64 -0.00 7.1999 -8.2249 0.1166 -0.1592 0.0172 0.5425 0.3573 0.1852 -1.1430 20.08 -0.00 4.1014 -7.4045 0.0104 0.0515 0.0284 0.5967 0.3405 0.2562 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	3		••									
28.53 0.00 6.6795 -5.4472 0.1701 -0.3052 0.0723 0.5394 0.3514 0.1860 -1.2646 29.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1860 -1.2064 30.64 -0.00 7.1999 -0.2299 0.1166 -0.1592 0.6172 0.5425 0.3573 0.1852 -1.1438 20.08 -0.00 4.1014 -7.7045 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	4						_					
79.59 0.00 6.9781 -2.4186 0.1579 -0.2837 0.0370 0.5386 0.3525 0.1860 -1.2064	5											
30.44 -0.00 7.1999 -0.2249 0.1166 -0.1592 0.0172 0.5425 0.3573 0.1852 -1.1430 20.08 -0.00 4.1014 -7.4045 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	6		0.00									
20.08 -0.00 4.1014 -7.9045 0.0104 0.0515 0.0284 0.5967 0.3405 0.2542 -1.9468 9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.6241	7											
9.92 -0.00 2.0005 -5.2495 -0.0308 0.1214 0.0239 0.5869 0.2896 0.2974 -2.624}	9											
	0											
	1											
	•					******	F 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				******	
						_						
-·												
											-	
		•				•						

AGE	LNGINEL 1 OF 1 1 OF 1	_	<u>vel opment</u>	CENTER(A	LOC) P			WEL FACILITY ALL EFFECTS		AEÁ	ODYNAMIC	-	TUMMEL	<u> </u>
		5467 M	ALH RELO-	5 PH1	CONF	L OEL1	051.2				·			
	1		26 2.3			0.0	DELE	DEL3 CEL4			· ·	•		
POINT	ALPHA	PFTA	"CN"	CLM	CA	CLN	CLL	CA	CAB	CAF	ACP			
1	-0.00	-0.0v	-0.0009	-0.0400	-0.0284	0.0959	0.0227	0.5694		-	50.8254			
2	1.99	-0.0C	0.3866	-1.0742	-0.0215	0.0771	0.0244	0.5607	0.1777 0	.3830	-2.7915			
3 .	3.45	-0.0v	0.7644	-5-061+	-0.0170	0.0633	0.0261	0.5519		.3668	-5.6969			
•		-0.00		-3.0714	-0.0151	0.0447	8+50.0	0.5620		.3711	-2.6405			
5	7.95	-0.00	1.5409	-3.4672	-0.0075	0.0311	PF20.0	0.5794		.3A39	-2.5746			 .
6	9,95	-0.0u	1.9365	0015	-0.0039	0.0753	0.0219			.3912	-2.4795			
7	11.96	-0.00	2.3234	-5-20-0	0.0015	0.0159	0.0216			.3930	-2.3692			
8	13.99	-0.03	2.7144	-6.1098	0.0117	0.0004	0.0183			.3892				
		-0.00	3.1353	-6.6346	0.0101	0.0013	0.0249			.3828	-2.1161	_		. <u> </u>
10		-0.00	3.6361	-6.6763	0.0114	-0.0005	0.0245			. 3751	-2.0355 -1.9392			
11		-0.00	3.8890	-7.0511 -7.0253	0.0100	0.0071 0.0141	0.0254			-3649				
12				-7.1385			0.0383			.3495	-1.8065			
13	21.22	-0.00	4.4518	-7.2254	0.0145	0.0171	0.0374).3345).3714				
15	27.27	-0.00	4.7A7d	-7.3230	0.0550	0.0137	0.0396			3090				
16	23.33	-0.00		-7.3564	0.0357		0.0355			2991				·- · —
17	24.40	-0.00		-7.3767	0.0419	-0.0129	0.0325			.2933				
16	25.46	-0.0u		-7.4033	0.0540		0.0336			2875				
19	26.51	0.04	6.0839	-7.4167	0.0994		0.0441			2791				
20	27.56	0.00	6.4248	-7.4647	0.1565		0.0604			0.2707				
21	28.63	0.00		-7.5071	0.1511		0.0460				-1-1111			
55	29.69	0.00		-7.5554	0.2012		0.0188				-1.0709			
23	30.74	0.00		-7.7237	1605.0		0.0269				-1.0375			
24	20.17	-0.00	4.1722	-7.4925	0.0157	0.0093	0.0394				-1.7000			
25	20.17	-0.00	4.1679	-7.1161	0.0164	-0.0011	0.0404		0.2A14	0.3056	-1.7074			
26	9,95	-0.00	1.9362	-4-8500	-0.0037	0.0244	0.0219	0.5927			-2,4894			
27	-0.00	-0.00	-0.0009	-0.0512	-0.0272	0.0918	0.0253	0.5700	0.2032	.3667	50.2523	١ _		
			- -									•		
	—					•								
													_	
													 .	
												_		

POINT ALFHA BETA CN CLM 1				UNKNOWN			
1 -0.00 -0.00 -0.0753		CLL ""	CA	CAB	CAF	XCP	
2 1.99 -0.01		0.0248	0.5350	0.1964		-1.6510	
5.97 -0.00 1.0492 -2.566 5 7.98 -0.00 1.4213 -3.364 6 9.99 -0.00 1.4113 -4.121 7 12.00 -0.00 2.1995 -4.77 8 14.03 -0.00 2.1995 -4.77 9 16.08 -0.00 3.0351 -5.74 10 17.12 -0.00 3.2926 -5.93 11 18.15 -0.00 3.5721 -6.69 12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1626 -6.31 15 22.34 -0.00 4.7619 -6.36 16 23.41 -0.00 5.3697 -6.66 18 25.53 -0.00 5.3697 -6.66 19 26.60 -0.00 5.3697 -6.66 20 27.65 -0.00 6.7012 -6.37 21 28.70 -0.00 6.7012 -6.37 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 6.7016 -6.91 24 20.25 -0.00 4.1515 -6.25 25 20.25 -0.00 4.1626 -6.26 25 20.25 -0.00 4.1626 -6.26 25 20.25 -0.00 4.1626 -6.26		0.0249	0.5294	0.1993	0.3301	-2.4881	-
\$ 5.97 -0.00		0.0279	0.5225	0.1978	0.3748	-7.4403	
5 7.98 -0.00 1.4213 -3.366 6 9.99 -0.00 1.8113 -4.126 7 12.00 -0.00 2.1995 -4.776 8 14.03 -0.00 3.5674 -5.29 9 16.08 -0.00 3.2926 -5.93 11 18.15 -0.00 3.5721 -6.09 12 19.20 -0.00 3.8664 -6.226 13 20.25 -0.00 4.1626 -6.316 15 22.34 -0.00 4.7619 -6.36 16 23.41 -0.00 5.3897 -6.46 18 25.53 -0.00 5.3897 -6.47 18 25.53 -0.00 5.3897 -6.47 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 5.3897 -6.47 20 27.65 -0.00 6.7012 -6.51 21 28.70 -0.00 6.7012 -6.51 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1626 -6.25 25 20.25 -0.00 4.1626 -6.26		0.0266	0.5333	0.1946	0.3387	-2.4274	
6 9.99 -0.00 1.6113 -4.121 7 12.00 -0.00 2.1995 -4.771 8 14.03 -0.00 3.0351 -5.791 9 16.06 -0.00 3.0351 -5.741 10 17.12 -0.00 3.2926 -5.93 11 18.15 -0.00 3.5721 -6.09 12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1626 -6.311 14 21.79 -0.00 4.4647 -6.39 15 22.34 -0.00 4.7619 -6.39 16 23.41 -0.00 5.0731 -0.43 17 24.46 -0.00 5.3897 -6.66 18 25.53 -0.00 5.7002 -6.7 19 26.60 -0.00 6.0617 -6.51 20 27.65 -0.00 6.0617 -6.91 21 28.70 -0.00 6.7010 -6.91 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1626 -6.20 25 20.25 -0.00 4.1626 -6.20 25 20.25 -0.00 4.1626 -6.20 26 9.78 -0.00 1.8135 -4.12	- · •	0.0254	0.5476	0.1937	0.3539	-2.3701	
7 12,00 -0.00 2.1995 -4.776 8 14.03 -0.00 2.5674 -5.29 9 16.06 -0.00 3.0351 -5.741 10 17.12 -0.00 3.5721 -6.674 11 18.15 -0.00 3.5721 -6.674 12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1626 -6.31 14 21.24 -0.00 4.7614 -6.39 15 22.34 -0.00 4.7614 -6.39 16 23.41 -0.00 5.3897 -6.66 17 24.46 -0.00 5.3897 -6.66 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 6.4042 -6.58 21 28.70 -0.00 6.4042 -6.58 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 6.7515 -6.21 24 20.25 -0.00 4.1626 -6.26 25 20.25 -0.00 4.1626 -6.26 25 20.25 -0.00 4.1626 -6.26		0.0241	0.5611	0.1938	0.3673	-2.2793	
8 14.03 -0.00 2.567a -5.29 9 16.06 -0.00 3.0351 -5.74 10 17.12 -0.00 3.5721 -6.60 11 18.15 -0.00 3.5721 -6.60 12 19.20 -0.00 3.8664 -6.20 13 20.25 -0.00 4.1626 -6.31 14 21.29 -0.00 4.4422 -6.31 15 22.34 -0.00 4.7619 -6.39 16 23.41 -0.00 5.7701 -6.43 17 24.46 -0.00 5.3897 -6.66 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 6.4042 -6.60 21 28.70 -0.00 6.4042 -6.50 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1626 -6.22 26 9.78 -0.00 4.1626 -6.25 26 9.78 -0.00 1.8135 -6.25		0.0224	0.5713	0.1979		-2.1717	
9 16.06 -0.00 3.0351 -5.741 10 17.12 -0.00 3.2926 -5.93 11 18.15 -0.00 3.5721 -6.69 12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1626 -6.31 14 21.79 -0.00 4.442 -6.31 15 22.34 -0.00 4.7619 -6.39 16 23.41 -0.00 5.3897 -6.43 17 24.46 -0.00 5.3897 -6.47 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 6.7012 -6.51 20 27.65 -0.00 6.7616 -6.91 21 28.70 -0.00 6.7616 -6.91 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1515 -6.25 25 20.25 -0.00 4.1626 -6.26		0.0203	0.5759	1602.0	0.3728	-2.0453	
10 17.12 -0.00 3.2926 -5.93 11 18.15 -0.00 3.5721 -6.09 12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1626 -6.31 14 21.29 -0.00 4.492 -6.33 15 22.34 -0.00 4.7619 -6.39 16 23.41 -0.00 5.3697 -6.49 17 24.46 -0.00 5.3697 -6.47 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 6.7012 -6.51 20 27.65 -0.00 6.4092 -6.68 21 28.70 -0.00 6.7012 -6.91 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1515 -6.25 25 20.25 -0.00 4.1625 -6.26		0.0220	0.5777	0.2153	0.3624	-1.8938	
11		0.0293	0.5764	6555.0	0.3541	-1.8032	
12 19.20 -0.00 3.8664 -6.22 13 20.25 -0.00 4.1620 -6.31 14 21.24 -0.00 4.7614 -6.39 15 22.34 -0.00 5.0731 -6.43 17 24.46 -0.00 5.3897 -6.66 18 25.53 -0.00 5.7002 -6.47 19 26.60 -0.00 5.7002 -6.47 20 27.65 -0.00 6.7616 -6.91 21 28.70 -0.00 6.7616 -6.91 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1515 -6.25 25 20.25 -0.00 4.1612 -6.26		0-0289	0.5749	0.2278	0.3471	-1.7063	
13		0.0309	0.5741	1565.0	0.3421	-1.6099	
14		0.0302	0.5729	0.2367	0.3363	-1.5173	
16		0.0235	0.5670	0.2369	0.3301	-1.4248	
16		0.0235	0.5651	0.2405	0.3246	-1.3437	
17		0.0236	0.5590	0.2430	0.3160	-1.2691	
19		0.0263	0.5578	0.2503	0.3075	-1.2025	
19 26.60 -0.00 6.0417 -6.51 20 27.65 -0.00 6.4042 -6.68 21 28.70 -0.00 6.7816 -6.41 22 29.76 -0.01 7.1407 -7.11 23 30.82 -0.00 7.5030 -7.34 24 20.25 -0.00 4.1515 -6.25 25 20.25 -0.00 4.1625 -6.26 26 9.78 -0.00 1.8135 -4.12	8J U.0406 -0.01=0	0.0218	0.5528	0.2543	0.2985	-1-1365	
21	19- 0.0-50 -0.0127	0.0273	0.5559	5195.0		-1.0791	
22	0.0030 -0.0n79	0.0408	0.5572	0.2688	0.2884	-1.0430	
22	154 0.070H -0.0652	0.0369	0.5598	0.2770	8585.0	-1.0197	
24			0.5628	0.2455	0.2773	-0.9966	
24	11 0.0935 -0.1206		0.5629	0.2933	0.2695	-0.9764	
25 20.25 -0.00 4.1424 -6.26 26 9.78 -0.00 1.8135 -4.12		0.0313	0.5694	0.2965	0.2729	-1.5050	
26 9.78 -0.00 1.8135 -4.12			0.5703	0.2834	0.2869	-1.5120	
			0.5588	0.2418	0.3170	-2.2759	
		0.0259	0.5397	0.2190		-1.6791	
						·	
							

17.08												
0.00		TEST 1					L DEL	0 0			ON	
0.00	INT"	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA -	CAB	CAF	ACP
**************************************		0.00	0.00	0.0101					0.2363	0.0942	0.1421	-1.0272

5.99 0.00 0.9731 -7.2-12 0.0127 -0.032 -0.0043 0.2741 0.1171 0.1570 -2.3032 7.99 0.00 1.7367 -3.1764 0.0072 -0.0348 0.0014 0.2937 0.1261 0.1676 -2.3763 10.00 -0.00 1.5274 -3.3526 -0.0142 0.0435 0.0305 0.3289 0.1389 0.199 0.1900 -2.1921 12.02 0.00 1.7577 -3.5305 0.0001 -0.0386 0.0076 0.3589 0.1654 0.1934 -2.0378 14.04 0.00 7.0439 -3.4375 0.0014 -0.0420 0.0125 0.3783 0.1669 0.1914 -1.0265 14.06 0.00 7.0439 -3.4375 0.0014 -0.0420 0.0125 0.3783 0.1669 0.1914 -1.0265 17.08 0.00 7.4454 -4.2630 0.0022 -0.0048 0.0044 0.3941 0.2339 0.1603 -1.7433 18.10 0.00 7.6111 -4.4112 0.0064 -0.0266 0.0024 0.4130 0.2683 0.1447 -1.6849 19.11 0.00 7.7326 -4.3759 0.0597 -0.1373 -0.0155 0.4280 0.3154 0.1125 -1.6014 19.11 0.00 7.7326 -4.3759 0.0597 -0.1373 -0.0155 0.4280 0.3154 0.1257 -1.6014 19.11 0.00 7.9838 -0.201 0.0049 -0.0344 -0.0051 0.4351 0.3336 0.1098 -1.5147 19.11 0.00 7.9838 -0.201 0.0049 -0.0344 -0.0051 0.4351 0.3336 0.1098 -1.5147 19.11 0.00 7.9838 -0.201 0.0049 -0.0344 -0.0051 0.4351 0.3336 0.1098 -1.5147 19.11 0.00 7.9838 -0.201 0.0049 -0.0344 -0.0051 0.4351 0.3346 0.1305 -1.4278 19.11 0.00 7.9838 -0.201 0.0049 -0.0344 -0.0051 0.4351 0.3466 0.1305 -1.3457 19.12 0.1365 -1.3457 19.12 0.1365 -0.0138 0.2003 0.0201 0.4386 0.3646 0.1305 -1.3457 19.12 0.3766 19.12 0.0064 19.12 0.0064 19.12 0.0064 19.12 0.0064 19.12 0.0064 19.12 0.0064 19.1365 19.12 0.0064 19.12 0.006	_											
7.99 0.00 1.3367 -3.176 0.0072 -0.0368 0.0014 0.2937 0.1261 0.1676 -2.3763 10.00 -0.00 1.5274 -3.5328 -0.0142 0.0435 0.0305 0.3289 0.1389 0.1960 -2.1921 12.02 0.00 1.7577 -3.5605 0.0001 -0.0366 0.0076 0.3589 0.1654 0.1934 -2.0370 14.04 0.00 7.0438 -3.4375 0.0014 -0.0420 0.0125 0.3783 0.1869 0.1914 -1.9265 14.06 0.00 7.0438 -3.4375 0.0014 -0.0420 0.0125 0.3783 0.1869 0.1914 -1.9265 17.08 0.00 7.0438 -3.4375 0.0086 -0.0217 0.0069 0.3901 0.2248 0.1653 -1.6094 17.08 0.00 7.6181 -4.6112 0.0064 -0.0266 0.0084 0.3941 0.2339 0.1603 -1.7433 18.10 0.00 7.6181 -4.6112 0.0064 -0.0266 0.0024 0.3941 0.2339 0.1603 -1.7433 18.10 0.00 7.6181 -4.6112 0.0064 -0.0266 0.0024 0.3180 0.2683 0.1447 -1.6849 19.11 0.40 7.3326 -4.3759 0.0557 -0.1373 -0.0155 0.4280 0.3154 0.1125 -1.6014 19.11 0.40 7.3326 -4.3025 0.0715 -0.2451 -0.0318 0.4434 0.3336 0.1098 -1.5147 19.11 0.40 7.3326 -4.3025 0.0715 -0.2451 -0.0318 0.4434 0.3336 0.1098 -1.5147 19.11 0.40 7.3326 -4.3025 0.0715 -0.2451 -0.0318 0.4434 0.3336 0.1098 -1.5147 19.11 0.40 7.3326 -4.3025 0.0715 -0.2451 -0.0318 0.4434 0.3336 0.1098 -1.5147 19.11 0.40 7.3326 0.00098 0.3336 0.1098 -1.5147 19.11 0.40 7.3326 0.13336 0.1098 -1.5147 19.11 0.40 7.3326 0.03336 0.1098 -1.5147 19.11 0.40 7.3338 0.00098 0.3336 0.1098 -1.5147 19.11 0.40 7.3338 0.00098 0.3336 0.1098 -1.3338 19.11 0.1006 -1.3408 19.11 0.1006 -1.3408 19.11 0.1006 -1.3408 19.11 0.1006 1.3408 19.11 0.1006 1.3408 19.11 0.1006 1.3408 19.11 0.1006 1.2491 19.11 0.4004 0.1115 -1.3338 19.11 0.1006 1.2491 19.11 0.1006 1.2491 19.11 0.1006 1.2491 19.11 0.1006 1.2491 19.11 0.1006 1.2491 19.11 0.1006 1.2408 19.11 0.1006 1.2408 19.11 0.1006 1.2408 19.11 19.11 0.1006 1.2408 19.11 19.11 0.1006 1.2408 19.11 19.11 0.1006 1.2408 19.11 19.11 0.1006 1.2408 19.11 19.		T										
10.00 -0.00												
12.02	ž	_								-		
14.04												
17.08		14.04	0.00	2.0438	-3.4375	0.0014	-0.0420	0.0125				
19.10 0.00 7.6181 -4.4112 0.0064 -0.0268 0.0024 0.4130 0.2683 0.1447 -1.6849 19.11 0.00 2.7326 -4.3759 0.059 -0.1373 -0.0155 0.4280 0.3154 0.1125 -1.6014 20.13 0.00 2.8405 -4.3025 0.0715 -0.251 -0.0318 0.4334 0.3336 0.1098 -1.5147 21.16 0.00 2.9438 -4.2501 0.0069 -0.0344 -0.0051 0.4351 0.3446 0.1305 -1.4278 22.18 -0.01 3.1056 -4.2508 -0.0318 0.2003 0.0201 0.4386 0.3646 0.1340 -1.3667 22.18 -0.01 3.3051 -4.057 -0.0272 0.2463 0.0277 0.5018 0.3817 0.1201 -1.3766 23.20 -0.01 3.3051 -4.057 -0.0272 0.2168 0.0232 0.5119 0.4004 0.115 -1.3338 -2.23 -0.01 3.4960 -4.5417 -0.0019 0.1345 0.0148 0.5197 0.4151 0.1066 -1.2991 25.24 -0.01 3.6873 -4.6697 0.0240 0.0633 0.0098 0.5223 0.4190 0.1033 -1.2664 26.26 -0.01 3.6959 -4.6474 0.1563 -0.1901 0.0077 0.5121 0.4326 0.0794 -1.2244 27.28 -0.00 4.1253 -5.0512 0.2569 -0.478 0.0216 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0002 0.4965 0.4543 0.4764 0.0035 -1.3143 30.34 0.01 4.6515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875		44.06	0.00				-0.0717					
19.11			-		_							
20.13	2.											
21.16												
22.16 -0.01 3.1365 -4.3164 -0.0387 0.2463 0.0277 0.5018 0.3817 0.1201 -1.3760 23.20 -0.01 3.3051 -4.6057 -0.0272 0.2168 0.0232 0.5119 0.4004 0.1115 -1.3338 24.23 -0.01 3.4960 -4.5417 -0.0019 0.1345 0.0148 0.5197 0.4151 0.1066 -1.2991 25.24 -0.01 3.6873 -4.6697 0.0240 0.0633 0.0098 0.5223 0.4190 0.1033 -1.2664 26.26 -0.01 3.6959 -4.6474 0.1563 -0.1961 0.0077 0.5121 0.4326 0.0794 -1.2442 27.28 -0.00 4.1253 -5.0512 0.2569 -0.4478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0042 0.4965 0.4563 0.0022 -1.2124 26.31 -0.00 4.3500 -5.5080 0.4001 -0.8763 0.0388 0.4981 0.4646 0.0335 -1.1943 30.34 0.01 4.6515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875						_						
22.18 -0.01 3.1365 -4.3164 -0.0387 0.2463 0.0277 0.5018 0.3817 0.1201 -1.3766 23.20 -0.01 3.3051 -4.4057 -0.0272 0.2168 0.0232 0.5119 0.4004 0.1115 -1.3338 24.23 -0.01 3.4960 -4.5417 -0.0019 0.1345 0.0148 0.5197 0.4151 0.1046 -1.2991 25.24 -0.01 3.6873 -4.6697 0.0240 0.0633 0.0098 0.5223 0.4190 0.1033 -1.2664 26.26 -0.01 3.6959 -4.6474 0.1563 -0.1901 0.0077 0.5121 0.4326 0.0794 -1.2442 27.28 -0.00 4.123 -5.0512 0.2569 -0.478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4646 0.0335 -1.1943 30.34 0.01 4.8515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	-											
23.20 -0.01 3.3051 -4.4057 -0.0272 C.2168 0.0232 0.5119 0.4004 0.1115 -1.3338 24.23 -0.01 3.4960 -4.5417 -0.0019 0.1345 0.0148 0.5197 0.4151 0.1046 -1.2991 25.24 -0.01 3.6873 -4.6697 0.0240 0.0633 0.0098 0.5223 0.4190 0.1033 -1.2664 26.26 -0.01 3.6959 -4.6474 0.1563 -0.1961 0.0077 0.5121 0.4326 0.0794 -1.2442 27.28 -0.00 4.1253 -5.0512 0.2569 -0.478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4664 0.0335 -1.1943 30.34 0.01 4.8515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	6 7											
24.23 -0.01 3.4960 -4.5417 -0.0019 0.1345 0.0148 0.5197 0.4151 0.1046 -1.2991 25.24 -0.01 3.6873 -4.6647 0.0240 0.0633 0.0098 0.5223 0.4190 0.1033 -1.2664 26.26 -0.01 3.6959 -4.6474 0.1563 -0.1961 0.0077 0.5121 0.4326 0.0794 -1.2442 27.28 -0.00 4.1253 -5.0512 0.2569 -0.478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.4789 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4640 0.0335 -1.1943 30.34 0.01 4.8515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875												
26.26 -0.01 3.6959 -4.6474 0.1563 -0.1961 0.0077 0.5121 0.4326 0.0794 -1.2442 27.28 -0.00 4.1253 -5.0512 0.2569 -0.4478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4640 0.0335 -1.1943 30.34 0.01 4.8515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	9											
27.28 -0.00 4.1253 -5.0512 0.2569 -0.4478 0.0218 0.5073 0.4576 0.0497 -1.2244 26.30 -0.00 4.3500 -5.2744 0.4109 -0.7859 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4640 0.0335 -1.1943 30.34 0.01 4.8515 -5.7610 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	Ö	25.24	-0.01	3,6873	-4.6697	0.0240	0.0633	0.0098	0.5223	0.4190		
26.30 -0.00 4.3500 -5.274L 0.4109 -0.7859 0.0402 0.4965 0.4543 0.0422 -1.2124 29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4640 0.0335 -1.1943 30.34 0.01 4.8515 -5.761u 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	<u> </u>					·						
29.32 0.00 4.6120 -5.5080 0.4401 -0.8763 0.0388 0.4981 0.4646 0.0335 -1.1943 30.34 0.01 4.8515 -5.761u 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875	?											
30.34 0.01 4.8515 -5.761u 0.6355 -1.3390 0.1067 0.4843 0.4764 0.0079 -1.1875												
		_										
9.99 -0.00 1.5344 -3.4357 -0.0116 0.0372 0.0235 0.3229 0.2409 0.0819 -2.2333	3 5 6 7	26.30 29.32 30.34 20.13	-0.00 0.00 0.01 0.00	4.3500 4.6120 4.8515 2.8616 1.5384	-5.2740 -5.5080 -5.7610 -4.3082	0.4109 0.4401 0.6355 0.0593	-0.7859 -0.8763 -1.3390 -0.1719 0.0372	0.0402 0.0386 0.1061 -0.0106	0.4965 0.4981 0.4843 0.4580 0.3229	0.4543 0.4646 0.4764 0.4223 0.2409	0.0422 0.0335 0.0079 0.0357 0.0819	-1.2124 -1.1943 -1.1875 -1.5265 -2.2333
	_	-0.00	0.00		-0.1388					0.1189		
-0.00 0.00 0.0315 -0.1388 -0.0063 0.0136 -0.0076 0.2392 0.1189 0.1203 -4.4834		-0.00		444313	-441300	-0.0003	444134	-00001	. V.E.J.E	*****	4.15.3	

5	0.2499
2 7.00 0.00 0.3023 -0.6661 -0.0002 -0.0111 -0.0112 0.7520 0.1082 0.1437 -2.2034 3 3.99 0.00 0.6356 -1.4730 0.0015 -0.0208 -0.0093 0.7565 0.1086 0.1479 -2.3184 5 5.99 0.00 0.9866 -2.3869 0.0093 -0.0027 0.2673 0.1163 0.1510 -2.3888 5 7.98 0.00 1.3289 -3.1720 0.0166 -0.0666 -0.0006 0.7989 0.1246 0.1743 -2.3878 6 9.99 0.00 1.5385 -3.3975 -0.0133 0.0267 0.0261 0.3815 0.1416 0.2001 -2.2083 7 12.01 0.00 1.7776 -3.6626 0.0047 -0.0228 0.0099 0.3737 0.1593 0.2144 -2.9718 8 14.03 0.00 2.7100 -4.1611 0.0166 -0.0626 0.0103 0.4016 0.1939 0.2075 -1.9811 9 16.06 0.00 2.3817 -4.4613 0.0172 -0.0617 0.0062 0.4177 0.2271 0.1906 -1.8667 10 17.07 0.00 2.5204 -4.5360 0.0197 -0.0023 0.4025 0.4223 0.2716 0.1506 -1.7999 11 18.09 0.00 2.6646 -4.6143 0.0355 -0.1268 -0.0072 0.4348 0.2663 0.1446 -1.7317 12 19.11 0.01 2.7834 -0.5640 0.0072 -0.2518 -0.0283 0.4516 0.3107 0.1409 -1.6471 13 20.14 0.01 2.7834 -0.5640 0.0072 -0.2518 -0.0283 0.4516 0.3107 0.1409 -1.6471 13 20.14 0.01 3.3652 -4.5930 0.0135 -0.0016 0.0078 0.5021 0.3348 0.1673 -1.6624 15 22.19 -0.01 3.1865 -4.4673 -0.0171 0.1356 0.0224 0.5196 0.3718 0.1478 -1.4613 16 23.20 -0.01 3.5864 -4.7431 -0.0018 0.1167 0.0244 0.5359 0.4004 0.1351 -1.3375 17 24.22 -0.01 3.5864 -4.7431 -0.0018 0.1167 0.0244 0.5359 0.4004 0.1351 -1.3375 18 25.24 -0.01 3.7878 -0.8882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2905 22 28.31 -0.00 4.4647 -5.5029 0.4097 -0.6071 0.0055 0.5076 0.4933 0.4864 -1.2434 23 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0557 0.5018 0.4086 0.0185 -1.2202 22 28.31 -0.00 4.4647 -5.5029 0.4099 -0.8396 0.0085 0.0085 0.4087 0.0149 -1.5222 22 28.31 -0.00 4.4647 -5.5029 0.4099 -0.8396 0.0085 0.0085 0.4087 0.0149 -1.5575 25 20.13 0.01 2.9015 -4.5192 0.0709 -0.8396 -0.0085 0.0085 0.4087 0.0149 -1.5575 25 20.13 0.01 2.9015 -4.5192 0.0709 -0.8396 -0.0085 0.0085 0.4087 0.0149 -1.5575 25 20.13 0.01 2.9015 -4.5192 0.0709 -0.8396 -0.0085 0.0085 0.4087 0.0149 -1.5575	0.27520
3 3.94 0.00 0.6356 -1.4730 0.0015 -0.0728 -0.0093 0.7565 0.1066 0.1479 -2.3184 5.99 0.00 0.9866 -2.3489 0.0093 -0.0470 -0.0057 0.2673 0.1163 0.1510 -2.3888 7.98 0.00 1.3289 -3.1720 0.0146 -0.0646 -0.0006 0.7989 0.1246 0.1743 -2.3678 0.0146 0.1743 -2.3678 0.0146 0.1743 -2.3678 0.0146 0.1743 -2.3678 0.0146 0.1743 -2.3678 0.0047 0.0261 0.3415 0.1414 0.2001 -2.2083 0.0047 0.0261 0.3415 0.1414 0.2001 -2.2083 0.0047 0.0261 0.3415 0.1414 0.2001 -2.2083 0.0047 0.0261 0.3415 0.1414 0.2001 -2.2083 0.0047 0.0261 0.03415 0.1414 0.2001 -2.2083 0.0047 0.0528 0.0047 0.0528 0.0089 0.3737 0.1593 0.2144 -2.9718 0.0047 0.0047 0.0052 0.4777 0.2271 0.1906 -1.8647 0.0047 0.0047 0.0052 0.4777 0.2271 0.1906 -1.8647 0.0047 0.0047 0.0052 0.4723 0.2716 0.1506 -1.7999 0.0047 0.0047 0.0052 0.4723 0.2716 0.1506 -1.7999 0.0047 0.0047 0.0047 0.0052 0.4723 0.2716 0.1506 -1.7999 0.0047 0.004	0.2565
5.99 0.00 0.9860 -2.3489 0.0073 -0.0470 -0.0057 0.2673 0.1163 0.1510 -2.3800 7.98 0.00 1.3289 -3.1720 0.0146 -0.0646 -0.0006 0.7989 0.1246 0.1743 -2.3870 0.1266 9.99 0.00 1.5385 -3.3975 -0.0133 0.0267 0.0261 0.3415 0.1614 0.2001 -2.2083 0.1246 0.1743 -2.3870 0.1260 0.000 0.17770 -3.6820 0.0047 -0.0528 0.0089 0.3737 0.1593 0.2144 -2.0718 0.1614 0.0001 -2.2083 0.0001 0.0001 0.1939 0.2075 -1.9811 0.1000 0.0001 0.1939 0.2075 -1.9811 0.1000 0.0001 0.1939 0.2075 -1.9811 0.1707 0.0001 0.0001 0.1939 0.2075 0.1981 0.1993 0.1993 0.	0.2673
7.98 0.00 1.3289 -3.1720 0.0146 -0.0646 -0.0006 0.2989 0.1246 0.1743 -2.3679	0.2989
9.94 0.00 1.5385 -3.3975 -0.0133 C.0267 0.0261 0.3615 0.1416 0.2001 -2.2083	0.3415
7 12.01 0.00 1.7776 -3.6828 0.0047 -0.0528 0.0089 0.3737 0.1593 0.2144 -2.0718 8 14.03 0.00 2.1000 -4.1611 0.0106 -0.0076 0.0103 0.4014 0.1939 0.2075 -1.9811 9 16.06 0.00 2.3817 -4.4413 0.0172 -0.0617 0.0062 0.4177 0.2271 0.1906 -1.8647 0 17.07 0.00 2.5204 -4.5360 0.0197 -0.0623 0.025 0.4223 0.2716 0.1506 -1.7999 1 18.09 0.00 2.6646 -4.6143 0.0365 -0.1208 -0.0072 0.4348 0.2663 0.1486 -1.7317 2 19.11 0.01 2.7834 -4.5460 0.0672 -0.2815 -0.0283 0.4516 0.3107 0.1409 -1.4671 3 20.14 0.01 2.6966 -4.5203 0.0789 -0.2815 -0.0281 0.465 0.3309 0.1376 -1.5665 8 21.17 -0.00 3.0270 -4.4200 0.0135 -0.0016 0.0078 0.5021 0.3348 0.1673 -1.4624 5 22.19 -0.01 3.1645 -4.4673 -0.0171 0.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 6 23.20 -0.01 3.5840 -4.7431 -0.0014 0.1107 0.0244 0.5318 0.478 -1.4011 7 24.22 -0.01 3.5840 -4.7431 -0.0014 0.1107 0.0244 0.5318 0.4212 0.1105 -1.2334 8 25.24 -0.01 3.7878 -4.8882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2334 9 26.28 -0.01 3.7878 -4.8882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2334 1 27.30 -0.00 4.2428 -5.2753 0.2531 -0.4321 0.0257 0.5163 0.4518 0.0558 -1.2328 2 28.31 -0.00 4.4820 -5.5220 0.4192 -0.8081 0.0457 0.5078 0.493 0.0185 -1.2328 2 28.31 -0.00 4.4647 -5.5059 0.4287 -0.8081 0.0457 0.5078 0.493 0.0185 -1.2328 3 29.33 0.00 4.7251 -5.7190 0.4111 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2321 5 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0252 0.4472 0.0451 0.0457	0.3737
14.03	0.4014 0.1939 0.2075 -1.9811 0.4177 0.2271 0.1906 -1.8647 0.4223 0.2716 0.1506 -1.7999 0.4348 0.2663 0.1486 -1.7317 0.4516 0.3107 0.1409 -1.6471 0.4685 0.3309 0.1376 -1.5605 0.5021 0.3348 0.1673 -1.4624 0.5196 0.3718 0.1478 -1.4011
0 17.07 0.06 2.5204 -4.5366 0.0197 -6.0623 0.0025 0.4223 0.2716 0.1506 -1.7999 1 18.09 0.00 2.6646 -4.6143 0.0365 -0.1268 -0.0072 0.4348 0.2863 0.1486 -1.7317 2 19.11 0.01 2.7834 -4.5846 0.0672 -6.2518 -0.0283 0.4516 0.3107 0.1409 -1.6471 3 20.14 0.01 2.6966 -4.5203 0.0789 -0.2815 -0.0291 0.4685 0.3309 0.1376 -1.5665 4 21.17 -0.00 3.0270 -4.4200 0.0135 -0.0016 0.0078 0.5021 0.3348 0.1673 -1.4624 5 22.19 -0.01 3.1865 -4.4673 -0.0171 0.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 6 23.20 -0.01 3.3652 -4.5956 -0.0196 0.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 7 24.22 -0.01 3.5840 -4.7431 -0.0014 0.1167 0.0244 0.5355 0.4004 0.1351 -1.3234 8 25.24 -0.01 3.7870 -4.8802 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2965 9 26.28 -0.01 3.9939 -5.0499 0.1452 -0.1872 0.0142 0.5228 0.4363 0.8655 -1.2632 0 27.30 -0.00 4.2428 -5.2753 0.2531 -0.4351 0.0257 0.5163 0.4518 0.0644 -1.2434 1 24.33 -0.00 4.4820 -5.5250 0.4192 -0.8021 0.0450 0.5076 0.4518 0.0558 -1.2328 2 28.31 -0.00 4.4647 -5.5059 0.4287 -0.8051 0.0457 0.5076 0.4818 0.0558 -1.2328 2 28.31 -0.00 4.7251 -5.7190 0.4111 -0.8041 0.0550 0.5076 0.4876 0.0185 -1.2321 3 29.33 0.00 4.7251 -5.7190 0.4111 -0.8041 0.0555 0.4087 0.0148 -1.1412 5 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	0.4223 0.2716 0.1506 -1.7999 0.4348 0.2863 0.1486 -1.7317 0.4516 0.3107 0.1409 -1.6471 0.6685 0.3309 0.1376 -1.5605 0.5021 0.3348 0.1673 -1.4624 0.5196 0.3718 0.1478 -1.4011 0.5310 0.3799 0.1511 -1.3575
17.07 0.06 2.5200 -0.5360 0.0197 -0.0023 0.0025 0.4223 0.2716 0.1506 -1.7999 18.09 0.00 2.6646 -0.0143 0.0365 -0.1266 -0.0072 0.0348 0.2663 0.1486 -1.7317 19.11 0.01 2.7834 -0.5846 0.0072 -0.2616 -0.0283 0.4516 0.3107 0.1409 -1.6471 3 20.10 0.01 2.6966 -0.5203 0.0789 -0.2615 -0.0291 0.0685 0.3309 0.1376 -1.5605 4 21.17 -0.00 3.0270 -0.4260 0.0135 -0.0016 0.0078 0.5021 0.3348 0.1673 -1.4624 5 22.19 -0.01 3.1865 -0.4673 -0.0171 0.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 6 23.20 -0.01 3.3652 -0.5956 -0.0196 0.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 7 24.22 -0.01 3.5860 -0.7431 -0.0014 0.1107 0.0244 0.5355 0.4004 0.1351 -1.3236 8 25.24 -0.01 3.7870 -0.0802 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2905 9 26.28 -0.01 3.9939 -5.0449 0.1652 -0.1872 0.0142 0.5228 0.4363 0.0865 -1.2632 0 27.30 -0.00 4.2026 -5.2753 0.2531 -0.4351 0.0257 0.5163 0.4518 0.0644 -1.2434 1 28.33 -0.00 4.4020 -5.5220 0.4192 -0.8021 0.0450 0.5076 0.4518 0.0558 -1.2328 2 29.33 0.00 4.7251 -5.7190 0.4111 -0.8061 0.0550 0.5076 0.4887 0.0185 -1.2321 3 29.33 0.00 4.7251 -5.7190 0.4111 -0.8061 0.0550 0.5002 0.4876 0.0185 -1.2321 5 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	0.4223 0.2716 0.1506 -1.7999 0.4348 0.2663 0.1486 -1.7317 0.4516 0.3107 0.1409 -1.6471 0.6685 0.3309 0.1376 -1.5605 0.5021 0.3348 0.1673 -1.4624 0.5196 0.3718 0.1478 -1.4011
19.11 0.01 2.7834 -0.5846 0.0672 -C.2518 -0.0283 0.4516 0.3107 0.1409 -1.6471 20.14 0.01 2.6966 -4.5203 0.0789 -0.2615 -0.0291 0.4685 0.3309 0.1376 -1.5605 21.17 -0.00 3.0770 -4.4200 0.0135 -0.0016 0.0078 0.5021 0.3346 0.1673 -1.4624 22.19 -0.01 3.1865 -4.4673 -0.0171 C.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 23.20 -0.01 3.3652 -4.5956 -0.0196 0.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 24.22 -0.01 3.5840 -4.7431 -0.0014 0.1167 0.0244 0.5355 0.4004 0.1351 -1.3234 25.24 -0.01 3.7878 -4.8822 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2805 26.28 -0.01 3.9939 -5.0449 0.1552 -0.1872 0.0142 0.5228 0.303 0.0865 -1.2632 27.30 -0.00 4.226 -5.2753 0.2531 -0.4351 0.0257 0.5163 0.4518 0.0644 -1.2434 28.33 -0.00 4.420 -5.5220 0.4192 -0.8051 0.0450 0.5076 0.4518 0.0558 -1.2328 28.31 -0.00 4.4647 -5.5059 0.4297 -0.8081 0.0457 0.5078 0.4993 0.0185 -1.2328 29.33 0.00 4.7251 -5.7190 0.4111 -0.8041 0.0550 0.5076 0.4876 0.0185 -1.2321 30.37 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4672 0.0255 -1.5575	0.4516
19.11	0.4516
21.17 -0.0V 3.0270 -4.4200 0.0135 -0.0016 0.0078 0.5021 0.3340 0.1673 -1.4624 22.19 -0.01 3.1865 -4.4673 -0.0171 C.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 23.70 -0.01 3.3852 -4.5956 -0.0196 0.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 24.22 -0.01 3.5860 -4.7431 -0.0014 0.1107 0.0244 0.5355 0.4004 0.1351 -1.3234 25.24 -0.01 3.7878 -4.0882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2905 26.28 -0.01 3.9934 -5.0449 0.1452 -0.1872 0.0142 0.528 0.4363 0.0865 -1.2632 27.30 -0.00 4.2426 -5.2753 0.2531 -0.4391 0.0257 0.5163 0.4518 0.0644 -1.2434 28.33 -0.00 4.2420 -5.5240 0.4192 -0.6071 0.0450 0.5076 0.4518 0.0558 -1.2328 28.31 -0.00 4.4627 -5.5054 0.4192 -0.6071 0.0450 0.5076 0.4933 0.0185 -1.2328 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0550 0.5008 0.4887 0.0185 -1.2321 29.33 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0149 -1.1412	0.5021 0.3348 0.1673 -1.4624 0.5196 0.3718 0.1478 -1.4011 0.5310 0.3799 0.1511 -1.3575
22.19 -0.01 3.1665 -4.4673 -0.0171 C.1356 0.0224 0.5196 0.3718 0.1478 -1.4011 23.70 -0.01 3.3652 -4.5956 -0.0196 C.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 24.22 -0.01 3.5860 -4.7431 -0.0014 0.1167 0.0244 0.5355 0.4004 0.1351 -1.3234 25.24 -0.01 3.7878 -4.8882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2965 26.78 -0.01 3.9934 -5.0449 0.1452 -0.1872 0.0142 0.527 0.4363 0.0865 -1.2632 27.30 -0.00 4.2426 -5.2753 0.2531 -0.4391 0.0257 0.5163 0.4518 0.0644 -1.2434 28.33 -0.00 4.4820 -5.5220 0.4192 -0.8021 0.0450 0.5076 0.4518 0.0558 -1.2320 28.31 -0.00 4.4647 -5.5054 0.4287 -0.8081 0.0457 0.5078 0.4993 0.0185 -1.2321 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0550 0.5002 0.4876 0.0185 -1.2321 29.33 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0149 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	0.5196
23.20 -0.01 3.3652 -4.5956 -0.0196 (0.1512 0.0270 0.5310 0.3799 0.1511 -1.3575 24.22 -0.01 3.5640 -4.7431 -0.0014 0.1107 0.0244 0.5355 0.4004 0.1351 -1.3234 25.24 -0.01 3.7878 -4.0882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2965 26.28 -0.01 3.9934 -5.0449 0.1452 -0.1472 0.0142 0.528 0.4363 0.0865 -1.2632 27.30 -0.00 4.2426 -5.2753 0.2531 -0.4381 0.0257 0.5163 0.4518 0.0644 -1.2434 24.33 -0.00 4.4820 -5.5240 0.4192 -0.8071 0.0450 0.5076 0.4518 0.0558 -1.2328 28.31 -0.00 4.4820 -5.5054 0.4287 -0.8081 0.0457 0.5078 0.4993 0.0185 -1.2328 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2321 29.33 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0149 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	0.5310
24.22 -0.01 3.5840 -4.7431 -0.0014 0.1167 0.0244 0.5355 0.4004 0.1351 -1.3234 25.24 -0.01 3.7878 -4.0882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2905 26.78 -0.01 3.9934 -5.0444 0.1452 -0.1872 0.0142 0.528 0.4363 0.0865 -1.2632 27.30 -0.00 4.2426 -5.2753 0.2531 -0.4351 0.0257 0.5163 0.4518 0.0644 -1.2434 28.33 -0.00 4.2426 -5.220 0.4192 -0.8021 0.0450 0.5076 0.4518 0.0558 -1.2320 28.31 -0.00 4.4637 -5.5054 0.4287 -0.8081 0.0457 0.5078 0.4933 0.0185 -1.2321 29.33 0.00 4.7251 -5.7140 0.411 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2103 30.37 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0148 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	
25.24 -0.01 3.7878 -4.8882 0.0472 0.0141 0.0144 0.5318 0.4212 0.1105 -1.2905 26.28 -0.01 3.9934 -5.0449 0.1452 -0.1872 0.0142 0.528 0.4363 0.0865 -1.2632 27.30 -0.00 4.2428 -5.2753 0.2531 -0.431 0.0257 0.5163 0.4518 0.0644 -1.2434 24.33 -0.00 4.4820 -5.5220 0.4192 -0.8071 0.0450 0.5076 0.4518 0.0558 -1.2320 28.31 -0.00 4.4637 -5.5059 0.4287 -0.8081 0.0557 0.5078 0.4933 0.0185 -1.2321 29.33 0.00 4.7251 -5.7140 0.411 -0.8041 0.0550 0.5062 0.4867 0.0185 -1.2103 30.37 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0148 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	
26.78 -0.01 3.993v -5.044v 0.1452 -0.1472 0.0142 0.528 0.4363 0.0665 -1.2632 27.30 -0.00 4.2426 -5.2753 0.2531 -0.4391 0.0257 0.5163 0.4518 0.0644 -1.2434 28.33 -0.00 4.4820 -5.5240 0.4192 -0.8071 0.0450 0.5076 0.4518 0.0558 -1.2320 28.31 -0.00 4.4647 -5.505v 0.4287 -0.8081 0.0657 0.5078 0.4993 0.0185 -1.2321 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2103 30.37 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0149 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	
27.30 -0.00 4.2426 -5.2753 0.2531 -0.4391 0.0257 0.5163 0.4518 0.0644 -1.2434 24.33 -0.00 4.4820 -5.5220 0.4192 -0.8071 0.0450 0.5076 0.4518 0.0558 -1.2328 28.33 -0.00 4.4647 -5.5050 0.4287 -0.8081 0.0657 0.5078 0.493 0.0185 -1.2321 29.33 0.00 4.7251 -5.7140 0.4111 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2103 30.37 0.01 5.0351 -5.4477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0148 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	
29.33	
29.33 0.00 4.7251 -5.7190 0.4111 -0.8041 0.0550 0.5062 0.4876 0.0185 -1.2103 30.37 0.01 5.0351 -5.9477 0.4099 -0.8396 0.0835 0.5035 0.4887 0.0148 -1.1412 20.13 0.01 2.9015 -4.5192 0.0764 -0.3053 -0.0242 0.4725 0.4472 0.0253 -1.5575	0.5076 0.4518 0.0558 -1.2320
Z0.13	0.5078 0.4993 0.0185 -1.2321
20.13	0.5062
	0.5035 0.4887 0.0149 -1.1412
Ya'Y GaDO 1a3019 -1a9783 -DaDIDO GADENA DADZAA DAZAKE DAZATI DADXOS -ZAZSAT	
	0.3282
-0.01 0.00 0.0305 -0.1507 -0.0067 0.0090 -0.0073 0.2422 0.1330 0.1092 -4.9497	0.5655 0.1330 0.1045

ANNOLD ENGINEERING DEVELOPMENT CENTER (AEDC)	PROPULSION WIND TUNNEL FACILITY (PHT)	AEROGYNAMIC WIND TUNNEL (41)
PAGE 1 OF 1 SHEET 1 OF 1	MARTIN MISSILE TAIL EFFECTS DATA	

	1		4ACH RX10- .92 2.3		CUNF 14=0F16 0	.O	0 0	DEL3 DEL	TRANSIT	N	
POINT	ALPHA	- BETA	CN	CLM	CY	CLN	CLL .	_ CA	CAB	ČAF	XCP
1	-0.00	0.06	0.0191	-0.1036	-0.0076	0.0085	-0.0070	0.2571	0.0796	0.1775	-5,4270
2	2.01	0.00	0.3072	-0.5877	-0.0022	-0.0134	-0.0059	0.2594	0.0987	0.1607	-2.2302
3	3.99	6.00	0.6356	-1.5176	0.0064	-0.0245	-0.0038	0.2608	0.1092	0.1516	-2.3868
4	5.96	-0.00		-2.5546	-0.0130	0.0617	0.0055	0.2876	0.1016	0.1860	-2.4584
5	7.98	-0.00		-3.0771	-0.0125	0.0478	0.0135	0.3159	0.1348	0.1811	-2.3459
6	10.00	0.01	1.5790	-3-5358	0.0205	-0.1048	0.0002	0.3569	0.1585	0.1984	-5.5393
7	12.02	0.00		-3.4461	0.0014	-0.0406	0.0135	0.4033	0.1747	0.2785	-2.1084
8	14.02	0.07		-4.5024	0.0113	-0.0439	0.0178	0.4339	0.2177	0.2161	-2.0637
9	16.00	0.00		-4.9048	0.0171	-0.0514	0.0095		0.2651	0.1864	-1.9626
10	16.04	0.00	5.5169	-4.7677	0.0185	-0.0655	0.0062	0.4536	2045	0.1694	-1.9738
11	17.04	0.00		-5.1731	0.0203	-0.0651	0.0059	0.4635	0.3026	0.1609	-1.9273
12	18.07	0.00		-5.3124	0.0264	-0.0788	0.0022	0.4697	0.3274	0.1424	-1.8674
13	19.09	0.00		-5.3745	G-0-01	-0-1556	-0.0069	0760	0.3401	0.1359	-1.7965
14	20.11	0.01		-5.2747	0.0924	-0.3750	-0.0432		0.3608	0.1259	-1.6993
15	21.15	0.01		-5.2744	0.0449	-0.3563	-0.0355		0.3668	0.1371	-1.6091
16	21.14	0.01		-5.3494	0.0910	-0.3966	-0.0421	0.5049	0.3593	0.1457	-1.6319
17	22.16	0.00		-5-1102	0.0217	-0.0418	0.0150		0.3805	0.1528	-1.5119
18	53.50	-0.00		-5.2443	-0.0028	0.0645	0.0316		0.3852	0.1676	-1.4593
19	24.24	-0.0u		-5.3050	0.0004	0.0862	0.0344		0-4099	0.1367	-1.4028
20	25.26	-G. ol		-5.4243	0.0436	G.0123	0.0281		0.4216	0.1361	-1.3494
51_	26.29	-0.01		-5.5149	0.1335	-0.1640	0.0344		0.4426	0.0963	-1.2860
55	27.34	-0.00		-5.5429	0.1655	-0.2902	0.0532		0.4549	0.0724	-1.2139
53		-0.00		-5.4767	0.1713	-0.2442	0.0549		U-4593	0.0526	-1.1193
24		-0.0u		-5-4172	0.5101	-0.3393	0.0635		0.4642	0.0340	-1.0351
25	29.45	-0.00		-5.4181	0.5116	-0.3228	0.0656		0.4848	0,0175	-1.0436
56	30.63	-0.0		-5.2066	0.1230	-0.1343	0.0357		0.5024	-0.0126	-0.9520
27	20.11	0.01		-5.3443	0.0542	-0.3617	-0.0362		0.4547	0.0413	-1.7123
28	9.99	-0.00		-3.5148	0.0085	0.0171	0.0295		0.3137	0.0281	-2.2713
29	-0-01	0.00	0.0357	-0.1681	-0.0085	0.0116	-0.0003	0.2526	0.1547	0.0980	-4.7033

				4 542	CONF					•		
	1	45 0.4	1CH RX10-		CONF 4mof16 0	.OEL	1 DEL2 0	OEL3 DEL4	TRANSITI			• •
INT.	ALPHA"	BETA	CN	CL#	CY	CLN	CLL	- C4 ·	CAB	CAF -	ACP	
1	-0.01	0.00		-0-1351	-0.0074		-0.0036	0,2689	0.1002		-5,6193	
5	1.99	0.00	0.3168	-0.7755	-0.0029	-0.0010	-0.0085	0.2679	0.1139	0.1539	-2.4322	
3 _	3.98	0.00	0.6857	-1.7184	0.0027	-0.0147	-0.0067	0.2730	0.1219	0.1511	-2.5068	
5	5.97	-0.00	1.0804		-0.0122 -0.0634	0.0496	-0.0009 0.0736	0.3025	0.1734	0.1792	-2.5678	
6	7.97 10.00	0.00 -0.01	1.3876	-3.433J -3.6204	0.0057	0.2488	-0.0136	0.3435 0.3715	0.1298	0.2137	-7.4741	
7	17.00	0.00	1.8486	-3.9656	-0.0065	-0.0247	0.0199	0.4080	0.1832	0.2271	-2.1452	
-	14.01	0.01	2.2066	-4.6452	0.000	-0.0752	0.0225	0.4454	0.2323	0.2131	-2.1049	
9	16.03	0.01	2.5582	-5-1362	0.0020	-0.0731	0.0239	0.4629	0.2786	0.1843		
lo ·	16.03	0.00	2.5953	-5.2941	0.0008	-C.0480	0.0224	0.4669	0.3209		-2.0399	
11	17.04	0.00	2.7562	-5.4394	0.0068	-0.0614	0.0172	0.4710	0.3327		-1.9735	
12	18.06	0.00	2.9141	-5.5773	0.0094	-0.0661	0.0136	0.4774	0.3422	0.1351	-1.9139	
13	19.06	0.00	3.0666	-5.6513	0.0187	-0.0725	0.0058	0.4815	0.3574	0-1240	-1,8415	
1 4	20.10	0.00	3.2357	-5.7415	0.0269	-0-1117	-0.0087	0.4905	0.3623	0.1262	-1.7744	
15	21.14	0.01	3.3479	-5.7077	0.0741	-0.3171	-0.0357	0.5048	0.3566	0-1481	-1.6647	
16	22.17	0.01	3.5659	-5.7249	0.0710	-0.3392	-0.0333	0.5153	0.3771	0.1382	-1.6055	
17	53.50	0.00	3.7158	-5.5866	0.0320	-0.0977	0.0105	0.5322	0.3892	0.1429	-1.5040	
18	24.24	-0.00	3.9261	-5.5317	0.0025	0.0404	0.0420	0.5452	0.4021		-1.4082	
19	25.26	-0.0G	4.1713	-5.5541	0.0497	0.0178	0.0486	0.5444	0.4143	0.1301	-1.3315	
50	26.32	-0.00	4.4129	-5.5647	0.1370	-0.1695	0.0610	0.5339	0.4330	0.1009	-1.2610	
51 —	_27.37	+0.00	4.6728	-5.5227	0.1755	-0.2548	0.0655	- 0.5218	0.4534		-1.1819	 —
2 2 23	28.42	~0.00 0.00	5.05ml 5.4132	-5.4527	0.1744		0.0631	0.5175 0.5059	0.4539		-1.07 00 -0.98 64	
<u> </u>	29.50	-0.00	5.7542	-	0.1105	-0.1277		0.4957	0.4835		-0.9043	
25	20.10	0.00	3.2061	-5.4759	0.0331		-0.0090	0.4882	0.4549		-1.7703	
26	9.48	0.00	1.6000		0.0055	-0.0477		0.3646	0.3212		-2.3187	
27		-0.01		-3.6176	-0.0639		0.0739	0.3363	0.2529		-2.5542	
28 -	-0.01			-0.1703		0.0151	0.0046	0.258A	0.1748		-7.0630	
								, , , , , , , , , , , , , , , , , , , ,				
	·											
												
												

•	TEST 1		ACH RX10- 96 2.3			L DEL	DEFS	OEL3 DEL4	TRANSITI	on	
OINT	ALPHA	BETA	- CN	CLM	CY	CLN	ČLL	_ _{CA}	CAB	CAF	ACP
1	-0.01	0.00	0.0711	-0.1396	-0.0095	0.0150	-0.0036	0.2980	0.1072		-6,6178
5	1.99	-0.00	0.3337	-0.8630	-0.0045	D.0203	-0-0017	0.2949	0.1143	0.1805	
3	3.99	-0.00	0.7021	-1.8229	-0.0034	0.0126	-0.0095	0.3055	0.1238	0.1783	-2.5964
•	5.96	-6-90	1.1216	-2.4444	-0.0025	0.0111	-0.0043	0.3291	0.1317		-5.6662
5 .	5.95	0.00	1.1166	-3.0055	-0.0614	-0.0003	-0.00	0.3366	0.1332	0.2034	-5.6060
9	7.95	-0.01	1.4370	-3.7041	-0.0455	0.1659	0.0615	0.3686	0.1508	0.2176	-2.5777
8	9.97	-0.01	1.7196	-4.1772	-0.0847	0.3308	0.1241	0.4141	0.1561	0.2581	-7.4269
9	12.01	0.00	2.7436	-4.2384	0.0102	-0.0:39	-0.0094	0.4239	0.1912	0.2327	-2.2026
10	14.02	0.01	2.6358	-5.4794	0.0016	-0.0500 -0.0310	0.0257	0.4572	0.2526 0.3033	0.2047	-2.1321 -2.0788
11	17.02	0.00	2.8447	-5.1974	0.0021	-0.0310	0.0272	0.4995	0.3189	0.1806	-2.0344
iż	18.06	0.00		-5.4146	0.0046	-0.0271	0.0237	0.4971	0.3379	0.1592	
13	19.07	-0.00	3.2092	-4.0684	0.0369	-0.0094	0.0205	0.5032	0.3401	0.1631	-1.6973
1.	20.09	-C.OU	3.3722	-6.1495	0.0384	-0.0021	3.0202		0.3554	0.1541	
15	21.14	-0.00	3.5772	-6.2043	0.0520		0.0172		0.3535	0.1617	
16	22.16	0.00	3.7313	-6-1075	0.0772	-0.1566	0.00-6	0.5136	0.3660	0.1476	-1.6368
17	23.21	-0.00	3.9296	-5.9564	0.0602		0.0386	0.5299	0.3756	0.1543	-1.5159
18	24.74	-0.01	4.1359	-5.8147	0.0575	0.0715	0.0762	0.5463	0.3888		-1.4059
19	25.30	-0.01	4.3487	-5.7066	0.0059	0.0003	0.0765		0.4130		-1.3123
20	26.35	-0.30	4.6505	-5.6734	0.1536	-0.1467	0.0928	0.5389	0.4246	0.1143	-1.2164
21	27.40	0.00	4.9149	-5.5834	0.1769	-0.2523	0.1034	0.5270	0.4435	0.0835	-1.1360
25	28.46	-0.00	5.3036	-5.4654	0.1133	-0.1105	0.0746	0.5289	0.4479	0.0811	-1.0305
53		-0.00	5.6178		0.1793		0.0865	0-5161	0.4699	0.0462	-0.9537
24				-5.2065	0.1218		0.0529		0.4802	0.0245	
25	20.10			-6.1185	0.0383		0.0216		0.4231		-1.8166
	9.78 -0.01	0.00		-3.7966		-0.0390	0.00+3		0.3365		-2.3430
26 27		0.00	0-0213	-0.1635	-0.0106	0.0164	0.0013	0.3059	0.1649	_ 0-1411	7.6695

16F	ENGINEES 1 OF 1 1 OF 1					RUPULSIUN MARTIN MI	SSILE TA	IL EFFECTS	TY (PUT) DATA	AER	ODYNAMIC WIN	D TUNNEL (4T)
	TEST 1	PAUT MA 47 0.5	CH PX10-		CONF 4=0+16 0		DELZ	DEL3 DEL4 0 0	TRANSITI UNKNOWN			
01NT	ALPHA	BETA	CN	CLM	- CŸ -	CLN	CLL	CA -	CAB -	CAF	XCP T	
1	-0.01	0.00		-0-1-27		0.0161	0.0075	0.3362	0.1176	0.2146	-7.6589	·
2	1.99	0.00	0.3330	-0.4656		0.0094	0.0012	0.3341	0.1755		-2.5848	
	3.97	-0.00		-17-5	-0.0031		-0.0063	0.3453	0.1368		-2.6374	
4	5.94	0.00		-3.012.		-0.0252	0.0005	0.3697	0.1579	0.2116	-5.6923	
🦫	7.94	0.00		-4-0461	-0.0016	-0.0056	0.014B	0.4127	0-1667	1962.0	-2.6737	
•	9,96	-0.01	1.7423	-4.3505	-0.0745	0.2947	0.1149	0.4445	0.1873		-2.4970	
	11.99	0.00	5.5465	-4.4706	0.0059	-0,0129	0.0215	0.4541	0.2140		-2.2550	
9	16.03	0.00		-5.5620	0.0185	-0.0267	0.0211	0.4832 0.5194	0.2605		-2.1400 -2.8939	
10	17.03	-0.00		-5-4425		-0.0135	0.0242	0.5254	0.3214		-2.0560	
ii	17.03	-0.00	2.4306	-6.323e	0.0555	-0.0193	0.0272	0.5263	0.3210		-2.0553	
is	10.03	-0.00	3.1354	-6.2746	0.0277	-0.0138	0.0286	0.5379	0.3330		-5.0015	
13	19.06	-0.00	3.3317	-6.4520	0.0344	-0.0279	6857.0	0.5318	0.3449		-1.9367	
14	20.09	-0.00	3.5465	-0.5007	0.0512		0.0290	0.5379	0.3439		-1.0572	
15	21.12	-0.00	3.7457	-6.e12v	0.0605	-0.0850	0.0266	0.5289	0.3521		-1.7652	
16	22.16	-0.00	3.9436	-6-5520	0.0761	-0.1303	0.0223	0.5301	0.3620	0.1661	-1,6616	
. 17	23.21	-0.00		-6.3512	0.0951	-0-121A	0.0391	0.5213	0.3603	0-1411	-1.5425	
18		-0.01	4.3763	-6.2055	0.0631	0.0512	0.0899	0.5425	0.3A57	0.1568	-1.4188	
19	25.32		4.6302	-6-6-64	0.0645	0-1028	0.1282	0.5520	0.3960		-1.3043	
50	26.39	-0.00	4.9514	-5.4331		-0.0349	0.1536	0.5512	0.4050		-1-1983	
_21 _	27.45	-0.00		-5.7159		-0.1312_	0-1324		-0.4279		-1.1039	
SS	28.53	-0.01	5.6057	-5.5647	0.1006	-0.0207			0.4328		-0.9926	
		-0-01		-5.7485	0.1027	-0.0367	_ 0.0825	0.5442	0.4535	0.0907	-0.9928	
24	29.60	-0.00		-5.4600			G.0956	0.5339	0.4650		-0.9287	
<u> 25</u>		-0.00		-5.3723		-0.1396	0.066R 0.0367	0.5300	0.4769		-0.8609 -1.8558	
27		-0.01			-0.0730			0.4280	0.3365		-2.5005	
28		0.00	0.0256	-0.1762	-0-00.00	0.0126	0-0091	0.3412	0.1960		-6.0722	
										•		

8FT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0 0.0000 0 0.3571 0 0.7356 u 1.1307 0 1.5204 u 1.9255 u 2.5661	-0./854 -0./854 -0.4681 -1.4766 -3.0242 -4.0350 -4.9748 -5.6477	CY -0.0146 -0.0124 -0.0076 -0.003H 0.0042 0.0026	0.046 0.0214 0.0174 -0.0075	-	0 0 CA 0.49n4 0.4786 0.4908 0.5217	UNKNOWN C48 0.1785 0.1920 0.1920	CAF 0.3176*	XCP •••••• •2.7109 •2.6869	
01 -0.0 0 0.0 0 0 0 0.0 0 0 0 0.0 0 0 0 0.0 0 0 0 0.0 0 0 0 0.0 0 0 0 0.0 0 0 0.0 0 0 0.0 0 0 0 0.0 0 0 0.0 0 0 0.0	0 0.0000 0 0.3571 0 0.7356 u 1.1307 0 1.5204 u 1.9255 u 2.5661	-0.7854 -7.7661 -1.9766 -3.0242 -4.0350 -4.9748 -5.6977	-0.0146 -0.0124 -0.0076 -0.0034 0.0042 0.0026	0.0466 0.0214 0.0124 -0.0025 -0.0233	0.0071 0.0072 0.0014 0.0061	0.4786 0.4786 0.4908	0.1786 0.1920 0.1920	0.3176-	-2.7109	
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.3571 0.7356 0.1307 0.15204 0.19295 0.2961 0.25661	-7.4681 -1.4766 -3.0242 -4.0350 -4.9748 -5.6477	-0.0124 -0.0076 -0.003H 0.0042	0.0214 0.0124 -0.025 -0.0233	0.0072 0.0014 0.0061	0.4786 0.4908	0.1920	0.2867	-2.7109	
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.7356 0.1.1307 0.1.5204 0.1.9295 0.2.2961 0.2.5661	-1.9766 -3.0242 -4.0350 -4.9748 -5.6977	-0.0076 -0.003H 0.0042 0.0026	0.0174 -0.0025 -0.0233	0.0014	0.4908	0-1920			
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	U 1.1307 0 1.5204 U 1.9255 U 2.7961 U 2.5661	-3.0242 -4.0350 -4.9748 -5.6977	-0.003M 0.0042 0.0026	-0.0025 -0.0233	0.0061					
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 1.5204 u 1.9255 u 2.2961 u 2.5661	-4.0350 -4.9748 -5.6477	0.0042 0500.0	-0.0733			0.1942		-2.6746	
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	u 1.9295 u 2.7961 u 2.5661	-4.9748 -5.6977	0.0026			0.5586	0.2034		-2.6539	
95 0.0 99 -0.0 13 -0.0 05 0.0	v 2.5661				0.0171	0.5873	0.2173		-2.5822	
13 -0.0 5 0.0	v 2.5661			-0.0084	0.0310	0.5832	0.2324		-2.4815	
0.0	U 2.7944		-0.0374	0.1634	0.0836	0.6036	0.2313	0.3723		
		-5.7526	0.0102	-0.0049	0.0233	0.6169	0.2650		-2.0549	••
7 -0-0	0 3.0122	-6.0440	0.0178	-0.0207	8550.0	0.6298	0.2785		-7.0065	
	3.2432	-6.3440	0.0266	-0.0305	0.0257	0.6247	0.2959	0.3338	-1.9563	
0.0-	0 3.4RZ4	-6.5646	0.0396	-0.0553	8420.0	0.6319	0.3063	0.3256	-1.8904	
11 0.0	0 3.7215	-6.7487	0.0556	-0.0913	0.0290	0.6273	0.3143	0.3130	-1.8134	
15 0.0		-6.8777		-0-1153	0.0326	0.6217	0.3213		-1.7214	
						0.6156	0.3338			
23 0.0	0 4.5891									
								0.2130	-1.2705	
		-6.7337	0.1341	-0.2263						
		-6.5300	0.1000	-0.1631						
					0.0084	0.5069				
								44541	404544	
									 	
										
	9 0.0 9 0.0 9 0.0 5 0.0 6 0.0 6 0.0 6 0.0 6 0.0 6 0.0 6 0.0	9 0.00 4.2943 3 0.00 4.5891 9 0.01 5.2151 51 0.01 5.4942 66 0.01 5.8224 65 0.01 6-1067 62 0.00 6.3797 67 0.00 6.7026 61 0.00 1.9376	9 0.00 4.2943 -7.0107 3 0.00 4.5891 -7.0064 9 0.01 4.6453 -7.0061 9 0.01 5.45151 -7.0076 10 0.01 5.4542 -6.4853 16 0.01 5.8224 -6.4327 15 0.01 6.7057 -6.5300 17 0.00 6.7026 -6.5807 11 0.00 3.7041 -6.7207 13 0.00 1.9375 -5.0766	9	9 0.00 4.2943 -7.0107 0.0794 -0.1443 3 0.00 4.5891 -7.0664 0.1001 -0.1923 9 0.01 4.6453 -7.0861 0.1165 -0.2412 15 0.01 5.4512 -7.0876 0.1336 -0.2723 10 0.01 5.4512 -6.9853 0.1745 -0.310 16 0.01 5.8224 -6.9323 0.1949 -0.3883 17 0.01 6.1067 -6.7554 0.1341 -0.2203 18 0.00 6.3797 -5.6300 0.1080 -0.1644 18 0.00 6.7026 -6.5807 0.1091 -0.1531 18 0.00 3.7081 -6.7207 0.0575 -0.1013 19 0.00 1.9376 -5.0766 -0.0012 -0.0060	9	0	9 0.00 4.2943 -7.0107 0.0794 -0.1443 0.0393 0.6156 0.3338 0.00 4.5891 -7.0664 0.1001 -0.1923 0.0548 0.6096 0.3434 0.01 4.6453 -7.0661 0.1165 -0.2412 0.0793 0.6016 0.3555 0.01 5.2151 -7.0676 0.1336 -0.2723 0.0916 0.5975 0.3678 0.1 0.01 5.4562 -6.4653 0.1745 -0.3701 0.1125 0.5879 0.3750 0.1 5.4562 -6.4653 0.1745 -0.3683 0.1205 0.5839 0.3764 0.01 5.8224 -6.4324 0.1949 -0.3683 0.1205 0.5839 0.3764 0.01 5.8224 -6.4324 0.1341 -0.2283 0.1038 0.5770 0.4011 0.2 0.00 6.3797 -6.6300 0.1080 -0.1644 0.0898 0.5725 0.4047 0.7 0.00 6.7026 -6.5807 0.1041 -0.1531 0.0744 0.5734 0.4123 0.00 3.7041 -6.7207 0.0575 -0.1013 0.0333 0.6313 0.3985 0.3 0.00 1.9376 -5.0706 -0.0012 -0.0010 0.0174 0.5673 0.3202	9	9 0.00 4.2943 -7.0107 0.0794 -0.1443 0.0393 0.6156 0.3338 0.2818 -1.6326

	TEST 1		ACH RX10-6		CONF 14 ± 0F 16	0.0	DEL1 0	OFFS	DEL3 DEL4 0 0	TRANSITION		· · - · · · · ·	
THI	ALPHA	-0.00	CN -0.0027	CUM	CY		 704	CLL 0.0101	CA :0.5340	CAB		XCP	
2	1.77	-0.6		-0.9111				0.0072	10.5222				
3	3.97	-6.00		-1.6961				:00046	0.5295		0.3283	-2.6329	
4	5.96	-0.00	1.0974	-2.8644	-0.0076	:0 -0	253	.0.0090	0.65458		0.3263		
5	7.95	0.00	1.4756	-3.0026		_	- 2	0.0135	0.5691			-2.5771	
6	9.94	0.00	1.8674	-4.7148		-		0.0165	0.587.2		0.3540		
7_	11.95	0.00		-5.4564	0.00.09			·00239	0.6001			-2.4190	
9	16.04	0.00 0.00	2.7446	-5.9633	0.0015			.0.0541.	0.6003 0.6071			-2.2834 -2.005g	
10	17.07	-0.00	2-9967	-5.8212	0.0150			0.0206	0.6167			-1.9412	
ii	19.08	-0.00		-6.1165	0.02.15			0.0168	06239		0.3476		
12	19.11	-0.00		-6.3606	1050.01			00258	0.6246		0.3376	-1.6330	· ·-
13	20.13	-0.00	3.7202	-6.5444	0.0510	·-0.0	451	0.0781	0.6185	0.2965	0.3220	-1.7555	
14	21.17	-0.00	4,,,003>	-4.6774				0.0287	0-6130		0.3115	-1.6600	
15	55.50	-0.00	43007	-6.8419	00044			.0.0339	0.6127		0.3048	-1.5909	<u>.</u>
16	23.26	0.00		-6.9164	0.0732			.0.0431	0.6041		2005	-1.4999	
17 18	24.32 25.39	0.00 6.00	4.9408 5.2H21	-6.9907 -7.0065	01011 0-1105			0.0694	0.5968		0.2751	-1.4147 -1.3265	
19	26.43	0.01	5.6230	-7.1016	0.1542			0.0823	0.5846	0.3371	0.2600	-1.2630	
50	27.50	0.01		-7.20e1				0.0811				-1.2132	
21	28.54	0.00		-7.2625				0.0815				-1.1565	
25	29.60	-0.00	6.5907	-7.2499	0.0930	-G.1	055	0.0494	0.5680			-1.1000	
23	30.66	-0.00		-7.1630				0.0408			0.1869	-1.0431	
24	20.14	-0.00	3.7206	-6.4656		-0.0		0.0294			0.2631	-1.7377	
25	9,94	0.00			-0.007		505	0.0155	0.5737	0.3052		-2.5603	
26	-0.31	-0.00	-0.0023	-0.08//	-00214	0.0	607	0.0115	0.5382	0.2295	0.3087	36.5093	
		 -											
		•											

	1E51		ACH RX10-6		COMF MUDF16	L OEL1	DELZ		TRANSITIO			
PO1NŤ	ALPHA -	BETA	CN	CLM	CY	. CLN -	CLL	· · CA	CAB	CAF	TCP	
1	-0.00	0.00	-0.0290	0.0424	-0.0063		0.0103	0.5331	0.1733		-1.4651	
5	1.99	0.00	0.330	-0.847	-0.0040	-0.0114	0.0077	0.5176	0.1809	0.3287	-2.5688	
3	3.98	0.00	0.6993	-1.7702	0.0034	-0.0356	0.0091	0.5240	0.1860	0.3380	-5.2315	
•	5.97	0.00	1.0561	-2.6464	0.0074	-0.0443	0.0134	0.5448	0.1892	0.3556	-2.5015	
5	7.97 9.97	0.00	1.4125	-3.4326 -4.1917	0.0110	-0.0604	0.0105	0.5635	0.1931 0.1990		-2.4297	
7	11.99	0.00	2.1684	-4.8684	0.0205		0.0118	0.5902	0.2073	0.3834	-2.34 61 -2.2454	
8	14.02	0.00	2.5333	-5.3316	0.0205		0.0273	0.5907	0.2085	0.3822	-2,1046	
9	16.07	0.00	2.9226	-5./012	0.0753		0.0223	0.5910	0.2114	0.3796	-1.9507	
10	17.10	-0.00	3.0608	-5.5598	0.0008	0.0644	0.0835		0.2175	0.3740	-1.8165	
11	18.13	0.00	3.2620	-5.5700	0.0262	-0.0151	0.0576	0.5896	0.2224	0.3672	-1.7096	
15	19.16	-0.00	3.4942	-5.5756	0.0440	-0.0667	0.0087	0.5866	0.2339	0.3527	-1.5957	
13	50.51	-0.00	3.7865	-5.7623	0.0438		0.0111	0.5887	0.2452	0,3435	-1,5210	
14	21.27	-0.00	4.0951	-5.4026	0.0497		0.0157	0.5869	0.2545	0.3324	-1.4414	
15	22.33	-0.00	4.4116	-6.0443	0.0638		0.0187		0.2664	0.3197	-1.3701	
16	23.36	-0.00	4.7338 4.7208	-6.1946 -6.1521	0.0778		0.0243		0.2776	0.3100	-1.3086	
17	24.42	0.00	5.0645	-6.2687	0.0785		0.0309		0.2780 0.2851	0.2983	-1.3032 -1.2370	 · -
19	25.48	0.00			0.1374		0.0462		0.2935	0.2878	-1.1761	
20	26.55	0.00	5.7670	-6.4990	0.1549		0.0499		0.2994	0.2757		
21	27.60	0.01	6.1491	-6.6542	0.1863		0.0595		0.3052	0.2640	-1.0838	
SS	25.64	0.01	6.4594	-6.7570	0.1855	-0.3732	0.0583	0.5598	0.3191	0.2408	-1.0461	
23	29.70	0.00	6.0047	-6.0145		-0.3731	0.0511	0.5578	0.3171	0.2447	-1.0022	
24	30.77	0.00	7.1684	-6.9543		-0.3607	0.0485		0.3231	0.2332		
25	20.52	0.00	3.7835	-5.6755		-0.0792	0.0176		0.3200	0.2771	-1.5001	
26	9,97	0.00	1.7465	-4.2654		-0.0561	0.0148		0.2682	0.3078	-2.3745	
	-0.00	0.00	-0-050¢	0.0512	-0.0027	0.0098	0.0145	0.5321	02034_	0.3287	-0.8069	

-	TEST 1		ACM RX10-1 30 2.3	0.0 H	CUMF Namof16 0	L DELI	DELS	DEL3 DEL4	TRANSIT	DW		
DINT	ALPHA .	BETA	. CN	ČL⊨	CA	CL+	CLL	CA .	. CAB	CAF	ACP	
1	0.00	0.00	-0.0342	0.0764	-0.0060	0.0034	0.0141	0.4968	0.1478	0.3289	-2.2506	
5	2.00	0.00	0.7457	-0.7041	-0.0099	0.0164	0.0144	0.4856	0.1753	0.3103	-2.3612	
3	3.95	0.00	0.6366	-1.5005	-0.0077	0.0107	0.0132	0.4905	0-1751		-2.3549	
•	6.00	0.00	0.9764	-5.5000	-0.0134	0.0066	0.0132	0.5071	0.1749		-2.3167	· · — — — — — — — — — — — — — — — — —
5	7.99	0.00	1.3272	-2.9833	-0.0007	0.0010	0.0133	0.5283	0.1806		-2.2478	
6	10.01	0.00	1-6903	-3.4444	0.0053	-0.0158	0.0130	0.5474	0.1850		-2.1565	
8	15.05	0.00	2.0666	-4.2454	0.0123	-0.0268	0.0140	0.5628	0.1923		-2.0541	
9	14.07	0.00	2.4613	-4.7222	0.0236	-0.050-	0.0145	0.5722	0.2012	0.3710	-r.9186	
10	16.12	0.00	2.8617 3.0966	-5.0413 -5.1737	0.0326	-0.0713	0.0150	0.5641	0.2077		-1.7616	
11	18.16	0.00	3.3664	-2.5484	0.0246	-0.0636 -0.0569	0.0554	0.5665	0.2120 0.2173		-1.6788 -1.5737	
12	19.23	0.00		-5.4161	0.0360	-0.06#3	0.0201	0.5599	0.2732		-1.4841	
13	20.27	0.00	3.9304	-5.5263	0.0503	-0.1023	0.0215	0.5561	0.2295		-1.4060	·
14	20.29	0.06	3.9354	-5.4909	0.0074	-0.0975	0.0199	0.5542	0.2325	0.3217		
15	21.33	0.00		-5.4268	0.0491	-0.0719	0.0493	0.5537	0.2340		-1.2938	
16	22.36	G. 0u		-5.4107	0.0708	-0.1395	0.0239	0.5555	0.2361		-1.2146	
17	23.44	0.00	4.7741	-5.5274	0.0769	-0.1525	0.0241	0.5558	0.2395		-1.1570	
16	24.48	0.00	5.0943	-5-5618	0.0957	-0-1748	0.0256	0.5565	0.2459	0.3106	-1.1144	
19	25.55	0.00	5.4616	-5.8556	0.1030	-0.1960	0.0281	0.5566	0.2566	0.3000	-1-0721	
20	26.60	0.00	5.0783	-5.9386	0.1254	-0.2468	0.0317	0.5562	0.2654		-1-0361	
51	27.67	0.00	6.2073	-5.2478	0.1235	-0.2499	0.0373	0.5559	0.2707	0.2851	-1.0069	
55		-0.00	6.5677	-6.4786	0.1137		0.0314	0.5583	0.2766		-0.9834	
23	29.77	-0.00		-6.854	0.1115		0.0218	0.5599	0.5855		-0.9627	
24	30.92	-0.00		-6.6930	0.1074	-0.1770	0.0193	0.5594	0.2865		-0.9439	
25	20.28	0.00		-5.4214	0.0472		0.0237	0.5590	0.2700		-1.3798	
50	10.00	0.00		-3.6619		-0.0136 0.0030	0.0144		0.2360		-2.1758	
27	-0.00	0.00	-0.03-1	0.0301	-0.0041	0.0030	0.0156	0.5005	0.5025	0.5421	1 .6696	

ARNOLD ENGINEERING DEVELOPMENT CENTER (AEDC)	PROPULSION WIND TUNNEL FACILITY (PUT)	AERODYNAMIC WIND TUNNEL (4T)
PAGE 1 OF 1	MARTIN MISSILE TAIL EFFECTS DATA	
SHEET 1 OF 1		

-	TEST	57 0	ACH RX10-0		CONF S4#0F2Z 0	L DEL1		DEL3 DEL	4 TRANSITI				
Ol NT	ALPHA	UE TA	CÁ	CLM	Ċ	, CLN	CLL .	ČA	·- CAB	CAF	XCP		
1	-0.00	0.00	0.0101	-0.0280	-0.0099	0.0164	0.0033	0.2169	0.0965	0.1225			
-	2.00	-0.0v	0.1954	-0.2374	-0.00/9	0.0169	0.0011	2612.0	0.0972	0.1220	-1.2273		
3	4.03	-0.00	0.3942	-0.5066	-0.0058	0.0169.	0.0026	0.7214	0.1015		-1.2852		
4	6.03	-0.00	0.6122	-0.8375	-0.0060	0.0740	0.0002	6955.0	0.1102		-1.3680		
5	8.03	-0.00	0.8530	-1.7176	-0.0005	0.0217	0.0040	0.2414	0.1180	0.1234	-1.4300		
6	10.06	0.00	1.1157	-1.6134	-0.0068	0.0135	0.0054	0.2508	0.1262	0.1246	-1.4461		
7	12.07	0.00	1.3824	-1.9781	-0.0114	0.0170	0.0104	0.2552	0.1308	0.1244	-1.4309		
	14.09	0.00	1.6681	-5.5403	-0.01a5	0.0241	0.0099	0.2539	0.1508	0.1031	-1.3766		
10	16.15	6.00	1.9166	-2.4542			-0.0003	0.2506	0.1595	0.0911	-1.2790		
11	17.14	-0.00	2.0466	-7.4954	-0-0206	0.0538	0.0069	0.2498	0.1599	0.0899	-1.2193		
12	16.17	-0.00	5.5018	-7.6292	-0.0189	0.0528	0.0046	0.2505	0.1646	0.0858	-1.1941		
13	19.17	-0.00	2.3643	-2.7567	-0.0150	0.0442	0.0023	0.2480	0.1772	0.0709	-1.1660		
1.	20.17	-0.00	2.5197	-2.9825	-0.0120	0.0413	0.0037	0.2461	0.183A	0.0623	-1.1440		
15	51.50	-0.00	5.6850	-2.9789	-0.0103	0.0384	0.0031	0.2417	0.1903	0.0514	-1.1107		
17	55.55	0.00	2.8795	-3.6562		-0.0140	0.0056		0.2047	0.0304	-1.0801		
16	23.23	0.00	3.0151	-3.1338	0.0367	-0.0866	0.0062		0.2148	0.0127	-1.0394		
19	24.27	0.00	3.1675	-3.1452		-0.1318	0.0177		0.2205	0.0001	-0.9930		
50	25.29	0.00	3.3306	-3-1261	0.0994	-0.2003	0.0452		0.2267	-0.0121	-0.9386		
21	26:32	0.00	3.50	-3-1320		-0.2156	0.0569		0,2383	-0.0279	-0.8939		
55	27.32	0.01	3.6747	-3-1352		_	0.10-7		0.2474	-0.0372	-0.8532		
23	28.39	0.02	3.8516	-3-1704			0.1581		0.2600	-0.0406	-0.8102		
24 25	28.40	0.02	3.8654	-3.1450 -3.2573		-1.0904	0.1664		0.3064	-0.0846	-0.8110		
59	29.40	0.02	4.2885	-3.3745		-1.2079	0.1459		0.3025		-0.8004		
27	30.40	0.02	2.4922	-7.0736			0.0198		0.3007 0.1917	-0.1180 0.0423			
28	10.24	0.00	1.0953	-1.6671			0.0234				-1.1531 -1.5220		
29	-0.01	0.06		-0.0960							-16.7928		
			• • • • • •						io.	_,,,,,,,	-1041,550		
									 -				
													
					· 								
													

	TEST	PART MA	CH #X10-6		4005 0 \$\$ 10 a 46	L DEL1	DELS	DEL3 DEL4				. –	
BINT	•						-	ب غ <u>ث</u>					- '``
THIO	ALPHA	BETA	CN	CLH		CLN	CLL	-	C # 17	CAF	ACP	•	.50
	-0.01	0.00	0.0030		-0.0109	-0.0015	0.0205	0.2306	0.0751		-26.7981		
5	-0.00	0.00	0.0054	-0.0/65	-0.0121	0.0063	0.0166	0.2301	0.0935		-14-0755		
130	2.01	0.00	0.1825	-0.7645	-0.0096	0.0011	1020.0	0.2317	0-1014	0.1303			
•	4.03	0.00	0.3801	-0.5346	-0.0670	0.0030	0.0182	0.2346	0.1045		-1.4194		
2	8.04	0.00	0.6036	-0.6870	-0.0062	0.0032	0.0214	0.2414	0.1091		1-4691		
7	10.04	0.00	0.8429	-1.57502	-0.0066	-0.0045 -0.0069	0.0261	0.2595	0.1213	0.1284	-1.5022		
	12.07	0.00	1.3422	-Z. Ú64H	-0.0131	-0.0052	0.0325	0.5905	0.1412	0.1278	-1.5162		
ŝ	14-10	0.00	1.6704	-2.3818	-0.0131	0.0032	0.0339	0.2576	0.1532		-1.4938 -1.4259		
10	16.12	0.00	1.9294	-2.3010	-0.0146	-0.0036	0.0223	0.2484	0.1559	0.0926			
11	17.16	0.00	2.0600	-2.5893	-0-0190	0.0359	0.0223	0.2484	0.1587	0.0928			
12	18.18	0.00	2.2069	-2.7022	-0-0555	0.0356	0.0241	J. 2484	0.1684		-1.2233		
13	19.17	0.00	2.3817	-2.8436	-0.0146	0.0253	0.0248	0.2480	0.1844	0.0636			
15	20.10	0.00	2.5420	-2.7484	-0.0104	0.0279	0.0260	0.2455	0.2005	0.0450			
16	21.20	0.00	2.7066	-3.0263	-0.0075	0.0237	0.0236		0.2023		-1.1100		
17	22.25	0.00	2.0612	-3.0639	0.0121	-0.0319	0.0206		0.2134	0.0238			
18	23.76	0.00	3.0314	-3.0892	0.0437	-0.1066	0.0209		0.2186		-1.0191		
19	24.27	0.00	3.1965	-3.0771	0.0598	-0.1399	0.0321	0.2283	0.2323		-0.9620		
20	25.33	0.00	3.3642	-3.0460	0.0428	-0.1786	0.0554	0.2240	0.2439		-0.9054		
21	26.36	0.00	3,5354	-3.0606	0.1137	-0.2213	0.0701	0.2180	0.2584	-0.0404			
55	27.36	0.01	3.7343	-3.0AY8	0.1860	-0.3707	0.1112	0.2146	0.2513	-0.0467	-0.8274		
23	28.41	50.0	3.9154	-3.1223	0.4584	-0.9905	0.1706	0.2181	0.2696	-0.0515	-0.7974		
24	24.42	0.01	4.1711	-3.2424	0.4198	-0.8795	0.1433	0.1959	0.3008	-0.1050	-0.7773		
25	30.47	0.01	4.4101	-3.2882	0.4535	-0.9342	0.1319	0.1750	0.3021	-0.1272	-0.7456		
26	20.20	0.00	2.5301	-2.9213	-0.0117	0.0133	0.0361	0.2513	0.2497	0.0016	-1.1546		
27	10.04	0.00	1.1106	-1-7427	-0.009A	-0.0060	0.0364		0.1662	0.0874	-1.5691		
58	-0.01	0.00	0.0008	0.1077	-0.0144	0.0015	0.0327	8952.0	0.1130	0.1158	-136.9431		
		_				<u>-</u> -							
				 ·									
		_											
												·	
											·		
													

AERODYNAHIC WIND TUNNEL (4T)

AEDC-TR-75-125

ARNOLD ENGINEERING DEVELOPMENT CENTER (AEDC) PROPULSION BIND TUNNEL FACILITY (PBT)
PAGE 1 OF 1 MARTIN MISSILE TAIL EFFECTS DATA
SHEET 1 OF 1

	1651	DADT M	ALH RX10-	b PHI	CONF	L DEL1	DELZ	DEL3 DEL4	TRANSIT	7.04		
	1		₩ 2.3		4#0F22 (0 0				
01NT "	ALPHA	BETA	CN	CLM	CY	· CLN -	CLL	- CA	CAB	···· ČAF	KCP	
	-0,00	0,00	0.0165	-0-0484	-0.0033	-0.0092	0.0076	0.2494	0,1035		-2,9347	
5	2.02	0.04	0.1957	-0.2-03	-0.0060	0.0057	0.0057	0.2460	0.1069	0.1411	-1.2278	
3	4.03	0.00	0.4056	-0.5501	-0.0015	0.0017	0.0055	0.2535	0.1102	0.1433	-1.3556	 . – –
	8.04	0.0v	0.0436	-0.9576	0.0034	-0.0171 -0.0137	0.0086	0.2659 0.2786	0.1145	0.1514 0.1519	-1.4876 -1.5781	
6	10.06	0.00	1.1778	-1.8713	0.0104	-0.0322	0.0112	0.2863	0.1364	0.1498	-1.5888	
	12.06	0.00	1.4604	-2.2712	0.0065	-0.0277	0.0159	0.2849	0.1425	0.1423	-1.5546	
	14.09	0.00	1.7483	-2.5921	-0.0053	-0.0009	0.0188		0.1449	0.1365	-1.4830	
	16.11	-0.00	2.0443	-2.08641	-0.0178	0.0532	0.0185	0.2805	0.1619	0.1156	-1.4010	
	17.16	0.00	2.1691	-2-8-79	-0.0066	0.0195	0.0076		0.1842	0.0946	-1.3129	
	18.16	0.00	5.3545	-2.4530	-0.0091	0.0248	0.0086		0.1787	0.1091	-1.2566	 -
	19.19	-0.00	84170	-3-0161	-0-0112 0-0074	0.0433	0.0042	0.2858 0.2792	0.2244	0.0614	-1.2102 -1.1740	
10	21.23	-0.00	2.4041	-3.1140	-0.0000	0.0272	0.0003		0.2310	0.0542	-1.1105	
15	95.55	-0.00	2.9501	-3.0832	0.0015	-0.0076	-0.0075		0.2417	0.0355	-1.0451	
	23.30	-0.00	3-1197	-3.07Am	0.0191	-0.0403	-0.0102	0.2753	0.2485	0.0268	-0.9869	
17	24.32	0.00	3.3142	-3.0245	0.0334	-0,0752	-0.0050		0.2606	0.0104	-0.9141	
18	25.35	-0.0ü	3.5002	-2.4776	0.0806		0.0049		0.2806	-0.0185	-0.8507	
20	27.45	0.00	3.4647	-2.9459	0.1158		0.0268		0.2846	-0.0320		
55	29.58	-0.01	4.5567	-2.4319	0.2015		0.0378		0.3148		0.5337	
53	30.65	-0.01	4,9069	-2.1437	0.1654		0.0103		0.3192	-0.1036	-0.4369	
25	10.06	0.00	1.1757		0.0071		0.0213		0.1871		1.6506	
28	-0.00	0.00	0.0073	-0.0551	-0.0057	-0.009A	0.0240	0.2459	0.1047	0.1413	-7.5479	
	· · · · · · · · · · · · · · · · · · ·			-								
												

٠.

	TEST 1		98 5.3 98 5.3		CONF	L. DEL1		OEL3 DEL4	TRANSIT!			
THIC	ALPHA	BFTA	CN	CLM	CY	CLN	"CLL	CĀ .	\CAB	CAF	ACP	
1	-0.00	0.00	0.0045	-0.0350	-0.0065	0.0035	0.0232	0.3107	0.1188	0.1918	-6,4169	
2	7.02	0.00	0.2059	-0.3038	-0.0045		0.0228	0.3097	0.1297	0.1800		
3 .	4.01	0.00	P-4109	-0.6177	-0-0012		0.0243	0.3111	0:1267	0.1644	-1.5034	
•	6.05	0.00		-1.0078	-0.0019		0.0257	0.3195	0-1335	0.1863		
5	8.04	0.00	0.9022	-1-4167	0.0020		0.0569	0.3419	0.1455	0.1964	-1.5703	
6	10.05	0.00	-1-1736	-1.6306	0.0038	-0.0160	0.0267		0-1701	0.1797	-1.5595	
7	10.05	0.00	1.1678	-1.8287	0.0049		0.0282	\ 0.3493	0.1408	0.1685	-1.5660	
	15-00	0.00	1.4566	-2-1452	0.0001		0.0310	0.3509	0.1902	0.1606	-1.5069	
9	14.11	0.00	1.7561	-2.5154	-0.0120		0.0352	0.3565	0.2209	0.1356	-1 -4324	
10	16.15	0.00	2.0601	-7.1755	-0.0206		0.0345	0.3582	0.2293	0.1289	-1.3433	
11	17.16_ 17.16_	0.00	2.2411	-2.9353	-0.0141		0.0329	0.3524	0.2422	0.1102	-1.3096 -1.3097	
12 13	18.15	0.00	2.4062	-2.4227			0.0325		0.2405	0.1196	-1.2635	
14	19.19	0.00	2.5975	-3.1717			0.0318		0.2561	0.0964	-1.2210	
15	20.23	-0.00	2.7832	-3.2184			0.0200		0.2587	0.0853	-1.1566	
16	21.25	-0.00	2.9765	-3.2165			0.0550		0.2576	0.0894	-1.0734	
17	22.29	-0.00		-3.1500	Ü.0303		0.0234	0.3410	0.2742	0.0668	-0.9867	
18	23.35	-0.00	3.4042	-2.9972			0.0310		0.2861	0.0467	-0.8792	
19	24.41	-0.00	3.6771	-2.9183	0.0010		0.0277		8595.0	0.0312		
20	25.46	-0.0u	3.9153	-2.0034	0.0921		0.0245		0.3030	0.0094	-0.7160	
51	26.51	-0.0u	4.1651	-2.6402	_		0.0260		0.3060	-0.0028	-0.6328	
<u> 55</u> –		-0.01	4,5634	-2.4443			0.0255		0.3094	-0.0056	-0.5365	
23	28.66	-0.01	4.8552	-2.2354			0.0235		0.3153	-0.0191		
74	29.74	-0.01	5.2404	-2.0014	0.2047	-0.2000	0.0303		0.3228		-0.3972	
25	30.51	-0.00	5.5514	-1.5690	0.1645	-0.2476	0.0307	0.2771	0.3265	-3.0494	-0.3547	
26	20.24	-0.0u	2.7865	-3-1661	-0.0404	0.1136	0.0278	0.3580	0.3083	0.0497	-1.1362	
27	10.06	0.00	1.1765	-1.6763	0.0040	-0.0070	0.0314	0.3481	_0.2082	0.1398	-1.5948	
								-				

-	TEST	PART MA	CH #X10-		CONF		DELS (DEL3 DEL4	TRANSITI		· · · · · · · · · · · · · · · · · · ·	•
INT AL	PMA -	RETA		CLM "	CY	CLN "	cil	<u>c</u> a	CAS	CAF		
-	0.00	-0.00	0.0011	0.0235	-0.0133	6.0355	0.0067	0.4805	0.1871		20.6462	
	2.02	-0.00	0.2145	-0.7044	-0.0220	0.0844	0.0068	0853	C-1659 -		-1.2559	
	5.05	-0.00	0.2032	-0.2360	-0.0127	0.0461	0.0049	0.4806	0.1986		-1-1712	
	.03	-0.00	n.4173	-0.5251	-0.0179	0.0689	0.0063	0.4818	0.1897		-1.2585	
	05	-0-0u	0.6454	-0 - +365	-0.0105	0.0453	0.0073	0.4911	0.1955		-1.2960	
	8.07	-0.00	0.8903	-1.1625	-0.0099 -0.0018	0.0502	0.0069	0.5072	0.1948		-1.3050	
	0.10	-0.00	1.1446	-1.44/6	0.0040	0.0330	0.0055	0.5016	8455.0		-1.3369 -1.3064	
	2.11	-0.00	1.4190	-1.7723	0.0059	0.0196	0.0072	0.5066	0.2268		-1.2463	
	. 15	-0.00	1.7249	-2.0195	0.0019	0.0253	0.0123	0.5050	0.2331		-1.1708	
	6.16	-0.00	2.0507	-2.2145	-0.0153	0.0712	0.0100	0.5030	0.2389		-1.0799	
	7.23	-0.00	2.2244	-7.2678	-0.0187	0.0892	0.0080	0.5005	0.2484		-1.0195	
	8.25	-0.00	2.4160	-2.3340	-0.0177	0.0990	0.0058	0.495A	8095.0	0.2349	-0.9681	
	9.27	-0.01	2.6167	-2.3421	-0.0209	0.1192	0.0055	0.4894	0.2649	0.2246	-0.9103	
	0.33	-0.01	2.8457	-2.3760	-0.0328	0.1634	-0.0031	0.4821	0.2745		-0.8349	
	2.43	-0.01	3.3246	-2.4350	-0.0107	0.0974	0-0001	0.4633	0.2852		-0.7313	
	2.43	-0.01	3.3431	-2.3637	0.0010	0.1025	-0.0045	0.4610	0.2764		-0.7070	·~ ——
1117	3.47	-0.01	3.5993	-2-3505	0.0055	0.0641	0.0030	0.4503	0.2802	0.1701	-0.6531	
	5.57	-0.01	3.R751 4.1757	-2.1744	0.0223	0.0626	0.0043	0.4423	0.2811	0.1570	-0.5898 -0.5207	
	6.62	-0.01	4.4746	-2.1103	0.0583	20002	0.0080	0.4293	0.2888		-0.4716	
		-0.01		-2.061+	0.0853	-0.0298	0.0077	0.4269	0.2945		-0.4296	
	8.79	-0.01	5.1374	-2.0334	0.0811	-0.0450	0.0027	0.4229	0.2900			
		-0.01	5.4170	-1.4922	G-1411	-0.1916	0.0075	0.4182	0.2938	0.1244		
	0.88	-0.00		-1.9757	0.1334	-0.2076	0.0071	0.4142	0.3038		-0.3462	
27 20	0.34	-0.01	2.8306	-2.3063	-0.033A	6.1614	0.0012	0.4827	0.2895	0.1932	-0.8148	
		-0.00	1.1462	-1.5156	0.0041	.0.0255	_0.0109	0.5047	0.2656	0.2391	-1.3200	
29	0.00	-0.00	-0.0009	0.0154	-0.0133	0.0335	0.0126	0.4761	0.2037	0.2724	-10.0271	

ر شد.

-	TEST		ACH RX10- 2u 2.3		CONF	L DEL1	DELS	DEL3 DEL4	TRANSITI	DN		
POINT	AL PHA	BETA	CN	CLM	<u>C.</u>	CLN	c	CA	CAB	CAF	KCP	
1	0.01	0.00	-0.0173		-0.0751	-0.0039	0.0128	0.4761	0-1800		-6.0+00	
2	2.02	0.00	0.1853	-0.1339	-0.00-2	-0.0044	0.0127	0.4748	0.1460		-0.7223	
3 .	4.05	0.00	0.3473	-0.3942	-0.0019	-0.0065	0.0138	0.4724	0.1568	0.3055	-0.9921	
4	6.05	0.00	0.6214	-0.6597	0.000-	-0.0104	0.0147	0.4833	0.1727	0.3105	-1.0607	
5 _	8.10	0.00	0.8586	-0.4551	0.0059	-0.0186	0.01+1	0.4931	0-1410		-1.0747	
6	10.11	0.00	1.0917		0.0053	-0.0713	0.0164	0.4917	0.1891		-1.0651	
7	12.14	0.00		-1.3904	0.0152	-0.0262	0.0141	0.4865	0.1965		-1.0112	
•	14.19	0.00	1.0007	-1.07454	0.0125	-0.0243	0.01-7	0.4866	0.1986		-0.9430	
9	14.20	0.00		-1.5975	0.0176	-0.034R	0.0144	0.4874	0.5050		-0.9347	
10	16.24	-0.00			-0.0095	0.0379	0.0160	0.4881	0.2070		-0.8575	
11 12	17.27	-0.00	5.2463	-1./9/9	-0.0154	0.0430	0.0145	0.4666	0.2091		-0.0011	
	18.32	-0.00	7.4740	-1.8386	-0.0175	0.0769	0.0110	0.4789	0.2167		-0.7573	
13	20.41	-0.01	2.7091 2.8918	-1.6372	-0.0135 -0.0107	0.0776	0.0081	0.4403	0.2238		-0.6763	
15	21.45	-0.01			-0.0045	0.0850 0.0883	0.0059	0.4764	0.2322	0.2442	-0.6353 -0.5586	
16	22.52	-0.01	3.4819		-0.0023	0.0924	0.0042	0.4687	0.2435	0.2350		
17	23.57	-0.01	3.7669	-1.6542	0.0119	0.0661	0.0038	0.4679	0.2481	0.2199		
17		-0.01	4.0636	-1.563	0.0344	0.0162	0.0047	0.4658	26+2•0	0.2167		
19	25.70	-0.01	4.3727	-1.4795	0.0552	-0.0148	0.0084	0.4617	0.2547	0.2071	-0.3383	
50	26.77		4.7117		0.0930	-0.0758	0.0133	0.4598	2695.0	0.1906	-0.3015	
51		-0.01		-1.4076	0.1087	-G.1180	0.0143	0.4596	0.2722		-0.2803	
55		-0.01		-1.3911	0.1190		0.0144	0.4578	0.2756		-0.2607	
23	29.96	-0.00	5,6023	-1.4034		-0.1751	0.0163	0.4580	0.2762		-0.2505	
54	31.03	-0.00	6.0227	-1.5125	0.1797	-0.3163	0.0181	0.4589	0.2802		-0.2511	
25	20.43	-0.00	2.9441	-1.7414	-0.0061	0.0793	0.0109		0.2737		-0.5915	
56	10.12	0.00	1.1201	-1.1432	0.0094	-0.0167	0.0192	0.4943	0.2313	0.2630	-1.0652	
27	0.00	0.00	-0.0213	0.0933		-0.0026	0.0172	0.4754	0.1856	0.2897	-4.3857	
29	0.01	0.00	-0.0202	0.1048	-0.0032	-0.0209	0.0174	0.4490	0.1716	0.2774	-5.2001	

POINT ALPMA	071 268 039 948 901 120 629 365 570 694 242 782 270 797 270
1 0.01 0.00 -0.0101 0.1016	268 039 948 901 120 629 365 570 694 242 702 270
3	039 948 901 120 629 365 570 694 242 707 270
4	748 901 120 629 365 570 694 242 702 270 707
5 6.10 -0.00 0.5892 -0.5245 0.0070 -0.0007 0.0219 0.4498 0.1684 0.2814 -0.8981 6 8.10 -0.00 0.7962 -0.7260 0.0149 0.0024 0.0228 0.4569 0.1715 0.2854 -0.9128 7 10.14 -0.00 1.0798 -0.9534 0.0065 0.0057 0.0206 0.4606 0.1755 0.2851 -0.8829 8 12.16 -0.00 1.3661 -1.1378 0.0179 0.0020 0.0197 0.4620 0.1607 0.2813 -0.8365 9 14.24 -0.00 1.6512 -1.2499 0.0114 0.0051 0.0172 0.4623 0.1849 0.2775 -0.7578 10 16.28 -0.00 2.0250 -1.3555 0.0209 0.0045 0.0129 0.4658 0.1905 0.2752 -0.6694 11 17.31 -0.00 2.2315 -1.3929 0.0114 0.0168 0.0135 0.4631 0.1905 0.2752 -0.6694 12 18.36 -0.01 2.4804 -1.4342 0.0151 0.0560 0.0113 0.4642 0.2044 0.2598 -0.5762 13 19.42 -0.01 2.7421 -1.4452 0.0301 0.0326 0.0113 0.4642 0.2044 0.2598 0.2599 -0.5762 14 20.46 -0.01 2.7421 -1.4452 0.0379 0.0256 0.0113 0.4642 0.2044 0.2598 0.2529 -0.5276 14 20.46 -0.01 2.7421 -1.4452 0.0379 0.0256 0.0113 0.4617 0.2088 0.2529 -0.5276 14 20.46 -0.01 2.7421 -1.452 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4797 15 21.52 -0.01 3.7630 -1.3960 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4278 16 22.56 -0.01 3.5233 -1.3645 0.0355 -0.0071 0.0109 0.4675 0.2211 0.2464 -0.3884 17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2387 -0.3845 18 24.73 -0.01 4.0647 -1.3310 0.0115 -0.1500 0.0169 0.4723 0.2362 0.2360 -0.2978 20 26.81 -0.00 4.4002 -1.3103 0.1115 -0.1500 0.0169 0.4723 0.2362 0.2360 -0.2978 20 26.81 -0.00 4.4002 -1.3103 0.1115 -0.1500 0.0169 0.4775 0.2430 0.2345 -0.2004	901 120 629 365 570 694 242 702 270 797
6	120 629 365 570 694 242 762 270 797
7 10.14 -0.0U 1.07v8 -0.9534 0.0065 0.0057 0.0206 0.4606 0.1755 0.2851 -0.8829 8 17.18 -0.00 1.36u1 -1.137m 0.017v 0.0002 0.0197 0.4620 0.1607 0.2813 -0.8365 9 14.24 -0.0U 1.6512 -1.2499 0.0114 0.0051 0.0172 0.4623 0.1849 0.2775 -0.7576 10 16.28 -0.00 7.0250 -1.3555 0.0209 0.0045 0.0129 0.4658 0.1905 0.2752 -0.6694 11 17.31 -0.00 7.2315 -1.342v 0.0211 0.0168 0.0135 0.4631 0.1982 0.2649 -0.6242 12 18.36 -0.01 2.4604 -1.4342 0.0153 0.0500 0.0113 0.4642 0.2044 0.2598 -0.5762 13 19.42 -0.01 2.7421 -1.4452 0.0301 0.0326 0.0113 0.4617 0.2088 0.2529 -0.5278 14 20.46 -0.01 2.9978 -1.4342 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4797 15 21.52 -0.01 3.7630 -1.3464 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4278 16 22.56 -0.01 3.7523 -1.3645 0.0365 -0.0071 0.0109 0.4675 0.2211 0.2464 -0.3884 17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2367 -0.3844 18 24.73 -0.01 4.0647 -1.3414 0.0764 -0.0764 0.0157 0.4708 0.7321 0.2367 -0.3361 19 25.76 -0.00 4.402 -1.3103 0.1115 -0.1540 0.0169 0.4775 0.2430 0.2345 -0.2978 20 26.81 -0.01 4.7198 -1.3234 0.1062 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2906	829 365 570 694 242 702 270 707 270
8 17.16 -0.00 1.36u1 -1.137u 0.017y 0.0002 0.0197 0.4620 0.1607 0.2813 -0.8365 9 14.24 -0.0u 1.4512 -1.249y 0.0114 0.0051 0.0172 0.4623 0.1849 0.2775 -8.7570 10 16.28 -0.00 2.0250 -1.3555 0.0209 0.0045 0.0129 0.4658 0.1905 0.2752 -0.6644 11 17.31 -0.00 7.2315 -1.392y 0.0211 0.0168 0.0135 0.4631 0.1902 0.2649 -0.6242 12 18.36 -0.01 2.4604 -1.4342 0.0153 0.0500 0.0113 0.4642 0.2044 0.2579 -0.5702 13 19.42 -0.01 2.7421 -1.4452 0.0301 0.0326 0.0113 0.4617 0.2088 0.2529 -0.5270 14 20.46 -0.01 2.9878 -1.3334 0.0297 0.0256 0.0100 0.4620 0.2122 0.2498 -0.4797 15 21.52 -0.01 3.7630 -1.346J 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4278 16 27.56 -0.01 3.5233 -1.3645 0.0365 -0.0071 0.0109 0.4675 0.2211 0.2464 -0.3884 17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2367 -0.3884 18 24.73 -0.01 4.0647 -1.3414 0.0764 -0.0843 0.0157 0.4708 0.7321 0.2367 -0.3361 19 25.76 -0.00 4.4002 -1.3103 0.1115 -0.1500 0.0109 0.4775 0.2430 0.2345 -0.2301	365 570 694 242 270 270 270
9 14.24 -0.00 1.6512 -1.2499 0.0114 0.0051 0.0172 0.4623 0.1949 0.2775 -0.7570 10 16.28 -0.00 2.0250 -1.3555 0.0209 0.0045 0.0129 0.4658 0.1905 0.2752 -0.6694 11 17.31 -0.00 2.2315 -1.3929 0.0211 0.0168 0.0135 0.4631 0.1982 0.2649 -0.6242 12 18.36 -0.01 2.4604 -1.432 0.0153 0.0500 0.0113 0.4642 0.2044 0.2598 -0.5782 13 19.42 -0.01 2.7421 -1.4452 0.0331 0.0500 0.0113 0.4647 0.2088 0.2599 -0.5782 14 20.46 -0.01 2.9878 -1.4334 0.0297 0.0256 0.0100 0.4620 0.2122 0.2488 0.2599 -0.5782 15 21.52 -0.01 3.7630 -1.3460 0.0379 0.0164 0.0111 0.4636 0.2188 0.2448 -0.4797 15 21.52 -0.01 3.5233 -1.3455 0.0399 -0.0071 0.0109 0.4675 0.2211 0.2464 -0.3884 17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2387 -0.3641 18 24.73 -0.01 4.0647 -1.3103 0.1115 -0.1500 0.0169 0.4723 0.2362 0.2360 -0.2978 20 26.81 -0.01 4.7198 -1.3230 0.1062 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2004	570 694 694 242 702 270 797 276 276
10	694 242 762 279 797 278
11 17.31 -0.00 7.2315 -1.392 0.0211 0.0168 0.0135 0.4631 0.1982 0.2649 -0.6242 12 18.36 -0.01 2.4604 -1.4342 0.0153 0.0500 0.0113 0.4642 0.2044 0.2598 -0.5782 13 19.42 -0.01 2.7421 -1.4452 0.0301 0.0326 0.0113 0.4617 0.2088 0.2529 -0.5278 14 20.46 -0.01 2.9878 -1.4334 0.0297 0.0756 0.0100 0.4620 0.2122 0.2498 -0.4797 15 21.52 -0.01 3.7630 -1.3963 0.0379 0.0164 0.0111 0.4636 0.2168 0.2448 -0.4278 16 27.56 -0.01 3.5233 -1.3645 0.0385 -0.0071 0.0109 0.4675 0.2211 0.2464 -0.3884 17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2387 -0.3844 18 24.73 -0.01 4.0647 -1.3410 0.0764 -0.0843 0.0157 0.4708 0.7321 0.2387 -0.3361 19 25.76 -0.00 4.4067 -1.3103 0.1115 -0.1540 0.0169 0.4775 0.2430 0.2345 -0.2978 20 26.81 -0.01 4.7198 -1.3234 0.1082 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2804	242
12	762 270 797 276
13	276 797 276
14	797 278
16	
17 23.63 -0.01 3.7412 -1.3623 0.0575 -0.0377 0.0137 0.4651 0.2263 0.2387 -0.3641 18 24.73 -0.01 4.0647 -1.3410 0.0764 -0.0843 0.0157 0.4708 0.7321 0.2387 -0.3301 19 25.76 -0.00 4.4002 -1.3103 0.1115 -0.1540 0.0189 0.4723 0.2362 0.2360 -0.2978 20 26.81 -0.01 4.7198 -1.3234 0.1082 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2804	684
18	
19 25.76 -0.00 4.4002 -1.3103 0.1115 -0.1540 0.0189 0.4723 0.2362 0.2360 -0.2978 20 26.41 -0.01 4.7198 -1.3234 0.1062 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2804	641
20 26.41 -0.01 4.7198 -1.3234 0.1062 -0.1231 0.0190 0.4775 0.2430 0.2345 -0.2604	
TY	
21 27.84 40.01 5.0647 41.4244 41.1137 40.1109 0.0205 0.4761 0.2477 0.2284 40.2824	
22 2A.95 -0.01 5.4241 -1.5080 0.1344 -0.1208 0.0177 0.4804 0.2519 0.2285 -0.2788	
24	
25	
27 -0.00 0.00 0.0190 -0.0713 -0.0157 0.0256 0.0236 0.4531 0.1751 0.2760 -1.7471	A80
Enera neam menta -nenta -nenta neama neama neama neamat nemiat nemiat nemiat	P80
	P80
	P80

												
			CH RX10-		CONF		1 DEFS	DEL3 DEL4	TRANSIT	ION		
	1	71 0-6			4m0+23 0	• 0	•			~		
_	BLPHA	BETA	CN	CLM	C4	CLN	CLL	CA	CAB	CAF	ACP	·
	-0.00	0.00			-0.0062		-0.0047	0.2345	0.1038		-2,3048	
2	2.01	0.00	0.1962	-0.2443	-0.0030	-0.0078	-0.0137	0.2372	0.1056	0.1316	-1.2705	
3	4.02 6.03	0.00	0.4044	-0.5826	0.0030	-0.0153 -0.0227	-0.0140	0.2346 0.2350	0.1115	0.1230 0.1231	-1.5922	
5	A. 03	0.00	0.8822	-1.4121	0.0057	-0.0261	-0.0162	0.2350	0.1114	0.1337	-1.5722	
-	10.06	0.00	1.1222	-1.7323	0.0056	-0.0273	-0.0129	0-5606	0.1267	0.1337	-1.5437	
	12.10	0.00	1.3496	-1.9291	-0.0020	-0.01-3	-0.0116	0.2657	0.1440	0.1217	-1.4294	
	14.79	0.00	1.5540	-1.9745	-0.0048	-0.0021	-0.0125	0.2660	0.1564	0.1116	-1.2706	
9	16.15	-0.00	1.7322	-1-6376	-0.0243	0.0513	-0.0117	0.2773	0.1749	0-1024	-1.0609	
10	17.17	-0.0v	1.6551	-1.e103	-0.0240	0.0610	-0.0123	0.2805	0-1960	0.0845	-0.9758	
	18.16	-0.00		-1.POO7	-0.0307	G.0796	-0.0127	0.2855	0.2209	0.0646	-0.4212	
	19.21	-0.0v	5-1015	-1.7011	-0.0243	0.0751	-0.0172	0.2979	0.2553	0.0427	-0.8477	
	20.19	-0.00	2.2161	-1.7520	-0.0368	0.0844	-0.0179	0.3028	0.2751	0.0278	-0.7906	
	21.22	-0,0v	2.3339	-1.7005	-0.0269	0.0724		0.3107	0.2926	0.0181	-0.7286	
	22.27 23.30	-0.00	2.4524	-1-6401	-0-0045	0.0433		0.3176	0.3186	-0.0008		
	24.32	-0.00 -0.00	2.7A79	-1.5674	0.0010	0.0723	-0.0154 -0.0130	0.3281 0.3294	0.3287	-0.0005	-0.59 88 -0.562 3	
_	25.33	-0.00	2.9606	-1.5730	0.0469	-0.0673		0.3301	0.3570	-0.0268	-0.5313	
_	26.40	-0.00	3.1491	-1.6174	0.0-84	-0.0573		0.3303	0.3719		-0.5136	
	27.42	0.00	3.3317	-1.6763	G-17ty	-0.3448	0.0205	0.3168	U.3737		-0.5091	
_	25.43	0.00	3.5417	_	0.2514	-0.4945		0.3100	0.3709		-0.5039	
55	29.45	0.00	3.7336	-1.6465	0.3210	-0.6409		0.3026	0.3761	-0.0735	-0.4946	·
23	30.46	0.01	3.9725	-2-0121	0.4593	-0.9556	0.0807	0.7949	0.3971	-0.1022	-0.5065	
24	24.46	0.00	3.7577	-1.9148	0.3223	-0.6742	0-0471	0.3007	0.3974	-0.0967	-0.5096	
25	30.49	0.01	3.9613	-1.9995	0.4720	-0.9777		0.2947	0.3995		-6.5048	
_	32.6Z	-0.00	2.2130			0.0706		0.3099	0.3227		-0.7854	
27	50.55	-0.00		-1.7420		0.0739		0.3070	0.3550		-0.7666	
5 9	10.06	0.00		-1.7234				0.2609	0.1791		-1.5484	
	-0.00		-0.0025	-u+uu3+	-0.0004	0.0014	0.0042	0.5370	-0-1031	0-1546		

-0.00 0.00 -0.0026 -0.0003 -0.0073 -0.0020 -0.0041 0.2385 0.1045 0.1340 0.1359 2.00 0.00 0.1026 -0.7264 -0.0030 -0.0114 -0.0007 0.2379 0.1056 0.1343 -1.2425 4.03 0.00 0.4011 -0.5527 -0.0014 -0.0168 -0.0097 0.2377 0.1120 0.1257 -1.4527 6.03 0.00 0.6649 -1.0517 0.0045 -0.0323 -0.0118 0.2411 0.1038 0.1373 -1.6309 8.05 0.00 0.8602 -1.4298 0.0054 -0.0323 -0.0118 0.2411 0.1038 0.1373 -1.6309 8.05 0.00 0.8602 -1.4298 0.0054 -0.0339 -0.0108 0.2560 0.1358 0.1182 -1.6245 10.08 0.00 1.1104 -1.7369 0.0071 -0.0388 -0.0108 0.2569 0.1385 0.1283 -1.5542 17.08 0.00 1.3488 -1.9474 -0.0038 -0.0131 -0.0077 0.2717 0.1466 0.1271 -1.4438 14.09 0.00 1.5729 -7.0551 -0.0112 -0.0011 -0.0009 0.2710 0.1695 0.1015 -1.3064 14.09 0.00 1.5778 -7.0554 -0.0110 -0.0041 -0.0049 0.2741 0.1831 0.0909 -1.3839 16.13 0.00 1.7729 -1.9884 -0.0209 0.0788 -0.0099 0.2874 0.1920 0.0955 -1.1193 17.15 -0.00 1.8980 -1.9492 -0.0270 0.0524 -0.0102 0.3001 0.2209 0.0792 -1.0281 18.18 0.00 2.0099 -1.9492 -0.0270 0.0524 -0.0125 0.2988 0.2393 0.0594 -0.9568 19.73 -0.00 2.1263 -1.9034 -0.0290 0.0595 -0.0125 0.2988 0.2393 0.0594 -0.9568 19.73 -0.00 2.2279 -1.8372 -0.0223 0.0523 -0.0155 0.3208 0.2830 0.3777 -0.0266 21.76 -0.00 2.4044 -1.7621 -0.0121 0.0427 -0.0169 0.3304 0.2207 0.0373 -0.0524 22.30 -0.00 2.6637 -1.5778 0.0134 0.0027 -0.0169 0.3304 0.2271 0.0333 -0.7328 22.31 -0.00 2.6637 -1.5778 0.0134 0.0027 -0.0169 0.3304 0.2271 0.0333 -0.7328 22.33 -0.00 3.8058 -1.5989 0.0260 -0.0037 0.3490 0.3524 -0.0034 -0.5593 25.38 -0.00 3.8058 -1.5989 0.0260 -0.0033 -0.0077 0.3490 0.3524 -0.0034 -0.5593 25.38 -0.00 3.8034 -1.5995 0.0433 -0.0595 -0.0037 0.3490 0.3524 -0.0034 -0.5593 25.38 -0.00 3.8039 -1.5710 0.19405 -0.0069 0.0037 0.3040 0.3979 -0.0599 -0.5074 27.42 -0.00 3.8034 -1.5999 0.2666 -0.5050 0.0037 0.3040 0.3979 -0.0599 -0.5074 27.42 -0.00 3.8034 -1.5999 0.2666 -0.5050 0.0037 0.3040 0.3995 -0.0085 -0.0085 -0.0090		1											·- -
-0.00		- •	16 00				L DEL	1 DEFS	OEL3 OEL4 0 0	TRANSIT!	ION		
-0.00		ALPHA	BETA	CN	CLM	CY -	ČLN -	CLL	CA	CAB -	CAF	XCP	
4.03 0.00 0.4011 -0.5b27 -0.0014 -0.0168 -0.0049 0.2377 0.1120 0.1257 -1.4527 6.03 0.00 0.6449 -1.0517 0.0045 -0.0323 -0.0118 0.2411 0.1038 0.1373 -1.6309 0.05 0.00 0.8802 -1.4248 0.0054 -0.0359 -0.0104 0.2540 0.1358 0.1162 -1.6245 0.1040 0.00 0.00 0.00 0.1104 -1.7369 0.0071 -0.0368 -0.0108 0.2669 0.1385 0.1283 -1.5642 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		-0.00	0.00	-0.0026						0.1045			
6.03 0.00 0.6649 -1.0517 0.0065 -0.0323 -0.0118 0.2411 0.1038 0.1373 -1.6308 10.08 0.00 0.6602 -1.4248 0.0052 -0.0354 -0.0104 0.2540 0.1358 0.1182 -1.6245 10.08 0.00 1.1104 -1.7369 0.0071 -0.0368 -0.0108 0.2669 0.1385 0.1283 -1.5642 17.08 0.00 1.3486 -1.4474 -0.0038 -0.0118 -0.0077 0.2717 0.1446 0.1271 -1.4438 17.09 0.00 1.5778 -7.0551 -0.0112 -0.0011 -0.0069 0.2710 0.1695 0.1015 -1.3066 14.09 0.00 1.5778 -7.0552 -0.0112 -0.0011 -0.0069 0.2710 0.1695 0.1015 -1.3066 16.13 0.00 1.7729 -1.9045 -0.0209 0.2788 -0.0099 0.2741 0.1831 0.0009 -1.3038 17.15 -0.00 1.8960 -1.4492 -0.0270 0.0524 -0.0102 0.3001 0.2209 0.0792 -1.0281 18.18 -0.00 1.8960 -1.4492 -0.0270 0.0595 -0.0125 0.2988 0.2393 0.0596 -0.9568 19.73 -0.00 2.2779 -1.8172 -0.0290 0.0595 -0.0125 0.2988 0.2393 0.0596 -0.9568 19.73 -0.00 2.2779 -1.8172 -0.0223 0.0526 -0.0131 0.3033 0.2621 0.0412 -0.8951 20.24 -0.00 2.2279 -1.8172 -0.0223 0.0526 0.3006 0.2803 0.0377 -0.8246 21.26 -0.00 2.2279 -1.8172 -0.0223 0.0526 -0.0156 0.3206 0.2830 0.0377 -0.8246 22.30 -0.00 2.5295 -1.6515 -0.0026 0.0296 -0.0156 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0277 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0277 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0277 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0134 0.0027 -0.0169 0.3304 0.2071 0.0333 -0.7328 22.33 -0.00 2.6637 -1.5776 0.0024 0.0024 0.0024 0.0004 0.3221 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.3021 0.0004 0.0004 0.3021 0.0004 0.3021 0.0004 0.0004 0.0004 0.3021 0.0004 0.0004 0.		2.00	0.00								0.1343	-1.2425	
8.05													
10.08													
17.08													
14.09					_	_		-		_			
14.09													
16.13 0.00 1.772\(-1.486\) -0.020\(0.078\) -0.010\(0.300\) 0.220\(0.079\) -1.020\\ 17.15\) -0.00\(1.896\) -1.449\(0.027\) 0.05\(0.05\) -0.010\(0.300\) 0.220\(0.079\) -1.020\\ 18.18\) -0.00\(0.070\) -1.470\(0.029\) 0.05\(0.070\) -0.012\(0.300\) 0.220\(0.079\) -1.020\\ 18.18\\ -0.00\(0.277\) -1.021\(0.029\) 0.05\(0.070\) -0.012\(0.303\) 0.262\(0.04\) 0.09\\ 20.24\(-0.00\) 2.1263\(-1.993\) -0.026\(0.070\) -0.013\(0.303\) 0.262\(0.04\) 0.037\(-0.0826\) -0.082\\ 21.26\(-0.00\) 2.4044\(-1.762\) -0.012\(0.026\) 0.022\(0.027\) -0.016\(0.330\) 0.27\(0.330\) 0.27\(0.330\) 0.27\(0.033\) -0.732\\ 22.30\(-0.00\) 2.663\(-1.577\) 0.013\(0.026\) 0.022\(0.027\) -0.016\(0.3483\) 0.342\(0.343\) 0.015\(-0.592\) 23.31\(-0.00\) 2.663\(-1.577\) 0.013\(0.026\) 0.022\(0.007\) -0.011\(0.3483\) 0.342\(0.353\) 0.055\(-0.052\) -0.592\\ 25.38\(-0.00\) 3.025\(0.033\) -1.577\(0.043\) 0.026\(0.026\) -0.003\(0.349\) 0.352\(-0.003\) -0.5503\(25.38\) -0.00\(0.379\) -1.5710\(0.066\) -0.099\(0.000\) 0.032\(0.037\) 0.349\(0.379\) -0.036\(0.037\) -0.036\(0.037\) -0.503\(0.379\) -0.059\(0.379\) -0.503\(0.379\) -0.503\(0.379\) -0.503\(0.379\) -0.063\(0.379\) -0.503\(0.379\) -0.503\(0.379\) -0.638\(0.379\) -0.638\(0.379\) -0.638\(0.379\) -0.638\(0.379\) -0.638\(0.379\) -0.639\(0.399\) -0.533\(0.399\) -0.533\(0.399\) -0.533\(0.399\) -0.533\(0.399\) -0.533\(0.399\) -0.533\(0.399\) -0.638\(0.399\) -0.638\(0.399\) -0.638\(0.399\) -0.638\(0.399\) -0.639\(0.													
17.15 -0.00													
10.18 -0.00													
19.73 -0.00			-										
20.24 -0.00													
21.76 -0.00													
22.30 -0.00													
23.31 -0.00											0.0333	-0-6539	
24.33 -0.00 2.8458 -1.5889 0.0260 -0.0003 -0.0077 0.3490 0.3524 -0.0034 -0.5583 25.38 -0.00 3.0265 -1.5952 0.0433 -0.0515 -0.0037 0.3461 0.3702 -0.0240 -0.5271 26.36 -0.00 3.7038 -1.6254 0.0004 -0.0998 0.0004 0.3421 0.3791 -0.0369 -0.5074 27.42 -0.00 3.7955 -1.7101 0.1905 -0.3500 0.0309 0.3245 0.3836 -0.0591 -0.5036 28.43 0.00 3.6137 -1.7929 0.2646 -0.5050 0.7664 0.3160 0.3798 -0.0638 -0.4961 29.48 -0.00 3.8634 -1.9093 0.2217 -0.4020 0.0375 0.3040 0.3925 -0.0885 -0.4961 30.53 -0.00 4.1206 -2.0200 0.2996 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 2.2535 -1.9249 -0.0163 0.0363 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7562 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
25.38 -0.00 3.0265 -1.5952 0.0033 -0.0515 -0.0037 0.3461 0.3702 -0.0240 -0.5271 26.36 -0.00 3.2036 -1.6258 0.0668 -0.0998 0.0004 0.3421 0.3791 -0.0369 -0.5074 27.42 -0.00 3.7955 -1.7101 0.1905 -0.3560 0.0309 0.3245 0.3836 -0.0591 -0.5036 28.43 0.00 3.6134 -1.7929 0.2646 -0.5050 0.0464 0.3160 0.3798 -0.0638 -0.4961 29.48 -0.00 3.8634 -1.9093 0.2217 -0.4020 0.0375 0.3040 0.3925 -0.0885 -0.4942 30.53 -0.00 4.1206 -2.0200 0.2996 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 7.2535 -1.9249 -0.0163 0.0333 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7502 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
26.36 -0.00 3.7038 -1.6258 0.0668 -0.0998 0.0004 0.3421 0.3791 -0.0369 -0.5074 27.42 -0.00 3.7955 -1.7101 0.1405 -0.3540 0.0309 0.3245 0.3836 -0.0591 -0.5036 28.43 0.00 3.6134 -1.7929 0.2646 -0.5050 0.9464 0.3160 0.3798 -0.0638 -0.4961 29.48 -0.00 3.8634 -1.44093 0.2217 -0.4020 0.0375 0.3040 0.3425 -0.0885 -0.4942 30.53 -0.00 4.1206 -2.0200 0.2946 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 7.2535 -1.4249 -0.0163 0.0333 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7502 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
27.42 -0.00 3.795 -1.7101 0.1405 -0.3500 0.0309 0.3245 0.3836 -0.0591 -0.5036 28.43 0.00 3.6134 -1.7924 0.2646 -0.5050 0.9464 0.3160 0.3798 -0.0638 -0.4961 29.48 -0.00 3.8634 -1.4093 0.2217 -0.4020 0.0375 0.3040 0.3425 -0.0885 -0.4942 30.53 -0.00 4.1206 -2.0200 0.2746 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 2.2535 -1.4249 -0.0183 0.0333 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7502 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
28.43 0.00 3.6137 -1.7927 0.2646 -0.5050 0.7464 0.3160 0.3798 -0.0638 -0.4961 29.48 -0.00 3.8634 -1.7093 0.2217 -0.4020 0.0375 0.3040 0.3925 -0.0885 -0.4942 30.53 -0.00 4.1206 -2.0200 0.2976 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 7.2535 -1.7249 -0.0183 0.0383 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7562 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
29.48 -0.00 3.8634 -1.4093 0.2217 -0.4020 0.0375 0.3040 0.3925 -0.0885 -0.4942 - 30.53 -0.00 4.1206 -2.0200 0.2946 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 7.2535 -1.4749 -0.0183 0.0383 -0.0125 0.3263 0.3554 -0.0791 -0.8098 10.05 0.00 1.1175 -1.7562 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
30.53 -0.00 4.1206 -2.0200 0.2996 -0.5412 0.0531 0.2911 0.3916 -0.1006 -0.4902 20.22 -0.00 2.2535 -1.9249 -0.0183 0.0383 -0.0125 0.3263 0.3554 -0.0291 -0.8098 10.05 0.00 1.1175 -1.7562 0.0072 -0.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
20.22 -0.00 7.2535 -1.4744 -0.0183 0.0383 -0.0125 0.3263 0.3554 -0.0791 -0.8098 10.05 0.00 1.1175 -1.7562 0.0072 -0.0349 -0.0073 0.2674 0.2130 0.0549 -1.5714	,												
10.05 0.00 1.1175 -1.7562 0.0072 -G.0349 -0.0073 0.2679 0.2130 0.0549 -1.5714													
0.000.000.00+0.00+50.00+70.000,70.00+10.23990.12950.11041.9184									0.2679	0.2130	0.0549	-1.5714	
		-0.00	0.00	-0.00-9	-0-0095	-0-0097	-0-0007	-0.0041	0.2399	0.1295	0-1104	1.9186	
			~~~		. 111000	,,,,,,,,				_ 00 iE33	\$00.00		
·											·	<del></del>	
·	- —							<del></del>				<del></del>	

	TEST		ACH RX10-		CONF		DEL2	DEL3 DEL4	THANSIT	104		
					o w							<del> </del>
POINT	-0.00	BETA 0.00	-0.0045	CLM 0.0141	CY -0.0071	-0.0077	CLL -0.0007	CA 0.2515	CA8 0.1057	CAF 0.1458	XCP	•
- 1	-0.00	0.00	-0.0072	0.0107	-0.00+1	-0.000	-0.0073	0.2516	0.1094	0.1422	-1.4780 -1.4858	
3	2.00	0.06	0.1802	-0.2124	-0.0040	-0.0152	-0.0078	0.2529	0.1152	0.1377	-1.1815	
•	4.01	0.00	0.3936	-0.5679	-0.0006	-0.0758	-0.0080	0.2498	0.1700	0.1298	-1.4428	
5	6.01	0.00	0.6624	-1.1104	0.0042	-0.06-2	-0.0134	0.7516	0.1226	0.1290	-1.6752	
6	8.03	0.00	0.9768	-1.e1/1	-0.0001	-0.0167	0.0019	0.2673	0.1268	0.1405	-1.7447	
7	10.07	0.00	1.1654	-1.4735	0.0057	-0.0470	-0.0087	0.7814	0.1406	0.1408	-1.6491	
8	15.00	0.00	1.4022	-2-1-02	-0.0022	-0-07-8	-0.0024	0.2933	0.1567	0.1366	-1.5263	
•	14.09	0.00	1.6343	-2.2042	-0.0134	-0.0059	0.0002	0.3034	0.1669	0.1365	-1.3934	
10	16.15	0.00	1.90+1	-2.3580	-0.0155	0.0005	-0.0093	0.3072	0.2144	0.0928	-1.2364	
11 .	17.17	0.00	5.0025	-2.3159	-0.0155	0.0144	-0.0081	0.3196	0.2370	0.0826	-1.1567	
12	18.19	-0.00	2.1342	-2.3026 -2.361	-0.0210 -0.0213	0.0306 0.03m7	-0.0121 -0.0125	0.3276	0.2596	0.0681	-1.0764 -1.0138	
14	20.25	-0.00	2.3706	-2.100.	-0.0119	0.0747	-0.0172	0.330A 0.3497	0.2832	0.0476	-0.8694	·
15	21.26	-0.0v	2.4912	-1.913n	-0.0174	0.0463	-0.0165	0.3627	0.3200	0.0427	-0.7682	
16	22.32	-0.00	7.6395	-1.7861	-0.0033	0.0511	-0.0092	0.3835	0.3418	0.0417	-0.6767	·
17	23.31	-0.00	2.7858	-1.7458	-0.0006	0.0579	-0.0066	0.3843	0.3522	0.0321	-0.6267	
18	24.38	-0.00	2.9416	-1.7426	0.01/3	0.0211	-0.0079	0.3806	0.3697	0.0109	-0.5834	
19	25.41	-0.00	3.1824	-1.7543	0.0490	-0.045B	-0.0060	0.3772	0.3775	-0.0003	-0.5512	
50	26.42	-0.0ú	3,4013	-1.7231	0.1287	-0.1995	0.0134	0.3674	0.3A22	-0.0148	-0.5068	
21	27.49	-0.00	3.6348	-1.6460	0.1461	-0.2245	0.0202	0.3597	0.3930	-0.0332	-0.4524	
55		-0.01	3.9187	-1 - +2 + 1	0.1803	-0.2377	0.7215	0.3545	0.3886	-0.0341	-0.3634	
53		-0.01	4.2818	-1.0476		-0.1298	0.0130	0.3538	0.3974		-0.2563	
54		-0.01	4.5647	-0.8827		-0.0557	0.0066	0.3448	0.4123		-0.3935	
25	20.24	-0.00	2.3754	-2.1265			-0.0088	0.3555	0.3411	-0.0256		
26	10.04	0.00	1.1675	-1.4491		-0.032B		0.2864	0.2617	0.0247	-1.6694	
27	-0.00	0.00	0.0045	. 0.0019	-0.0043	0.0014	_0.0011	0.5483 _	nº i azā	-a. rosē	-0.5018	<del></del>
						<del></del>					<del></del>	
						<del>-</del>	<u> </u>				<del></del>	

<del></del> -	TEST		46 5.3		CONF 4=0f23 0	.0 UEL	1 DEL2 0 <b>0</b>	DEL3 DEL4	TRANSIT		
POINT	ALPHA "	BETA	CN	CLM	CA	CLH	CLL	: CA	CAB	ČAF	ACP
2	-0.00	-0.00	0.0066		-0.0151		-0.0099	0.3186	0.1337		-7.3165
3	2.63	0.00	0.2319	-0.4294	-0.0117	0.0159	-0.011A	0.3160	0.1373		-1.8538
_ •	4.01	0.00	0.4766	-0.8794	-0.0046	-0.0011	-0.0137	0.3165	0.1515		-1.8672
5	6.04	0.00	0.7009	-1-3420	-0.0010	-0.0235	-0.0124	0.3288	0.1517		-1.9147
<u> </u>	8.12	0.00	0.9945	-1.8820	0.0001	-0.0705	-0.0078	0.3473	0.1630		-1.8930
	12.07	0.00	1.5449	-2.6644	-0.0106	-0.0132	0.0091	0.3583	0.2066	0.1516	-1.7246
	14.10	0.00	1.7990	-2.7677	-0.0236	0.0312	0.0087	0.3695	0.2187	0,1508	-1.5470
10	16.14	0.00	2.0397	-2.51Yn	-0.0133	0.0733	-0.0050	0.3716	0.2566	0.1150	-1.3025
11	17.14	-0.00	2.1846 2.3247	-2.8471 -2.8554	-0.0106	0.0235	-0.0089	0.3801	0.2682	0.1120	-1.3032
13	19.22	-0.00	2.5111	-2.8430	-0.0130	0.0311 0.0359	-0.0095	0.3840	0.2809		-1.2263 -1.1322
14	20.22	-0.00	2.6800	-2.8011	-0.0209	0.6119	-0.0224	0.3831	0.3074	0.0790	-1.0452
15	21.29	-0.00	2.8515	-2.7220	-0.0139	0.0-15	-0.0252	0.3755	0.3236		-0.9546
16	22.34	-0.00	3.0252	-5.5615	0.0108	0.0177	-0.0170	0.3707	0.3370	0.0520	-0.8467
17	23.37	-0.00	3.2751	-2.4591	0.0308	-0.C198	-0.0156	0.3696	0.3359	0.0337	
18	24.41	-0.01	3.5057	-2.J022	0.0342	-0.0744	-0.0138	0.3623	0.3418	0.0205	-0.6567
19	25.40	-0.01	3,6757	-2.1295	0.0579	-0.0732	-0.0040	0.3553	0.3519	0.0034	-0.5793
20	26.57	-0.01	4.0001	-1.8039	0.1016	-0.0468	0.0064	0.3595	0.3588	0.0007	
21	27.61	-0.01	4.3250	-1.5871	0.0997	-0.0073	0.00-6	0-3554	0.3596	-0.0041	-0.3669
25	28.74	-0.01	4.6617	-1-3551	0.0827	-0.00+8	-0.0043	0.3385	0.3576	-0.0191	-0.2907
23	29.74	-0.01	5.0895	-1.2814	0.0987	-0.0622	-0.0056	0.3286	0.3563	-0.0296	-0.2519
24	30.82	-0.01	5.3039	-1.0102	0.0646	0.0769	-0.0115	0.3361	0.3645	-0.0284	-0.1905
25	20.24	-0.00	2.6910	-2.7456	-0.0173	0.0550	-0.0193	0.3918	0.3474	0.0444	-1.0352
26	20.23	-0.00	2.6625	-2.1723	-0.0158	C.0431	-0.0210	0.3828	0.3454	0.0374	-1.0413
27	10.03	0.00	1.2654	-2.3235	-0.0024	-0.0320	-0.0050	0.3616	0.2572	0.1044	-1.8347
28	-0.20	-0.00	0.0049	-0.0591	-0.0151	0.0367	-0.0115	0.3217	0.1630	0.1587	-6.6695

	TEST 1		ACH RX10-0		CONF 14=0F23 0	.O DEL	O O	DEL3 DEL4	TRANSITI		
		BETA	CN	CLM	CY	CLN		- CA	CAB	CAF	
	2.03	-0.00	0.2301	-0.3854	-0.0176	3-0450	-0.0083	0.5010	0.2061	0.2956	-3.0213 -1.6767
	4.04	-0.00	0.4769	-0.8103	-0.0113	0.0348	-0.0116	0.4995	0.2005	0.2990	-1.7207
	6.03	-0.00		-1-2571	-0.0105	C.0285	-0.0103	0.5117	0.2069		-1.7350
	8.07	-0.00	0.9864	-1.6721	-0.0087	0.0175	-0.0091	0.5162	0.2168	0.2974	-1.6952
	14,13	-0.0C	1.63+8	-2.5877	-0.0133	0.0312	-0.0046	0.5150	0.2451		-1.4103
	4.13	-0.00	1.8425	-2.5A11	-0.0111	0.0335	-0.00+6	0.5160	0.2506		-1.4009
-	16.16	-0.00	2.1447	-2.7331	-0.0141	0.0503	-0.0101	0.5103	0.2527		-1.2744
	17.20 18.22	-0.00	2.3129	-2.78ce	-0.0186	0.0698	0.000B	0.5082	0.2562		-1.2032
	19.25	-0.01	2.6367	-2.6911	-0.0285	0.1259	-0.0121	0.5007	0.2668	0.2418	-1.0199
	0.31	-0.01	2.8870	-2.0485	-0.0749	0.1374	-0.0162	0.4962	0.2761	0.5550	-0.9174
	21.34	-0.01		-2.0192	-0.0062	0.0949	-0.0177	0.4901	0.2798		-0.6399
	27.40	-0.vl	3.3618	-2.5723	-0.0134	0.1006	-0.0147	0.4796	7085.0	0.1989	-0.7651
7 7	14.55	-0.01	3.3790	-2.4840	0.0076	0.0800	-0.0240	0.4790	0.2781		-0.7351
18 2	23.46	-0.01	3.6353	-2.4322	-0.0085	0.0969	-0.0149	0.4701	0.2852	0.1849	-0.6690
	24.55	-0.01	3.9220	-5.3510	0.0106	0.0570	-0.0199	0.4611	0.2927		-0.5910
	25.58	-0.01	4.2323	-7-1861	0.0189	0.0617	-0.0187		0.5821		-0.5165
		-0.0.	4.5626	-2-1211	0.0643	-0.0138	-0.0074	0.4423	0.2853		-0.4649
	27.75 28.79	-0.01 -0.01	4.8879 5.7641	-5-1069	0.0677	0.0224	-0.0147 -0.0197		0.2868 0.2878	0-1504	-0.4310 -0.3914
		-0.01	5.5660	-1.9958	0.0943	-0.0945	-0.0164	0.4289	0.2911		-0.3566
	30.91	-0.01	5.7255	-1.0342		-0.0663	-0.0204		0.2949		-0.3212
		-0.01	7.9706		-0.0+04	0.1655	-0.0191		495.0		-0.9056
	12.0A	0.00			-0.0123	9.0238	-0.0025		0.2708		-1.5095
28	10.07	-0.00	1.2506		-0.0079	0.0190	-0.0049		0.2605		-1.6347
29 -	-0.00	-0.00	-0.0116	0.02-4	-G.0195	0.0568	-0.0051	0.4963	0.2295		-2-1036

ENT "	1	74 1.		PH1	CONF		DELS	DEL3 DEL4			
INT '		***	20 2.3	0.0 t	94=0F23 (	0.0	0	0 0	UNKNOWN	i	
	AL PHA	BETÄ	CN	CLM	CA .	CLN -	CLI	CA	CAR	CAF	XCP
_	0.01	0.00	-0.0255	n.1140			-0.0042	0.4982	0.1962	0.3019	
5	0.00	0.00	-0-0240	0-1166	-0.0072	0.0023	-0.0057	3.4977	7.1855	0.3122	-3.9399
3	2.04	0.00	0.2105	-0-5850	-0.0054	-0.0089	-0.0058	0,4944	0.1817	0.3127	-1.3399
<u>.</u>	4.05	0.00	0.4475	-0.6697	-0.0023	-0.0165		0.4895	0.1824	0.3072	-1.4965
	10.09	0.00	1.2073	-1.6916	0.0127	-0.0331	-0.0072	0.5134	0.1960		1.4011
	12.14	0.00 0.00	1.8007	-1.9196	0.0127 0.0115	-0.0373 -0.0412	-0.0066 -0.0078	0.5121	0.1990 0.2070	0.3131	-1.2882 -1.1635
	16.20	0.00	2.1311	-2.2764	0.0054	-0.0209	-0.0089	0.5153	0.2134	0.3083	-1.0447
	17.23	-0.00	7.3149	-2.2346	0.0057		-0.0097	0.5101	0.2150	0.2951	-0.9653
	16.20	-0.00	2.5104	-2-1616	-0.0094	0.0328	-0.0148	0.5044	0.2198	0.2846	-0.8678
3	19.33	-0.00	2.7594	-2-1224	-0.0168	0.0634	-0.0145	0.5022	0.2251	0.2771	-0.7693
	20.43	-0.01	3.0141	-2.042+	-0.0044	0.0626	-0.0160		0.5540	0.2687	-0.6765
	21.48	-0.01	3.2935	-1.4437	-0.0027	0.0633	-0.0176		0.2305	0.2647	-0,5902
	22.51	-0.G1	3.5440	-1.0324	0.0019		-0.0176		0.2329	0.2531	-0.5163
	23,58	-0.01 -0.01	3.817v	-1.7245	0.0153		-0.0178	• • • • • •	0.2377	0.2388	-0.4517
	25.70	-0.01	4.4201	-1.5067	0.0370 0.0508	0.0234 0.00#9	-0.0155 -0.0130		0.2400 0.2430	0.2798	-0.3884 -0.3409
	27.85	-6.01	5.0678	-1.4325	0.1067		-0.0068		0.2569	0.1999	-0.2027
-	29.90	-0.01	5.3674	-1.3973	0.1193		-0.0087		0.2609	0.1914	-0.2603
	29.95	-0.G1	5.6590	-1.4214	0.1843		-0.0034		0.2561	0.1868	-0.2513
4	31.02	-0.00	6.0264	-1 9 9 4	0-1404		0.0004		0.2715	0-1784	-0.2488
	20.39	-0.ûu	3,0106	-1.9944			-0.0133		0.2605	0.2405	-0.6626
	26.77	-0.01	4.7501	-1.4426			-0.0067		0.2445		-0.3030
	8.07	0.00	1.2116	-1.6915	0.0067		-0.0031		0.2320	0.2033	-1.3961
8	6.73	0.00	0.9409	-1.0557			-0.0023		0.2105	0.3012	-1.4825 -1.5244
0	0.00	0.00		0-1117		0.0011			0.1970		-3.1355
								· • • • • • • • • • • • • • • • • •	- 27-27-0		
					•						
								- <del></del> -	<del></del> -		

	TEST		ACH RELO-		CONF			DEL3 DEL4		>N		
	1	77 1.	30 5.3	0.0 8	440123 0	•0	0	0 0	UNKNOWN		_	
OINT	ALPHA	HETA	CN	CLM	CY	CLN	CLL T	ČÀ	CAB	CAF	TCP	
1	0.00	0.00	-0.0322	0.1242	0.0025	-0.0180	-0.0029	0.4760	0.1843	0.2917	-3.8554	
Ş	2.02	0.00	0.1855	-0.1630	-0.0069	-0.0102	-0.0031	0.4743	0.1943	0.2900	-0.8790	
3	4.04	-0.00	0.4077	-0.460H	0.0024	0.0005	-0.0010	0.4736	0.1A39	0.2898	-1.1302	•
4	6.08	0.00	0.6327	-0.7557	-0.0010	-0.0051	-0.0022	0.4766	0.1821	0.2944	-1.1953	
5	8.08	0.00	0.AR6.	-1.050/	0.0035	-0.0168	-0.0029	0.4951	0.1859		-1.1854	
6	10.13	-0.0u	1.1545	-1.3241	0.0073	-0.0155	-0.0048	0.4981	0.1900	0.3081	-1.1420	·
8	12.15	0.00	1.4561	-1.5210	0.0094	-0.0251	-0.0045	0-5047	0.2047	0.3000	-1.0431	
9	14.22	-0.00	1.7732	-1.6477	0.0135	-0.0275	-0.00	0.5060	0.2068	0.2991	-0.9293	
10	16.27	-0.00	2.1296	-1.7716	0.0046	0.0016	-0.0030	0.5056	0.2135	0.2921	-0.8084	
11	17.31	-0.00	2.3509	-1.7352	-0.0043	0.0301	-0.0039	0.5032	0.2178	0.2855	-0.7350	
12	16.35	-0.00	7.6125	-1.7293	0.0620	0.0300	-0.0005	0.5006	0.2707	0.2799	-0.6619	_
13	19.41	-0.00	5.8623	-1.6912	0.0130	0.0150	-0.0079	0.4987	0.2243	0.2744	-0.5909	
14	20.46	-0.01	3.1044	-1.6324	0.0555	0.0144	-0.0065	0.4936	0.2275	0.2661	-0.5259	
15	21.56	-0.01	3.3724	-1.5360	0.0209	0.0196	-0.0067	0.4893	8622.0	0.2595	-0.4557	
16	27.58	-0.01	3.6661	-1.4495	0.0276	0.0154	-0.0055	0.4869	0.2322	0.2546	-0.3954	
17	23.65	-0.61	3.9469	-1.3943	0.0265	0.0268	-0.0070	0.4831	0.2364	0.2466	+0.3533	
18	24.73	-0.01	4.2530	-1.3402	0.0343	0.0093	-0.0048	0.4836	0.2409	0.2426	-0.3151	
19	25.80	-0.01	4.5677	-1.2440	0.0470	-0.0004	-0.0035	0.4823	0.2446	0.2377	-0.2834	
50	26.A7	-0.01	4.9264	-1.3405	0.0640	-0.0232	-0.0011	0.4605	0.2508	0.2297	-0.2721	
51	26.87	-0.01	4.9351	-1.3425	0.0611	-0.0256	0.0002	0.4776	0.2550	9555.0	-0.2720	
22	27.92	-0.01	5.2697	-1.4023	0.0742		-0.0026	0.4782	0.2583	0.2198	-0.2661	
23	28.97	-0.01	5,6073	-1.4640	0.0747	-0.0289	-0.0093	0.4807	0.2602	0.2205	-0.2611	
24	30.05	-0.01	5.9625	-1.5413	0.0771	-0.0541	-0.0101	0.4844	0.2644	0.2200	-0.2545	
25		-0.01	6.2799	-1.6462	0.0837	_	-0.0127	0.4837	0.2700	0.2137	-0.2621	
56		-0.00	3.1350	-1.5654	0.0261		-0-0017	0.4944	0.2540		-0.4994	
		0.00		-1-2970		-0.0211		0.5038	0.2351		-1-1247	
27		0.00	-0.0357	0.1314	-0.0053	-0.0157	0.0026	0.4772	0.2079	0.2693	-3,6828	

NT AL	l Pm≜ .03 •	85 0.	ACH RX10-6 Bu 2.3	0.0	CONF	L DEL	) DEL2	DEL3 DEL4				
2	.03 -						0 0	0 0	NWK MOM			
6			CN	" CLM "	CY	CLN	" CLL	CÃ	CAB	CAF	KCP	<del></del>
6	-05	-0.00			-0.0030	0.0054	-0.0136	0.7447	0.1021		-1,1278	
		-0.00	0.3932	-0.5133	-0.0046	0.0170	-0.0156	0.7443	0-1054		-1.3054	
A	.01 -	-r.00	0.5402	-0.8001		-0.0002.	-0.0197	0.2504	0.1090	0.1414	-1.3555	
		-0.0u	0.797#	-1.0370	0.0047		-0.0184	0.2701	0.1252	0.1446	-1.2996	
		-0.00		-1-1437		0.0616	-0.0021	0.2874	0.1412		-1.1756	
		-0.00.		-1.2079	-0.0134	0.0495	-0.0068	0.3037	0.1467		-1.0235	
		-0.00		-1.2426	-0.0229	0.0443	-0.0079		0.1741		-0,9091	
		-0-00	1.6176	-1-3211	-0.0255	0.0643	-0.0106	0.3176	0.2077	0.1099	-0.8167	
		-0.00		-1-3350	-0.0243	0.0685	-0.0111	0.3179	0.2247		-0.7733	
		-0.0u		-1.3593		0.0622	-0.0135		0.2375		-0.7314	
_		-0.00		-1.3484	-0.0052	0.0537 0.0522	-0.0143 -0.0096	0.3251	0.2547	0.0705	-0.6745	<del></del>
		-0.06 -0.01		-1.3094	-0.0027 0.0135	0.0485	-0.0031	0.3313 0.3403	0.2921	0.0392	-0.6179	
		-0.01	2.3562	-1.1025	-0.0177		0.0058		0.3132	0.0396	-0.4679	
		-0.01		-1.0322	-0.0046		0.0066		0.3205	0.0432	-0.4134	
	-	-0.01		-1.0214	0.0142		0.0053		0.3203	0.0299	-0.3047	
		-0.01		-1.0415	0.0370		0.0059		0.3508	0.0159	-0.3699	
		-0.01		-1.0633	0.0425		0.0012		0.3614	0.0047		<del></del> -
		-0.00	3.1959	-1.1296	0.0729		-0.0004		0.3708	-0.0127	-0.3534	
	3.45	0.00	3.3003	-1.1931	0.1453		0.0127		0.3675	-0.0162		
28	3,44	0.00	3.3677	-1-1972	0.1927	-0.3885	0.0129	0.3477	0.3941	-0.0504	-0.3525	
29	8.0	-0.01	3.5800	-1.3171	-0.0140	0.0522	-0.0278	0.3399	0.3994	-0.0595	-0.3674	
30	.48	0.00	3.7655	-1.3672	0.1131	-0.2525	-0-0042	0.3294	0.3956	-0.0663	-0.3631	
	•5•	-0.00	2.1037	-1.2913	-0.0028	0.0458	-0.0006	0.3283	0.3333	-0.0050	-0.6138	
	0.05			-1-1420			0.0046		0-1979	0.0870	-1.1737	
-0	0.00	0.00	0.0076	-0.0288	-0.0087	0.0041	-0.0005	0.2383	0.1061	0.1321	-3.7750	

	1		CH RX10-		CONF 4m0F21 0	.0 DEL	0 0	0 0	UMKMOMI THAMSIT!	N		· · ·
01NT	ALPHĀ"		CN	CLM	. CY		CLL	CA	CAB		XCP	
-	2.02	0.00		-0.0376	-0.0066	0.0056	-0.0027	0.2408	0.0990		-14,6327 -1,1853	
3	4.01	0.06	0.3821	-0.5167		0.0076	-0.0080	0.2402	0.1025		-1,3523	
•	6.03	0.00	0.5856	-0.7958		-0.0170	-0.0087	0.2531	0.1041		-1.3589	
5	8.06	0.00		-1.0213	0.0022	-0.0165	-0.0074	0.2756	0.1799		-1.2985	_
6	10.07	-0.00		-1.1789	-0.0147	0.0396	0.0064	0.2896	0.1495	0.1401		<del></del>
7	12.10	-0.00		-1.2804	-0.0163	0.0419	0.0021	0.3058	0.1588		-1.0744	
8	14.11	0.00	1.4075	-1.3472	-0.0214	0.0355	0.0010	0.3145	0.1782		-0.9572	
9	16.16	0.00	1.6449	-1-4101	-0-0203	0.0370	-0.0053	0.3254	0.2133	0-1121	-0.6572	
0	17.18	-0.00	1.7687	-1-4404	-0.0152	0.0397	-0.0040	0.3281	0.2298	0.0983	-0.6146	
1	18.20	-0.00	1.9136	-1.4588	-0.0100	0.0365	-0-0095	0.3344	0.2514	0.0830	-0.7626	
5	19.22	-0.00	2.0262	-1.4414	-0.0028	0.0363	-0.0036	0.3360	0.2704	0.0657	-0.7114	
3	20.23	-0.00	2.1478	-1.3525	0.0069	-0.0136	-0.0005	0.3493	0.2869	0.0624	-0.6297	
•	21.27	-0.01	2.2709	-1.2297	0.0120	0.0725	0.0020	0.3642	0.2940	0.0702	-0.5415	
5	55.30	-0.01	2.4064		-0.031-	0.1456	0.0123		0.3251		-0.4642	
6	23.36	-0.01	2.5547			0.1224	0.0108		0.3366		-0.4202	
7	24.37	-0.01	2.7251	-1-0917	0.0104	0.0711	0.0113		0.3457		-0.3969	
8	25.38	-0.01		-1-091>	0.0253	0.0354	0.0119		0.3729		-0.3767	
9	27.43	-0.00	3.0882	-1.1243	0.0596	-0.0366	0.0123		0.3756	-0.0002		
				-1.2130	0.1461	-0.2403	0.0174		0.3762	-0.0157	-0.3531	
?1 ?2	28.47	-0.00		-1.3085	-0.02+3		-0.0228		0.3762	-0.0163	-6-3246	
23		-0.00		-1.3990	-0.0440		-0.0309		0.4079		-0.3562	
-		-0.00		-1.3452	0.0101	-0.0111	0.0003		0.3526	-0.0044	-0.6266	
5		-0.00			-0.0136	0.0417	0.0134		0.2252	0.0661	-1.1994	
6	-0.30	0.00		-0.0396		0.0018	0.0065		0.1075	0.1312	8,4443	
									·			

30.72 -0.00

0.00

0.00

0.00

2.7347 -1.5081

2.2523 -1.3656

20,25

20.25

10.06

29 -0.00

27

26

2	CAF KCP 0.1591 0.6456 0.1501 -1.1195 0.1329 -1.3691 0.1439 -1.3515	CAE	0 CA 0.2466	CLL	CL4	84=0f21 0	0.0		PART		TET_
1 84 U.V. 2.3 0.0 8400F21 0.0 0 0 0 UNKNOWN  OINT ALPHA BETA Ch CLM CY CLM CLL CA CAB  1 -0.00 0.00 -0.0044 -0.0276 -0.0054 -0.0077 0.0060 0.2466 0.0875  2 7.01 0.00 0.1671 -0.1093 -0.0014 -0.0142 0.0027 0.7465 0.0984  3 4.02 0.00 0.3839 -0.5257 -0.0030 -0.0161 0.0003 0.2466 0.1159  4 6.06 0.00 0.5813 -0.7856 -0.0044 0.0116 0.0036 0.2679 0.1240  5 8.06 -0.00 0.4027 -1.0662 -0.0151 0.0566 0.0118 0.2948 0.1586  6 10.09 0.00 1.0012 -1.2244 0.0003 -0.0032 0.0007 0.3166 0.1620  7 12.10 0.00 1.7263 -1.3930 -0.0167 0.0375 0.0118 0.3249 0.1803  8 14.12 0.00 1.4654 -1.5425 -0.0266 0.0387 0.0075 0.3412 0.1955  9 16.16 0.00 1.7176 -1.6433 -0.0206 0.0294 -0.0002 0.3526 0.2368  10 17.19 0.00 1.4534 -1.6817 -0.0146 0.0243 -0.0041 0.3569 0.2690  11 18.19 -0.00 1.9706 -1.7058 -0.0168 0.0243 -0.0041 0.3569 0.2690  12 19.24 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103  13 20.28 -0.00 2.3816 -1.4094 0.0369 -0.1037 -0.0134 0.3910 0.3172  14 21.27 0.00 2.3816 -1.4094 0.0369 -0.1037 -0.0134 0.3910 0.3172  15 21.28 -0.00 2.3987 -1.4396 0.0362 -0.0310 0.0037 0.4003 0.3470  16 22.33 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.4128 0.3431  17 23.35 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.4137 0.3533  18 24.38 -0.01 2.6622 -1.2597 -0.0085 0.1256 0.0102 0.4155 0.3634	CAF KCP 0.1591 0.6456 0.1501 -1.1195 0.1329 -1.3691 0.1439 -1.3515	CAE	0 CA 0.2466	CLL	CL4	84=0f21 0	0.0			TEST	
OINT ALPHA BETA CN CLM CY CLM CLL CA CAB  1  -0.00	CAF KCP 0.1591 6.6456 0.1501 -1.1195 0.1329 -1.3691 0.1439 -1.3515	CAE 6 0.05	CA 0.2466	CLL	- CL4			1.45 5.3	84 (	1	
1 -0.00	0.1591 6.6456 0.1501 -1.1195 0.1329 -1.3691 0.1439 -1.3515	5 0.09	0.2466			CY				-	
2	0.1501 -1.1195 0.1329 -1.3691 0.1439 -1.3515	5 0.09		0.0060	-0 0077		CLM	CM .	HE TA	ALPHA	DINT
3	0.1329 -1.3691 0.1439 -1.3515		0.7485		-0.0077			-0.0044	0.00	-0.00	1
6.06 0.00 0.5813 -0.7856 -0.0064 0.0116 0.0036 0.2679 0.1240  5 8.06 -0.00 0.4027 -1.0462 -0.0151 0.0586 0.0118 0.2948 0.1586  6 10.09 0.00 1.0012 -1.2244 0.0003 -0.0032 0.0007 0.3166 0.1620  7 12.10 0.00 1.7263 -1.3930 -0.0167 0.0175 0.0118 0.3249 0.1803  8 14.12 0.00 1.4654 -1.5425 -0.0266 0.0367 0.0075 0.3412 0.1955  9 14.14 0.00 1.7178 -1.6433 -0.020f 0.0294 -0.0002 0.3526 0.2368  10 17.19 0.00 1.4534 -1.6419 -0.0146 0.0243 -0.0041 0.3569 0.2690  11 18.19 -0.00 1.9706 -1.7058 -0.0168 0.0263 -0.0041 0.3569 0.2690  12 19.24 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103  13 20.28 -0.00 7.2453 -1.5707 0.0157 -6.336 -0.0102 0.3723 0.3212  14 21.27 0.00 2.3816 -1.4694 0.0369 -0.1037 -0.0134 0.3910 0.3172  15 21.28 -0.00 2.3987 -1.4396 0.0362 -0.0310 0.0037 0.4003 0.3470  16 22.33 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.4128 0.3431  17 23.35 -0.01 2.6755 -1.2653 -0.0105 0.1256 0.0102 0.4155 0.3534	0.1439 -1.3515	6 0-11									2
5 8.06 -0.00 0.402 -1.0462 -0.0151 0.0586 0.0118 0.2948 0.1586 6 10.09 0.00 1.0012 -1.224 0.0003 -0.0032 0.0007 0.3166 0.1620 7 12.10 0.00 1.263 -1.3930 -6.0167 0.0375 0.0118 0.3249 0.1803   8 14.12 0.00 1.4654 -1.5425 -0.6256 0.0367 0.0075 0.3412 0.1955   9 16.16 0.00 1.7176 -1.6433 -0.0206 0.0294 -0.0002 0.3526 0.2368   10 17.19 0.00 1.4534 -1.6419 -0.0146 0.0243 -0.0041 0.3569 0.2660   11 16.19 -0.00 1.9706 -1.7058 -0.0169 0.0369 -0.0029 0.3605 0.2694   12 19.24 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103   13 20.28 -0.00 2.3816 -1.6494 0.0157 -0.0336 -0.0102 0.3723 0.3212   14 21.27 0.00 2.3816 -1.4694 0.0369 -0.1037 -0.0134 0.3910 0.3172   15 21.28 -0.00 2.3987 -1.4396 0.0362 -0.0310 0.0037 0.4003 0.3470   16 22.33 -0.01 2.5053 -1.2741 -0.0065 0.1191 0.0159 0.4137 0.3533   16 24.38 -0.01 2.6622 -1.2599 -0.0085 0.1256 0.0102 0.4155 0.3634											3
6 10.09 0.00 1.0012 -1.2244 0.0003 -0.0032 0.0007 0.3166 0.1620 12.10 0.00 1.2763 -1.3930 -6.0167 0.0175 0.0118 0.3249 0.1803											•
7 12.10 0.00 1.2263 -1.3930 -G.0167 0.0375 0.0118 0.3269 0.1803 8 14.12 0.00 1.4654 -1.5425 -0.6266 0.0367 0.0075 0.3412 0.1955 9 14.16 0.00 1.7178 -1.6433 -0.0206 0.0294 -0.0002 0.3526 0.2368 10 17.19 0.00 1.9534 -1.6414 -0.0146 0.0243 -0.0041 0.3569 0.2690 11 18.19 -0.00 1.9706 -1.7058 -0.0168 0.0369 -0.0029 0.3605 0.2694 12 19.24 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103 13 20.28 -0.00 2.2453 -1.5707 0.0152 -0.0336 -0.0102 0.3723 0.3212 14 21.27 0.00 2.3816 -1.4694 0.0369 -0.1037 +0.0134 0.3910 0.3172 15 21.28 -0.00 2.3987 -1.4396 0.0362 -0.0310 0.0037 0.4003 0.3470 16 22.33 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.4128 0.3431 17 23.35 -0.01 2.6622 -1.2599 -0.0085 0.1256 0.0102 0.4155 0.3634	0.1362 -1.3528										5
8 14-12 0.00 1.4654 -1.5426 -0.0266 0.0367 0.0075 0.3412 0.1955 9 16-16 0.00 1.7176 -1.6433 -0.020F 0.0294 -0.0002 0.3526 0.2348 10 17-19 0.00 1.4534 -1.6419 -0.0146 0.0243 -0.0041 0.3569 0.2690 11 16-19 -0.00 1.9706 -1.775H -0.0169 0.0369 -0.0029 0.3605 0.2694 12 19-24 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103 13 20.28 -0.00 2.1109 -1.6751 -0.0052 0.0266 -0.0004 0.3645 0.3103 13 20.28 -0.00 2.3416 -1.694 0.0369 -0.1037 -0.0134 0.3910 0.3172 14 21.27 0.00 2.3816 -1.694 0.0369 -0.1037 -0.0134 0.3910 0.3172 15 21.28 -0.00 2.3987 -1.6396 0.0362 -0.0310 0.0037 0.6003 0.3470 16 22.33 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.6128 0.3431 17 23.35 -0.01 2.6622 -1.2599 -0.0095 0.1256 0.0102 0.4155 0.3534	0.1545 -1.2229										6
9	0.1446 -1.1360										7
10	0.1457 -1.0528										8
11	0.1158 -0.9566								-	_	9
12	0.0879 -0.9075										
13	0.0712 -0.8656										
14	0.0542 -0.7935										
15	0.0511 -0.6995										
16 22.33 -0.01 2.5053 -1.2741 -0.0064 0.1067 0.0151 0.4128 0.3431 17 23.35 -0.01 2.6755 -1.2653 -0.0150 0.1191 0.0159 0.4137 0.3533 18 24.38 -0.01 2.8622 -1.2549 -0.0085 0.1256 0.0102 0.4155 0.3634	0.0737 -0.6170										
17 23.35 -0.01 2.6755 -1.2653 -0.0150 0.1191 0.0159 0.4137 0.3533 16 24.38 -0.01 2.8622 -1.2599 -0.0085 0.1256 0.0102 0.4155 0.3634	0.0533 -0.6002										
18 24.38 -0.01 2.8622 -1.2549 -0.0085 0.1256 0.0102 0.4155 0.3634	0.0697 -0.5086										
	0.0604 -0.4729										
	0.0522 -0.4402										_
	0.0366 -0.4154		0.4094	0.0043	0.1163					25.42	19
	0.0254 -0.3805								_		
	0.0040 -0.33 <del>62</del> -0.0040 -0.2699										

4.3945 -0.5863 -0.3968 0.7593 -0.0683

0.9944 -1.2110 -0.0031 -0.0040 0.0071

0.00 -0.0067 -0.0299 -0.0092 -0.0065 0.0124 0.2484

0.0117 -0.0400 -0.0037

0.0164 -0.0410 -0.0037

0.3615

0.3781

0.3790

0.3184

0.3509

0.4082 -0.0466 -0.1334

0.3742 0.0039 -0.7017

0.2669 0.0514 -1.2117

0.1432 0.1052 4.4702

0.0181 -0.7041

-2046 -0.2858 -04263 -0779 -06910 -1.1816 06809 -1.356 -00896 -1.3607 02809 -1.4421 05463 -1.6789 -08337 -1.6833 -09916 -1.9679 01368 -2.0056 03070 -2.0464 05087 -2.0540 06974 -1.9831 06964 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 0.	CV CLN -0043 0.0159 -0011 0.0078 -0000 0.0133 -0109 -0.0132 -0103 0.0734 -0053 0.0251 -0108 0.0490 -0061 0.0374 -0063 0.0414 -0133 0.0370 -0243 0.0271 -0243 0.0271 -0243 0.0111 -0049 -0.0149	-0.0103 -0.0136 -0.0077 -0.0087 -0.0059 0.0092 0.0092 0.0066 0.0056	0.3079 0. 0.3050 0. 0.3143 0. 0.3496 0. 0.3610 0. 0.3930 0. 0.4078 0. 0.4078 0. 0.4272 0. 0.4272 0. 0.4215 0. 0.4235 0. 0.4235 0.	1078 0.200 1309 0.174 1218 0.192 1478 0.201 1637 0.197 1876 0.205 2286 0.164 2704 0.137 2986 0.1186	6 -0.8870 9 -0.8188	
-2046 -0.2858 -04263 -0779 -06910 -1.1816 06809 -1.356 -00896 -1.3607 02809 -1.4421 05463 -1.6789 -08337 -1.6833 -09916 -1.9679 01368 -2.0056 03070 -2.0464 05087 -2.0540 06974 -1.9831 06964 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 06974 -1.9831 0.	-0011 0.0078 -000r 0.0133 -0109 -0.0132 -0103 0.0734 -0127 -0.0093 -0015 0.0074 -0053 0.0251 -0108 0.0490 -0063 0.0374 -0133 0.0370 -0243 0.0271 -0705 0.0303 -0243 0.0111	-0.0103 -0.0136 -0.0077 -0.0059 0.0092 0.0022 0.0046 0.0056 0.0056 0.0051 0.0053	0.3050 0. 0.3143 0. 0.3496 0. 0.3610 0. 0.3927 0. 0.4078 0. 0.4078 0. 0.4272 0. 0.4272 0. 0.4255 0. 0.4235 0.	1309 0.174 1218 0.192 1478 0.201 1637 0.197 1876 0.205 2286 0.164 2704 0.137 2986 0.118 3186 0.108 3346 0.096 3310 0.097	0 -1.3971 5 -1.5903 7 -1.7100 3 -1.5163 0 -1.2480 5 -1.1258 4 -1.0858 6 -1.0271 6 -0.9881 9 -0.8870 9 -0.8188	
-4263 -0.6779 -0.6910 -1.1816 0.6809 -1.3356 -0.6789 -0.356 0.6809 -1.3607 0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6833 -0.6	.000n 0.0133 .0109 -0.0132 .0103 0.0734 .0127 -0.0093 .0015 0.0074 .0053 0.0251 .0108 0.0490 .0061 0.0374 .0063 0.0414 .0133 0.0370 .0263 0.0271 .0263 0.0373	-0.0136 -0.0077 0.0087 -0.0059 0.0022 0.0022 0.0046 0.0051 0.0051 0.0051	0.3143 0.03496 0.03610 0.03927 0.03927 0.04078 0.4172 0.4272 0.4215 0.4235 0.4235 0.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.4216 2.42	121b 0.1921 1478 0.201 1637 0.197 1876 0.205 2286 0.164 2704 0.137 2986 0.118 3186 0.108 3246 0.091 3357 0.087	5 -1.5903 7 -1.7100 3 -1.5163 0 -1.2488 5 -1.1258 4 -1.0858 6 -1.0271 6 -0.9881 9 -0.9881 9 -0.8878	
.6910 -1.1016 06809 -1.3356 -00096 -1.3567 02609 -1.4421 05463 -1.6789 -08337 -1.68933 -09916 -1.9679 01368 -2.0056 05067 -2.0560 05067 -2.0560 05067 -1.9831 06016 -1.0159 06016 -1.6339 02936 -1.4483 0.	.0109 -0.0132 .0103 0.0734 .0127 -0.0093 .0015 0.0074 .0053 0.0251 .0108 0.0490 .0061 0.0374 .0063 0.0414 .0133 0.0370 .0243 0.0271 .0263 0.0211 .0298 0.0111	-0.0077 0.0087 -0.0059 0.0092 0.0022 0.0046 0.0056 0.0051 0.0051 0.0053 0.0060	0.3496 0. 0.3610 0. 0.3927 0. 0.3930 0. 0.4078 0. 0.4172 0. 0.4272 0. 0.4215 0. 0.4235 0. 0.4216 3.	1478	7 -1.7109 3 -1.5163 -1.2488 5 -1.1258 4 -1.0858 6 -1.0271 6 -0.9881 9 -0.9881 9 -0.8870 9 -0.8188	
.0896 -1.3607 0 .2609 -1.6421 0 .5663 -1.6789 -0 .8337 -1.6833 -0 .9916 -1.9679 0 .1366 -2.0056 0 .3070 -2.066 0 .5067 -2.0560 0 .6974 -1.9631 0 .8666 -1.0159 0 .6810 -1.6339 0 .2936 -1.6483 0	0.0127 -0.0093 0.0015 0.0074 0.0053 0.0251 0.0041 0.0063 0.0414 0.0063 0.0414 0.0133 0.0271 0.0243 0.0271 0.0243 0.0374 0.0243 0.0271 0.0243 0.0313 0.0244 0.0111	0.0087 -0.0059 0.0092 0.0022 0.0046 0.0056 0.0051 0.0051 0.0051	0.3610 0. 0.3927 0. 0.3930 0. 0.4078 0. 0.417? 0. 0.4272 0. 0.4215 0. 0.4235 0. 0.4235 0.	1637 0.197 1876 0.205 2286 0.164 2704 0.137 2986 0.118 3186 0.108 3246 0.096 3310 0.091 3357 0.087	3 -1.5163 0 -1.2488 5 -1.1258 4 -1.0858 6 -1.0271 6 -0.9881 9 -0.9386 6 -0.8870 9 -0.8188	
-2009 -1.6421 0.5663 -1.6789 -0.8337 -1.68333 -0.9916 -1.9679 0.3070 -2.0056 0.5087 -2.0560 0.5087 -2.0560 0.6974 -1.9831 0.8666 -1.0159 0.6810 -1.6339 0.5358 -1.6483 0.5358 -1.6703 0	0.0015 0.0074 0.0053 0.0251 0.0061 0.0490 0.0063 0.0414 0.0133 0.0270 0.0243 0.0271 0.0243 0.0373 0.0243 0.0373 0.0243 0.0373 0.0243 0.0373	0.0092 0.0022 0.0046 0.0051 0.0051 0.0051 0.0023	0.3930 0. 0.4078 0. 0.4172 0. 0.4272 0. 0.4215 0. 0.4226 0. 0.4235 0. 0.4216 3.	1876 0.205 2286 0.164 2704 0.137 2986 0.118 3186 0.108 3246 0.096 3310 0.091 3357 0.087	0 -1.2488 5 -1.1258 4 -1.0858 6 -1.0271 -0.9381 9 -0.9386 6 -0.8870 9 -0.8188	
-5463 -1.6789 -0.8337 -1.66933 -0.9916 -1.9679 0.3070 -2.0056 0.5067 -2.0560 0.5067 -2.0560 0.5067 -1.9631 0.8666 -1.0159 0.6610 -1.6339 0.5358 -1.6483 0.5358 -1.6703 0	0.0053	0.0022 0.0046 0.0056 0.0051 0.0051 0.0053	0.4078 0. 0.4172 0. 0.4272 0. 0.4215 0. 0.4226 0. 0.4235 0. 0.4216 0.	2704 0.137 2986 0.118 3186 0.108 3246 0.096 3310 0.091 3357 0.087	4 -1.0858 6 -1.0271 6 -0.9881 9 -0.9386 6 -0.8870 9 -0.8188	
.8337 -1.6933 -0.6979 0.1360 -2.0056 0.3070 -2.0560 0.5067 -2.0560 0.5067 -2.0560 0.6974 -1.9931 0.8666 -1.0159 0.6810 -1.6339 0.2936 -1.4843 0.5350 -1.2703 0	0.0108 0.0490 0.0061 0.0374 0.0063 0.0414 0.0133 0.0370 0.0263 0.0271 0.0263 0.0313 0.0298 0.0111	0.0046 0.0056 0.0051 0.0044 0.0051 0.0023	0.4172 0. 0.4272 0. 0.4215 0. 0.4226 0. 0.4235 0. 0.4216 3.	2986 0.1186 3186 0.1086 3246 0.096 3310 0.0916 3357 0.087	6 -1.0271 6 -0.9881 9 -0.9386 6 -0.8870 9 -0.8188	
.9916 -1.9679 0 .1368 -2.0056 0 .3070 -2.0066 0 .5067 -2.0560 0 .6074 -1.9631 0 .6010 -1.6339 0 .2936 -1.4483 0 .5358 -1.2703 0	0.0061 0.0374 0.0063 0.0414 0.0133 0.0370 0.0263 0.0271 0.0705 0.0303 0.0298 0.0111 0.0449 -0.0154	0.0056 0.0051 0.0044 0.0051 0.0023	0.4272 0. 0.4215 0. 0.4226 0. 0.4235 0. 0.4216 0.	3186 0.1086 3246 0.0966 3310 0.0916 3357 0.087	6 -0.9881 9 -0.9386 6 -0.8878 9 -0.8188	
1350 -2.0056 0 3070 -2.0666 0 5087 -2.0560 0 6974 -1.9831 0 8666 -1.0159 0 6810 -1.6334 0 2936 -1.4483 0 5350 -1.2703 0	0.0063 0.0414 0.0133 0.0770 0.0243 0.0271 0.0705 0.0333 0.0244 0.0111 0.0449 -0.0154	0.0051 0.0044 0.0051 0.0023 0.0040	0.4215 0. 0.4226 0. 0.4235 0. 0.4216 0.	3246 0.096 3310 0.091 3357 0.087	9 -0.9386 6 -0.8870 9 -0.8188	
.3070 -2.0064 0 .5087 -2.0560 0 .6974 -1.9931 0 .8666 -1.0159 0 .6810 -1.6339 0 .2936 -1.6483 0 .5358 -1.2703 0	0.0133 0.0270 0.0243 0.0271 0.0205 0.0303 0.0298 0.0111 0.0449 -0.0154	0.0044 0.0051 0.0023 0.0040	0.4226 0. 0.4235 0. 0.4216 0.	3310 0.091 3357 0.087	6 -0.8870 9 -0.8188	
-5087 -2.0540 0 -6974 -1.9831 0 -8646 -1.0159 0 -0810 -1.6339 0 -2936 -1.4483 0 -5358 -1.2703 0	0.0243	0.0051 0.0023 0.0040	0.4235 0.	3357 0.087	9 -0.8186	
.6974 -1.9831 0 .8646 -1.0159 0 .0810 -1.6339 0 .2936 -1.4483 0 .5358 -1.2703 0	0.0705 0.0303 0.0298 0.0111 0.0449 -0.0154	0.0023	3-4216 3.			
.8646 -1.0159 0 .0810 -1.6339 0 .2936 -1.4483 0 .5398 -1.2703 0	0.029A 0.0111 0.0449 -0.0154	0.0040				
.0810 -1.6339 0 .2936 -1.4483 0 .5358 -1.2703 0	.0449 -0.0154			3821 0.032		
.2936 -1.4483 .0 .5358 -1.2703 0		0 0 0 0 0 0		3882 0.027		·
.5358 -1.2703 0		0.0051		3996 0.013		
	-0.0346	0.0127		3925 0.021		
.7549 -1.0240 Q	0.1080 -0.0779	0.0252		3796 0.036		
	0.1241 -0.0721	0.0266		3690 0.046		
.4155 -0.4345 0	0.1299 -0.1378	0.0271	0.4100 0.	3657 0.044	2 -0.0984	
	.2133 -0.2775	0.0502	0.410B 0.	3746 0.036	3 -0.0452	
	0.2175 -0.2587	0.0441			8 -0.0067	
-0072 0.0288 -0	0.0010 0.0182	0.0556	0.3229 0.	1475 0.175	4 -3.9937	
					<del></del>	
					·	

· E i ·	OF 1		·· <del>·</del>								
	TEST		MACH RX10-		CONF	L DELI	DELZ	DEL3 DEL4	TRANSITI	04	
DINT	ALPHA "			CLM	C4 .	CLN"	CLL	CA	CAB	CAF	XCP
_1	0.00	-0.00			-0.0202		-0.0094	0.4961	0.2738		-4,7484
S		-0.00		-0.3911	-0.019-	0.0744	-0.0108	0.4951	0.5161		-1.6697
3	2.02	-0.00		-0.3836	-0.0158		-0.0097	0.4959	0.2065		-1.6269
200	4.01 6.03	-0.00		-0.8040	-0.0108		-0.0156	0.4928	0.2149		-1.6925
7	A. 04	-0.00		-1.2041 -1.5489	-0.0094		-0.0130 -0.0119	0.5019 0.5158	0.1985 0.1997		-1.6855
7	10.08	-0.00			-0.0116		-0.0078	0.5169	0.2093		-1,4910
<u> </u>	12.04	-0.00			-0.0236		-0.0041	0.5104	0.2181	0.2928	-1.3503
9	14.13	-0.00			-0.0196	0.0843	-0.0071	0.5237	0.2311		-1.0623
10	16.22	-0.01		-1.7063	-0.0177	0.1132	-0.0068	0.5273	0.2591	0.2681	-0.8866
īī	17.21	-0.01		-1.78/6	-0.0117	0.1115	-0.0089	0.5267	0.2711	0.2556	-0.6513
12	19.25	-0.01	2.2947	-1.8777	0.0034	0.0456	-0.0113	0.5262	0.2814	0.2449	-0.8167
13	19.31	-0.01			0.0066	0.0950	-0.0137	0.5216	0.2483		-0.7631
14	20.36	-0.01	2.7450	-1.915.	0.0257	0.05+0	-0.0136	0.5173	0.248B	0.2285	-0.6978
15	21.39	-0.01	2.9660	-1.9000	0.0453	-0.00-9	-0.0047	0.5136	0.2922	0.2214	-0.6428
16	22.44	-0.61	3.2336	-1.7938	0.0366	0.0224	-0.0076	0.5064	0.2898	0.2165	-0.5547
17		-0.01		-1.6833	0.0578	-0.0090	-0.0020	0.5009	0.2887	0.2122	-0.4800
16	24.55	-0.01			0.0760	-0.0471	0.0050	0.4953	0.2905	0.2048	-0.4121
19	25.63	-0.01		-1.3867	0.0779	-0.0387	0.0000		0,2870		-0.3377
50	26.70	-0.01		-1-3515	0.0505	0.0111	-0.0092		0.2906	0.1900	
21	27.75	-0.01		-1.2996	0.0745				0.2971	0.1818	
55	24.63	-0.01		-1.2321	0.0987				0.2981		-0.2416
<u> 23</u> –	29.90	-0.01		-1.0982	0.0429		-0.0190		0.3036		-0.2057
24	30.95	-0.01	2.2464	-0.8837	0.1407	-0.1848	-0.0246	0.4757	0.3103	0.1654	-0.1593
		<del></del>		<del></del>			<del></del>				
	-										
										•	
								-			

	TEST 1	PART M	ACH RE10-	6 PH1 0.0 t	CONF	L DE	DEL2	DEL3 DEL4	TRANSITI UNKNOWN	ON		<del></del> -
DINT	ALPHA	BETA	- CN	CLM	CY -		- CLL	CA .	CAS		*CP	
1	0.01	-0.00	-0.0058				-0.0199		0.1976		-55.5856	
2	2.03	-0.00	0.2372	-0.3034	0.0016		-0.0712	0.5031	0.1796		-1.2702	
3	2.03	-0.00	0.2291 0.4543	-0.6038	0.0006		-0.0212		0.1929 0.176.		-1.1563 -1.3290	
5	6.94	-0.00	0-6943	-0.9413	0.0054				0.1489		-1.3678	
6	6.07		0.9315	-1.2267	0.0049				0.1808		-1.3166	·
7		-0.00		-1.4361	0.0065				0.1907		-1.2169	
8	12.14		1.4471	-1.5795	0.001		-0.0198		0.1954		-1.0915	
ē	14.17			-1.6604	0.0034				0.1988	0.3176		
		-0.01		-1.2874	0.0163				0.1993	0.3325		
i	17.29			-1.2659	0.0230		-0.0326		0.2081	0.3263		
2	18.35			-1.2545	0.0115				0.2178		-0.5326	
3	14.41	-0.01		-1 - 2583	0.0053		-0.0349		0.2239		-0.4794	
•	20.46	-0.01		-1-2314			-0.0321		D.2795		-0.4257	
•	21.51			-1-1695			-0.0309		0.2332		-0.3701	
6		-0.01	3.4361	-1.0954			-0.0296		0.2356		-0.3188	·- <del>-</del> -
7		-0.01	3.7124	-0.9966					0.2373	0.2701		
3		-0.01		-0.6941	•		-0.0272		0.2423		-0.2240	
<u> </u>		-0.01		-0.8539			-0.0261		0.2464		-0.1911	
0		-0.01		-0.789H			-0.0226		0.2529		-0.1700	
1		-0.01		-0.7772			-0.0188		0.2593		-0.1566	
2		-0.01 -0.01		-0.7687	9-1435	-0.1740	+0.0219	0.4900	0.2598		-0.1461	
3		-0.01		-0.8406				0.4874	0.2711	0.2814	-0-1338 -0-1420	
	31.00	-0.01	3.4101	-0.0400	0.2423	-0.4327	-0.0132	V01-	0.5/11	0.5103	-0-1468	
											•	
									<b></b>			
											<del></del>	
					_							

PAGE 1 OF 1

SHEET 1 OF 1

POINT ALPHA BETA

0.00

1.97

3.96

5.95

7.90

9.49

13-85

24.95

10

iı

12

13

14

15

16

17

18

19

22

23

TEST PART MACH RX10-6

-0.00

-0-00

-0-00

-0.01

-0-01

-0-01

-0-Ul

15.79 -0.01

15.45 -0.01

17.84 -0.01

17.84 -0.01

14.B3 -0.01

19.88 -0.02

20.90 -0.02

21.91 -0.02

22.97 -0.02

23.97 -0.02

26.00 -0.02

26.00 -0.03

27.01 -0.63

28.03 -0.03

-0.04

97 0.60 2.3

CN

0.5670

1-0940

	28.03	-0-04	7.5216	-15.6658	0.0165	0.5902	0.1489 0.1498	0.4511 0.4305	0.3321 0.3438	0.1190	-2.0757 -2.0828	 	
				-15.7393	0.1013	0.6543	0.1906	0.4807	0.3437	0.1370			
				-15-6593	0.1565	0.4244	0.1288	0.4112	0.3547			 	<del>.</del>
_										0.0564	-1.9992		
28	19.59	-0.01		-14.6135	0.0339	0.0859	-0.0546	0.4389	0.2185	0.2203	-2.4686	 	
29	19.59	-0.05		-14.8636	0.0353	0.1057	-0.0563	0.4405	0.2009	0.2395	-2.4729		
30	9.56	-0.00	3.2193	-9.1135	0.0239	-0.03%6	-0.0505	0.33R4	0.1002	0.2382	-2.8309		
31	-0.00	0.00	0.0624	-0.1830	0.0057	-0.0741	-0.0351	0.2648	0.0855	0.1792	-2.9310		
												 <u> </u>	<del></del>
	······································											 	

MARTIN MISSILE TAIL EFFECTS DATA

0

ĆLL

-0-0620

-0.0631

-0.0717

-0.0759

-0.0690

-0.0759

-0.0747

-0.0869

-0.0807

-0.0585

0.0031

0.0583

0.1046

0-1605

0.1652

0.1551

0.1456

0.0268

0

0.0747 -0.0628

0.0675 -0.0766

0-0403 -0-0639

0.0969 -0.0835

CLN

0-0731

0.0873

0-0849

0.073

0.0390

0.2540

0.0356

0.0300

0.0215

0.1364

0.1421

0.2590

0.4799

0.4182

0.6761

0.7157

0.6262

0.58**

. ....

DELI DELE DELE DELA TRANSITION

CA

0.7877

0.3049

0.3170

0.3417

0.3645

0-4199

0-4771

0.4879

0.4852

0.5131

0.4871

0.5053

0.4908

0.4825

0.4718

0.4958

0.5012

0.4890

0.5036

0.5001

0.4925

0.4664

O UNKNOWN

CAB

0.0870

0-0423

0.0856

0.0488

0.0957

0.1258

0.1201

0.1307

0.1375

0.1287

0.1769

0.1698

0.1826

0.1934

0.1919

0.2143

0.2320

0.2502

0.2680

0.2905

0.3114

0.3131

AERODYNAMIC WIND TUNNEL (4T)

CAF KCP

0.2007 -1.4153

0.2226 -2.6915

0.2314 -2.7893

0.2529 -2.7577

0.2888 -2.7564 0.3140 -2.7673

0.3571 -2.7271

0.3572 -2.6735

0.3478 -2.6324

0.3844 -2.5905

0.3102 -2.5927

0.3355 -2.5458

0.3072 -2.4866

0.2891 -2.4277

0.2799 -2.3637

0.2A15 -Z.3I32

0.2692 -2.2649

0.2389 -2.2228

0.2356 -2.1692

0.2095 -2.1683

0.1811 -2.1229

0.1533 -2.0763

 $\triangleright$ 

DC-TR-75-125

ARNOLD ENGINEERING DEVELOPMENT CENTER(ALDC) PROPULSION WIND TUNNEL FACILITY(PWT)

0.0 B4m0F35 0.0

CY

-0.0159

-0.0177

-0.0130

-0-0095

-0.0057

0-0015

0.0103

0.0173

0.0200

0.0349

0.0254

0.0219

0.0147

0.0021

-0.0476

-0.0028

-0.0538

-0.0690

0.0023

0.0601

-0.0445

PHI CONF

CL.

0-0245 -0.0347 -0.0191

-1.5260

-3-(515

1.7728 -4.688-

2.4494 -6.7514

3-1-15 -4-6936

4-5389 -12-3781

5.2344 -13.9+44

5.4348 -14.3068

5.4005 -14.5267

5.6559 -14.6643

5-8525 -14-8991

6.0549 -15.0560

6.3010 -15.2971

6-4075 -15-1456

6-6403 -15-3604

6.7647 -15.3216

6.9439 -15.4347

7.0832 -15.3650

7.1176 -15.433U

7.2902 -15.4767

7.4928 -15.5572

E 1	ENGINEER LOF 1 LOF 1		VELOPMENT	CENTERIA	EDC1 P			NEL FACILITY		^ER	DOYNAMIC #1MO TO	UNNEL (AT)
			ACH RX10-		CONF	L DELI		OEL3 DEL4				
	1	94 0.	85 2.3		4#0F35 0	.0 0	0	0 0	UNKNOWN			
INT	ALPHA	6F TA	CŃ	CLM	CA.	CLN	" CLL "	C4	CAB	CAF	XCP	
1	-0.00	0.00	0.0555	-0.1658	0.0055	-0.0253		0.2769	0.0493		-2,9876	
?	1.96	-0.00	0.6400	-1.726e	0.01.0		-0.0352	0.7896	0.0826	0.2069	-5.6985	
3 .	3.93	-0.00	1.2052	-3.4263	0.0155		-0.0379	0.3005	0.0894	0.2111	-2.0359	
•	5.93	-0.00	1.6756	-5.2876	0.0180		-0.0443	0.3199	0.0986	0.2213	-5.0195	
	5.43	-0.00	1-8751	-5.3243	0.0140		-0.0439	0.3188	0-0931	0.2758	-5-8363	
-	7.A7	-0.00	2.5665	-7.3440	0.0209	-0.0224	-0.0502	0.3454	0.1023	0.2431	-2.8615	-
7 B	7.87	-0-00	2.5744	-7.3772 -7.3567	0.0210		-0.0503	0.3421	0.1049	0.2332	-2.8651	
9	7.87 9.87	-0.00	2.5711	-9.3321	0.0210		-0.0500	0.3393	0.1102	0.2291	-2.8613	
0	11.65	-C.00		-11.2297	0.0263 0.031	-0.0347 -0.0627	-0.0494	0.3826	0.1133 0.1164	0.2693 0.3056	-2.8473	
i.	13.76	-0.00		-13.0746	0.0365	-0.0781	-0.0465	0.4297	0.1277	0.3020	-2.7963	
ż	15.90	-0.00		-14.3696	0.0414	-0.0714	-0.0517	0.4654	0.1384	0.3269	-2.7195	
3	16,81	-0.01		-14.4161	-0.0396	0.2672	0.0792	0.4635	0.1328	0.3306	-2,6490	
4	17.92	-0.01		-14.4175	0.0587	-0.0856	-0.0611	0.4788	0.1449	0.3339	-2.5836	
5_	18.82	-0.01		-14.6748	0.0609	-0.0759	-0.0566	0.4806	0.1663	0.3144	-2.5310	
6	19.87	-0.01		-14.6936	50+0.0	0.0511	-0.0446	0.4408	0.1721	0.2687	-2.4650	
7	20.47	-0.02		-14.7865	0.0181	0.1757	-0.0215	0.4259	0.1875	0.2384	-2.3988	
8	21.90	-0.02		-14.6369	0.0164	0.2320	0.0296	0.4461	0.2053	0.2408	-2.3463	<del>-</del>
9	86.55	-0.02	6.497R	-14.9119	-0.0164	0.4252	0.0854	0.4666	0.2306	0.2360	-2.2949	
0	23.97	-0.04		-14.9662	-0.0486	0.4735	0.1217	0.4788	0.2379	0.2409	-2.2434	
1	25.01	-0.0 <i>č</i>		-15-1192	-0.0083	0.4127	0.1357	0.4860	0.2639	0.2221	-2.1981	
2	25.01	-0.02		-15.0444	-0.0247		0.1373	0.4764	0.2716	0.2048	-2.1910	
3	25.99	. <b>-0.</b> 03		-15.0914	-0.0590		0.1830	0.4884	0.2840	0.2044	-2.1461	
•	27.05	-0.4		-15.1424	-0.0636		0.2234	0.4944	0.3080	0-1864	-2.1026	
5	28.07	-0.04		-15.2325	0.0087		0.2005	6.4777	0.3169	0-1607	-2.0524	
6	29.04	-0. ub		-15.3685	0.0443		0.7418	0.5038	0.3504	0.1534	-2.0039	
<u> </u>	30.13	-0.06		-15.4000	0.2100		0.3205		0.3715	0.1273	-1.9542	
9	19.88	-0.01		-14.4516 -9.423s	0.0079		-0.0376		0.2159	0.2015	-2.4485	
0	9.82	0.00		-0.2003	0.0093		-0.0420		0.1367	0.2044	-2.8638	
·	-0.00	0.00	.0.0103	-002003	0.009.3	-0.0200	-0.0232	0.2662	0.0908	0.1754	-2.8476	
					· <del>- · </del>							<del></del>
												··
						<del></del> - ·						

PAGE 1 OF 1

SHEET 1 OF 1

POINT ALPHA BETA

9 9.81 -0.01 3.7004 -9.1222 -0.0023 0.0561 -0.0883 0.8008 0.2263 0.4664 -2.8553 10 9.81 -0.01 3.1954 -9.1202 0.0053 -0.0506 0.0664 0.7100 0.2184 0.4669 -2.8553 11 11.87 -0.01 3.8008 -10.7203 0.0088 0.0702 -0.0446 0.7407 0.2192 0.5210 -2.7927 12 13.87 -0.01 4.4043 -11.9347 0.0101 0.0042 -0.0449 0.7516 0.2218 0.5298 -2.7908 13 15.84 -0.01 4.7078 -11.9433 0.0165 -0.0030 -0.0537 0.7218 0.2353 0.4800 -2.5369 14 16.86 -0.01 4.5015 -11.9507 0.0011 0.0504 -0.0605 0.4699 0.255 0.4402 -2.5369 15 17.91 -0.01 5.7276 -0.000 0.0094 0.0566 -0.0565 0.4695 0.2659 0.2750 0.2711 -2.3017 17 19.99 -0.00 5.4044 -12.4053 0.0120 0.0055 -0.0657 0.7791 0.2266 0.2711 -2.3017 17 19.99 -0.00 5.6044 -12.4053 0.0120 0.0055 -0.0657 0.7791 0.2266 0.5271 -2.3017 18 21.04 -0.02 5.8002 -12.0221 0.0236 0.0047 -0.0697 0.4029 0.5561 2.2422 19 27.06 -0.02 6.7143 -12.4186 0.0467 0.002 -0.0797 0.7025 0.2535 0.4400 -2.6028 20 23.08 -0.0 6.5111 -12.4485 0.0047 0.0029 -0.0792 0.6657 0.2595 0.4607 -1.9082 21 24.14 -0.02 6.8364 -13.1314 0.0093 -0.0299 -0.0792 0.6657 0.2595 0.4057 -1.9082 22 25.22 -0.02 7.1720 -13.7701 0.0559 0.0057 0.0657 0.2595 0.0557 1.9088 22 25.23 -0.02 7.17457 -13.0847 0.0957 -0.0979 -0.0792 0.6657 0.2595 0.4090 -2.6028 23 25.23 -0.02 7.1657 -13.0847 0.0957 -0.0979 -0.0792 0.6657 0.2595 0.490 -2.6028 24 26.29 -0.02 7.1750 -13.2986 0.1441 -0.1315 -0.0378 0.6888 0.3070 0.3778 -1.6893 25 27.35 -0.02 7.7953 -13.4383 0.1441 -0.1315 -0.0378 0.6888 0.3070 0.3778 -1.6893 26 28.43 -0.01 8.4085 -13.6691 0.1648 -0.0219 -0.0550 0.2595 0.2595 0.0055 -1.6893 27 29.40 -0.02 8.7627 -13.8088 0.0461 -0.0097 -0.0097 0.0550 0.2799 0.3099 -0.0788 -1.68311 28 20.00 -0.01 8.55395 -13.2808 0.0461 -0.0097 -0.0097 0.0550 0.2799 0.3099 -0.0788 -1.68311 29 20.00 -0.01 8.55395 -12.4089 0.0503 -0.0000 -0.0550 0.2999 0.3099 -0.0966 -2.8808 31 0.00 -0.00 0.0012 0.0012 -0.0129 -0.0128 0.0037 -0.0031 0.5998 0.2158 0.3809 10.8091
11 11.82 -0.01 3.840M -10.7203 0.00e8 0.0702 -0.0449 0.7407 0.2192 0.5218 -2.7928 12 13.82 -0.00 4.4043 -11.4347 0.0101 0.0042 -0.0449 0.7516 0.2218 0.5298 -2.7098 13 15.84 -0.01 4.7078 -11.4433 0.0185 -0.0030 -0.0537 0.7234 0.2353 0.4860 -2.5369 14 16.86 -0.01 4.9815 -11.4507 0.0019 0.0541 -0.0605 0.0899 0.2455 0.4444 -2.4481 15 17.91 -0.01 5.9491 -12.0660 0.0094 0.0756 -0.0565 0.4695 0.2419 0.4276 -2.3698 16 18.95 -0.01 5.3285 -12.2644 0.0017 0.1141 -0.0586 0.6736 0.2466 0.4271 -2.3017 17 19.99 -0.02 5.6044 -12.4483 0.0120 0.0995 -0.0657 0.7791 0.2468 0.5324 -2.2212 18 21.04 -0.02 5.65402 -12.4021 0.0236 0.0870 -0.0697 0.8109 0.2498 0.5510 -2.1429 19 27.06 -0.02 6.7143 -12.4166 0.0467 0.0402 -0.0779 0.7025 0.2535 0.4490 -2.0628 20 23.08 -0.02 6.5119 -17.4445 0.0216 0.0772 -0.0730 0.6652 0.2595 0.4057 -1.9878 21 2-014 -0.02 6.8364 -13.1314 0.0093 -0.0229 -0.0792 0.6467 0.2851 0.3816 -1.9206 22 25.22 -0.02 7.1720 -13.2701 0.0550 -0.0211 -0.0711 0.0307 0.28679 0.3428 -1.8503 23 25.73 -0.02 7.5451 -13.2464 0.1144 -0.0949 -0.0583 0.6700 0.3042 0.3658 -1.7568 25 27.35 -0.02 7.5501 -13.2264 0.1144 -0.0315 -0.0378 0.6888 0.3070 0.3778 -1.6894 27 29.46 -0.02 8.7627 -13.0006 0.0755 -0.0357 -0.0803 0.5841 0.3107 0.2733 -1.5818 28 30.51 -0.01 9.1018 -14.0142 0.1413 -0.2077 -0.0803 0.5841 0.3107 0.2733 -1.5818 29 20.00 -0.01 5.5395 -12.0949 0.0503 -0.01010 -0.0650 0.2939 0.3066 -2.8848
12 13.82 -0.00 4.6643 -11.9367 0.0101 0.0042 -0.0469 0.7516 0.2218 0.5298 -2.7698   13 15.64 -0.01 4.7076 -11.9433 0.0165 -0.0030 -0.0537 0.7234 0.2353 0.4660 -2.5369   14 16.86 -0.01 4.9815 -11.9507 0.0019 0.0541 -0.0605 0.6899 0.2455 0.444 -2.4481   15 17.91 -0.01 5.7916 -12.0660 0.0094 0.0756 -0.0565 0.6695 0.2419 0.4276 -2.3698   16 18.95 -0.01 5.7285 -17.2644 0.0017 0.1151 -0.01580 0.6736 0.2466 0.4271 -2.3017   17 19.99 -0.02 5.6044 -12.4483 0.0120 0.0055 -0.0657 0.7791 0.2468 0.5324 -2.2212   18 21.04 -0.02 5.6044 -12.4483 0.0120 0.0055 -0.0657 0.7791 0.2468 0.5324 -2.2212   18 21.04 -0.02 6.7143 -12.4186 0.0677 0.0002 -0.0797 0.7025 0.2535 0.4490 -2.0628   20 23.08 -0.02 6.5114 -12.9484 0.00772 -0.0797 0.7025 0.2535 0.4490 -2.0628   21 24.14 -0.02 6.8364 -13.1314 0.0093 -0.0249 -0.0792 0.6667 0.2651 0.3816 -1.9208   22 25.22 -0.02 7.1120 -13.2701 0.0590 -0.0211 -0.0711 0.6307 0.2879 0.3428 -1.6583   25.73 -0.02 7.9593 -13.4383 0.1441 -0.0999 -0.0583 0.6700 0.3042 0.3658 -1.7568   25 27.35 -0.02 7.9593 -13.4383 0.1441 -0.1315 -0.0378 0.6888 0.3070 0.3778 -1.6694   27 29.46 -0.02 6.7627 -13.6091 0.1648 -0.0909 -0.0583 0.5650 0.3111 0.2818 -1.6260   27 29.46 -0.02 6.7627 -13.6091 0.1648 -0.0357 -0.0803 0.5650 0.3111 0.2818 -1.6260   28 30.51 -0.01 9.1016 -14.0142 0.1413 -0.2017 -0.0438 0.6605 0.2639 0.3069 -0.0096 -2.1838   30 9.79 -0.01 3.1874 -9.1326 -0.0017 0.0017 -0.0438 0.6605 0.2639 0.3966 -2.8648
13
14 16.86 +0.01 4.9815 -11.9507 0.0019 0.0541 -0.0605 0.0899 0.2455 0.444 -2.4481 15 17.91 -0.01 5.7916 -12.0660 0.0094 0.0756 -0.0565 0.4695 0.2419 0.4276 -2.3698 16 18.95 -0.01 5.3285 -17.2644 0.017 0.1161 -0.0586 0.6736 0.2466 0.4271 -2.3017 17 19.99 -0.02 5.6044 -12.4483 0.0120 0.0955 -0.0657 0.7791 0.2468 0.5324 -2.2212 18 21.04 -0.02 5.6902 -12.4221 0.0736 0.0870 -0.0697 0.8109 0.2498 0.5610 -2.1429 19 27.06 -0.02 6.7143 -12.4186 0.0467 0.0402 -0.0797 0.7025 0.2535 0.4490 -2.0628 20 23.08 -0.02 6.5114 -12.4445 0.0218 0.0772 -0.0730 0.6652 0.2595 0.4057 -1.9678 21 24.14 -0.02 6.8364 -13.1314 0.0693 -0.0249 -0.0792 0.6467 0.2651 0.3816 -1.9208 22 25.22 -0.02 7.1720 -13.2701 0.0550 -0.0211 -0.0711 0.6307 0.2879 0.3428 -1.8503 23 25.73 -0.02 7.1457 -13.0847 0.0957 -0.0949 -0.0707 0.4339 0.3016 0.3324 -1.8311 24 26.29 -0.02 7.5501 -13.2464 0.1144 -0.0949 -0.0583 0.6700 0.3082 0.3658 -1.7568 25 27.35 -0.02 7.7553 -13.4383 0.1441 -0.1315 -0.0378 0.6888 0.3070 0.3778 -1.6894 26 28.43 -0.01 8.4065 -13.6591 0.1649 -0.2304 -0.0311 0.5928 0.3110 0.2818 -1.6260 27 29.46 -0.02 8.7627 -13.6068 0.0755 -0.0357 -0.0803 0.5841 0.3107 0.2733 -1.5818 28 30.51 -0.01 9.1018 -14.0142 0.1613 -0.0777 -0.0438 0.6605 0.2639 0.3966 -2.8848
15
16 18.95 -0.01 5.3285 -17.2664 0.0017 0.1161 -0.0586 0.6736 0.2666 0.4271 -2.3017 17 19.99 -0.02 5.6044 -12.4443 0.0120 0.0955 -0.0657 0.7791 0.2666 0.5324 -2.2212 18 21.04 -0.02 5.6902 -12.6221 0.0736 0.0870 -0.0697 0.8109 0.2498 0.5610 -2.1429 19 27.06 -0.02 6.7143 -12.4186 0.0667 0.0402 -0.0797 0.7025 0.2535 0.4490 -2.0628 20 23.08 -0.02 6.5119 -12.9445 0.0218 0.0772 -0.0730 0.6652 0.2595 0.4057 -1.9878 21 24.14 -0.02 6.8364 -13.1314 0.0693 -0.0229 -0.0792 0.6667 0.2651 0.3816 -1.9208 22 25.22 -0.02 7.1720 -13.2701 0.0590 -0.0211 -0.0711 0.6307 0.2879 0.3428 -1.8503 23 25.73 -0.02 7.1557 -13.0867 0.0957 -0.0969 -0.0707 0.6339 0.3016 0.3324 -1.8311 24 26.29 -0.02 7.5501 -13.2464 0.1144 -0.0909 -0.0583 0.6600 0.3042 0.3658 -1.7568 25 27.35 -0.02 7.9543 -13.4383 0.1441 -0.1315 -0.0378 0.6848 0.3070 0.3778 -1.6894 26 28.43 -0.91 8.4065 -13.6591 0.1649 -0.2384 -0.0311 0.5928 0.3110 0.2818 -1.6568 27 29.46 -0.02 8.7627 -13.6608 0.0755 -0.0357 -0.0803 0.5841 0.3107 0.2733 -1.5818 28 30.51 -0.01 9.1018 -14.0142 0.1413 -0.2707 -0.0438 0.6605 0.2639 0.3966 -2.8648 30 -2.000 -0.01 5.5395 -12.0969 0.0503 -0.1010 -0.0650 0.2639 0.3966 -2.8648
16
18
18 21.04 -0.02 5.8902 -12.6221 0.0736
20
20
22
22
26
24
26
26
28 30.51 -0.01 9.1018 -14.0142 0.1413 -0.2077 -0.0430 0.5650 0.3111 0.2539 -1.5397 29 20.00 -0.01 5.5395 -12.0969 0.0503 -0.1010 -0.0650 0.2993 0.3089 -0.0096 -2.1838 30 9.79 -0.01 3.1874 -9.1325 -0.0017 0.0401 -0.0438 0.6605 0.2639 0.3966 -2.8648
28
3C 9.79 -0.01 3.187H -9.132b -0.0017 0.0401 -0.0438 0.6605 0.2639 0.3966 -2.8648
30 9.79 -0.01 3.187H -9.132b -0.0017 0.0401 -0.0438 0.6605 0.2639 0.3966 -2.8648
31 0.00 -0.00 0.0012 0.0129 -0.0128 0.0304 -0.0327 0.5958 0.2158 0.3808 10.8001

MARTIN MISSILE TAIL EFFECTS DATA

UEL1 DEL2 DEL3 DEL4 TRANSITION ____

0.5749

0.5805

0.5750

0.5851

0.5842

0.5868

0.6075

--- CA

0 UNKNOWN

CAB

0.1430

0.1390

0.1750

0.1643

0.1714

C.1619

0.1572

CAF

0.4320 -9.6973

0.4415 -0.7846

0.4000 -0.2246

0.4208 -2.9314

0.4128 -2.9194

0.4249 -2.9204

0.4503 -2.9080

0.4699 -2.8885

ARNOLD ENGINEEPING DEVELOPMENT CENTER (AEDC) PROPULSION WIND TUNNEL FACILITY (PWT)

0.0 8440F35 0.0

0.0301 -0.0179

0.0024 -0.0301

CLM

**50.0- 5000.0- 8000.0

0.5718 -1.6762 -0.0267

1.1737 -3.4265 -0.0146

1.1819 -3.4516 -0.0211

1.8024 -5.2414 -0.0196

CY

7.85 -0.01 2.4318 -7.0243 -0.0118 0.0950 -0.0532 0.6394 0.1695

CLN

0.0437 -0.0446

0.1240 -0.0475

0.0534 -0.0481

0.1117 -0.0483

C.0753 -0.0498

0.0911 -0.0493

0.1156 -0.0537

CLL

TEST PART MACH RX10-6 PHI CONF

103 1-10 2-3

0.00 -0.00 -0.0031

-0.00 -0.01 -0.0036

0.00 -0.00

1.97 -0.01

3.90 -0.01

5.87 -0.01

3.90 -0.00

AERODYNAMIC WIND TUNNEL (4T)

		•				MARTIN M	ISSILE TA	IL EFFECTS	DATA		
	TEST 1	PART M 104 1.	ALH RX10- 20 2.3		CONF 4=0F35 0	L DEL	1 DEL2	DEL3 DEL4	TRANSITI	ION	
THIO	ALPHA .	6ETA	ĊN.	CLH	ÇY	CLN	CLL		CAB		KCP
1	0.01	0.00	-0.0319	0.1314	0.0185	-0.0A97		0.6016	0.1963		-4,1314
2	1.94 3.91	0.00 0.0u	0.5332	-1.505u -3.2766	0.0237	-0.1028 -0.1046	-0.0349	0.6109	0.1972	0.4106	-2.1962 -2.854 <b>2</b>
<b>A</b>	5.07	0.00	1.7695	-5.0647	0.0344	-0.1056	-0.0342	0.6212	0.1916	0.4296	-2.0651
5	7.87	0.00	2.4105	-6.4663	0.0354	-0.1023	÷0.0375	0.6449	0.1955	0.4495	-7.8484
6	9.83	0.00	3.0534	-8.5634	0.0406	-0.1083	-0.0399	0.6750	0.2011	0.4739	-2.8047
7	4.63	0.00		-8.5384	0.0424	-0.10-2	-0.0383	0.6658	0.1961	0.4697	-2,8047
8	11.78	0.00		-10.0295	0.0494	-0-1256	-0.0396	0.7118	0.1994	0.5124	-2.7397
9	13.80	0.00	4.2415	-11-2453	0.0403	-0.11-0	-0.0354	0.7307	0.1948	0.5359	-2.6513
	15.88	0.00		-11.5050	0.0362	-0.12-1	-0.0596	0.7154	0.2015	0.5139	-2.4620
11	16.69	-0.00		-11-5914	. 0.0373	-0.0909	-0.0311	0.6922	0.2052	0.4869	-2.3980
12	17.93	-0.00	_	-11.7352	0.0546	-0.1358	-0.0377	0.6830	0.2171	0.4659	-2.3111
13	19.00	-0.00		-11.873/	0.0446	-0.1152	-0.0411	0.6813	0.2733	0.4579	-2.2166
14 15	20.04	-0.00 -0.01		-12.0120	0.0471	-0.0780 -0.1185	-0.0-84	0.6691 0.6512	0.2753 0.2287	0.4438	-2.121 <b>8</b> -2.0383
16	22.10	-0.01		-12.3188	0.0592	-0.1151	-0.0546	0.6411	0.2327	0.4084	-1.9587
17	23.16	-0.41		-12.5171	0.0924	-0.1652	-0.0573	0.6271	0.2393	0.3878	-1-0052
18	24.21	-0.01		-12-6907	0.1061	-0.1916	-0.0583	0.6313	0.2466	0.3847	
19	25.28	-0.01	7.3035	-12.4384	0.0997	-0.1.23	-0.0545	0.6175	0.2528	0.3647	-1.7578
20	24.31	-0.01	7.6763	-13.C373	0.1536	-0.2456	-0.0548	0.6509	0.2585	0.3925	-1.6979
51	27.42	-0.01		-13.2482	0.1871	-0.3783	-0.0459	0.6372	0.2483		1.6373
55		-0.01		-13.4470	0.2036	-0.3472		0.6193	0.2936		-1.5900
_23		-0.01		-13.5844	0.1985		-0.0450	0.6185	0.2897		-1.5454
54	30.56	-0.00		-13.6066	0.2215		-0.0284	0.5741	0.2974		-1.5039
25	9.31	0.00		-8.5767	0.0605	-0.1434		0.5706	0.2879	0.2827	
27	0.01			0.1327		-0.1210		0.5420	0.2388	0.4032	-2.8167 -4.7288

Ð
ш
0
5
R.7
Ϋ́
25

AGE	enginee 1 of 1 1 of 1		velopment			MARTIN M	SSILE TO	NNEL FACILI' ALL EFFECTS	TY(PWT) DATA	AER	ODYNAMIC WI	ND TUNNEL (41)
	TEST		ACH RX10-		CONF 14=0F35 0		0 0	DEL3 DEL4	TRANSIT!			
POINT	ALPHA	SETA .	. CM	CLM	CY	CLN	CLL"	ČA	CAB	CAF	ACP.	
1	-0.00	0.00		-0.184#	0.0087	-0.0250			0.0666	0.2341	-2.8993	
5	5.00	0.00		-1.4285	0.0161	-0.0376	_		0.0744		-2.6560	
3 .	4.	-6.00	1.2621	-3.6715	0.0163	-0.0307	-0.0237		0.081-		-2.9091	
•	5.90	-0.00	. 1.9372	-5.0477	0.0163	-0.0247			0.6891		-2.9154	
5	7.82	-0.00	2.5717		0.0745	-0.0374	-0.0383		9-1056	0.5651	-2.9508	- ·- <u></u> -
6	7.82	-0.00		-7.9014	0.0235	-0.0306	-0.0392		0.0675		-2.9567	
	9.80	-0.00		-10.0164	0.0295	-0.0501	-0.0402		0.1026		-2,9457	
В	11.40	-0.00		-12-0006		-0.0409	-0.0362		0.1119		-2.9105	
9	13.76	-0.00		-13-2405	0.6383	-0.0996	-0.0380		0.1217		-2.0272	
10		-0.00		-13.4322			-0.0480		0.1251		-2.6805	
11	16.81	0.00		-13.47/1			0.0214		0.1294		-7-6056	
12	17.85	-0.00		-13.5902		0.1175	0.0902		0.1468		-2.5388	
13	19.87	-0.01		-13-6092		-0.11-9	-0.0207		0.1709		-2.4633	
_	20.92	-0.02		-13.7041	_	9-2441	-0.0089		0.1883	0.2681		
15 16	21.94	-0.02		-13.6387		0.4615	0.0098		0.2057 0.2240		-2.3422 <u>-</u>	
17	22.97	-0.03		-13.4035		0.4732	0.0694		0.2343		-5.5555	
18	23.94	-0.02		-14.0857		0.4207	0.1001		0.2595		-2.1715	
19	25.04	-0.03		-14.1582		0.5944	0.1027	_	0.2475		-2.1106	
20	26.00	-0.03		-14.2970		0.5408	0.1002		0.2850	0.2035		
21	27.10	-0.0+		-14.4148		0.5700	0.1414		0.2996	0.1512		•
55	28.15	-0.02		-14.5288		0.3455	0.1443	· ·	0.3044		-1.9199	
23	29.23	-0.01		-14.6028		0.1669	0.0946		0.3070		-1.8418	
- 24	29.22	-0.01		-14.6538					0.3210		-1.8515	
25	30.30	-0.01		-14.8423		0.0426	0.0377		0.3730		-1.7602	
26	19 90	-0.03			-0.0734	0.4959			0.2465		-2.3877	
27	9.80	-0.Qu		-10-1484			-0.0382		0.1364	0.2411		
78	-0.00	-0.00	0.0655	-0.1627	0.0087	-0.0171	-0.0202		0.0915		-2.7918	
29	-0.00	0.00	0.0633	-0.1758	0.0099	-0.0226	-0.0181	0.2934			-2.7778	

GE EET	ENGINEE 1 OF 1 1 OF 1	PING DE	/ŁLOP#EN1 		EOC) P	ROPULSION MARTIN M	WIND TUN	WEL FACILI'	TY (PUT) DATA	AER	ODYNAMIC = IND TUNNEL (4T)
	_		CH RE10-		CONF	L OEL	DELS	DEL3 DEL4	TRANSITI	ON	
	1	100 0.9	2.3	0.0	4=0F35 0	•0	•	0 0	UNKHOUR	•	
POINT	ALPHA -	BETA	- CN	CLM	CY	ČLN.	CLL	CA	CAB	CAF	ACP
1	-0.00	0.00	0.0613	-0-1774	0.0094	-0.0294	-0.0295	0.4100	0.6478	0.3422	-2,8967
2	-0.00	0.00	0.0515		0.0094	-0.0359	-0.0297	0.4167	G.0974	0.3194	-2.8944
3	1.95	0.00	0.6274	-1.8060	0.0221	-0.0537	-0.0321	0.4268	0.1090		-2.8727
•	3.91	-0.00	1.7514	-3.6288	0.0227	-0.0457	-0.0360	0.4251	0.1172		-2.8990
5	5.8#	-0.00	1.9159	_	0.0259	-0.0382	-0.0410	0.4545	0.1153		-5-6101
•	7.85	-0.00	5.6098		0.0251	-0.0362	-0.0432	0.4869	0.1280	0.3589	-2.9163
7	9.81	-0.00		-9.5206	0.0585	-0.0509	-0.0406	0.5240	0.1367	0.3873	-2.8984
	11.76	-0.00		-11.3789	0.0291	-0.0690	-0.0359	0.5612	0.1520	0.4092	-2.8592
		-0.00		-11-3717	0.0303	-6.0706	-0.0361	_0.5605	0-1515	0.4088	-2.8597
10	13.73			-12.7321	0.0341	-0.0554	-0.0367	0.5704	0.1594	0.4110	-2.7963
11	15.A3	-0.01		-12-433-	0.0309	-0.0769	-0.0402	0.5121	0.1694	0.3427	-2.6400
15	16.81	-0.01		-13-0056	U. 0446	-0.0471	-0.0537	0.5212	0.1863	0.3349	-2.5813
13	17.88	-0.01		-17-9719	0.0476	-0.0477	-0.054A	0.5072	0.1751	0.3321	-2.5731
15		-0.01		-13-1305	0.0517		-0.0604		0.1921	0.3634	-2.4972
16	19.93	-0.00		-13.2561	0.0517	-0.0757	0.0567		0.2014 0.2097		-2.4214 -2.3396
17	20.97			-13.4034	0.0927		0.0361	0.5045	0.2299	0.3745	-2.2781
15	22.04	-0.01		-13.4743	0.0538	0.0007	-0.0463		0.2349	0.3206	-2.1864
19	23.02	-0.00		-13.6193	0.0560	-0.0342	9620.0		0.2481	0.3149	-2.1204
50	24.08	-0.00		-13.7458	0.0769		0.0716		0.2599		
21	25.11	-0.01		-13.6804	6.0946	0.0105	0.1082		0.2740		-1.9809
25	26.14	-0.00		-14.0164	0.0999	0.0441	0.1692		0.2840		-1.9110
53	27.20	0.00		-14.1953		-0.1014	0.2453		0.2939		-1.8346
	28.29	-0.00	8.1460	-14.3988	0.1707	-0.0315	0.2238	0.4325	0.3040		-1.7672
25	29.35	0.00		-14.5552		-0.1826	0.0575		0.2984		-1.6894
56	30.44	0.01		-14.7945		-0.2051	0.1291	0.3943	S+0E.0	0.0901	-1.6317
27.	19.93			-13.0876		-0.1256	0.0574		0.2933		-2.3152
		-0.00	3.3161	-9.6544	0.0296	-0.0479	-0.0390		0.2036		-2.9096
58		0.00	0.0677	-0.1903	0.0127	-0.0304	-0.0246	0.4089	0.1036	0.3053	-2.8132

ARMOLD ENGINEERING DEVELOPMENT CENTER (AEDC) _ PROPULSION WIND TUNNEL FACILITY (PUT) AERODANAMIC WIND TUNNEL (4T) MARTIN MISSILE TAIL EFFECTS DATA PAGE 1 OF 1 SHEET 1 OF 1 DEL1 DELS DELS DELS THANSITION TEST PAPT MACH PRIO-6 PHI CONF L 105 1.30 2.3 0.0 B4#0f35 0.0 0 O UNKNOWN - CN POINT ALPHA BFTA CLM CY CL4 CLL CA CAB CAF ICP 0.01 0.00 -0.0507 0.2176 0.0030 -0.0530 -0.0211 0.5696 0-1949 0.3747 -4.2947 -0.U514 -0.0253 0.5754 0.1994 0.3761 -2.5631 1.98 0.00 0.4932 -102642 6-0045 3.44 0.00 1.0443 -2.8861 0.0127 -0.0511 -0.0283 0.5742 0.1968 0.3774 -2.7505 5.91 0.00 1.6358 -4.4845 0.0123 -0.0373 -0.0275 0.5888 0.3928 -2.7415 0.1960 7.85 -0.00 2.2488 -6.1831 0.0238 -0.0497 -0.0283 0.4151 -2.7495 0.60Bl 0.1929 2.8568 -7.7424 9.66 -0-90 0.0323 -0.0584 -0.0279 0.1958 0.4433 -2.7102 0.6391 11.6--0.00 3.4576 -9.1587 0.0366 -0.0779 -0.0292 0.4704 -2.6489 0.6667 0.1963 13.A5 6.00 4.0778 -10.4643 0.0352 -0.0986 -0.0261 0.6492 0.1979 0.5013 -2.5662 15.99 0.00 4.6060 -11.2233 0.0446 -0.1708 -0.0289 U-7029 0.2026 0.5003 -2.4367 16.92 -0-1196 -0-0187 10 0.00 4.8521 -11.3639 0.0431 0-6790 0-2097 154E.S- E984.0 17.96 5.1375 -11.5212 -0.1233 -0.0181 11 0.00 0.0419 0.6676 0.2157 0.4520 -2.2426 17.97 5.1219 -11.4271 0.0409 -0.1018 -0.0151 0.4267 -2.2318 12 0.00 0.6528 1955.0 5.4004 -11.5012 0.0535 -0.1469 -0.0256 19-02 0.00 0.6390 0.2345 0.4045 -7.1297 10 20.07 -0.00 5.7221 -11.7033 0.0455 -0.1162 -0.0269 0.4519 8-65-0 0.4171 -2.0453 15 20.07 -0.00 5.7198 -11.6362 0.0436 -0.1071 -0.0747 0.6093 0.2411 0.3682 -2.0344 21.12 -0.00 6.0704 -11.4230 -0.1196 -0.0340 0.3930 -1.9642 0.0561 0.6362 0.2432 21.12 -0.00 17 6.0526 -11.6280 0.0647 -0.1547 -0.0341 0.2517 0.3882 -1.9541 0.6399 0.3443 -1.8685 18 22-18 -0-01 6.3530 -11.4706 0.0615 -0.0968 -0.0313 0.6035 0.2592 22-16 -0-04 6.3691 -11.8948 0.0320 -0.0814 -0.0343 0.4222 0.2583 0.3640 -1.8676 20 23.23 -0.00 6.7010 -12.1005 0.0755 -G.1484 -0.03A2 0.6182 0.2581 0.3601 -1.8058 24.29 -0.01 7-0552 -12-307-0.0792 -0.1067 -0.0414 0.3738 -1.7444 21 0.6346 0.2607 25.33 -0.01 7.4131 -12.5212 0.1365 -0.2243 -0.0432 0.3494 -1.6891 0.6125 0.2631 25.34 -0.01 7.3932 -12.4385 0.0868 -0.1337 -0.0384 0.5866 0.2713 0.3153 -1.6824 20.42 -0.01 7.7487 -12.5376 0.11e3 -C.1880 -0.0315 0.3309 -1.6168 0.6123 0.2814 27.45 -0.01 8.1247 -17.6005 0.1405 -0.2460 -0.0196 0.6267 0.2815 n.3451 -1.5755 28.53 -0.00 540%-51- 2870BZ 0.1532 -0.3082 -0.0164 0.6014 0.3174 0.2841 -1.5107 0.1752 -0.3721 -0.0133 27 29.59 -0.00 8.8488 -13.025Y 0.6124 0.3189 0.2935 -1.4721 30.65 9.1985 -13.1926 0.1549 -0.2820 -0.0218 -0-44 0.6196 0.3239 0.2958 -1.4288 5.6941 -11.4762 0.0447 -0.1241 -0.0211 20.08 0.00 0.5711 0.3084 0.2627 -2.0155 30 9.85 2.8533 -7.7545 0.0267 -0.0600 -0.0262 -0.00 0.6072 0.2333 0.3739 -2.7177 0.01 0.00 -0.0450 0.1900 0.0003 -0.0382 -0.0169 0.5623 0.2056 0.3566 -4.2211

HEE <u>Y</u>	i of 1 1 of 1					MARTIN M	ISSILE TA	AIL EFFECTS	DATA		DDANVMÍC MÌND AÑWNÉT (4	
-	TEST	PART M	SCH RX10-		CONF 14#0F35 0		DEL2	DEL3 DEL4	TRANSITI UNKNOWN			
POINT	ALPHA	HETA "	CN	CLM	<u>C</u> ¥	CLN	. CLL	CA	CAB	CAF	xc•	
1	-0.00	0.90		-0.0200		0.0002	0.0082	0.2743	0.0844		-6.5143	
3	1.97	0.00	0.5512		-0-0025	-0.00m0	0.0053	0.2871	0.0970	0.2002	-2.8296	
•	3.95	0.00	1.1537		0.0025	-0.0090	0.0027	0.2927	0.0930	0.1997	-2.8335	
3	5.91 7.88	-0.00 -0.00		-5.1092 -7.1446	0.0023	-0.0005 -0.0064	-0.0035	0.3098	0.0929	0.2170	-2.8479	
- 5	9.84	0.00		-9.1646	0.005	-0.0055	-0.0035	0.3257 0.3478	0.1032		-2.8643	<del></del>
	11.91	0.00		-11-1485	G.013m	-0.0455	0.0024	0.3807	0-1144	0.2663	-2.8334	
9	13.79	0.00		-17-4645	0.0113	-0.0642	0.0116	0.4101	0.1227	0.2874	-2.7961	
10	15.79	0.00		-14.2520	0.00+A	-0.0eul	0.0170	0.4253	0.1273	0.2979	-2.7270	
11	16.81	0.00		-14.4023	0.0139	-0.0782	0.0200	0.3969	0.1297	0.2672	-2,6584	
12	17.83	0.00		-14.4481	0.0311	-0.1268	-0.0093		0.1411	0.3139	-2.5929	
13	18.85	0.00		-14.5941	0.0254	-0.1109	0.0029		0.1567	0.2783	-2.5353	
14	18.8e	0.00		-14-4743	0.0326	-0.1311	0.0009	0.4305	0.1580	0.2725	-2.5207	
15	19.80	0.00		-14.6162		-0.0744	0.0098		0.1767	0.2146	-2.4670	
16	20.90	-0:00		-14-6778	0.0318	-0.0313	0.0047		0-1844	0.2120	-2.4052	
17	21.93	-0.01		-14.7653	0.067-	-0.0827	0.0253		0.1971	0.1620	-2.3447	
16	22.95	-0.01		-14.6387	0.0226	0.1235	0.0582		0.2144		-2.2944	
•	23.97	-0.01		-15-0339	0.0431	0.1611	0.1034	0.4190	0.2370 0.2330		-2.2409	
51	23.97	-0.01		-14.0137	-0.0194	0.1326	0.1522		0.2708		-2,233 <u>1</u> -2,1863	
55	59.05	-0.02		-15.0002	0.0050	0.5496	0.1966		0.2885		-2.1453	
- 23	27.05	-0.02		-15.1269		0.5580	0.1858		0.3068		-2.0916	
24	29.08	-u.03		-15.1616	0.0544	0.5793	0.1727		0.3127		-2.0405	
25	29.10	-0.04		-15.2567	0.1346	0.5238	0.2056		0.3280		-1.9923	
26	30.13	-0.04		-15.3575	0.2300	0.5838	0.3351	0.4326	0.3438	100 100 100 100 100 100 100 100 100 100	-1.9559	
27	19.59	-0.00		-14.4406		0.0437	0.0412		0.2596		-2.4496	
26	9.83	0.00	3.2659	-9.3970	0.0464	-0.1312	0.0099	0.3329	0.1464	0.1865	-2.6773	
	-0.00	0.00	0.0413	-0.1383	0.0160	-0.0807	0.0234	0.2703	0.0981		-3.3469	

HEET 1	OF 1	•	<u></u>	CENTEH (		PROPULSION N ITRAM	WIND TUN ISSILE TA	NEL FACILI IL EFFECTS	TY(PWT) OATA		TO THE WIND TUNNEL (41)
•	TE51	PART MA			CONF B4m0F34 (	L DEL	0 0 1 DELS	DEL3 DEL4	TRANSITI		
OINT A	ALPHA -	BETA -	CN	CLM .	CY	CLN	CLL	CĀ -	CAB	CAF	XCP
	-0.00	-0.01		-0.0518		0.1949	-0.0738	0.2906	0.0890	0.2017	-2.4336
2	1.96	-0.01	0.5834			0.1644	-0-0730	0.3206	0.0487	0.2319	-2.7371
. 3	3.95	-0.01	1.2010			0.1745	-0.0819	0.3539	0.0877	0.5445	-2.7072
•	5.91	-0.01	1.9173			0-1661	-0.0916	0.3837	0.0995	2.65.0	-2.005
5	7.56	-0.01	2.5977			0.1265	-0.0946	0.3A68	0.1008	0.2840	-5.9310
6	54.6	-0.01		-9.5972		0.1322	-0.0860	0.4086	0.1042	0.3043	-2.9426
	11.42	-0.01		-10.3886		0.1251	-0.0A73	0.4465	0.1217	0.3268	-2.9045
	13.82	-0.01		-11.0277		0.1219	-0.0806	0.4637	0.1370	0.3267	-2.8086
	15.83	-0.00		-11.5489		0.0902	-0.0693	0.4908	0.1619	0.3789	-2.6029
	16.87	-0.01		-11.3251		0.1357	-0.0356	0.5127	0.1969	0.3158	-2.6179
	17.99	-0.01		-11090		0.1901	-0.0526	0.5448	0.2393	0.3055	-2.5493
	14.91 19.92	-0.01 -0.01		-11.4500 -11.4535		0.2745	-0.0603	0.5833 0.6174	0.2640	0.3193	-2.4897 -2.4255
	20.94	-0.01		-11.4363			-0.1032	0.6538	0.3375	0.3163	-2.3652
	21.96	-0.01		-11.67/6			-0.1141	0.6839	0.3636	0.3703	-2.3032
	22.97	-0.02		-11.6435		0.1780	-0.1106	0.6896	0.4214	0.2682	-2.2642
_	22.97	-0.01		-11.9374			-0.1272	0.6916	0.4245	0.2671	-5-5615
	23.99	-0.03		-12.3296			-0.1365	0.7100	0.4340	0.2760	-2-2313
	24.99	-0.03		-12.6469			-0.1530	0.7110	0.4582	0.2528	-2-2122
	26.00	-0.04		-13.3756			-0.1796	0.7135	0.4746	0.2340	-2.1908
55 5	27.00	-0.04	6.3618	-13.9015	0.0347	0.3025	-0.2043	0.7072	0.4889	0.2183	-2.1783
23 3	28.01	-0.06	6.7414	-14.5330	0.0791	0.4488	-0.2205	0.6965	0.4909	0.2076	-2.1558
24	29.03	-0.07	6.9504	-14.7707	0.1530	0.4034	-0.2398	0.6729	0.4953	0.1776	-2.1227
25 .	30.05	-0.06	7.1703	-14.4013	0.132-	0.4115	-0.2186	0.6550	0.5926	0.1523	-2.0782
		-0.01		-11.6361		0.2736	-0.0601	0.5827	0-4159	0.1668	-2.4373
27	9.02			-9.9003					0.2278		-2.9750
28	-0.01	-0.01	_ 0 • ō • ≥ 3	-0.2045	0.0532	0.1904	-0-0655	0.2328	0.1062	0.1266	-4.6202

	TEST	PART M	ACH RX10-	-6 PHI	CONF	L DEL	DELS	DEL3 DEL4	TRANSIT	I DN	
	1	112 0.	65 2.3			Tall.	0		UNKNOW	•	
POINT"	ALPHA	RETA	CN	CF.4	CY .	CLN	CLL	CA	CAB	CAF	ACP
<u>1</u>	-0.01	-0.01	0.0336	-0.1621	-0.0576	0.1975	-0.0704	0.2413	2880.0	0.1531	-4,8228
5	1.97	-0.01	0.6258	-1-5007	-0.0479	0.1634	-0.0701	0.2383	0.0886	0.1498	-2.8914
3 .	3.93	-0.01	1.1074	-3.3197	-0.0046	0.1620	-0.0738	0-2377	0.0880	0.1496	-2.9966_
•	5.88	-0.01	2.0016	-5.9679	-0.0390	0.1556	-0.0830	D.2724	0.0868	0.1856	-2.9816
5	7.0	-0.01		_	-0.0369	0.1511	-0.0820	0.3251	0.10.0		-3.0001
6	9.81	-0.01			-0.0355	0.1537	-0.0866	0.3802	0.1065		-2.9758
	10.77	-0.01		-16.5736	-0.0346	0.1471	-0.0895	0.3972	0.1150	0.2821	-2.9563
8	11.79	-0.01		-11-1940		0.1336	-0.0911	0.4103	0.1207	0.2897	-2.9354
	13.86	-0.61		-11.6836	-0.0360	0.1351	-0.0722	0.4533	0.1350		-2.8677
10	15.81	-0.00		-12-0263		0.0812	-0.0664	0.4845	0.1654		-2.7408
11	16.85	-0.01		-11.6760		0.1974	-0.0423	0.5214	0.2104	0.3110	-2.6520
12	17.45	-0.01		-11.9261		0.2677	-0.0419	0.4556	0.2385	0.3171	-2.5944
13	18.47	-0.01		-11.4796		0.2833	-0.0371	0.5850	0.2765	0.3085	
	19.89	-0.01		-11.4353		0.1917	-0.0530	0.6204	0.3075	0.3129	-2.4557
. 15 	19.90	-0.01		-11-4541	-0.0412	0.0524	-0.0667 -0.0956	0.6298	0.3253 0.3499	0.3045	-2.4603
_	21.94	-0.01		-17-1514		-0.0006	-0.1177	0.6591 0.6802	0.3773	0.3092	-2.3976
17 18	22.97	-0.01		-12.3865		0.1072	-0.1169	0.6939	0.3999	0.2940	-2.3354 -2.2072
19	23.97	-0.04		-12.7763		0.4294	-0.1502	0.7013	0.4162	0.2451	-2.2512
20	24.99	-0.03		-13.7478		0.32.0	-0.1431	0.7174	0.4341	0.2833	-2.2276
21	25.99	-0.03	-	-13.7133		0.2854	-0.1401	0.7236	0.4551	0.2685	-5.5058
- 55	26.99	-0.0		-14.0678		0.2877		0.7159	0.4752	0.2406	-2.1752
23	2A.03	-0.04		-14.1884			-0.1761		0.4775		-2.1226
>= -	29.06	-0.05		-14.3943			-0.1616		0.4955	0.1855	
25	30.10	-0.05		-14.5260		-0.0542		0-6609	0.5161	0.1448	-2.0110
26	19.90	-0.05		-11.6973		0.3523	-0.0593		0.4520	0.1560	-2.4611
27	9.80	-0.01		-9.9415		0.1620	-0.0791		0.2081		-3.0116
28 -	-0.01	-0.01		-0.2165		0.2060	-0.0646		0.0986		-4.2589
	- • • • •		************	******		***************************************	-00000	***************************************	440,00	00.30	-46301

ARNOLD ENGINEERING DEVELOPMENT CENTER (AEDC)

DINT	125		2.3	0.0 t	CONF 14#0F34		0 0	DEL3 DEL4	TRANSITIO	· —-		
1 4	ALPHA	BETA	CN	CL#	CY	" CLN	CLL	CA	CAB	CAF	XCP -	
	-0.00	-0.01			-0.0525		-0.0669	0.3101	0.0516		-7,6487	
2	1.97	-0.01		-1.6274			-0.0687	0.3088	0.0701		-2.7366	
3		-0.01		-3.7253			-0.0726	0.3165	0.0762	0.2383	-2.8948	
•		-0.01		-5.9202			-0.0751	0.3451	0.0445		-2,9379	
5		-0.01		-4.2092				0-4072	0.0879		-3.0069	
	-	-0.01	_	-10-3452		_	-0.0958	0.4740	0.0902		-3.1241	
		-0.00		-12.0202			-0.0289	0.4817	0.0995		-2,9919	
	13.76	-0.00		-12-5-52			-0.0730 -0.0567	0.5257	0.1350	0.3907	-2.890	
	16.81	-0.00 -0.00		-12./slo -12.e123			-0.0550	0.5559	0.1706	0.3853	-2.76 <b>81</b> 2.70 <b>79</b>	
	17.83	-0.00		-12.7701				0.5546	0.3163	0.3061	-2.6375	
	19.85	-0.00		-12.7537			-0.00379	0.659R	0.3157	0.3441	-2.5744	
	18.85	-0.00		-12.7790			0.0061	0.5617	0.3376	0.3241	-2.5685	
	19.87	0.00		-12.0292					0.3A51	0.3050	-2.5063	
-	20.91	0.01		-12.4453			-	0.7122	0.39-9	0.3174	-2.4389	
	21.92	0.01		-17.9715					0.4137	0.3073	-2.3777	
	22.94	0.01		-13.082A					0.4363	0.2923	-2.3211	
_	23.97	0.00		-13.1336			-0.0736		0.4848	0.2410	-2.2508	
	24.99	-0.01		-13.320+					0.4894		-2.1922	
21	26.01	-0.01		-13.5045		U.0675	-0.0899	0.7252	0.5038	0.2213	-2.1406	
55	26.02	-0.01	5.3216	-13.4379	-0.0002	0.0976	-0.0793	0.7244	0.5194	0.2051	-2.1209	
23	27.06	-0.03	6.5832	-13.6000	0.062	0.2469	-0.0847	0.7100	0.5311	0.1789	-2.0659	
	28.10	-0.03	6.9071	-13.7190	0.079	0.1463	-0.0679	0-7074	0.5164	0.1910	-1.9862	
25	29.15	-0.02		-13.0755		0.1504	-0.0893	0.6681	0.5303	0.1578	-1.9169	
	30.19	-0.01		-14.06HD					G.5470		-1.8468	
	30.20	-0.01		-14.0226					0.5594	0.1150	-1.8443	
	19.88	0.01		-12.6224					0.4864		-2.4618	
_	19.86	0.00		-12-7-80					0.4539		-2.4965	
30 _	9.75	-0.01		-11.1215					0.2251		3.0761	
31	9.76	-0.01		-11.0577					0.1743		-3.0500	
	-0-00	-0.01			-0.0-6		-0.0386		0.0913		<u>-2.7520</u>	
32 33		-0.01			-0.041	0.1650	-0.0482	0.3284	0.0574	0.2710	-2.0694	

PROPULSION WIND TUNNEL FACILITY (PUT)

AERODYNAMIC -IND TUNNEL (4T)

AGE	ENG14EE	ING U	EVELOPMENT	CENTERIA	VEDĆ) . I	PROPULSION MARTIN M	WIND TU	NMEL FACILI AIL EFFECTS	TY(PUT)	AEA	ODYMAMIC WIND TUNNEL (4T)
	TEST		MACH RE10-			L DEL			TRANSITI		
POINT	ALPHA	BETA	cn	. CL# -	cy	CLN	CLL	CA	- CAB	CAF -	KCP
1	_	-0.01			-0.0527		-0.0684		0.0984		-1.0965
Ž		-0.01			-0.0490		-0.0659		0.1052		-2.9128
3	3.91	-0.01		-4.13er			-0.0665		0.1175		-3-0122
•		-0.01			-0.0276		-0.0794		0.1163	0.3641	
. 5 _		-0.01		-6-5060		0.1458	-0-0791		0.1488		-3.0749
6		-0.01		-9.0052					0.1532		-3.0948
		-0.01			-0.0147		-0.0950		0.1661		-3.1022
		-0.01			-0.0057	0.0399			0.1531		-2.9688
10	13.78	0.00			-0.0163 -0.0280		-0.0753		0.1840 0.2001		-2.6638 -2.6638
11	16.44			-12-2130			-0.0569		0.2121		-2.5905
iż		-0.00		-17.2118		0.0793			0.2466		-2.593/
13	17.46				-0.0340		-0.0536		0.2514	-	-2.5277
14	14.66	-0.00			-0.0468		-0.0539		0.2636		-2.4749
15	19.91	-0.00	5.2151	-12.4673	-0.0342	0.0150	-0.0910	0.5675	0.2687	0.2988	-2.3944
16	20.94	-0.04	5.4332	-12-518-	0.0323	-0.1778	-0.1694	0.5583	0.2717		-2.3041
17	21.96	0.01		-12-543/			-0.4345		0.3069		-2,230)
18	23.01	0.01		-12.7035			-0.3919		0.3807		-2.1024
19	24.06			-17.8645			-0.327		0.3959		-2.0849
50	25.08			-17.9962			-0-1092		0.4064		-5.0518
21	_26.14_			-13-1456					0.4331		-1.9394
22	27-17			-13.2861			-0.0020		0.4644		-1.6633
- <del>23</del> —	28.25			-13-5095					-0.4641		-1.7626
25	29.30 24.30			-13.5854			-0.0143		0.4822		-1.7095
26	29.30			-13-6664					0.4949		-1.7148 -1.7126
27	30.36			-13.8901					0.5231		-1.6529
50	19.92			-12-2063					0.4029		-2.3681
29		-0.0		-11.3566					0.2430		-3.1011
30	-0.00			-0.0952			-0.062		0.1453	0.2763	-5.1540

				TOANETTE	E. 3 . DE. :	0613 (	L DEL	CONF	6 PH1	LH RX10-	EARY -	755*	-
			···	ON-WORM	0 0	D O	.0 DEL	4±0F34 0		_	110 1.	1	
		XCP	CAF	CAB	. C4		"-ĊLN"	CY-	CL#	CN -	HFTA	ALPHA	OINT
		0.0201	0,4331	0.2036	0,6367	-0.0595		-0.0731	0.0003	0.0146	-0.01	0.00	1_
		-2.9563		0.2013	0.6373	-0.0594	0.5640	-0.0081	+1.9547	0.4612	-0-01	1.95	3
		-2.9513 -2.9920		0.2104	0.6372 0.6439	-0.0566	0.2646	-0.0631 -0.0619	-1.9551 -4.0479	1.3524	-0.01 -0.01	1.95 3.90	3
		-3.0405		0.2026	0.6739	-0.0712	0.2514		-6.3342	2.08-9	-0.05	5.84	1
		-3.0400		0.2132	0.6671	-0.0745	0.2330	-0.0484	-6.3298	5.0855	-0.01	5.84	6 -
		-3.0569	0.4991	0.2158	0.7149	-0.0AD7	0.2038	-0.0418	-R.6225		-0.01	7.79	7
		-3.0512	0.5464	2112.0	0.7577	-0.0868	0.1644	-0.0325	-10.7905		-0.01	9.72	8
		-2.8780	0.4963	0.2213	0.7176	-0.0902	0.1344	-0.0215	-11.0473	3.4385	-0.01	11.75	9
		-2.6986	0.4706	0.2339	0.7046	-0.0803	0.1478	-0.0314	-11.1254	4.1227	-0.01	13.61	io
		-2.5424	0.4693	0.2404	0.7097	-0.0628	0.1463		-11.3416		-0.01	15.80	11
			0.4631	80+5.0	0.7239	-0.0491	0.1394		-11-4247		-0.01	16.48	12
		-2.3875	0.5176	0.2496	0.7672	-0.0482	0.1394	-0.0406	-11.5145		-0.01	17.91	13
		-2.3076	0.5593	0.2624	0.4518	-0.0486	0.1394		-11.6012		-0.01	19.94	14
<del></del>			0.6077	0.2747 0.2850	0.8393	-0.0444	0.1399	-0.0392 -0.0309	-11.7045		-0.01 -0.01	14.99 21.04	15
_		-2.0526		0.2930	0.6824	-0.044R	0.1360	-0.0252	-11.9763		-0.01	22.04	17
		-1.9671		0.2936	0.6784	-0.0513	D.12H4	-0.0142	-12.1210		-0.01	23.10	18
		-1.6960	0.2881	0.3220	0.6100	-0.0613	0.0773	0.0152	-12.2947		-0.01	24.16	19
		-1.8324		0.3324	0.6207	-0.0593	0.0729	0.0192	-12.4647		-0.02	25.19	\$0
		-1.7633		0.3370	0.6359	-0.0543	0.0429	0.0579	-12.6582	7.1767	-0.04	26.24	21
	,	-1.6937	0.2980	0.3419	0.6399	-0.0382	-0.0102	0.0564	-17.6352				55
	<u> </u>	-1.6276	0.2810	0.3492	0.6303	-0.0425	0.0473	0.0037	-12.9A9S		-0.01		23
		-1.5685		0.3566	0.5976	-0.0067	-0.0434	0.0862	-13.1246		-0.01		24
		-1.5277		0.3573	0.6105	-0.0207	-0.0065	0.0783	-13.2486		-0.01		25
		-2.1840		0.3422	0.3984	-0.0505	0.1026	-0.0278	-11.4606		-0.01		26
		-3.0106		0.2922	0.7296	-0.0564		-0.0354 -0.0768	-10.4584		-0.01 -0.01		27 28 -
	,	-1.8500	0.4282	0.2150	0.6432	-0.0364	0.3077	-0.0768	-0.0051	0.0334	-0-01	0.00	7.
						<del></del>							
										<u> </u>			
-									•				

TEST									•		
1		ACH RX10-		CONF	L 0EL	DEL2	DEL3 DEL4	TRANSITI	On		
ALPHA	RFTA	CÑ	CLM	ĊY	CLN	CLL"	CA	CAB	CAF	XCP	<del></del> · ·
0.01	-0.01			-0.0357	0.1467	-0.0540	0.6430	0.2177	0.4253	15.2227	
_	-0.01			-0.0217	0.0965	-0.0459	0.6428	0.2060	0.4368	-3.0417	
				-0.0210	0.0927	-0.0475	0.6389	0.2072			·
					0.0781		0.6471	0.2033			
											·
_											
	-										
						-					
25,32											
26.38	-0.02	7.4406	-12.2053	0.0639	-0.0512	-0.0865		0.3076			. <u>—</u>
27.44	-0.02	7.6360	-12.4180	0.1004	-0.1020	-0.0770	0.6680	0.3155	0.3524	-1.5847	
24.50	-0.02					-0.0744	0.6626	0.3171	0.3455	-1.5335	
29.55	-0.02							0.3256	0.3296	-1.4997	
								0.3362			
	-0.01							0.3197			
						-0.0540	0.6340	0.5505	0.4138	-0.0256	
0.01	-0.01	0.0131	. 0.0520	-0.0315	0.1452	-0.0515	0.6378_	_0.2061 _	0.4317		
	0,01 1,95 1,95 3,88 5,84 7,79 9,74 113,83 15,88 16,91 17,95 18,90 20,06 21,10 22,15 23,20 24,25 27,32 26,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38 27,38	0,01 -0,01 1,95 -0,01 1,95 -0,01 3,88 -0,01 5,84 -0,01 7,79 -0,01 11,73 -0,01 11,73 -0,01 13,83 -0,01 15,88 -0,01 16,91 -0,01 17,95 -0,01 20,06 -0,01 21,10 0,00 22,15 -0,01 23,20 -0,01 23,20 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01 25,32 -0,01	0.01 -0.01 0.0050 1.95 -0.01 0.6051 1.95 -0.01 0.6051 1.95 -0.01 0.6779 3.88 -0.01 1.3912 5.84 -0.01 2.0476 7.79 -0.01 2.7017 9.74 -0.01 3.3551 11.73 -0.01 3.7477 13.83 -0.01 4.0608 15.88 -0.01 4.6375 17.95 -0.01 4.6375 17.95 -0.01 5.1862 19.00 -0.01 5.1819 20.06 -0.01 5.1819 20.06 -0.01 5.1829 22.15 -0.01 6.7259 22.15 -0.01 6.7259 22.15 -0.01 6.7259 23.20 -0.01 7.0749 25.32 -0.01 7.0749 26.38 -0.02 7.6360 27.44 -0.02 7.6360 24.50 -0.02 8.2108 29.55 -0.02 8.2108 29.55 -0.01 8.9400 20.06 -0.01 3.3809 0.01 -0.01 0.0308	0.01 -0.01 0.0050 0.0767 1.95 -0.01 0.6051 -1.6525 1.95 -0.01 0.6779 -1.6773 3.88 -0.01 1.3912 -4.1704 5.84 -0.01 2.0476 -6.2563 7.79 -0.01 2.7017 -8.3623 9.74 -0.01 3.3356 -10.0779 11.73 -0.01 3.7477 -10.5013 13.83 -0.01 4.006 -10.7021 15.86 -0.01 4.6375 -11.0075 17.95 -0.01 4.6779 -11.1372 18.98 -0.01 5.1862 -11.2982 19.00 -0.01 5.1319 -11.1187 20.06 -0.01 5.4426 -11.2454 22.15 -0.01 6.0644 -11.5770 23.20 -0.01 6.7259 -11.8551 25.32 -0.01 7.0789 -12.0241 25.32 -0.01 7.0789 -12.0241 25.32 -0.01 7.0789 -12.0241 27.44 -0.02 8.2108 -12.5913 29.55 -0.02 8.2108 -12.5913 29.55 -0.04 8.5751 -12.7741 30.60 -0.01 5.4264 -11.19638 20.06 -0.01 5.4264 -11.19638 20.06 -0.01 5.4264 -11.19638 20.06 -0.01 5.4264 -11.19638 20.06 -0.01 5.4264 -11.19638	0.01 -0.01 0.0050 0.0767 -0.0352 1.95 -0.01 0.6051 -1.6525 -0.0217 1.95 -0.01 0.6779 -1.9773 -0.0210 3.88 -0.01 1.3912 -4.1704 -0.0137 5.84 -0.01 2.0476 -0.2563 -0.0067 7.79 -0.01 2.7617 -A.3423 -0.0065 9.74 -0.01 3.335h -10.0779 0.0060 11.73 -0.01 3.7477 -10.5613 0.0093 13.83 -0.01 4.0606 -10.7021 0.0112 15.86 -0.01 4.0606 -10.7021 0.0112 15.86 -0.01 4.0606 -10.7021 0.0067 16.91 -0.01 4.6375 -11.0075 0.0030 17.95 -0.01 4.6375 -11.0075 0.0030 19.00 -0.01 5.1839 -11.1157 0.0013 20.06 -0.01 5.1852 -11.2554 0.0061 21.10 0.00 5.7389 -11.3735 0.0170 22.15 -0.01 6.004 -11.5770 0.0064 22.15 -0.01 6.004 -11.5770 0.0064 23.20 -0.01 6.7259 -11.6551 0.0385 25.32 -0.01 7.0769 -12.0251 0.0557 26.38 -0.02 7.4466 -12.2053 0.0634 24.50 -0.02 8.2108 -12.5913 0.1260 24.50 -0.02 8.2108 -12.5913 0.1260 24.50 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 29.55 -0.02 8.2108 -12.5913 0.1260 20.06 -0.01 8.4000 -12.4688 0.1371 20.06 -0.01 8.4000 -12.4688 0.1371 20.06 -0.01 8.4000 -12.4688 0.1371 20.06 -0.01 8.4000 -12.4680 0.1000	0.01 -0.01 0.0050 0.0767 -0.0352 0.1467 1.95 -0.01 0.6051 -1.6525 ~0.0217 0.0955 1.95 -0.01 0.6779 -1.9773 -0.0210 0.0927 3.88 -0.01 1.3912 -4.1704 -0.0137 0.0761 5.84 -0.01 2.0476 -6.2563 -0.0067 0.0684 7.79 -0.01 2.7617 -8.3423 -0.005 0.0460 9.74 -0.01 3.3356 -10.0779 0.0060 0.0256 11.73 -0.01 3.7477 -10.5613 0.0093 0.0265 13.83 -0.01 4.0606 -10.7021 0.0112 0.0203 15.86 -0.01 4.6375 -11.0075 0.0030 0.6134 17.95 -0.01 4.6375 -11.0075 0.0030 0.6134 17.95 -0.01 5.1682 -11.2782 0.0007 0.0145 18.98 -0.01 5.1682 -11.2782 0.0033 0.0108 19.00 -0.01 5.1319 -11.1157 0.0013 0.0167 20.06 -0.01 5.4426 -11.2854 0.0041 0.0048 22.15 -0.01 6.0644 -11.5720 0.0064 0.0316 23.20 -0.01 6.7259 -11.8551 0.0385 -0.0231 25.32 -0.01 7.0769 -12.0241 0.0557 -0.0609 27.44 -0.02 7.6360 -12.4180 0.1004 -0.1020 24.50 -0.02 8.2108 -12.5913 0.1260 -0.1611 29.55 -0.02 8.2108 -12.5913 0.1260 -0.1612 29.55 -0.02 8.2108 -12.5913 0.1260 -0.1612 20.06 -0.01 5.4264 -12.5913 0.1260 -0.1611 29.55 -0.02 8.2108 -12.5913 0.1260 -0.1616 20.06 -0.01 5.4264 -11.1598 -0.0173 0.0949 0.01 -0.01 3.3809 -10.0567 0.0083 0.0299 0.01 -0.01 0.0308 -0.0000 -0.0361 0.1616	0.01 -0.01 0.0050 0.0767 -0.0352 0.1467 -0.0540 1.95 -0.01 0.6051 -1.6525 ~0.0217 0.0965 -0.0459 1.95 -0.01 0.6079 -1.9773 -0.0210 0.0977 -0.0459 3.88 -0.01 1.3912 -4.1704 -0.0137 0.0781 -0.0562 5.84 -0.01 2.0476 -6.2563 -0.0067 0.0084 -0.0648 7.79 -0.01 2.7017 -8.3423 -0.0005 0.0460 -0.0736 9.74 -0.01 3.3356 -10.0779 0.0060 0.0756 +0.0798 11.73 -0.01 3.7477 -10.5613 0.0093 0.0265 -0.0831 13.83 -0.01 4.0606 -10.7021 0.0112 0.0203 -0.0825 15.86 -0.01 4.6375 -11.0075 0.0030 0.0134 -0.0621 17.95 -0.01 4.6375 -11.0075 0.0030 0.0134 -0.0621 17.95 -0.01 5.1682 -11.2782 0.0037 0.0165 -0.0573 18.98 -0.01 5.1682 -11.2782 0.0033 0.0108 -0.0514 19.00 -0.01 5.1319 +11.1157 0.0013 0.0147 -0.0514 20.06 -0.01 5.4426 -11.2854 0.0041 0.0049 -0.0514 23.20 -0.01 6.7259 -11.6551 0.0047 0.0326 0.0305 24.26 -0.01 6.7259 -11.6551 0.0345 -0.0231 -0.0646 25.32 -0.01 7.0769 -12.0261 0.0557 -0.0649 -0.0560 26.26 -0.01 8.7259 -11.6551 0.0345 -0.0531 -0.0696 25.32 -0.01 7.0769 -12.0261 0.0557 -0.0609 -0.0816 26.38 -0.02 7.4466 -12.2203 0.0639 -0.0512 -0.0646 27.44 -0.02 7.6360 -12.4180 0.1004 -0.1020 -0.0770 24.50 -0.02 8.2108 -12.9913 0.1260 -0.1811 -0.0744 29.55 -0.02 8.2108 -12.9913 0.1260 -0.1811 -0.0744 29.55 -0.01 3.3809 -10.0567 0.0083 0.0299 -0.0534 0.01 -0.01 3.3809 -10.0567 0.0083 0.0299 -0.0534 0.01 -0.01 -0.01 0.0308 -0.0004 -0.0361 0.1616 -0.0540	0.01 -0.01	0.01 -0.01 0.0050 0.0767 -0.0352 0.1667 -0.0550 0.6630 0.2177  1.95 -0.01 0.6051 -1.6525 ~0.0217 0.0965 -0.0459 0.6628 0.2060  1.95 -0.01 0.6779 -1.9773 -0.0210 0.0977 -0.0475 0.6389 0.2072  3.88 -0.01 1.3912 -6.1706 -0.0137 0.0781 ~0.0562 0.6471 0.2033  5.84 -0.01 2.0476 -6.2563 -0.0067 0.0684 -0.0668 0.6797 0.2024  7.79 -0.01 3.7617 -8.3623 -0.0005 0.0480 -0.0738 0.7223 0.2023  9.74 -0.01 3.3356 -10.0779 0.0060 0.0256 -0.0831 0.7728 0.2023  9.74 -0.01 3.7477 -10.5013 0.0093 0.0265 -0.0831 0.770 0.2092  11.73 -0.01 3.7477 -10.5013 0.0093 0.0265 -0.0831 0.770 0.2092  15.86 -0.01 4.9606 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2166  15.86 -0.01 4.6375 -11.0075 0.0030 0.0134 -0.0621 0.6819 0.2236  16.91 -0.01 4.6375 -11.0075 0.0030 0.0134 -0.0621 0.6819 0.2291  17.95 -0.01 4.6789 -11.1372 -0.0007 0.0145 -0.0573 0.7050 0.2340  18.96 -0.01 5.1682 -11.2982 0.0038 0.0147 -0.0554 0.7604 0.2403  19.00 -0.01 5.1682 -11.2982 0.0038 0.0147 -0.0554 0.7604 0.2403  19.00 -0.01 5.4626 -11.2982 0.0038 0.0147 -0.0554 0.7604 0.2403  22.15 -0.01 6.0644 -11.5770 0.0064 0.0316 -0.0644 0.6600 0.2906  23.20 -0.01 6.7259 -11.8551 0.0385 -0.0231 -0.0644 0.6600 0.2906  23.20 -0.01 6.7259 -11.8551 0.0385 -0.0231 -0.0696 0.6573 0.2937  24.25 -0.01 7.0789 -12.0241 0.0557 -0.0699 -0.0865 0.6626 0.3376  27.44 -0.02 7.6360 -12.4180 0.1004 -0.1012 -0.0770 0.6680 0.3155  24.50 -0.02 8.5751 -12.7741 0.1379 -0.1611 -0.0744 0.6626 0.3171  29.55 -0.001 8.5264 -11.1596 -0.0173 0.0995 -0.0040 0.6526 0.3171  29.55 -0.001 8.5264 -11.1596 -0.0173 0.0995 -0.0040 0.5340 0.5216 0.3171  29.55 -0.001 8.5426 -11.5963 0.1321 -0.1817 -0.0540 0.6626 0.3171  29.55 -0.001 8.5426 -11.5963 0.1321 -0.1817 -0.0540 0.6626 0.3171  29.55 -0.001 8.5426 -11.5963 0.1321 -0.1817 -0.0550 0.6626 0.3171  29.55 -0.001 8.5426 -11.5963 0.1321 -0.1817 -0.0550 0.6626 0.3171  29.55 -0.001 8.5426 -11.5963 0.1321 -0.1817 -0.0550 0.6626 0.3171  29.55 -0.001 8.380 -10.0567 0.0083 0.0299 -0.0730 0.7359 0.2283  0.01 -0.01 0.0308 -0.0008 -0.0361 0.1616 -0.05540 0.6630 0.3280	0.01 -0.01 0.0050 0.0767 -0.0352 0.1467 -0.0540 0.6430 0.2177 0.4253 1.95 -0.01 0.6051 -1.6525 -0.0217 0.0965 -0.0459 0.6428 0.2060 0.4368 1.95 -0.01 0.6779 -1.9773 -0.0210 0.0977 -0.0475 0.6389 0.2072 0.4317 3.88 -0.01 1.3912 -4.1704 -0.0137 0.0781 -0.0562 0.6471 0.2033 0.4439 5.84 -0.01 2.0476 -6.2563 -0.0067 0.0644 -0.0648 0.6797 0.2024 0.4773 7.79 -0.01 2.7617 -8.3423 -0.0005 0.0460 -0.0736 0.7293 0.2023 0.5270 9.74 -0.01 3.335h -10.0779 0.0060 0.0268 -0.0798 0.7728 0.2049 0.5679 11.73 -0.01 3.7477 -10.5613 0.0093 0.0265 -0.0831 0.7470 0.2024 0.4988 11.73 -0.01 4.7606 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2164 0.4988 15.84 -0.01 4.7606 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2164 0.4988 15.84 -0.01 4.7606 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2164 0.4988 15.84 -0.01 4.6375 -11.0075 0.0030 0.0182 -0.0711 0.7281 0.2236 0.5046 16.91 -0.01 4.6375 -11.0075 0.0030 0.0184 -0.0621 0.6819 0.2291 0.4528 17.95 -0.01 4.7789 -11.1372 -0.0007 0.0145 -0.0573 0.7050 0.2340 0.4709 18.98 -0.01 5.1682 -11.2982 0.0039 0.0108 -0.0514 0.7604 0.2403 0.52014 19.00 -0.01 5.1682 -11.2982 0.0039 0.0108 -0.0514 0.7604 0.2403 0.52014 19.00 -0.01 5.4626 -11.2564 0.0041 -0.0514 0.7604 0.2403 0.52014 20.06 -0.01 5.4626 -11.2564 0.0041 -0.00514 0.7604 0.2403 0.52014 21.10 0.00 5.7309 -11.3936 0.0170 -0.0326 0.0305 0.0482 0.2900 0.4063 22.15 -0.01 6.7259 -11.6551 0.0385 -0.0231 -0.0696 0.6573 0.2964 0.3609 25.32 -0.01 7.0709 -12.0241 0.0557 -0.0609 -0.0816 0.6626 0.3171 0.3455 26.38 -0.02 7.6360 -12.4180 0.1004 -0.0120 -0.0770 0.6624 0.3376 0.3549 27.44 -0.02 8.2108 -12.2513 0.1209 -0.1811 -0.0744 0.6626 0.3171 0.3455 27.55 -0.02 8.2108 -12.5913 0.1209 -0.1811 -0.0744 0.6626 0.3171 0.3455 27.55 -0.01 8.2600 -12.4938 0.1371 -0.1834 -0.0657 0.6626 0.3171 0.3455 0.001 -0.01 5.4626 -11.1596 -0.0173 0.0995 -0.0440 0.5216 0.3197 0.2283 0.5076 0.01 -0.01 5.4626 -11.2563 0.03171 0.0895 -0.0640 0.3362 0.3079 0.01 -0.01 5.4626 -11.0567 0.0083 0.0299 -0.0730 0.7359 0.2283 0.5076 0.01 -0.01 5.4626 -11.0567 0.0083 0.0299 -0.0730 0.05280 0.2283 0.507	0.01 -0.01 0.0050 0.0767 -0.0352 0.1467 -0.0540 0.6030 0.2177 0.4253 15.2227 1.95 -0.01 0.6051 -1.6555 0.0.217 0.0955 -0.0459 0.6038 0.2060 0.4318 -2.9167 3.68 -0.01 0.6779 -1.9773 -0.0210 0.0927 -0.0475 0.6389 0.2072 0.4317 -2.9167 3.68 -0.01 1.3912 -4.1704 -0.0137 0.0781 -0.0562 0.6471 0.2033 0.4439 -2.9977 5.64 -0.01 2.0476 -0.2563 -0.0067 0.0084 0.60797 0.2024 0.4773 -3.0554 7.79 -0.01 2.7017 -4.3423 -0.0005 0.0460 -0.0736 0.7293 0.2023 0.5270 -3.0207 9.74 -0.01 3.335h -10.0779 0.0060 0.0758 -0.0831 0.7470 0.2023 0.5270 -3.0207 11.73 -0.01 3.7477 -10.5013 0.0093 0.0265 -0.0831 0.7470 0.2092 0.5378 -2.8181 13.83 -0.01 4.0006 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2164 0.4988 -2.6355 15.86 -0.01 4.0006 -10.7021 0.0112 0.0203 -0.0825 0.7152 0.2164 0.4988 -2.6355 15.86 -0.01 4.66375 -11.0075 0.0030 0.0134 -0.0621 0.6819 0.2291 0.4528 -2.3736 16.91 -0.01 4.6799 -11.1372 -0.0007 0.0145 -0.0573 0.7050 0.2340 0.4709 -2.2827 18.96 -0.01 5.1682 -11.2982 0.0039 0.0108 -0.0514 0.7604 0.2033 0.5291 -2.1861 18.90 -0.01 5.1682 -11.2982 0.0039 0.0108 -0.0514 0.7604 0.2033 0.5291 -2.1861 18.90 -0.01 5.1682 -11.2982 0.0039 0.0108 -0.0514 0.7604 0.2033 0.5291 -2.1861 18.90 -0.01 5.4626 -11.2954 0.0041 0.0044 0.0060 0.2906 0.3893 -1.0953 22.15 -0.01 6.0044 -11.5770 0.0064 0.0316 -0.0547 0.7211 0.2795 0.4416 -2.1666 23.20 -0.01 6.7259 -11.8551 0.0345 -0.0557 0.7604 0.3006 0.3893 -1.0953 22.25 -0.01 6.7259 -11.8551 0.0345 -0.0557 0.0660 0.3693 -1.0953 22.25 -0.01 7.0749 -12.0241 0.0557 -0.0609 -0.0816 0.6620 0.3155 0.3554 -1.5385 22.35 -0.02 8.2108 -12.2953 0.1379 -0.0557 0.0660 0.3155 0.3554 -1.5385 22.55 -0.02 8.2108 -12.5913 0.1260 -0.0161 -0.0044 0.6620 0.3155 0.3554 -1.5385 22.55 -0.02 8.2108 -12.5913 0.1260 -0.0161 -0.00557 0.0655 0.3556 0.3266 0.3266 -1.6897 33.60 -0.01 5.4264 -11.1596 -0.0013 0.0099 -0.0512 0.0668 0.3155 0.3554 -1.5385 22.55 -0.02 8.2108 -12.5913 0.1260 -0.1811 -0.0744 0.6626 0.3171 0.3455 -1.5335 22.55 -0.02 8.2108 -12.5913 0.1260 -0.1811 -0.0744 0.6626 0.3171 0.3455 -1.5335 22.55 -0.02 8.2108 -12.5913

1 0.02 -0.01 -0.0409 0.2809 -0.0424 0.1797 -0.0002 0.0080 0.2055 0.4025 -6.8671 2 1.97 -0.01 0.5844 -1.0192 -0.0335 0.1458 -0.0584 0.6060 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2378 -3.5751 -0.014 0.1457 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.88 -0.01 1.8919 -5.4608 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393 5 7.42 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.44 -0.01 4.0453 -10.4641 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4845 -2.5917 9 15.91 -0.01 4.4288 -10.5847 0.0264 -0.0084 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.6815 -10.7543 0.0147 6.0121 -0.0774 0.6622 0.2397 0.4225 -2.3911 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0048 -0.0681 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0074 -0.0680 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0060 -0.0774 -0.0680 0.7243 0.2600 0.4643 -2.0936 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0395 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.6376 0.0035 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753	1 120 1.3u 2.3	1 IZO 1.30 Z.3	1 120 1.30 2.3	
1 0.02 -0.01 -0.0409 0.2809 -0.0024 0.1797 -0.0002 0.0080 0.2055 0.4025 -0.8671 2 1.97 -0.01 0.5846 -1.6192 -0.0335 0.1458 -0.0586 0.6060 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2378 -3.5751 -0.0314 0.1457 -0.0080 0.6109 0.2075 0.4034 -2.8882 4 5.88 -0.01 1.8919 -5.5604 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9303 5 7.42 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1722 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.44 -0.01 4.0453 -10.4861 0.0153 0.0047 -0.0836 0.7003 0.2158 0.885 -2.9917 9 15.91 -0.01 4.4286 -10.5897 0.0263 -0.008h -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.8915 -10.7543 0.0147 (-0.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972 11 17.98 -0.01 4.49817 -10.9413 0.0172 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0680 0.7223 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.2875 -11.1340 0.0060 -0.0774 -0.0652 0.2065 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.6385 -10.0497 -0.0652 0.6408 0.2705 0.3839 -1.9984 15 22.19 -0.01 6.2107 -11.4350 0.0060 -0.0774 -0.0652 0.6408 0.2705 0.3839 -1.9984 16 23.25 -0.01 6.5253 -11.6376 0.0433 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2107 -11.4350 0.0060 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 16 23.25 -0.01 6.2107 -11.4350 0.0043 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 17 28.29 -0.01 6.2017 -11.4350 0.0043 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0321 -0.0005 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 8.3617 -17.4640 0.0043 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 22 2.00 0.01 8.3617 -17.4640 0.0043 -0.0060 0.6252 0.2953 0.3299 -1.5346 23 25.41 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 24 20.11 -6.01 5.5676 -10.49321 0.0013 -0.0064 -0.0088 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 8.3617 -7.0073 0.0027 0.0031 -0.0064 -0.0088 0.5801 0.3192 0.2609 -1.9705	1 0.02 -0.01 -0.0409 0.2809 -0.0624 0.1797 -0.0602 0.0606 0.2077 0.3983 -2.7518  2 1.97 -0.01 0.5846 -1.6192 -0.0335 0.1458 -0.0564 0.6060 0.2077 0.3983 -2.7518  3 3.91 -0.01 1.2376 -3.5751 -0.0314 0.1457 -0.0660 0.6109 0.2075 0.4034 -2.8882  4 5.86 -0.01 1.8919 -5.5604 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393  5 7.42 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.0744 0.6676 0.2030 0.4645 -2.9336  6 9.79 -0.01 3.1722 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926  7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0229 -0.0823 0.7196 0.2048 0.5108 -2.7799  8 13.46 -0.01 4.0453 -10.4861 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4865 -2.9311  10 10.96 -0.01 4.4286 -10.5897 0.0228 -0.008H -0.0774 0.6622 0.2397 0.4225 -2.3911  10 10.96 -0.01 4.4815 -10.7553 0.0147 (.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972  11 17.98 -0.01 5.2875 -11.0701 0.0219 -0.0084 -0.0683 0.7263 0.2554 0.4385 -2.1963  12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0088 -0.0683 0.7263 0.2000 0.4643 -2.0936  13 20.08 -0.01 5.2875 -11.1340 0.0660 -0.0774 -0.0657 0.6508 0.2765 0.3839 -1.9984  14 21.13 -0.01 5.8843 -11.2564 0.6385 -0.0499 -0.0652 0.6408 0.2703 0.3263 -1.9984  15 22.19 -0.01 6.2107 -11.4350 0.0660 -0.0774 -0.0652 0.6408 0.2705 0.3374 -1.9183  15 22.19 -0.01 6.2107 -11.4350 0.0638 -0.0392 -0.0665 0.6408 0.2705 0.3374 -1.9183  15 22.29 -0.01 6.201 -1.6436 0.0385 -0.0499 -0.0652 0.6408 0.2705 0.3374 -1.9183  16 23.25 -0.01 6.201 -1.6436 0.0385 -0.0594 -0.0665 0.6408 0.2705 0.3704 -1.9183  20 27.86 -0.01 7.0528 -12.173 0.0844 -0.1082 -0.0865 0.6408 0.2705 0.3704 -1.9183  20 27.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0652 0.0253 0.3299 -1.5346  20 27.86 -0.01 8.3617 -17.4640 0.0740 -0.0717 -0.0007 0.6252 0.2953 0.3299 -1.5346  20 27.86 -0.01 8.3617 -17.4640 0.0040 -0.0717 -0.0060 0.6252 0.2953 0.3299 -1.5346  20 27.86 -0.01 8.3617 -17.4640 0.0040 -0.0717 -0.0060 0.6252 0.2953 0.3299 -1.5346  20 27.86 -0.01 8.3617 -17.4640 0.0040 -0.0031 -0.0060 0.6252 0.2953 0.3299 -1.5346  20 27.86 -0.01 8.3617 -1.6430 0.0040 -0.0060 0.0060 0.6252 0.2953	1 0.02 -0.01 -0.0409 0.2809 -0.0428 0.1797 -0.0602 0.0080 0.2055 0.4028 -0.6867] 2 1.97 -0.01 0.5848 -1.6192 -0.0335 0.1458 -0.0584 0.6060 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2378 -3.5751 -0.0314 0.1457 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.86 -0.01 1.4919 -5.6608 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393 5 7.42 -0.01 2.5347 -7.4399 -0.0063 0.0819 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0830 0.7196 0.2088 0.5108 -2.7799 8 13.46 -0.01 4.0453 -10.0461 0.0153 0.0067 -0.0830 0.7090 0.2188 0.4845 -2.5917 9 15.91 -0.01 4.0453 -10.0461 0.0153 0.0067 -0.0836 0.7003 0.2188 0.4845 -2.5917 11 7.98 -0.01 4.0815 -10.7543 0.0147 0.0121 -0.0774 0.6622 0.2397 0.4225 -2.3911 11 7.98 -0.01 4.0815 -10.7543 0.0172 -0.0084 -0.0774 0.6622 0.2397 0.4225 -2.3912 12 19.00 -0.01 5.2875 -11.0701 0.0217 -0.0073 0.6938 0.2554 0.4385 -2.1043 13 20.00 -0.01 5.2875 -11.0701 0.0219 -0.0008 -0.0600 0.7243 0.2000 0.4643 -2.0936 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0097 -0.0652 0.6408 0.2705 0.3839 -1.9984 15 22.19 -0.01 6.2107 -11.4350 0.0043 -0.0557 -0.0887 0.6610 0.2691 0.3369 -1.6395 16 23.25 -0.01 6.2507 -11.0376 0.0385 -0.0399 -0.0652 0.6408 0.2705 0.3704 -1.9163 17 26.29 -0.01 6.2107 -11.4350 0.0043 -0.0557 -0.0887 0.6610 0.2691 0.3369 -1.6395 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0321 -0.0865 0.6444 0.2697 0.3747 -1.7166 22 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0603 -0.0657 0.6252 0.2953 0.3299 -1.5346 22 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0657 0.6625 0.6252 0.2953 0.3299 -1.5346 23 20.01 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0657 0.6257 0.6250 0.3704 -1.9163 24 20.11 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0657 0.6257 0.6250 0.3748 -1.4883 25 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0657 0.6257 0.0321 0.3111 -1.4132 26 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0603 -0.0657 0.6257 0.0321 0.3111 -1.4132 27 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0668 0.5901 0.3192 0.2609 -1.970	1 0.02 -0.01 -0.0409 0.2809 -0.022 0.1797 -0.0002 0.0080 0.2055 0.4025 -6.867] 2 1.77 -0.01 0.583a -1.6172 -0.0335 0.1458 -0.058a 0.6000 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2376 -3.5751 -0.0314 0.157 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.86 -0.01 1.4917 -5.5603 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393 5 7.42 -0.01 2.5347 -7.4359 -0.0003 0.0817 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1722 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 7 11.77 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0083 0.7196 0.2088 0.5108 -2.7799 8 13.44 -0.01 4.0453 -10.4541 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4865 -2.5917 9 15.91 -0.01 4.4288 -10.5847 0.0263 -0.0084 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.0815 -10.7543 0.0147 0.0121 -0.0701 0.6618 0.2580 0.4073 -2.2072 11 17.98 -0.01 4.9817 -10.9413 0.0172 -0.0074 -0.0673 0.6938 0.2556 0.4385 -2.1063 12 19.04 -0.01 5.2675 -11.0701 0.0214 -0.0084 -0.0600 0.7243 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.2675 -11.0701 0.0214 -0.0084 -0.0660 0.7243 0.2000 0.463 -2.0936 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0049 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2107 -11.4356 0.0066 -0.0774 -0.0673 0.6938 0.2756 0.3839 -1.9984 16 23.25 -0.01 6.5553 -11.6376 0.0355 -0.0685 0.5993 0.2750 0.3704 -1.9143 17 24.29 -0.01 6.2107 -11.4356 0.0359 -0.0657 -0.0865 0.6448 0.2907 0.3747 -1.7158 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0655 0.6665 0.2719 0.3550 -1.6625 21 20.55 -0.01 8.3617 -17.4444 0.0594 -0.1062 -0.0865 0.6444 0.2907 0.3747 -1.7154 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.46 -0.01 7.9646 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 22 29.60 -0.01 7.9646 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 23 20.11 -0.01 7.9646 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 24 29.61 -0.01 7.9646 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 25 9.78 -0.01 7.31846 -9.2679 0.0027 0.0027 0.0027 0.0028 0.0027 0.0027 0.0027 0.0027 0.0027 0.00	
1 0.02 -0.01 -0.0409 0.7809 -0.0024 0.1797 -0.0602 0.6080 0.2055 0.4025 -0.8671 2 1.97 -0.01 0.5864 -1.6192 -0.0335 0.1558 -0.0586 0.6080 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2378 -3.5751 -0.011 0.157 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.88 -0.01 1.8919 -5.5608 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393 5 7.82 -0.01 2.5347 -7.4359 -0.0083 0.819 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0028 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.84 -0.01 4.0453 -10.4841 0.0153 0.0047 -0.0836 0.7003 0.2158 0.8845 -2.5917 9 15.91 -0.01 4.4288 -10.5847 0.0283 -0.0088 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.8815 -10.7543 0.0147 0.0172 -0.0673 0.6938 0.2554 0.4385 -2.1963 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0673 0.6018 0.2550 0.4087 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0660 0.7243 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.5883 -11.2544 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3839 -1.9984 14 21.13 -0.01 5.6883 -11.2544 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2107 -11.4350 0.0600 -0.0774 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.29 -0.01 6.2107 -11.4350 0.0638 -0.0659 -0.0665 0.6408 0.2705 0.3704 -1.9143 15 22.29 -0.01 6.2107 -11.4350 0.0639 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 16 23.25 -0.01 6.5207 -11.6300 0.0639 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 16 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0662 0.0652 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0652 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0865 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0662 0.6273 0.3025 0.3748 -1.4883 22 20.11 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0668 0.6200 0.6273 0.3025 0.3248 -1.4883 23 30.66 -0.01	1 0.02 -0.01 -0.0409 0.7809 -0.0024 0.1797 -0.0602 0.06060 0.2077 0.3983 -2.7518 2 1.97 -0.01 0.5644 -1.6192 -0.0335 0.1558 -0.0564 0.6060 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2378 -3.5751 -0.0114 0.1557 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.86 -0.01 1.8919 -5.5608 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9336 5 7.87 -0.01 2.5347 -7.4359 -0.0063 0.8189 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.44 -0.01 4.0453 -10.4841 0.0153 0.0047 -0.0836 0.7003 0.2158 0.885 -2.8917 9 15.91 -0.01 4.4288 -10.5847 0.0283 -0.0088 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.8015 -10.7543 0.0147 0.0172 -0.0673 0.6938 0.2554 0.4385 -2.1963 11 17.98 -0.01 4.8917 -10.441 0.0172 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0680 0.7223 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0680 0.7223 0.2000 0.4643 -2.0936 14 21.13 -0.01 5.6843 -11.2544 0.0685 -0.0379 -0.0652 0.6408 0.2705 0.3839 -1.9984 15 22.19 -0.01 6.2107 -11.4350 0.0660 -0.0774 -0.0652 0.6080 0.2765 0.3839 -1.9984 16 23.25 -0.01 6.2107 -11.4350 0.0660 -0.0557 -0.06652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2207 -11.4350 0.0639 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 16 23.25 -0.01 6.201 -11.4510 0.0594 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 17 22.29 -0.01 6.201 -11.4510 0.0594 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0557 -0.0865 0.6408 0.2705 0.3704 -1.9143 18 25.33 -0.01 7.2526 -17.6573 0.0329 -0.0665 0.6652 0.2953 0.3299 -1.5346 20 27.66 -0.01 8.3617 -12.4640 0.0709 -0.0557 -0.0865 0.6640 0.2695 0.2719 0.3530 -1.6625 21 20.55 -0.01 8.3617 -17.4640 0.0709 -0.0557 -0.0865 0.6627 0.2719 0.3530 -1.6625 22 29.66 -0.01 8.3617 -17.4640 0.0709 -0.0717 -0.0007 0.6252 0.2953 0.3299 -1.5346 23 30.66 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0665 0.6252 0.2953 0.3299 -1.5346 24 20.	1 0.02 -0.01 -0.0409	1 0.02 -0.01 -0.0409 0.2809 -0.022 0.1797 -0.0002 0.000 0.2055 0.4025 -6.867] 2 1.97 -0.01 0.5848 -1.6192 -0.0335 0.1458 -0.0588 0.6000 0.2077 0.3983 -2.7518 3 3.91 -0.01 1.2376 -3.5751 -0.0314 0.1457 -0.0860 0.6109 0.2075 0.4034 -2.8882 4 5.86 -0.01 1.4919 -5.5608 -0.0247 0.1307 -0.0723 0.6397 0.2000 0.4157 -2.9393 5 7.42 -0.01 2.5347 -7.4359 -0.0003 0.0819 -0.0744 0.6676 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.44 -0.01 4.0453 -10.4841 0.0153 0.00047 -0.0836 0.7003 0.2158 0.4845 -2.5917 9 15.91 -0.01 4.4288 -10.5847 0.0263 -0.0084 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.0815 -10.7543 0.0147 0.0121 -0.0701 0.6618 0.2580 0.4075 -2.2972 11 17.98 -0.01 4.9917 -10.9413 0.0177 -0.0084 -0.00701 0.6618 0.2580 0.4075 -2.2972 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0088 -0.0660 0.7243 0.2000 0.4643 -2.0936 13 20.00 -0.01 5.2875 -11.0340 0.0060 -0.0774 -0.0673 0.2000 0.4603 -2.0936 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2107 -11.4350 0.0060 -0.0774 0.0652 0.2656 0.3839 -1.9984 16 23.25 -0.01 6.5553 -11.6376 0.0385 -0.0499 -0.0655 0.6408 0.2705 0.3704 -1.9143 17 24.29 -0.01 6.2107 -11.4350 0.0329 -0.0085 0.6444 0.2997 0.3730 0.3203 -1.8395 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0085 0.6666 0.5993 0.2730 0.3203 -1.6025 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.01 7.9666 -12.2220 0.0321 -0.0003 -0.0605 0.6252 0.2953 0.3299 -1.5346 20 27.86 -0.	
3 3.91 -0.01 1.2376 -3.5751 -0.0314 0.1457 -0.0680 0.6109 0.2075 0.4034 -2.8882 4 5.88 -0.01 1.8919 -5.6008 -0.0247 0.1307 -0.0723 0.6397 0.2000 0.4357 -2.9393 5 7.82 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.0744 0.6076 0.2030 0.4645 -2.9336 6 9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0836 0.7003 0.2158 0.6085 -2.77799 8 13.84 -0.01 4.0453 -10.4041 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4085 -2.5917 9 15.91 -0.01 4.0288 -10.5087 0.0263 -0.0088 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.0815 -10.7543 0.0147 0.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0638 0.7003 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 0.7243 0.2500 0.4663 -2.0936 13 20.06 -0.01 5.2875 -11.0701 0.0219 -0.0068 0.7243 0.2500 0.4663 -2.0936 14 21.13 -0.31 5.8683 -11.2684 0.0385 -0.0374 -0.0652 0.6088 0.2705 0.3839 -1.9984 15 72.19 -0.01 6.2107 -11.4350 0.0463 -0.0532 -0.0666 0.5993 0.2730 0.3203 -1.8395 16 23.25 -0.01 6.5553 -11.6376 0.0935 -0.0532 -0.0666 0.5993 0.2730 0.3203 -1.8395 17 24.29 -0.01 6.207 -11.4350 0.0352 -0.0554 0.0844 0.2097 0.3747 -1.7758 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0665 0.6084 0.2075 0.3704 -1.9143 19 26.41 -0.01 7.6238 -12.1733 -0.0844 -0.1556 0.0855 0.6084 0.2075 0.3704 -1.9143 22 29.60 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0665 0.6044 0.2097 0.3747 -1.7766 22 29.60 -0.01 8.3617 -17.4646 0.0740 -0.0717 -0.0605 0.6252 0.2953 0.3299 -1.5346 23 30.66 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0665 0.6080 0.5801 0.3126 0.3221 -1.4091 24 20.11 -0.01 7.6238 -12.1733 0.0044 -0.1556 0.0055 0.6088 0.5801 0.3126 0.3221 -1.4091 25 9.76 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0665 0.6088 0.5801 0.3126 0.3221 -1.5968 26 77.86 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0665 0.6088 0.5801 0.3126 0.3221 -1.4091 25 9.76 -0.01 7.9686 -12.2220 0.0321 -0.0003 -0.0668 0.5801 0.3126 0.3111 -1.4132 25 9.76 -0.01 7.8686 0.00 0.00 0.00 0.00 0.00 0.00 0.00	3 3.91 -0.01 1.2376 -3.5751 -0.0314	3 3.91 -0.01 1.2376 -3.5751 -0.0314	3 3.91 -0.01 1.2376 -3.5751 -0.0314	
\$ 5.88 -0.01	\$ 5.86 -0.01 1.8419 -5.5608 -0.0247 0.1307 -0.0723 0.6397 0.2040 0.4357 -2.9393	\$ 5.88 -0.01	\$ 13.86 -0.01 1.8914 -5.5608 -0.0247	
5 7.82 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.0746 0.6676 0.2030 0.4645 -2.9336 0.7799 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7111 0.2050 0.5061 -2.8924 0.7093 0.7111 0.2050 0.5061 -2.8924 0.7093 0.7111 0.2050 0.5061 -2.8924 0.7093 0.7093 0.7111 0.2050 0.5061 -2.8924 0.7093 0.7093 0.7111 0.2050 0.5061 -2.8924 0.7093 0.7093 0.7111 0.7094 0.7093 0.7093 0.7093 0.7111 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093 0.7093	5 7.42 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.074	5 7.42 -0.01 2.5347 -7.4359 -0.0063 0.0819 -0.074 0.6676 0.2030 0.4645 -2.9336 0.7799 -0.01 3.1922 -9.2331 -0.0028 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.88928 -2.7799 -0.083 0.7196 0.2088 0.5108 -2.7799 -0.0831 0.0068 0.7003 0.2158 0.4845 -2.5917 -0.0846 0.7003 0.2158 0.4845 -2.5917 -0.0846 0.7003 0.2158 0.4845 -2.5917 -0.0846 0.7003 0.2158 0.4845 -2.5917 -0.0846 0.7003 0.2158 0.4845 -2.5917 -0.0846 0.0704 0.6622 0.2397 0.4225 -2.3911 -0.0704 0.6622 0.2397 0.4225 -2.3911 -0.0704 0.6622 0.2397 0.4225 -2.3911 -0.0704 0.6622 0.2397 0.4225 -2.3911 -0.0704 0.6622 0.2550 0.4079 -2.2972 -0.0847 0.00147 -0.0704 0.6622 0.2550 0.4079 -2.2972 -0.0847 0.6021 -0.0774 0.6622 0.2550 0.4079 -2.2972 -0.0847 0.6021 -0.0774 0.6021 -0.0774 0.6622 0.2550 0.4079 -2.2972 -0.0847 0.2014 -0.0774 0.6622 0.2550 0.4085 -2.1963 -0.0847 0.2550 0.4079 -0.2550 0.4084 -2.0936 -2.1963 -0.0860 0.7243 0.2500 0.4643 -2.0936 -2.1963 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0860 0.7243 0.2500 0.4643 -2.0936 -0.0936 -0.0860 0.2765 0.3839 -1.9984 -0.0860 0.2765 0.3839 -1.9984 -0.0860 0.5993 0.2730 0.3263 -1.9936 -0.0860 0.5993 0.2730 0.3263 -1.9935 -0.0860 0.5993 0.2730 0.3263 -1.9935 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5993 0.2730 0.3263 -1.9395 -0.0860 0.5996 0.5995 0.5996 -0.0860 0.5995 0.5996 0.5995 0.5996 0.5996 0.5996 0.5995 0.5996 0.5995 0.5996	5 7.82 -0.01 2.5347 -7.4359 -0.0063 0.081y -0.0744 0.6676 0.2030 0.4645 -2.9336 0.799 -0.01 3.1922 -9.231 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 0.11.7y -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 0.11.7y -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0826 0.7003 0.2158 0.4845 -2.5917 0.774 0.6627 0.2397 0.4255 -2.3911 0.0047 0.0047 -0.0836 0.7003 0.2158 0.4845 -2.5917 0.0047 0.0047 -0.0084 0.0774 0.6622 0.2397 0.4225 -2.3911 0.0049 -0.0774 0.6622 0.2397 0.4225 -2.3911 0.0049 -0.0701 0.6618 0.2550 0.4079 -2.2972 0.0047 0.0047 0.0047 0.0047 0.0047 0.0047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2047 0.2	
9.79 -0.01	6	9.79 -0.01 3.1922 -9.2331 -0.002K 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8926 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 13.74 -0.01 4.0453 -10.4941 0.0153 0.0047 -0.0836 0.7003 0.2158 0.885 -2.5917 15.91 -0.01 4.0453 -10.5847 0.0263 -0.008K -0.0774 0.6622 0.2397 0.4225 -2.3911 10.96 -0.01 4.6815 -10.5545 0.0147 0.0121 -0.0701 0.6618 0.2540 0.4079 -2.2972 11.7.98 -0.01 4.9817 -10.9413 0.0172 -0.0064 -0.0633 0.7003 0.2554 0.4085 -2.5963 12.19.04 -0.01 5.2475 -11.0701 0.0214 -0.0068 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.2575 -11.0701 0.0214 -0.0068 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0060 -0.0774 -0.0630 0.7243 0.2600 0.4643 -2.0936 14 21.13 -0.01 5.8843 -11.2604 0.0385 -0.0074 -0.0680 0.7243 0.2600 0.3839 -1.9984 15 22.19 -0.01 6.2167 -11.4356 0.0483 -0.0385 -0.0052 0.6686 0.2705 0.3839 -1.9984 15 22.19 -0.01 6.2167 -11.4356 0.0443 -0.0392 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.0376 0.0035 -0.0557 -0.0847 0.0161 0.2691 0.3469 -1.7753 16 23.25 -0.01 6.9041 -11.6514 0.0594 -0.1062 -0.0685 0.6444 0.2697 0.3747 -1.7164 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0337 -0.0804 0.2609 0.2710 0.3590 -1.6525 0.3784 -1.7166 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0857 0.0804 0.2709 0.3530 -1.6625 0.2908 0.2700 0.3520 -1.5968 19 26.41 -0.01 7.6238 -12.1731 0.0844 -0.1558 -0.0857 0.6319 0.27800 0.3520 -1.5968 19 26.41 -0.01 7.6238 -12.1731 0.0844 -0.1558 -0.0857 0.6319 0.27800 0.3520 -1.5968 12 25.55 0.01 8.3617 -12.44491 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0	9.79 -0.01 3.1922 -9.2331 -0.0024 0.0652 -0.0754 0.7111 0.2050 0.5061 -2.8924 7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.84 -0.01 4.0453 -10.4641 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4845 -2.5917 9 15.91 -0.01 4.0288 -10.5847 0.0263 -0.0084 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.6815 -10.7543 0.0147 0.0121 -0.0701 0.6618 0.2500 0.4079 -2.2972 11 17.98 -0.01 4.9917 -10.9413 0.0177 -0.0047 -0.0630 0.7243 0.2554 0.4385 -2.1963 12 19.06 -0.01 5.2475 -11.0701 0.0219 -0.0068 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2765 0.3839 -1.9984 13 20.08 -0.01 5.5716 -11.1340 0.0660 0.0774 -0.0739 0.6504 0.2765 0.3839 -1.9984 15 22.19 -0.01 6.2107 -11.4356 0.0443 -0.0385 -0.0652 0.6680 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2107 -11.4356 0.0443 -0.0392 -0.0666 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.6376 0.0435 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.4519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7166 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1737 0.0844 -0.1558 -0.0857 0.6319 0.7800 0.3520 -1.5968 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4483 12 20.11 -0.01 5.55476 -10.9321 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 12 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4483 12 20.11 -0.01 5.55476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.5346 12 20.11 -0.01 5.55476 -0.07221 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 12 20.11 -0.0404 0.0688 0.5801 0.3192 0.2609 -1.9705 12 20.11 -0.0404 0	
7 11.7y -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.84 -0.01 4.0453 -10.4841 0.0153 0.0047 -0.0836 0.7003 0.2158 0.4845 -2.5917 9 15.91 -0.01 4.4288 -10.5897 0.0267 -0.0086 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 16.96 -0.01 4.6815 -10.7543 0.0147 (.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0054 -0.0680 0.7243 0.2600 0.4643 -2.0936 13 20.06 -0.01 5.5716 -11.1340 0.0060 -0.0774 -0.0680 0.7243 0.2600 0.4643 -2.0936 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3839 -1.9984 15 72.19 -0.01 6.2107 -11.4356 0.0443 -0.6382 -0.0846 0.5993 0.2730 0.3263 -1.6395 16 23.25 -0.01 6.5553 -11.0376 0.043 -0.0552 -0.0686 0.5993 0.2730 0.3263 -1.6395 17 20.29 -0.01 6.9041 -11.8519 0.0043 -0.0554 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 20.29 -0.01 6.9041 -11.8519 0.0043 -0.0554 -0.0865 0.6444 0.2097 0.3747 -1.7166 0.2691 0.3469 -1.7753 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0162 -0.0865 0.6444 0.2097 0.3737 -1.7166 0.2691 0.3609 -1.96625 20 77.86 -0.01 8.3617 -17.4446 0.0740 -0.1558 -0.0857 0.6319 0.2600 0.3520 -1.5968 21 20.55 -0.01 8.3617 -17.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3249 -1.5346 22 29.66 -0.01 8.3617 -17.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3249 -1.5346 23 30.66 -0.01 8.3617 -17.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3249 -1.5346 24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0466 0.5881 0.3102 0.3210 0.3111 -1.4132 25 9.78 -0.01 3.1846 -9.2679 0.0027 0.0553 -0.0688 0.5881 0.3102 0.2609 -1.9705	7         11.79         -0.01         3.7029         -10.2936         0.0124         0.0297         -0.0823         0.7196         0.2088         0.5108         -2.7799           8         13.84         -0.01         4.0453         -10.4661         0.0153         0.0007         -0.0836         0.7003         0.2158         0.4845         -2.5917           9         15.91         -0.01         4.0815         -10.7583         0.0147         0.0121         -0.0774         0.6622         0.2397         0.4225         -2.3911           10         10.96         -0.01         4.6815         -10.7563         0.0147         0.0121         -0.0701         0.6618         0.2550         0.4079         -2.2972           11         17.98         -0.01         4.9817         -10.9413         0.0177         -0.0673         0.6938         0.2554         0.4385         -2.1963           12         19.06         -0.01         5.2875         -11.0701         0.0719         -0.0680         0.7243         0.2000         0.4643         -2.0936           12         19.06         -0.01         5.2875         -11.1340         0.0660         -0.0776         0.0650         0.2465         0.3889         -1.9984	7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.84 -0.01 4.0453 -10.4661 0.0153 0.0047 -0.0836 0.7003 0.2158 0.485 -2.5917 9 15.91 -0.01 4.4284 -10.5897 0.0263 -0.0086 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 16.96 -0.01 4.6815 -10.7543 0.0147 (0.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0047 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2475 -11.0701 0.0219 -0.0068 0.7243 0.2600 0.4643 -2.0936 13 20.04 -0.01 5.5716 -11.1340 0.0060 -0.0776 -0.0739 0.6506 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8483 -11.2644 0.6385 -0.0499 -0.0652 0.6088 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2167 -11.4356 0.0433 -0.6392 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.0376 0.0935 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 20.29 -0.01 6.9041 -11.6519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7164 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0084 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1739 0.0844 -0.1558 -0.0857 0.68319 0.2800 0.3520 -1.65968 20 27.86 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6252 0.2953 0.3299 -1.5346 21 20.55 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6252 0.2953 0.3299 -1.5346 22 29.66 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6252 0.2953 0.3299 -1.5346 23 30.66 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6252 0.2953 0.3299 -1.5346 24 20.11 -6.01 5.5476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3126 0.3221 -1.4491 25 9.76 -0.01 3.1846 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	7 11.79 -0.01 3.7029 -10.2936 0.0124 0.0297 -0.0823 0.7196 0.2088 0.5108 -2.7799 8 13.84 -0.01 4.0453 -10.4841 0.0153 0.0067 -0.0836 0.7003 0.2158 0.8845 -2.5917 9 15.91 -0.01 4.4288 -10.5897 0.0263 -0.0088 -0.0774 0.6622 0.2397 0.4225 -2.3911 10 16.96 -0.01 4.6815 -10.7543 0.0147 (.0121 -0.0701 0.6618 0.2550 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0087 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.06 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0600 0.7243 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6508 0.2765 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.0385 -0.0099 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2167 -11.4356 0.0433 -0.0557 -0.0847 0.0161 0.2691 0.3263 -1.6195 16 23.25 -0.01 6.5553 -11.0376 0.0433 -0.0557 -0.0846 0.5993 0.2730 0.3203 -1.6195 17 28.29 -0.01 6.9041 -11.8519 0.0594 -0.1062 -0.0865 0.6446 0.2697 0.3747 -1.7166 18 25.33 -0.01 7.2526 -12.05/3 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1734 0.0844 -0.1558 -0.0857 0.6319 0.7800 0.3520 -1.5968 20 27.88 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3299 -1.5346 21 20.55 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3299 -1.5346 22 29.60 -0.01 8.3617 -12.4446 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3299 -1.5346 23 27 -0.01 9.0803 -12.8380 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.8380 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.8380 0.0920 -0.1131 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1846 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4160 -2.9964	
13.86	8 13.6 -0.01	13.86	8 13.84 -0.01	
9 15.01 -0.01 4.428 -10.5897 0.0263 -0.008h -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.6815 -10.7543 0.0147 0.0121 -0.0701 0.6618 0.2554 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0064 -0.0633 0.6938 0.2554 0.4385 -2.1963 12 19.06 -0.01 5.2675 -11.0701 0.0219 -0.0068 0.7243 0.2600 0.4664 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.0385 -0.0499 -0.0652 0.6408 0.2705 0.3839 -1.9984 15 22.19 -0.01 6.2107 -11.4356 0.0435 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.9133 15 22.29 -0.01 6.5553 -11.6376 0.0435 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.8519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7166 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1733 0.0844 -0.1558 -0.0857 0.6319 0.2800 0.3520 -1.5968 21 20.55 -0.01 8.3617 -1.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.5968 22 29.60 -0.01 8.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 7.9646 -12.2228 0.0921 -0.0003 -0.0005 0.6252 0.2953 0.3229 -1.5968 24 20.11 -0.01 5.5478 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3110 0.3111 -1.4132 25 9.78 -0.01 3.1895 -9.2679 0.0027 0.0553 -0.0088 0.5801 0.3120 0.3111 -1.4132	15.91 -0.01	9 15.91 -0.01	9 15.91 -0.01 4.4288 -10.5897 0.0267 -0.008h -0.0774 0.6622 0.2397 0.4225 -2.3911 10 10.96 -0.01 4.6815 -10.7543 0.0147 G.0121 -0.0701 0.6618 0.2560 0.4079 -2.2972 11 17.98 -0.01 4.9817 -10.9413 0.0172 -G.0047 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.00 -0.01 5.2875 -11.0701 0.0219 -0.0008 -0.0680 0.7243 0.2600 0.4643 -2.0936 13 20.00 -0.01 5.5710 -11.1340 0.0060 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 72.19 -0.01 6.2107 -11.4356 0.0043 -0.6392 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.6376 0.0035 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.8519 0.0594 -0.1062 -0.0865 0.6444 0.2997 0.3747 -1.7166 18 25.33 -0.01 7.2526 -12.05/3 0.0329 -0.0685 0.6644 0.2997 0.3747 -1.7166 19 26.41 -0.01 7.6238 -12.1734 0.0844 -0.1558 -0.0857 0.6319 0.27800 0.3520 -1.5968 20 77.46 -0.01 7.9646 -12.2220 0.0321 -0.0003 -0.0655 0.6252 0.2953 0.3299 -1.5346 21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 22 29.60 -0.01 7.791 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.66 -0.01 9.0803 -12.818 0.0810 -0.0931 -0.0662 0.6889 0.2708 0.4160 -2.9964	
10	10	10	10	
11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.6880 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2765 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2167 -11.4356 0.0438 -0.0332 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.0376 0.0035 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.4519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7166 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.66238 -12.1734 0.0844 -0.1558 -0.0857 0.6319 0.2780 0.3520 -1.5968 20 27.46 -0.01 7.9646 -12.2220 0.0321 -0.0603 -0.0605 0.6252 0.2953 0.3299 -1.5346 21 20.55 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 22 29.66 -0.01 8.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.818 0.0010 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -6.01 5.5678 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2604	11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0677 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0048 -0.0680 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.6385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2167 -11.4356 0.0443 -0.6322 -0.0686 0.5993 0.2730 0.3263 -1.6395 16 23.25 -0.01 6.5553 -11.6376 0.0435 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.4519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7164 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1737 0.0844 -0.1558 -0.0857 0.6319 0.2800 0.3520 -1.5968 20 27.46 -0.01 7.9646 -12.2220 0.0321 -0.0603 0.6650 0.6252 0.2953 0.3299 -1.5346 21 20.55 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 22 29.60 -0.01 8.3617 -12.4444 0.0740 -0.0717 -0.0407 0.6273 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.4318 0.0610 -0.0931 -0.0668 0.5801 0.3126 0.3221 -1.4491 23 30.64 -0.01 5.5476 -10.9321 0.0313 -0.0664 0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1846 -9.2679 0.0027 0.0553 -0.0724 0.6689 0.2708 0.4180 -2.9964	11 17.98 -0.01 4.9817 -10.9413 0.0177 -G.0047 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -7.0048 -0.0680 0.7243 0.2600 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.4843 -11.2644 0.6385 -7.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 22.19 -0.01 6.2167 -11.4356 0.0443 -0.6342 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.6376 0.0435 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.4519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7164 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1734 0.0844 -0.1558 -0.0857 0.6319 0.27800 0.3520 -1.5968 20 27.46 -0.01 7.9646 -12.2220 0.0321 -0.0603 -0.0605 0.6252 0.2953 0.3299 -1.5346 21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883 22 29.60 -0.01 8.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.8318 0.0010 -0.0931 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1846 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9964	11 17.98 -0.01 4.9817 -10.9413 0.0177 -0.0647 -0.0673 0.6938 0.2554 0.4385 -2.1963 12 19.04 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.6880 0.7243 0.2000 0.4643 -2.0936 13 20.08 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.0385 -0.0499 -0.0652 0.6408 0.2705 0.3704 -1.9143 15 72.19 -0.01 6.2167 -11.4356 0.0443 -0.6392 -0.0686 0.5993 0.2730 0.3263 -1.6395 16 23.25 -0.01 6.5553 -11.6376 0.0635 -0.0557 -0.0847 0.6161 0.2691 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.6519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7164 18 25.33 -0.01 7.2526 -12.0573 0.0329 -0.0337 -0.0804 0.6250 0.2719 0.3530 -1.6625 19 26.41 -0.01 7.6238 -12.1739 0.0844 -0.1558 -0.0857 0.6319 0.2800 0.3520 -1.5968 20 77.48 -0.01 7.9646 -12.2220 0.0321 -0.0603 -0.0655 0.6444 0.3999 -1.5346 21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3248 -1.4883 22 29.66 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3248 -1.4883 23 30.64 -0.01 9.0803 -12.6138 0.0010 -0.0931 -0.0668 0.5801 0.3120 0.3111 -1.4132 24 20.11 -6.01 5.5478 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.0889 0.2708 0.4180 -2.9064	
12	12	12	12 19.00 -0.01 5.2875 -11.0701 0.0219 -0.0068 -0.0680 0.7243 0.2600 0.4643 -2:0936 13 20.00 -0.01 5.5716 -11.1340 0.0660 -0.0774 -0.0739 0.6504 0.2665 0.3839 -1.9984 14 21.13 -0.01 5.8843 -11.2644 0.0385 -0.0499 -0.0657 0.6408 0.2705 0.3704 -1.9143 15 72.19 -0.01 6.2167 -11.4356 0.0443 -0.0329 -0.0686 0.5993 0.2730 0.3263 -1.8395 16 23.25 -0.01 6.5553 -11.0376 0.0043 -0.0557 -0.0847 0.0161 0.2601 0.3469 -1.7753 17 24.29 -0.01 6.9041 -11.4519 0.0594 -0.1062 -0.0865 0.6444 0.2697 0.3747 -1.7166 18 25.33 -0.01 7.2526 -17.0573 0.0329 -0.0377 -0.0804 0.6250 0.2719 0.3530 -1.6625 20 27.46 -0.01 7.6238 -12.1731 0.0844 -0.1558 -0.0857 0.6319 0.2800 0.3520 -1.5968 21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3299 -1.5346 21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3299 -1.5346 21 20.56 -0.01 8.7191 -12.64550 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.0318 0.0710 -0.0931 -0.0662 0.6321 0.3210 0.3111 -1.4132 24 20.11 -6.01 5.5476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	
13	13	13	13	··
16	14	16	16	
15	15	15	15	
16	16	16	16	
18	18	18	18	
19	19	19	19	
20	20	20	20	
21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -14883 22 29.60 -0.01 P.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.8318 0.0810 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -0.01 5.5478 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1886 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883  22 29.60 -0.01 A.7191 -12.4350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491  23 30.64 -0.01 9.0803 -12.4318 0.0410 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132  24 20.11 -6.01 5.5476 -10.4321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705  25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883  22 29.60 -0.01 R.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491  23 30.64 -0.01 9.0803 -12.8318 0.0810 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132  24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705  25 9.76 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	21 20.55 -0.01 8.3617 -17.4444 0.0740 -0.0717 -0.0407 0.6273 0.3025 0.3748 -1.4883  22 29.60 -0.01 8.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491  23 30.64 -0.01 9.0803 -12.6318 0.0610 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132  24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705  25 9.76 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	
22	22 29.60 -0.01 A.7191 -12.6350 0.0920 -0.1131 -0.0263 0.6347 0.3126 0.3221 -1.4491 23 30.64 -0.01 9.0803 -12.m318 0.0m10 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -6.01 5.5476 -10.4321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	22 29.60 -0.01	22 29.60 -0.01	
23 30.64 -0.01 9.803 -12.m318 0.0m10 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.76 -0.01 3.1886 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	23 30.64 -0.01 9.0803 -12-m318 0.0m10 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -6.01 5.5476 -10.4321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	23 30.64 -0.01 9.0803 -12.m318 0.0m10 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	23 30.64 -0.01 9.0803 -12.m318 0.0m10 -0.0931 -0.0462 0.6321 0.3210 0.3111 -1.4132 24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	
24 20.11 -0.01 5.5476 -10.4321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.76 -0.01 3.1886 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	24 20.11 -6.01 5.5476 -10.4321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	24 20.11 -0.01 5.5476 -10.4321 0.0313 -0.0464 -0.0688 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	24 20.11 -0.01 5.5476 -10.9321 0.0313 -0.0464 -0.0668 0.5801 0.3192 0.2609 -1.9705 25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	
25 9.76 -0.01 3.1895 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4160 -2.9064	25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0726 0.6889 0.2708 0.4180 -2.9064	25 9.78 -0.01 3.1896 -9.2679 0.0027 0.0553 -0.0724 0.6889 0.2708 0.4180 -2.9064	
				<del></del>

	TEST	PART W	ACH RX10-	6 PHI	CONF	L JEL1	DELZ	DEL3 DEL4	TRANSIT	ON	
	1	125 0.	Pn 5.3	0.0	440F33	0.0		0 0			
POINT.	ALPHA	BETA	ĊN"	CLM	CY	CLN	CLL	CA	CAB	CAF	ACP
1	-0.00	-0.00	0.0332	-0.0914	-0.0181		-0.0731	0.3039	0.0934		-2,7476
2	1.97	0.00	0.6151	-1.7628	-0.0071	0.00ml	-0.0763	0.3158	0.0914	0.2743	-2.8658
_ 3	3.94	0.00	1.2314	-3.5631	0.0032	-0.0309	-0.0833	0.3550	0.0959		-2.8926
2	5.90 7.86	0.00	1.4763	-5.5014 -7.5736	0.0091		-0.0970	0.3356	0.0990		-2,9269
	9.84	-0.00	2.8665	-8.3710	-0.003+ -0.0565		-0.0337	0.3825 0.4639	0.0986	0.2842	-2.977 <u>2</u> -2.9203
7	11.65	-0.00		-8.6372		0.0072	-0.0611	0.5266	0.1461		-2.0254
8	13.84	0.00		-9.8303			-0.0743	0,5715	0.1409		-2.7562
9	15.99	0.00	3.9647	-10.0609	-0.0103	-0.0350	-0.0631	0.6048	0.2099	0.3949	-2.6690
10	16.88	0.00		-10.4606		0.0058	-0.0486	0.6158	0.2464	0.3694	-2.6331
11	17.88	-0.00		-11-1879		0.1102	-0-0555	0.6455	G.2551	0.3903	-2.5779
12	19.95	-0.01		-10.0664		0.2463 0.1019	-0.0108 -0.0150	0.6949	0.2594		-2.4678
14	19.94	-0.00		-10.6467		0.7019	-0.0085	0.7342	0.3847		-2,3795 -2,3848
15	20.94	-0.00		-10.9432		0.1403	-0.0550	0.7551	0.3922		-2.3309
16	21.96	-0.01		-11.3715			-0.0477	0.7736	0.4115		-2.3092
17	22.97	-0.01		-11.7236		0.1910	-0.0617		0.4301	0.3496	-2.2705
10	23.97	-0.02		-17.2469			-0.0899		0.4450		
20	24,99	-0.03		-12.5991		0.3529	-9.1224		0.4697		-2.2173
51	25.99	-0.04		-13.0266			-0.1538 -0.1739		0.4697		-2.164 <b>2</b> -2.157 <b>3</b>
<u>_55</u>	20.02	-0.06		-13.7527		0.3589	-0.27+1	0.7829	0.5186		-2.1360
23	29.04	-0.07		-14.2928			-0.2739		0.5227		-2.1077
24	30.06	-0.07		-14.5893			-0.2869		0.5278		-2.0695
25	19.94	-0.00		-10-6475			-0.0068		0.4783	0.2747	-2,3825
56	19.93	-0.00		-10-6706			-0.0105		0.4090		-2.3925
27	9.84	-0.01		-8.5562			-0.0284		0.2252		-2.9500
28	-0.01	-0.01	0.0366	-0.5000	-0.0311	0.1336	-0.0702	0.2826	0.1156	0.1671	-3.5556

											•	
	TEST	126 0.E		6 Pml	CONF 4m0F33 0	.O DEL	1 DEL2	DEL3 DEL4	TRANSITI	ON		
INT .	ALPHA	HETA	ċn	CLH	- CY	CLN		. CA	CAB -	CAF	#CP	
-	-0.00			-0.1612			-0.06A2	0.293?	0.6842		-3,4272	
2	1.96	-0.00	0.6022	-1.0773	-0.01+2	0.0554		0.2994	0.0946	0.2036	-2.9230	
3		-0.00	1.2440				-0.0744	0.3019	0.0993		-2,9234	
•		-0.00		-3.7393			-0.0789	0.2994	0.0946	0.2048		
5		-0.00 -0.00		-5.4613		0.0147 0.0097		0.3050	0.0822		-2.9569	
7		-0.00		-8.1847		-150.0-		0.3040 0.3256	0.1016		-2.9803 -3.0043	
8	9.84	-0.01		-8.3554		0.3447	-0.0041	0.4421	0.1496		-2.9329	
_	11.06			-8.9175		0.0897		0.5115	0.1706		-2.8328	
0	13.83	-0.00	3.6410	-10.1394	-0.0165	0.0315	-0.0806	0.5614	0.1966		-2.7848	
1	15.83	-0.00		-11-3007		0.0102		0.6102	0.2161	0.3942	-2.7366	
	16.84			-11.6735		0.0041		0.6220	0.2429		-2.6850	
	17.46	0.00		-11.7766			-0.0196	0.6420	0.2615		-2,6379	
		-0.01		-11.4115		0.2614	0.0060	0.7032	0.2806		-5.5231	
	19.92	-0.01		-11.2075			-0.0084	0.7347 0.7363	0.3229		<u>-2.4267</u> -2.4459	
		-0.01		-11.5918			-0.0099	0.7611	0.3723		-2.3837	
	21.93	-0.01		-11.9222			-0.0190	0.7704	0.4034		-2.3429	
		-0.04		-12.2770			-0.0673	0.7824	0.4193		-2.3142	
20	23.95	-0.02	5.6128	-12.8207	-0.0256	0.2518	-0.0746	0.7994	0.4375		-2.2842	
		-0.03	5.8654	-13.1813	-0.0161		-0.1111	0.6018	0.4508		-2.2471	
	26.01	-0.04	6.1320	-13.5539	0.0044		-0.1545	0.8020	0.4710	0.3310	-2.2101	
	27.02	-0.05		-13.7850	0.0766		-0.2122	0.7990	0.4986	0.3003	-2.1620	<u></u>
	20.04	-0.06		-13.8756	0.1911		-0.2540	0.7820	0.5124		-Z.1034	
<u>25</u> 26	30.11	-0.06	7 0474	-13.9595	0.3564	-0.1977	-0.2317	0.7390	0.5180		-2,0496 -1,9986	
	19.91	-0.01		-11.3291			-0.0092	0.7302	0.4375	0.2007	-2.4314	
		-0.01		-8.3773			-0.0037	0.4261	0.2144		-2.9362	
		-0.00		-0.1770			-0.0647		0.1012		-3.4870	
29	-0.00							0.2902				

	ENGINEE 1 OF 1 1 OF 1					MARTIN MI	ISSILE TA	MEL FACILITAL EFFECTS	PATA	AER	
<u> </u>	TEST	PART M	ACH RX10-		CONF 84#0F33	L DELI	DEL2	DEL3 DEL4	TRANSITI	ON	
THEO	ALPHA"	BETA	CN .	CLM	CA_	CI N	CLL	·CA .	CAB	CAF	XCP
1	-0.00	0.00		-0.1003	_		-0.0626	0.3699	0.0985		-2.9922
5	1.97	0.00		-1.5003				0.3680	0.0971		-2.6909
3	7.93	-0.00	1.2602	-3.6424			-0.0755	0.3450	0.0955		-2.8904
4	-	-0.01			-0.0232		-0.0947	0.3676	0.0799		-2.9585
5	7.85	-0.01			-0.0406		0.0113	0.4317	0.1007		-Z.9716
6	9.45	-0.01			-0.1734		0.2627	0.5196	0.1354		-2.8712
7	111	<u>-0.01</u>			-0.2165		0.3227	0.5832	0.1584		-2.9137
Ğ.	13.51	-0.01			-0.0149		-0.0972		0.2235		-2.8364
. 9	15.79	-0.00			-0.0097		-0.0613	0.6680	0.2617		-2.6007
10 11	16.51 17.42	0.00 0.0u			-0.0110		-0.0301	0.6812 0.6865	0.2652 0.2903	0.4161	-2.7478 -2.6751
15	18.84	0.00			-0.0263	0.0123	-0.0186	0.6970	0.3019		-2.6091
13	19.66	-0.00			-0.0468		0.0071	0.7144	0.3028		-2.5367
14	PA.05	-0.01	5.1691	-12-7-87	-0.1164	0.4324	0.0635	0.7776	0.3141	0.4634	
15	21.41	-0.01			-0.0156		-0.0476		0.3466		-2.3996
16	22.94	-0.02			0.0041	0.1337	-0.0655		0.4613		-2.3209
17	23,97	-0.02	5.7475	-13.0411	-0.0131	0.21.7	-0.0722	0.8270	0.4874	0.3396	-2.2690
18	25.00				0.0106		-0.0779	8058.0	0.4894		-5.5010 ·
19	25.03	-0.03	6.2179	-13.3359	0.0549	0.1931	-0.1082		0.5093		-2.1446
20	27.05	-0.03			0.1259		-0.1229		0.5163	0.2783	
21	28.11	-0.04			0.2597				0.5111		-1.9950
22	29.15	-0.02			0.2184				0.5203		-1.9125
23		-0.01				-0.1566			0.5325		-1.8539
	19.87				-0.0499				0.4184		-2.5209
25	-0,00	-0.05			-0.1853	0.6977			0.2573		-2.8796
	-0.00		0-0-72	-0-130	0-0028	-0.0013	-0.0003	0.3653	0.1080		-2.7150 -3.0354

/ E	ENGINEE 1 OF 1 1 OF 1					ROPULSION MARTIN M	ISSILE TAI	NEL FACILI'	TY (PUT) _ DATA	AER	ODYNAMIC WIN	D TUNNEL (4T)
	TEST	PART M.	ACH HX10- 94 2.3	6 PHI 0.0 H	CONF 440F33 0		0 0		TRANSITI			
DINT	ALPHA	HETA	CN	CLM	C4	CLN	CFF	CA	CAB	CAF	ACP	· - · · · - · - · · - · · · · ·
1	-0.00	-0.00	0.0414	-0.106h	-0.0072		-0.0673	0.4297	0.0982	0.3315	-2,5751	
2	1.97	0.00	0.5589	-1.5004	0.0103	-0.0436	-0.0788	0.4125	0.1110		-2.6952	•
3	3.92	-0.00	1.2550	-3.5738	-0.0029	0.0132	-0.0856	2+0+0	0.1034		-2.8477	
•	5.87	-0.01		-5.6395	-0.0177		-0.1014	0.4150	0.1073		-2.9743	
) 2	7.84 9.83	-0.01		-7.9012	-0.0501		-0.0077	0.4641	0.1133		-3.0147	<del></del>
7	11.40	-0.04		-8.7093 -10.3149		0.6142	0.2927 0.3267	0.5531 0.6185	0.1374 0.1623		-2.9405 -2.9000	
-6	13.81	-0.01		-10.951-		0.0602	-0.0966	0.6333	0.1961		-2.8350	
9	15.79	-0.00		-12.2500		-0.0133	-0.9758	0.6767	0.2462		-2.7920	
10	16.80	0.00		-12.3804			-0.0488	0.6767	0.2695		-2.7208	
ii	17.A3	0.00		-12.4275		0.0045		0.6832	0.2799		-2.6446	
12	18.95	0.60		-12.5675		-0.0053	-0.0284	0.6876	0.2998		-2.5802	
13	19.A7	0.00	-	-12.5325			-0.0238	0.6969	0.3099		-2.5091	
14	20.84	-0.00	5.1934	-12.6444	-0.0hl3	0.2721	0.0036	0.7310	0.3190		-2.4443	
15	21.91	-0.02		-12.6632			0.0678	0.7800	6.3266	0.4534	2.3637	
16	22.95	-0.01		-12.7626			-0.0429	0.6154	0.3542		-2.2967	
17	23.96	-0.02		-12-9194			-0.0570	0.8254	0.3977		-S.5336	
18	25.00	-0.0ż		-13.0609	0.0150	0.1493		0.8104	0.4324	0.3780	-5.1663	
19	26.05	-0.02		-13.1816		C-1033		0.6086	0.4636		-2.1003	
50	27.10	-0.00		-13.2973			-0.0698	0.7617	0.4767		-2.0274	
<u> </u>	_28.13 29.16	-0.03		-13.4334		-0.2225		_ 0.7788 _	0.4899		-1.9468	<del></del>
2 <b>3</b>	30.24			-13.7961		-0.1114		0.7699 0.7057	0.5054		-1.8508 -1.7831	
24	19.88			-12.3631			-0.0200	0.6719	0.4614		-2.4611	
25	9.82			-8.8215	-0.1527			0.5359	0.3065		-2.9495	
26	6.06	-0.01		-6.0566			-0.1058	0.4419	0.1965		-3.0326	
27	111111	-0.00				0.0289		0.4158			-2,6635	
				<u>.</u>	. ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			** 12 - 5				
	•											
·												<del></del>

-6521 0.00~2 -0.0 -7576 0.0046 -0.0 -7576 0.0046 -0.0 -0541 -0.0141 0.0 -1619 -0.0146 0.0 -5747 -0.0179 0.6 -1369 -0.038 0.1 -6332 -0.0096 0.0 -9341 -0.1799 0.6 -9341 -0.1799 0.6 -2089 -0.0127 -0.0 -2089 -0.0127 -0.0 -2089 -0.0127 -0.0 -2395 -0.0276 0.0 -2395 -0.0276 0.0 -3367 -0.0156 0.0 -5132 -0.0156 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DEL3 DEL4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	UNKROWN  CAR  0-1110  0-1157  0-1158  0-1267  0-1163  0-1436  0-1679  0-1642  0-1662  0-2717  0-2945  0-2956  0-3051	CAF 0,3508 0.3457 0.3610 0.3454 0.3868 0.3859 0.3923 0.4556 0.5057 0.4080 0.3939 0.3939	-2.7747 -2.9201 -3.0248 -3.0310 -3.0905 -3.0263 -3.0009 -2.8636 -2.7650 -2.6732 -2.6847 -2.6114
-1205 -0.0102 0.0 -6521 0.0062 -0.0 -7576 0.0066 -0.0 -0561 -0.0161 0.0 -0561 -0.0164 0.0 -1619 -0.0166 0.0 -5747 -0.0179 0.0 -1369 -0.038 0.1 -8332 -0.0096 0.0 -9341 -0.1799 0.6 -9341 -0.1799 0.6 -0837 -0.016 0.0 -2089 -0.017 -0.0 -2089 -0.017 -0.0 -2395 -0.0276 0.0 -2395 -0.0276 0.0 -3467 -0.0156 0.0 -5743 -0.0156 0.0 -5743 -0.0156 0.0	11	0.4617 0.4614 0.4764 0.5051 0.5051 0.5295 0.5602 0.6194 0.6797 0.6811 0.6831 0.6835 0.6986 0.7073	0.1110 0.1157 0.1158 0.1267 0.1163 0.1436 0.1679 0.1662 0.1662 0.2717 0.2945 0.2995 0.3051	0.3508 0.3457 0.3610 0.3454 0.3859 0.3923 0.4556 0.5057 0.4080 0.38666 0.3939	-2.9548 -2.7747 -2.9201 -3.0248 -3.0318 -3.0905 -3.0263 -3.0009 -2.8836 -2.7658 -2.6732 -2.6847 -2.6114
-0521 0.0002 -0.0 -7570 0.0046 -0.0 -7570 0.0046 -0.0 -0541 -0.0141 0.0 -1619 -0.0146 0.0 -5747 -0.0179 0.6 -1369 -0.038 0.1 -6332 -0.0096 0.0 -9341 -0.1799 0.6 -9341 -0.1799 0.6 -2089 -0.0127 -0.0 -2089 -0.0127 -0.0 -2089 -0.0127 -0.0 -2395 -0.0276 0.0 -2395 -0.0276 0.0 -34406 -0.0156 0.0 -5743 -0.0156 0.0		0.4614 0.476A 0.4721 0.5051 0.5295 0.5602 0.619A 0.6919 0.6797 0.6811 0.6865 0.6986	0.1157 0.1158 0.1267 0.1163 0.1436 0.1679 0.1642 0.1862 0.2717 0.2945 0.2956 0.3051	0.3457 0.3610 0.3454 0.3859 0.3059 0.3923 0.4556 0.5057 0.4080 0.3966 0.3939	-2.7747 -2.9201 -3.0248 -3.0310 -3.0905 -3.0263 -3.0009 -2.8636 -2.7650 -2.6732 -2.6847 -2.6114
0.7576 0.0046 -0.0 0.0641 -0.0141 0.0 0.1619 -0.0146 0.0 0.5747 -0.0179 0.0 0.1369 -0.0338 0.1 0.8332 -0.0096 0.0 0.9341 -0.1799 0.6 0.2089 -0.0127 -0.0 0.2089 -0.0127 -	0047 -0.0856 0794 -0.1080 0793 -0.1087 9955 -0.1059 1414 -0.0215 0406 -0.0856 0.2980 0.154 -0.0826 0.078 -0.0675 0.071 -0.0675 0.071 -0.0675 0.0131 -0.0435 0.0142 -0.0342 0.008 -0.0188	0.476A 0.4721 0.5051 0.5295 0.5602 0.619A 0.6919 0.6797 0.6811 0.6865 0.6986	0.1158 0.1267 0.1163 0.1436 0.1679 0.1642 0.1862 0.2717 0.2945 0.2995 0.3051	0.3610 0.3454 0.3868 0.3859 0.3923 0.4556 0.5057 0.4080 0.3866 0.3939	-2.9201 -3.0248 -3.0310 -3.0905 -3.0263 -3.0009 -2.8836 -2.7650 -2.6732 -2.6847 -2.6114
-0841 -0.0141 0.0 -1619 -0.0146 0.0 -5747 -0.0179 0.0 -1369 -0.0338 0.1 -9341 -0.1749 0.6 -9341 -0.1749 0.6 -2089 -0.0127 -0.0 -2089 -0.0127 -0.0 -2395 -0.0276 0.0 -2395 -0.0276 0.0 -33467 -0.0115 0.0 -3440 -0.0763 0.0 -45132 -0.0156 0.0 -5743 -0.0520 0.3	0794 -0.1080 0793 -0.1087 0925 -0.1059 1414 -0.0215 0406 -0.0856 05460 -0.0826 0076 -0.0672 0071 -0.0672 00131 -0.0435 00132 -0.0342 00665 -0.0231 00608 -0.0188	0.4721 0.5051 0.5295 0.5602 0.6619P 0.6797 0.6811 0.6831 0.6835 0.6986	0.1267 0.1163 0.1436 0.1679 0.1642 0.1862 0.2717 0.2945 0.2992 0.2958	0.3454 0.3868 0.3859 0.3923 0.4556 0.5057 0.4080 0.3866 0.3939 0.3907	-3.0248 -3.0310 -3.0905 -3.0263 -3.0009 -2.8636 -2.7650 -2.6732 -2.6447 -2.6114
-1619 -0.0146 0.0 -5747 -0.0179 0.0 -1369 -0.0338 0.1 -8332 -0.0096 0.0 -9341 -0.1799 0.6 -0.037 -0.016 0.0 -2089 -0.0127 -0.0 -1652 -0.0180 0.0 -2395 -0.0276 0.0 -3395 -0.0276 0.0 -3395 -0.0156 0.0 -5132 -0.0156 0.0 -5132 -0.0156 0.0	793 -0.1087 995 -0.1059 1414 -0.0215 0406 -0.0826 0.2980 0154 -0.0826 0078 -0.0561 0071 -0.0672 00132 -0.0435 00182 -0.0342 00665 -0.0231 0008 -0.0188	0.5051 0.5295 0.5602 0.6194 0.6797 0.6811 0.6831 0.685 0.6986	0.1163 0.1436 0.1679 0.1642 0.1862 0.2717 0.2945 0.2995 0.3051	0.3868 0.3059 0.3923 0.4556 0.5057 0.4080 0.3866 0.3939 0.3907	-3.0310 -3.0905 -3.0263 -3.0009 -2.8836 -2.7650 -2.6732 -2.6847 -2.6114
-5747 -0.0179 0.0 -1369 -0.0338 0.1 -8332 -0.0096 0.0 -9341 -0.1799 0.6 -0837 -0.0116 0.0 -2089 -0.0127 -0.0 -1652 -0.0180 0.0 -2395 -0.0276 0.0 -3467 -0.0115 0.0 -4406 -0.0763 0.0 -5132 -0.0156 0.0 -5132 -0.0156 0.0	0945 -0.1059 1414 -0.0215 0406 -0.0854 0.2940 0.154 -0.0826 0.078 -0.0561 0.071 -0.0435 0.131 -0.0435 0.132 -0.0342 0.0665 -0.0231 0.008 -0.0188	0.5295 0.5602 0.6197 0.6919 0.6797 0.6831 0.6835 0.6865 0.6986	0.1436 0.1679 0.1642 0.1862 0.2717 0.2945 0.2958 0.3051	0.3059 0.3923 0.4556 0.5057 0.4080 0.3866 0.3939 0.3907	-3.0905 -3.0263 -3.0009 -2.8836 -2.7650 -2.6932 -2.6847 -2.6114
-136v -0.033h	1616 -0.0215 1646 -0.0856 1056 -0.0826 1057 -0.0561 1071 -0.0672 1012 -0.0435 10565 -0.0231 10508 -0.0188	0.5602 0.619A 0.6919 0.6797 0.6811 0.6831 0.6865 0.0986 0.7073	0.1679 0.1642 0.1862 0.2717 0.2945 0.2892 0.2958	0.3923 0.4556 0.5057 0.4080 0.3866 0.3939 0.3907	-3.0263 -3.0009 -2.8036 -2.7650 -2.6732 -2.6847 -2.6114
.8332 -0.0096 0.0 .9341 -0.1799 0.6 .0837 -0.0116 0.0 .2089 -0.0127 -0.0 .1652 -0.0180 0.0 .2395 -0.0276 0.0 .3-67 -0.0115 0.0 .4-406 -0.0763 0.0 .5132 -0.0156 0.0 .5743 -0.0920 0.3	0406 -0.0854 0.2980 0154 -0.0826 0078 -0.0561 0071 -0.0672 0131 -0.0435 0142 -0.0342 0665 -0.0231 0608 -0.0188	0.619P 0.6919 0.6797 0.6811 0.6831 0.6865 0.6986	0.1642 0.1862 0.2717 0.2945 0.2992 0.2958	0.4556 0.5057 0.4080 0.3866 0.3939 0.3907	-3.009 -2.8836 -2.7650 -2.6732 -2.6847 -2.6114
-9341 -0.1749 0.6 -0.037 -0.0116 0.0 -2089 -0.0127 -0.0 -1652 -0.0180 0.0 -2395 -0.0276 0.0 -3367 -0.0115 0.0 -3367 -0.0156 0.0 -5132 -0.0156 0.0 -5132 -0.0156 0.0	0.2980 0154 -0.0826 0078 -0.0561 0071 -0.0672 0131 -0.0435 0142 -0.0342 0665 -0.0231 0608 -0.0188	0.6919 0.6797 0.6811 0.6831 0.6865 0.6986 0.7073	0.1862 0.2717 0.2945 0.2992 0.2958	0.5057 0.4080 0.3866 0.3939 0.3907	-2,8836 -2,7650 -2,6732 -2,6847 -2,6114
2-0837 -0.0116 0.0 2-2089 -0.0127 -0.0 2-1652 -0.0180 0.0 2-2395 -0.0276 0.0 2-3467 -0.0115 0.0 2-4406 -0.0763 0.0 2-5132 -0.0156 0.0 2-5743 -0.0520 0.3	0154 -0.0826 0078 -0.0561 0071 -0.0672 0131 -0.0435 0132 -0.0342 0665 -0.0231 0608 -0.0188	0.6797 0.6811 0.6831 0.6865 0.6986 0.7073	0.2717 0.2945 0.2992 0.2958	0.4080 0.3866 0.3939 0.3907	-2.7650 -2.6732 -2.6847 -2.6114
2-2089 -0.0127 -0.0 2-1652 -0.0180 0.0 2-2395 -0.0276 0.0 2-3367 -0.0115 0.0 2-4006 -0.0763 0.0 2-5132 -0.0156 0.0 2-5743 -0.0520 0.3	0078 -0.0561 0071 -0.0672 0131 -0.0435 0192 -0.0342 0665 -0.0231 0608 -0.0168	0.6811 0.6831 0.6865 0.6986 0.7073	0.2945 0.2992 0.2958 0.3051	0.3866 0.3939 0.3907	-2.6932 -2.6847 -7.6114
2-1652 -0.0180 0.0 2-2395 -0.0276 0.0 1-3-67 -0.0115 0.0 1-4-06 -0.0763 0.0 1-5132 -0.0156 0.0 1-57-3 -0.0520 0.3	0071 -0.0672 0131 -0.0435 0142 -0.0342 0665 -0.0231 0608 -0.0168	0.6865 0.6865 0.6986 0.7073	0.2992 0.2958 0.3051	0.3939	-2.6847 -2.6114
2.3-67 -0.0115 0.0 2.4-06 -0.0763 0.0 2.5132 -0.0158 0.0 2.57-3 -0.0920 0.3	0132 -0.0342 0665 -0.0231 0608 -0.0186	0.6986 0.7073	0.3051		
2.4406 -0.0763 0.0 2.5132 -0.0158 0.0 2.5743 -0.0620 0.3	0665 -0.0231 0608 -0.0168	0.7073		A. 303E	
2.5132 -0.0156 0.0 2.57-3 -0.0620 0.3	0608 -0.0168				-2,5375
2.57-3 -0.0620 0.3		0.7126		0.3958	2.4672
	3310 0-0056				-2.3954
		0.7538	0.3298		2.3133
	5176 0.0463	0.7949	0.3583		-2.2374
	3900 <u>0.0128</u> 2354 -0.0113	0.8040	0.4443		-2.1638 -2.0929
	1530 -0.0140	0.8086	0.4511		-5.0568
	0030 -0.0208	0.7870	0.4960		-1.9570
					-1.6776
		0.7786	0.5152		-1.8577
		0.7640	0.5225		-1.7776
3.7802 0.0628 -0.0		0.7596	0.5330	9922.0	-1.719 <u>7</u>
		0.6824	0.4741		-2.4510
		0.5619	0.2994		-3.0536
0.1676 -0.0165 0.0	0692 -0.0676	0.4637	0.1598	0.3038	-3.0857
3.	1698 0.1034 0. 3653 0.1602 -0. 3492 0.1767 -0. 6325 0.0607 -0. 7802 0.0626 -0. 2669 -0.0261 0. 6241 -0.0334 0.	.1698	1698	1698	1698

GE	OF 1	ING DE	YELOPHEN1	CENTERIA	EDC) PI		WIND TUNI			AER	ÖNIF J <u>îm</u> vmāc	TUNNEL (4T)
	TEST	PART H 131 0.	ACH RX10-		CONF 4=0F33 0	L DEL	0 0		TRANSITI			•
THIO	ALPHA	BETA	CN	CL#	CY	CLN	CLL	CA	CAB	CAF	XCP	
1	-0.00	-0.00	0.0394	-0-1175		0.0900	-0.0663	0.5075	0.1121	0.3954	-2.9816	
S	1.96	-0.00	0.6222	-1.7941	-0.0047	0.0296	-0.0727	0.5125	0.1220	0.3905	-2.8833	
<u>-3</u>	1.96 3.93	-0.00	0.6247 1.3259	-1.7989 -3.8569	0.0080	0.0371	-0.0708	0.5183 0.5159	0.1205	0.3978_	-2.8795	
5	5.86	-0.01	5.0543	-6.1863	-0.0142	0.0681	-0.1012	0.5468	0.1319		-2.90 <b>89</b> -3.0560	
₹	7.78	-0.00	2.7826		-0.0139	0.0490	-0.1078	0.5890	-0.1520		-3.1171	
7	7.79	-0.01		-8.7573	-0.0121	0.0666	-0.1102	0.5966	0.1825	0.4140	-3,1256	
8	9.75	-0.01		-10-6612	-0.0126	0.0591	-0.0970	0,6273	0.1980	0.4293	-3.9878	
9	11.73	-0.01.		-11.6941	-0.0175	0.0649	-0.0807	0.6814	0.1921		-2.9856	
0	13.78	-0.00	4.1207	-11.7508	-0.1418	0.5145	0.2772	0.7096	0.2233	0.4862	-2.8517	
1	15.81	-0.00		-11.8766	-0.0106	0.0259	-0.0811	_0.7033	0.2562		-2.7271	
Z	16.82	-0.00		-11.9926	-0.0203	0.0319	-0.0706	0.6855	0.2587	0.3968	-2.6617	
3	17.85	-0.00		-12-0372	-0.0173	0.0220	-0.0583	0.6994	0.2829	0.4165	-2.5706	
ļ o	18.87	-0.00		-12-2177	-0.0349	0.0565	-0.0353	0.6834	0.3192	0.3642	-2.5158	
15 16		-0.00	4 8626	-12.1213	-0.0314	0.0447	_ =0.0566 =0.0445	0.6858	_ 0.3098 . 0.3256	0.3759_ 0.3640	-2.4842 -2.4927	<del></del>
17		-0.01		-12-2774	-0.0240	0.0767	-0.0434	0.6920	0.3432		-2.4311	
i 6	19.91			-17.7091	-0.0049	0.0417	-0.0606	0.6882	0.3296	0.3587	-2.4074	
19	20.93		5.7725	-12.3478	-0.0107	4580.0	-0.0390	0.7010	0.3476	0.3534	-2.3419	
20	21.96	-0.01	5.4R21	-12.4188	0.0167	0.0906	-0-0407	0.7059	0.3606	0.3453	-2.2653	
21	23.00	-0.01		-17.5772	-0.0774	0.3917	0.0519	0.7793	0.3629	0.4164	-2-1747	
22		-0.02		-12.6512	-0.0681	0.4977	0.1083	0.8069	0.3788		-2.0904	
23	25.09	-0.02		-12 <u>-6</u> 315	-0.0351	0.3598	0.0770	0.8077	0.4035		-2.0248	
25		-0.01		-13.1312	0.0855	0.0572	0.0374	0.7920	0.4619		-1.8956	
26		-0.01		~13.1385	0.0596	0.1346	0.0625	0.8076	0.4636		-1.8666	
27	29.23	-0.01		-13.2892	0.1263	-0.0530	0.0709	0.7952	0.4941		-1.7920 .	
28 <u> </u>	29.30 30.34	0.01		-13.5221 -13.7294	0.0536	-0.0174	0.0448_	0.7758_	0.5056		-1.7139	·
30		-0.00 -0.01		-12.0173	0.0359	0.1160	0.0200 -0.0553	0.7643	0.5265 0.3452		-1.66 <b>36</b> -2.3860	
31	9.74	-0.01		-10.8066		0.0755		0.6332	0.2726		-3.1037	
32		-0.00		-0-1197		0.1010		0.5044	0.1152		-2.7462	
								******		- 043071	-201102	
<u> </u>	-0000	-0000	000435	-,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-0000203		-446042	01304		043641	-201402	
			· · · · · · · · · · · · · · · · · · ·									

	TEST 1	PART P	ACH RX10- 10 2.3		CONF 4=0F33 0		0 OELZ	OEL3 DEL4	TRANSITI			
lit"	ALPHA	BETA	CN	CLH "	CY	CLN	CLL	CA.	CAB	CAF	XCP	
1	-0.00	-0.01	0.0391	-0.1259	-0.0462	0.1779	-0.0603	0.7248	0.2161	0.5086	-3.2186	
2	1.95	-0.01	0.6737	-1.9905	-0.0264	0.1087	-0.0556	0.7213	0.2193	0.5020	-2.9547	
	1.95 3.90	-0.01 -0.01	0.6766	-1.9961 -4.1149	-0.0262	0.1037	-0.0543	_ 0.7223 0.7277	0.2168		-2.9501 -3.0179	<del></del>
5	5.83	-0.01	2.0697	-6.3824	-0.0177	0.0872	-0.0919	0.7477	0.2215		-3.0837	
6		-0.01		-R. 6/84	-0.0194	0.0664	-0.0957	0.7797	0.2292	0.5506	-3,1107	
7	9.74	-0.01	3.4210	-10.5233	-0.0129	0.0436	-0.0987	0.8101	0.2412	0.5689	-3.0761	
8	11.77	-0.01		-1n.7556	-0.0032	0.0440	-0.0995	0.7936	0.2558	0.5378	-2.8878	<del>-</del>
<b>9</b>	13.62	-0.01		-10.9375	0.0123_	0.0571	0.0858	0.7972	0.2627		-2.7177	
0		-0.01 -0.01		-11-1267 -11-0345	-0.0165 -0.1125	0.0523	-0.0711 0.1506	0.7923	0.2671	0.5252		
ļ —	15.85	-0.01		-11.1406	-0.1309	0.4721	0.1853	0.7893	0.3025	0.4982	-2.5612 -2.4818	
•	18.94	-0.01		-11.3064	-0.0332	0.1131	-0.0430	0.7911	0.3320	0.4592	-2.3250	
5	19.97	-0.01		-11.4326	-0.0258	0.1457	-0.0561	6.7939	0.3413	0.4526	-2.2416	
6	21.01	-0.01	5.3923	-11-5903	-0.0171	0.1446	-0.0597	0.8131	0.3537	0,4593	-2.1494	
7	22.06	-0.02		-11.7249	0.0132	0.0898	-0.0608	0.7991	0.3593		-2,0623	
8_	23.11	0.01_		-11.8950	0.0239_	0.0535	-0.0517	0.8124	0.3670	0.4454	-1.9836	
9	24.14	-0.01		-12.0442	0.0311	0.0976	-0.0117	0.8060	0.3669	0.4391	-1.9069	
<u>0</u>	26.25	-0.01		-12.2016	0.0233	0.1003	0.0104	0.8057	0.3694	0.4426	-1.8338 -1.7700	
2	27.31	-0.00		-12.6143	0.0252	0.0727	0.0540	0.8245	0.3815	0.4430	-1.6955	
3	28.38	-0.00		-12.7982	0.0369	0.0666	0.0744	0.8523	0.3893	0.4630	-1.6323	
•	29.43	-0.00		-12.9731	-0.0384	0.1710	0.0225	0.7976	0.3994		-1.5851 -	
5	30.47	-0.01	A.5249	-13-1458	-0.0628	0.2668	-0.0062	0.7866	0.4140	0.3726	-1.5421	
6	19.98	-0.02		-11.2458	-0.0418	0.2316	-0.0465	0.6100	0.4030	0.2070	-7.2196	
7	9.74	-0.01		-10.2977	-0.0125	0.0593	-0.0914	0.8021	0.3265	0.4756	-3.0529	
•	9.74	-0.01		-16-3571	0.0077	0.0436	-0.0918		0.2824		-3.0658	
	-0.01	-0.01	0.0314	-0.1719	-0.0479	0.1939	-0.0543	0.7280	0.2067	0.5217	-3.3450	

	TEST	PART MA 133 1.	ACH RX10-		CONF 14m0F33	LDEI	DELS	DEL3 DEL4		DN		
INT	ALPHA .	BETA		CLH	CY	CLN	- : CLL	CA	CAS	CAF	ACP	·
1	-0.01	0.00	0.0393	-0.1465	0.0072		-0.0426		0.1876	0.5181	-3.7225	
5	-0.01	0.00	0.0354	-0.13/4	0.0071	-0.6161	-0.0426		0.1969	0,5087	-3.8774	
<del>,</del> -	0.00	-0.00	0.0241	-0.0378	-0.0154	_	0.0476		0.2187		-1.5661_	
	1.95 3.89	0.00 -0.00	0.6786 1.3476	-2.0173 -4.0974	-0.0025	-0.0034	-0.0471		0.2197 0.2154		-2 <b>.9</b> 726 -3.04 <b>05</b>	
-6	5.83	-0.00	2.0151	-6.1792	0.003¢				0.2161	0.5581	-3.0664	
7	7.78	-0.00	2.6573	-8.1151	0.0170				0.2163	0.5966	-3.0539	
8	9.73	0.00	3.3044	-9.7687	0.0175		-0.0890		0.2245	0.6240	-3,0168	
9	11.78	-0.01		-10.2961	0.0248				0.2347	0.6028	-2.8337	
0	. 13.83	-0.00	3.9465	-10.4542	0.0173	-0.0361	-0.0829	0.8244	0.2458	0.5786	-2.6490	
<u> </u>	15.88	-0.00		-10.6222	0.0166	-0.0545	-0.0730	0.7895	0.2740	0.5154	2.4689_	•
12	16.97	-0.00		-10.7378	0.0027				0.2526	0.5074	-2.3723	
3	17.94	-0.00		-10-054-	0.0151				0.2912	0.5234	-2.2902	<del></del>
4	19.00	-0.00		-10.9650	0.0094			The state of the s	0.2966	0.5349	-2.2053	
15 16 "	20.04	-0.01 -0.01		-11.1246 -11.2946	0.0163 0.0561		_		0.3099	_0.5066	2.1077_	
7	27.15	-0.01		-11.4648	-0.0003				0.3378 0.3516	0.4968	-2.0196 -1.9337	
8	23.19	-0.01		-11.5056	0.0275				0.3559	0.5079		
9	24.27	-0.01		-11-770+	0.0504		-0.0520		0.3615	0.4528	-1.7870	
20	25.34	-0.01		-11-9432	0.0705				0.3721	0.3825	-1.7203	
21	26.35	-0.01	7.2892	-12-1371	0.0560	-0.0647	-0.0376	0.8392	0.3730	0.4662	-1.6651	
55	27.41	-0.01	7.6777	-12.3242	U.1123			0.9164	0.3748	0.5416	-1.6052	
23_		-0.01		-15-2386	0.0Bd4		,		0.3A21_	0.4335	1.5544_	
24	29.59		6.0	-17.7164	0.0975				0.3A02	0.3844		
25	30.57	-0.01		-12.8915	0.1045				0.3828	0.4231	-1.4689	
26 27	20.35 9.78	-0.00		-10.9513	0.0053				0.3559	0.4028	-2.0875	
28	-0.00	-0.00		-9.8336 -0.0714	0.0211				_0.26 <b>26</b> _ _0.22 <b>86</b>	0.5649 0.4969		
	-0000	-0800	0.02-03	-00011-	-000201	0.000	-00000	001233	0.22.00	0.4707	-619469	
												······································
			-				·		· · · · · ·			
			<del></del>									
						·	-					

HOLD GE EET	1 OF 1	RING DEV	LLOPHENT	CENTER (A	<u>E</u> DC)P			NEL FACILI IL EFFECTS		AER	ODYNAMIC WIND TUNNEL	. (67)
	7ES <u>7</u>	PART MA	CM BK10-		CDMF 4=0F33 0	LDEL	1 DEL2	DEL3 DEL4	TRANSITI			
ČINT	ALPHA	BETA		CLH -	CA	CLN	<u>cu</u>	CA	CAB	CAF	XCP	
<u> </u>	1.94	-0.00	-0.0191	-1.6612	-0.0164	0.0669	-0.0412	0.6622	0.2083	0.4539	-6,4179	
3	3.91	-0.00	0.6297	-3.8306	-0.0119	0.0557	-0.0566	0.6724 0.6854	0.2061	0.4663	-2.9555 -3.02 <b>06</b>	
•	5.91	-0.00		-5.7557	-0.0061	0.0417	-0.0636	0.7222	0.1969		-3.0113	
_5	7.87	_0.00_		-7-4909	0.0045	0.0110	-0.0776	0.7643	0.2070		-2,9755	
6	9.78	-0.00		-9-1403	0-0092	-0.0155	-0.0837	0.0022	0.5501		-2.9316	
8	11.78	-0.00		-10-1044	0.0202	-0.0460	-0.0801 -0.0675	0.8254	0.2345	0.5540	-2.8097 -2.6054	
9	15.90	-0.00		-10.4889	0.0113	-0.0396	-0.0591	0.7789	0.2578	0.5210	-2.6173	
īo	16.95	-0.00		-10.6016	0.0072	-0.0046	-0.0555	0.6090	0.2654		-2.3179	
11	18.01	-0.00		-10.7415	0.0097	-0.0071	-0.0495	0.8024	0.2718		-Z.2129	
15	19.04	-0.00		-10-6960	0.0068	0.0001	-0.0409	0.7748	0.2780	0.4968	-2.1162	
13	20.10	-0.01		-11-0192	0.0077	0.0062	-0.0361	0.7602	0.28444	0.4758		
14	21.13	-0.01		-11-1974	0.0218	0.0005	-0.0396	0.7516	0.2868	0.4648	-1.9409	
15 16	23.25	-0.00 -0.01		<u>-11.3216</u> -11.4740	0.0404 0.0404	-0.0028		0.7434_ 0.7279	0.2916 0.2955	0.4519.	-1.8680	
17	24.36			-11-6419	0.0445	-0.0029	-0.0406	0.7692	0.3029		-1.7308	
ie —		-0.01		-11.7991	0.0483	-0.0093	-0.0441	0.7754	0.3124		-1.6762	
19	20.11	-0.01	5.4443	-10.9135	0.0031	0.0317	-0.0330	0.5694	0.3072-		-2.0046	
20	9.80	-0.01		-9.1967	0.0077	C-0090	-0.0809	0.7888	0.2796		-2.9364	
21	0.01	-0.00	-0.0020	0.0749	-0.0217	0.0876	-0-0410	0.6595	0.2299	0.4294	-36.6163	
			•									
										-		
							•					
											· · · · · · · · · · · · · · · · · · ·	
								-				
		<del></del>		<del></del>	<del></del>		<del></del>					
												•

	<u>0# 1</u>											
•	TEST	PART MA			CONF	L DEL	DELS	DEL3DEL+	TRANSITI			
7	ALPHA-	BĒŤA	CN	CLH_	CÝ	CLN	CLL	CA	CAB	CAF	ACP	<del></del>
	0.00	-0.00	0.0250	-0.0365	-0.0196	0.0501	-0.0129	0.7568	0.0868		-1.4604	
	2.03	-0.0v	0.2746	-0.3168	-0.0169 -0.0167	0.0585 0.0752	-0.0133 -0.0136	0-2640	0.0874	0.1766	-1.1527 -1.2886	
	6.06	-0.00		-1.3567	-0.0200	0.0861	-0.0136	0.2904	0.0965		-1.4740	
	8.06	-0.00		-2.1751	-0.0216	0.0971	-0.0118	0.3107	0.1055		-1,6342	
	10.07	-0.00	1.7947	-3.1380	-0.0232	0.1048	-0.0116	0.3273	0.1096	0.2177	-1.7485	
	12.10	-0.01	2.2889	-4.1813	-0.0312	0.1332	-0.0024	0.3543	0.1188	0.2355	-1,8268	
	14.10	-0.00 -0.00	3.4641	-5.3761 -6.7540	-0.0360 -0.0361	0.1350 0.1078	0.0095 0.0156	0.3719	0.1339	0.2380	-1.890Z -1.9497	
	17.07	-0.00		-7.366Ü		0.1095	0.0209	0.3787	0.1750		-1.9556	
	18.07	-0.00	4.0518		-0.0402	0.1109	0.0227	0.3813	0.1819	0.1994	-1.9619	
	19.11	-0.00	4.3644	-8.5763	-0.0421	0.1182	0.0247	0.3835	0.1930	0.1905	-1.9641	
	20.10	-0.00		-9.1534	-0.0418	0.1328	0.0210	0.3938	0.1898	0.2040	-1,9598	
	21.09	-0.00	4.9765	-9,7432		0.0944	0.0137	0.3972	0.2087	0.1885	-1.9578	
	22.11 23.14	-0.00		-10.7859	-0.0303 0.0007	0.1211	0.0100 0.0043	0.4051 _ 0.4031	0.2192	0.1859	-1.9463 -1.9366	
	_	-0.01		-11.3350	0.0515	-0.0254	0.0017	0.4064	0.2423	0.1641	-1.9254	
	25.13	-0.00		-11.7574		-0.1167	0.0098	0.4126	0.2526	0.1600	-1.9102	
	26.14	-0.00		-12.3307	0.1988	-0.3444	0.0352	0.4113	0,2730	0.1383	-1.8957	
	27.19	0.00	•	-12-74-1	0.2443	-0.5561	0.0765	0.4036	0.2898	0.1138	-1.8789	
-	29.25	- 0.03		-13.0417 -13.4857		-0.7356 -0.8050	0.1620	. 0.4009_			-1.8515	
	30.55	0.02		-13.5867	0.4901		0.2973	0.3939 0.4022	0.3054	0.0820	-1.83 <b>95</b> -1.8061	
	20.05	-0.00		-9.3390		0.1127		0.3334	0.1933	0.1401	-1.9906	
	10.07	-0.00		-3.2832		0.08-6		0.2737	0.1593	0.1144	-1.6170	
	-0.00	-0.00	0.0412	-0.1305	-0.01>5	0.0438	-0.0146	0.2297	0.0867	0.1430	-3.1709	
										<del></del>	·	
	•											•
							<del></del>		-			
_		<del></del>										
				····								
_						<del></del>					. <del> </del>	
_												

	TEST 1	PART =4	CH RX10-	0.0 B	CONF.	OEL	0 0	DEL3 DEL4 0 0	TRANSITI			
INT A		BETA	CN	- CLM	CY	CLN	CLL	CA	EAB	CAF	XCP	
	2.03	-0.00	0.0343	-0.0965	-0.0186	0.0537	-0.0157 -0.0179	0.2407	0.0866	0.1539	-2.0157 -1.3111	
_	4.05	-0.00	0.5819	-0.5023	-0.0199	0.0768	-0.0174	0.2541	0.0877		-1.3789	
<u> </u>	6.11	-0.00	0.9458	-1.4702	-0.0195	0.0932	-0.0181	2692.0	0.0950		-1.5544	
5	8.10	-0.01	1.3702	-2.3212	-0.0206		-0.0181	0.2866	0-1117		-1.6940	
-	0.06	-0.01	1.8214	-3.2663	-0.0221		-0.0178	0.3041	0.1111		-1.7933	
	80.5	-0.01	2,3446	-4.3981	-0.0294	0.1412	-0.0124	0,3206	0,1285		-1.8758	
_	4.09	-0.01	2.9137		-0.0396	0.1542	0.0001	0.3327	0.1469		-1.9395	
		-0.00	3.5232	-6.9875 -7.6092	-0.0369	0.1102	0.0102 0.0153	0.3377 0.3507	0.1597		-1.9634 -1.9679	
		-0.00	4.1369			0.1142	0.0153	0.3602	0.1757		-1.9923	
		-0.00		-8.8091	-0.0441	0.1769	0.0172	0.3666	0.1952		-1.9879	
		-0.00		-9.4140	-0.0485	0.1454	0.0154	0.3762	0.1992		-1.9845	
4	21.11	-0.00	5.0632	-10-0005	-0.0341	0.1163	0.0117	0.3836	0.2080	0.1756	-1.9751	
		-0.00		-10.5239	-0.0213	0.1089	0.0081_	0.3866	.0.2269	0.1597	-1,9623	
		-0.00		-11.0310	0.0162	0.0393	0.0075	0.3867	0.2176	0.1690	-1.9503	
	24.12	-0.01		-11.5995	0.0403	. 0.0051	0.0071	0.3933_	0.2328 _		-1.9341	
	25.14 26.14	0.00		-12.0303 -12.5040	0.1030	-0.1332	0.0216	0.4004	0.2465	0.1501	-1.9104 -1.8902	
	27.16	0.00		-12.5793	0.2993	-0.6189	0.2006	0.4076	0.2790	0.1286	-1.8581	
	28.22	0.01		-12-2403	0.2744	-0.3282	0.3275	0.4461	0.2987	0.1474	-1.7949	
	29.28	0.01		-12.8697	0.3294	-0.4321	0.3239	0.4355	0.3420	0.0936	-1.7858	
	30.25	0.02	7.7042	-13.9172	0.3362	-0.6966	0.2622	0.3864	0.3490	0.0374	-1.8064	
24	20.06	-0.00	4.7607		-0.0461	0.1269	0.0121	0.3258	0.2537	0.0721	-2.0046	
	10.06	-0.00		-3.3943	-0.0163	0.0875	-0.0234	0.2743	0.1691	0.1052	-1,0303	
,	-0.00	-0.06	0.0420	-0-1329	-0.0136	0.0422	-0-0209	0.2303	0.0799	0.1504	-3.1661	

. . .

	- TEST	PART =4	ACH RX10- D2 2.3	0.0 B	CONF 4w0F32 0	L DEL	1 DEL2	DEL3 DEL4	TRANSITI	ON	
NT	ALPHA	BETA	CN	CLM -		CLN	CLL .	ÇA	CAB	CAF	XCP
	-0.00	-0.00	0.0395	-0.1096			-0.0198	0.2394	0.0864	0.1530	-2.7749
	2.05	-0.00	0.2459	-0.3824	-0.0170	0.0650	-0.0201	0-2461	0.0762		-1.3067
<u> </u>	4.09	-0.04	0.5992		-0.0206		0.0204	0.2534	0.0903	0.1631	-1.3863
	6.07		0.9655		-0.0189		-0.0205	0.2674	0.1063	0.1611	-1.5607
	8.04 10.08	-0.01	1.4079		-0.0168		-0.0202	0-2861 .	0.1129		-1.7140
	12.05	-0.01 -0.01	2.4162	-3.4300 -4.6130	-0.0253	0.1309 0.1332	-0.0201	0.3051 0.3207	0.1252 0.1273		-1.8198 -1.9076
	14.06	-0.01		-5.40+8	-0.0376	0.1558	-0.0048	0-3402	0.1379		-1.9673
	16.10	-0.01	3.6221		-0.0610	0.2205	0.0090	0.3545	0.1600		-2.0038
		-0.01		-7.9095		0.2352	0.0173	0.3539	0.1634		-2.0163
	18.07	-0.01	4.2706		-0.0796		0.0242	0.3651	0.1689		-2.0188
	19.09	-0.00	4.5803		-0.0829	0.2594	0.0290	0.3744	0.1823		-2.0145
1	20.04	-0.00	4.8757	-9.7674	-0.0769	0.2406	0.0204	0.3864	0.1892	0.1972	-2.0033
	21.11	-0.01	5.2049	-10.3856	-0.0852	0.2760	0.0092	0.3917	0.1933		-1.9959
<u> </u>		-0.31		-10.9256		0.2296	_ 2500.0	0.3791	0.2240		-1,9850
	23.07			-11.3869		0.1699	0.0001	0.3892	0.2215		-1.9641
	24.12				-0,0024	0.1376	0.0012	0.3945	0-2289		-1.9403
}		-0.01		-12-3503	0.0438	0.0643	0.0137	0.3928	0.2418		-1.9139
	26.20	0.01		-17.7572 -17.9865	0-1194	-0.1069	0.0794	0.3962	0.2542		-1,6830
	28.26	0.01		-13.1372	0.2041	-0.2048	0.2273	0010 0.4030	0.2716		-1,8397 -1,7748
	29.29	0.00		-13-5360	0.1771		0.1926	0.3791	0.2A73		-1.7202
	29.27	0.00	_	-13.5619	0.1940	-0.2089	0.1919	0.3757	0.3098		-1.7377
,	30.32	0.06		-13.6522		-0.0653	0.2230	0.3688	0.3031		-1.6762
,	20.07	-0-00		-9.9410		0.2279	0.0173	0.3355	0.2474		-2.0275
	10.76	-0.01		-3.4974	-0.0169	0.1126	-0.0249	0.2637	0.1412	0.1425	-1.8465
	-0.00	-0.00	0.0491	-0.1476	-0.0128	0.0437	-0.0215	0.2298	0.0840	0.1458	-3.0050
								<del></del>			
						•					

PHA .00 .00 .02 .04	PART MA 142 0.9 BETA -0.00 -0.00 -0.00 -0.00	CN 0.0455 0.0434 0.2920	CL4 -0.1213 -0.118+	CONF 4m0F32 0	CL*	DELZ_	DET3 DET4	TRANSITI UNKNOWN	OM	
.00 .00 .02 .04	-0.00 -0.00 -0.00 -0.00	0.0455 0.0434 0.2920	-0.1213 -0.118	_		·				
.00 .D2 .04	-0.00 -0.00 -0.00	0.0434	-0-118-	-0.0170		CLL	CA	CAB	CAF	ACP
.02 .04	-0.00_	0.2920				-0.0194	0.2419	0.0745		-2.6641
.04	-0.00			-0.0171	0.0516	-0.0195	0.2399	0.0A1T	0.1582	-2.7264
.04		n. ca>:	-0.3707 -0.8017	-0.0179 -0.0168	0.0641	-0.0199 -0.0217	0.2452	0.0514	0.1639	-1 · 2696
		0.5921 0.5915		-0.0180	_	-0-0217	0.2548	0.0832		-1.3601
	-0.00	0.9726		-0.0171		-0.0201	0.2692	0.0925		-1.5341
	-0.01	1.4247	-2.4239	-0.0167	0.1050	-0.0201	0.2875	0.1102		-1.7014
	-0.01	1.9186		-0.0180		-0.01B2	0.3038	0.1183		-1.8252
										-1.9134
		_				_				
										-2.0281
-10					0.2301	0.0348		0.1970		-2,0074
. 05	-0.01	5.5872	-11.0974	-0.0562	0.2820	0-0180	0.3959	0.1973	_0,1987	-1.9862
.12	-0.01	5.9309	-11.6446	-0.0395	0.1871	0.0017	0.3986	0.2058	0-1927	-1.9634
-10	-0.01			0.0165		0.0121	0.3973	0.5510		-1.9292
										-1.8939
										-1.000&
										-1.6871
0.0€	-0-01			-0.0925	0.2975	0.0357	0.3409	0.2365	0.1045	-2.0392
.07	-0.01				0.0864	-0.0199	0.2863	0.1466		-1.8477
	-0.00	0.0462	-0.1308	-0.013A	0.0489	-0.0180	0.2353	0.0789	0.1563	-2.8327
	.07 .07 .07 .11 .06 .07 .09 .10 .05 .10 .16 .21 .28 .23 .24	.07 -0.01 .07 -0.01 .07 -0.01 .11 -0.01 .06 -0.01 .07 -0.01 .09 -0.01 .10 -0.00 .10 -0.01 .12 -0.01 .14 -0.01 .21 -0.01 .21 -0.01 .23 0.00 .35 0.00 .41 0.00	07 -0.01 2.4497 07 -0.01 3.0323 07 -0.01 3.6600 11 -0.01 4.3163 07 -0.01 4.6551 09 -0.01 4.6551 09 -0.01 5.5872 10 -0.01 5.5872 112 -0.01 5.5872 112 -0.01 6.2648 116 -0.01 6.2648 116 -0.01 6.2648 117 -0.01 6.2648 118 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648 119 -0.01 6.2648	07 -0.01 2.4497 -4.6874 07 -0.01 3.0323 -5.9977 07 -0.01 3.6600 -7.3839 11 -0.01 4.0091 -8.1314 0.6 -0.01 4.3163 -8.7733 0.7 -0.01 4.6551 -9.4465 0.9 -0.01 4.6551 -9.4465 0.0 -0.01 5.2933 -10.6258 0.0 -0.01 5.55872 -11.0974 0.10 -0.01 5.55872 -11.0974 0.11 -0.01 6.2648 -12.0662 0.10 -0.01 6.2648 -12.0662 0.10 -0.01 6.5763 -12.45571 0.21 -0.01 6.9338 -12.45571 0.23 6.00 7.2679 -13.1199 0.27 0.00 7.6772 -13.3631 0.35 0.00 8.4549 -13.711.5627 0.41 0.00 8.4549 -13.7627 0.07 -0.01 1.9318 -3.5695	.07       -0.01       2.4497       -4.6874       -0.0298         .07       -0.01       3.0323       -5.9977       -0.0375         .07       -0.01       3.6600       -7.383y       -0.0498         .11       -0.01       4.0041       -8.1314       -0.0498         .06       -0.01       4.0041       -8.1314       -0.0812         .07       -0.01       4.6551       -9.4005       -0.0812         .07       -0.01       4.6551       -9.4005       -0.0934         .09       -0.01       4.9704       -10.0804       -0.0758         .05       -0.01       5.5872       -11.0974       -0.0562         .12       -0.01       5.5872       -11.0974       -0.0562         .12       -0.01       5.9309       -11.646       -0.0395         .10       -0.01       6.2648       -12.0662       0.0165         .21       -0.01       6.5763       -12.4550       0.0610         .21       -0.01       6.9338       -12.4550       0.0610         .27       0.00       7.6772       -13.5627       0.1362         .41       0.00       8.4549       -13.7615       0.1262	.07         -0.01         2.4497         -4.6874         -0.0298         0.1601           .07         -0.01         3.0323         -5.9977         -0.0375         0.1481           .07         -0.01         3.6600         -7.3834         -0.0498         0.2182           .11         -0.01         4.0041         -8.1314         -0.0642         0.2117           .06         -0.01         4.3163         -8.7733         -0.0812         0.2618           .07         -0.01         4.6551         -9.4465         -0.0934         0.2996           .09         -0.01         4.9704         -10.0804         -0.0975         0.3079           .10         -0.00         5.2933         -10.6258         -0.0788         0.2305           .12         -0.01         5.5872         -11.0974         -0.0562         0.2024           .12         -0.01         5.9349         -11.6466         -0.0395         0.1871           .10         -0.01         6.2648         -12.0662         0.0165         0.0954           .21         -0.01         6.5763         -12.4550         0.0010         0.306           .21         -0.01         6.9338         -12.4550	.07         -0.01         2.4497         -4.6874         -0.0298         0.1601         -0.0227           .07         -0.01         3.0323         -5.9977         -0.0375         0.1481         -0.0063           .07         -0.01         3.6600         -7.3839         -0.0498         0.1782         0.0070           .11         -0.01         4.0091         -8.1314         -0.0642         0.2117         0.0169           .06         -0.01         4.3163         -8.7733         -0.0612         0.2618         0.255           .07         -0.01         4.6551         -9.4465         -0.0934         0.2996         0.0291           .09         -0.01         4.9704         -10.0804         -0.0975         0.3079         0.0402           .10         -0.01         5.5872         -11.0974         -0.0768         0.2301         0.0348           .05         -0.01         5.5872         -11.0974         -0.0395         0.1871         0.0017           .12         -0.01         5.5872         -11.0974         -0.0395         0.1871         0.0017           .10         -0.01         6.2648         -12.0662         0.0165         0.0954         0.0121	.07       -0.01       2.4497       -4.6874       -0.0298       0.1601       -0.0227       0.3217         .07       -0.01       3.0323       -5.9977       -0.0375       0.1481       -0.0003       0.3362         .07       -0.01       3.6600       -7.3839       -0.0498       0.1782       0.0070       0.3483         .11       -0.01       4.0091       -8.1314       -0.0642       0.2117       0.0169       0.3630         .06       -0.01       4.3163       -8.7733       -0.0612       0.2618       0.0255       0.3713         .07       -0.01       4.6551       -9.4465       -0.0934       0.2996       0.0291       0.3767         .09       -0.01       4.9704       -10.0804       -0.0975       0.3079       0.0402       0.3732         .10       -0.00       5.2933       -10.6258       -0.0788       0.2301       0.0348       0.3865         .05       -0.01       5.5872       +11.0974       -0.0395       0.1871       0.0017       0.3986         .12       -0.01       5.9309       -11.6446       -0.0395       0.1871       0.0017       0.3986         .10       -0.01       6.2648       -12.0662	0.07       -0.01       2.4497       -4.6874       -0.0298       0.1601       -0.0227       0.3217       0.1396         0.07       -0.01       3.0323       -5.9977       -0.0375       0.1481       -0.0063       0.3362       0.1436         0.07       -0.01       3.6600       -7.3839       -0.0498       0.1782       0.0079       0.3483       0.1551         1.1       -0.01       4.0091       -8.1314       -0.0642       0.2117       0.0169       0.3630       0.1629         0.06       -0.01       4.3163       -6.7733       -0.0812       0.2618       0.0255       0.3713       0.1707         0.07       -0.01       4.6551       -9.4465       -0.0934       0.2996       0.0291       0.3767       0.1600         0.09       -0.01       4.9704       -10.604       -0.0975       0.3079       0.402       0.3732       0.1803         0.10       -0.00       5.2933       -10.6258       -0.0768       0.2307       0.0402       0.3732       0.1873         0.12       -0.01       5.5872       -11.6974       -0.0562       0.2024       0.0180       0.3959       0.1973         0.12       -0.01       6.2648       -12.06	07 -0.01

7 PART WAR 143 0.4	ACH PX10- 96 2.3 CN 0.0449		CONF 4W0F3Z 0		1 DEL2 (	0EL3 _ DEL4	TRANSITI		
-0.00 -0.0u	0.0449		C_			•	Out-my En		
-0.00		-0.1236		CLN	CLL	CA"	CAS	CAF	ACP
-0.00	0.3075	- 4 7	-0.0146	0.0512	-0.0160	0.2553	0.0738		-7,7506
	A 4 A 4 7	-0.38/3	-0.0109	0.0570	-0.0180	Ø.2599	0.0803	0.1796	-1.2804
	0.6047	-0.8366 -1.5418	-0.0153 -0.0165		-0.0199	0.2718 0.2831	0.0717		-1.3835 -1.5516
-0.01	1.4301	-2.4430	-0.0203		-0.0182	0.2898	0.0995		-1.7083
-0.01	1.4520	-2.5021	-0.0166	0.0968	-0.0182	0.2983	0.0988		-1.7225
	1.9670	-3-6506	-0.0156	0.1069	-0.0178	0.3234	0.1119		-1.8559
	1.9305	-3.5609	-0.0184	0.1113	-0.0179	0.3103	0.1210	0.1893	-1.8445
			-0.0506	0.1100	-0.0083	0.3358_	0.1319		-1.9074
				0.2874	0.0365	0.3917	0.1858		
	5.3712	-10-7898	-0.0945	0.3307	0.0383	0.4053	0.1923	0.2130	-2.0080
: :				0.2291	0.0342	0.4109	0.2090		-1.9839
			-						-1.9499
									-1.7798
				-0.0892	0.0976		0.2527		-1.7613
-0.00	7.4820	-13.5072	0.1920	-0-1718	0.1471	0.3813	0.2773		-1.7137
2 -0.00	7.8843	-13.4972	0.1862	-0.1655	0.1402	0.3603	0.2721	0.1082	-1.7119
			_		0.1016	0.3608	0.2734		-1.6425
							0.2741		_1.5844
									-2.0443
	0-0520	-0-1457	-0-0114						
-0,00	000350	-004-31	-000100	0.000	-0.0144	0.5440	0.0100	0 1 1 005	-5.0033
	-0.01 -0.01 -0.01 -0.01 -0.00 -0.00 -0.00 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0	-0.01 1.9670 -0.01 1.9305 -0.01 2.5032 -0.01 3.0651 -0.01 3.7069 -0.00 4.3660 -0.00 4.7032 -0.01 5.0204 -0.01 5.0204 -0.01 5.7253 -0.01 6.0658 -0.01 6.0658 -0.01 7.1095 -0.01 7.54120 -0.01 7.54120 -0.01 7.6463 -0.01 7.6463 -0.01 7.6463	-0.01 1.9670 -3.6506 -0.01 1.9305 -3.5609 -0.01 2.5032 -4.7746 -0.01 3.0651 -6.0532 -0.01 3.7069 -7.4883 -0.00 4.0247 -8.1811 -0.00 4.3660 -8.6914 -0.01 5.0264 -10.1934 -0.01 5.0264 -10.1934 -0.01 5.0264 -10.1934 -0.01 5.7253 -11.3546 -0.01 6.0856 -11.8669 -0.01 6.0856 -12.3813 -0.01 6.0856 -12.3813 -0.01 6.0856 -12.723 -0.01 7.1045 -12.7923 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.7821 -0.01 7.5412 -13.8220 -0.01 7.5412 -13.7821	-0.01 1.9670 -3.6500 -0.0156 -0.01 1.9305 -3.5609 -0.0184 -0.01 2.5032 -4.7746 -0.0206 -0.01 3.0651 -6.0532 -0.0381 -0.01 3.7069 -7.4883 -0.0459 -0.00 4.3660 -8.6914 -0.0564 -0.00 4.3660 -8.6914 -0.0693 -0.01 5.0264 -10.1934 -0.0693 -0.01 5.0264 -10.1934 -0.0874 -0.01 5.3712 -10.7498 -0.0945 -0.01 5.7253 -11.3566 -0.0514 -0.01 6.0650 -11.8669 -0.0023 -0.01 6.0650 -12.3813 0.0600 -0.01 6.7168 -12.7823 0.1074 -0.01 7.1095 -12.9965 0.1302 -0.01 7.5412 -13.7821 0.1507 -0.01 7.5412 -13.7821 0.1507 -0.01 7.683 -13.4972 0.1862 -0.00 7.6843 -13.4972 0.1862 -0.01 8.3416 -13.7010 0.1045 -0.01 8.3416 -13.7010 0.1045 -0.01 8.3416 -13.7010 0.1045	-0.01	-0.01 1.9670 -3.6506 -0.0156 0.1069 -0.0178 -0.01 1.9305 -3.5609 -0.0184 0.1113 -0.0179 -0.01 2.5032 -4.7766 -0.0206 0.1100 -0.0083 -0.01 3.0651 -6.0532 -0.0381 0.1629 -0.0157 -0.01 3.7069 -7.4883 -0.0459 0.1637 0.0052 -0.00 4.0247 -8.1811 -0.0564 0.1798 0.0133 -0.00 4.3660 -8.6914 -0.0693 0.2081 0.0199 -0.00 4.7032 -9.5618 -0.0752 0.2081 0.0199 -0.01 5.0264 -10.1934 -0.0693 0.2081 0.0199 -0.01 5.3712 -10.7498 -0.0945 0.3307 0.0383 -0.01 5.3712 -10.7498 -0.0945 0.3307 0.0383 -0.01 5.3753 -11.3566 -0.0514 0.2291 0.0342 -0.01 5.7253 -11.3566 -0.0514 0.2291 0.0342 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 -0.01 6.0858 -12.3813 0.0600 0.0196 0.0273 -0.01 6.7168 -12.7423 0.1074 -0.0552 0.0484 -0.01 7.1045 -12.9965 0.1362 -0.0784 0.0804 -0.01 7.5412 -13.7821 0.1507 -0.0892 0.0976 -0.00 7.8843 -13.4972 0.1862 -0.1718 0.1471 -0.00 7.8843 -13.4972 0.1862 -0.1655 0.1402 -0.01 8.3416 -13.7010 0.1045 -0.0020 0.1016 -0.01 8.7236 -13.8270 0.1149 0.2275 0.0852 -0.01 5.0617 -10.3477 -0.0860 0.2275 0.0837 -0.0180	-0.01 1.9670 -3.6500 -0.0156 0.1069 -0.0178 0.3234 -0.01 1.9305 -3.5609 -0.0184 0.1113 -0.0179 0.3103 -0.01 2.5032 -4.7745 -0.0206 0.1100 -0.0083 0.3328 -0.01 3.0651 -6.0532 -0.0381 0.1629 -0.0157 0.3447 -0.01 3.7069 -7.4883 -0.0459 0.1637 0.0052 0.3672 -0.00 4.0247 -8.1811 -0.0566 0.1798 0.0133 0.3722 -0.00 4.3660 -8.6914 -0.0693 0.2081 0.0199 0.3824 -0.00 4.7032 -9.5614 -0.0752 0.2416 0.0314 0.3909 -0.01 5.0204 -10.1934 -0.0674 0.2874 0.0365 0.3917 -0.01 5.3712 -10.7498 -0.0945 0.3307 0.0383 0.4053 -0.01 5.0254 -11.3546 -0.0514 0.2291 0.0342 0.4109 -0.01 5.7253 -11.3546 -0.0514 0.2291 0.0342 0.4109 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 0.4114 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 0.4114 -0.01 6.8168 -12.7423 0.1074 -0.0552 0.0484 0.4025 -0.01 7.1095 -12.9965 0.1302 -0.0784 0.0804 0.3936 -0.01 7.5412 -13.7021 0.1522 -0.1239 0.1163 0.3854 -0.00 7.6843 -13.4972 0.1862 -0.0784 0.0892 0.0976 0.3970 -0.00 7.6863 -13.6922 0.1962 -0.1718 0.1471 0.3813 -0.00 7.6864 -13.7010 0.1045 -0.0020 0.1016 0.3608 -0.01 8.7236 -13.4972 0.1862 -0.1655 0.1002 0.3808 -0.01 8.7236 -13.4972 0.1862 -0.1655 0.1002 0.3808 -0.01 8.7236 -13.4972 0.1862 -0.1655 0.1002 0.3859 -0.01 1.9824 -3.7083 -0.0113 0.0837 -0.0180 0.2941	-0.01 1.9670 -3.6500 -0.0156 0.1069 -0.0178 0.3234 0.1119 -0.01 1.9305 -3.5609 -0.01w4 0.1113 -0.0179 0.3103 0.1210 -0.01 2.5032 -4.7746 -0.0206 0.1100 -0.0083 0.3328 0.1319 -0.01 3.0651 -6.0532 -0.0381 0.1629 -0.0157 0.3447 0.1452 -0.01 3.7069 -7.4883 -0.0459 0.1637 0.0052 0.3672 0.1532 -0.00 4.0247 -8.1811 -0.0564 0.1798 0.0133 0.3722 0.1617 -0.00 4.3660 -8.6914 -0.0693 0.2081 0.0199 0.3824 0.1719 -0.00 4.7032 -9.5614 -0.0752 0.2416 0.0314 0.3909 0.1401 -0.01 5.0264 -10.1934 -0.0874 0.2874 0.0365 0.3917 0.1858 -0.01 5.3712 -10.7898 -0.0945 0.3307 0.0383 0.4053 0.1923 -0.01 5.3725 -11.3546 -0.0514 0.2291 0.0342 0.4109 0.2090 -0.01 5.7253 -11.3546 -0.0514 0.2291 0.0342 0.4109 0.2090 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 0.4114 0.2240 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 0.4114 0.2240 -0.01 6.8168 -12.7423 0.1074 -0.0552 0.0484 0.4025 0.2389 -0.01 6.8628 -12.3813 0.0600 0.0196 0.0273 0.4035 0.2389 -0.01 6.8628 -12.3813 0.0600 0.0196 0.0273 0.4035 0.2389 -0.01 7.5412 -13.7821 0.1507 -0.0892 0.0976 0.3970 0.2527 -0.00 7.8843 -13.4972 0.1862 -0.1718 0.1671 0.3813 0.2773 -0.00 7.8843 -13.4972 0.1862 -0.1655 0.1402 0.3808 0.2734 -0.01 8.3416 -13.7010 0.1045 -0.0020 0.1016 0.3008 0.2734 -0.01 8.7236 -13.6027 0.1862 -0.1655 0.1402 0.3808 0.2734 -0.01 8.7236 -13.6027 0.1862 -0.1655 0.00852 0.3874 0.2741 -0.00 5.0617 -10.3877 -0.0860 0.2676 0.0333 0.3589 0.2542	-0.01 1.9670 -3.6500 -0.0156 0.1069 -0.0178 0.3234 0.1119 0.2115 -0.01 1.9305 -3.5609 -0.0184 0.1113 -0.0179 0.3103 0.1210 0.1893 -0.01 2.5032 -4.7746 -0.0206 0.1100 -0.0083 0.3328 0.1319 0.2209 -0.01 3.0651 -6.0532 -0.0381 0.1629 -0.0157 0.3447 0.1452 0.1995 -0.01 3.7669 -7.4883 -0.0459 0.1637 0.0052 0.3472 0.1532 0.2141 -0.00 4.0247 -8.1811 -0.0564 0.1798 0.0133 0.3722 0.1617 0.2105 -0.00 4.3660 -8.6914 -0.0693 0.2081 0.0199 0.3824 0.1719 0.2105 -0.00 4.7032 -9.5614 -0.0752 0.2416 0.0314 0.3909 0.1401 0.2109 -0.01 5.0264 -10.1934 -0.0075 0.2416 0.0314 0.3909 0.1401 0.2109 -0.01 5.3712 -10.7498 -0.0945 0.3307 0.0383 0.4053 0.1923 0.2130 -0.01 5.3712 -10.7498 -0.0945 0.3307 0.0383 0.4053 0.1923 0.2130 -0.01 5.7253 -11.3546 -0.0514 0.2291 0.0342 0.4109 0.2090 0.2019 -0.01 5.7253 -11.3546 -0.0514 0.2291 0.0342 0.4109 0.2090 0.2019 -0.01 6.0858 -11.8669 -0.0023 0.1473 0.0222 0.4114 0.2240 0.1874 -0.01 6.8658 -12.3813 0.0600 0.0196 0.0273 0.4035 0.2389 0.1646 -0.01 6.8168 -12.7423 0.1074 -0.0552 0.0484 0.4025 0.2406 0.1619 -0.01 7.1095 -12.9965 0.1302 -0.0784 0.0804 0.3936 0.2579 0.1357 -0.00 7.8843 -13.4972 0.1862 -0.1239 0.1163 0.3854 0.2664 0.1190 -0.00 7.8843 -13.4972 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.5072 0.1962 -0.1718 0.1471 0.3813 0.2773 0.1039 -0.01 8.3416 -13.7010 0.1045 -0.0020 0.1016 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1402 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1400 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1400 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1400 0.3808 0.2734 0.0875 -0.01 8.7236 -13.6072 0.1862 -0.1655 0.1400 0.3808 0.2734 0.0875

HA BF 00 -0. 06 -0. 04 -0. 07 -0. 07 -0.	00 0.0510 00 0.3194 00 0.6352 00 1.0149 01 1.4941	0.0 6 CLM -0.1392 -0.4471 -0.9466	CY		CLL -0.0143	. CA	TRANSITI UNKNOWN		
.00 -0. .06 -0. .09 -0. .04 -0. .07 -0.	00 0.0510 00 0.3194 00 0.6352 00 1.0149 01 1.4941	-0.1392 -0.4471 -0.9466	-0.0143	0.0391			CAB	CAS	
06 -0. 09 -0. 04 -0. 07 -0.	00 0.3194 00 0.6352 00 1.0149 01 1.4941	-0.4471 -0.9466	-0.0149		-0.0143				XCP
.04 -0. .04 -0. .07 -0.	00 0.6352 00 1.0149 01 1.4941	-0.9466			-0.0163	0.2730	0.0803	0.1927	-2.7286 -1.3999.
.04 -0. .07 -0.	00 1.0149 01 1.4941			0.0600	-0.0164	0.2970	0.0880		-1.4906
.07 -0.			-0.0104	0.0697	-0.0149	0.3039	0.1015	0.2023	-1.6164
			-0.0109		-0.0146	0.3314	0.1039	0.2274	-1-8070
A4 - A		-3.8578	-0.0155		-0.0129	0.3423	0.1225		-1.8965
	01 2.5925		-0.0173	0.1061	-0.0079	0.3670	0,1234	0.2436	-1.9942
.06 -0.			-0.0263	0.1230	-0.0122	0.3843	0.1438	0.2405	-2.0477
		. 7	-0.0390	_0.1425	0.0027	0.4023	0.1624	0.2399_	-2.05 <del>68</del> -2.0547
			-						-2.0498
-									-2.0434
			-0.0570	4155.0	0.0228	0.4331	0.2020	0.2311	-2.0285
.13 -0.			-0.0436	0.2315	0.0244	0.4453	0.2184	0.2269	-1.9999
			-0.0000	_0.1772	0.0285	0.4332	0.2685	0.1647	-1.9716
									-1.9205
									-1.8961
									-1.8508 -1.7946
									-1.7412
									-1.6703
			0.0511	0.1582	0.0204	0.3840	0.2696		-1.6068
.54 -0.	02 9.0357	-13.6839	0.0839	0.1158	0.0236	0.3671	0.2799	0.0872	-1.5366
				0.1827	0.0116	0-4120	0.2709	0.1411	-2.0385
				0.0728	-0.0145		0.2001	0.1156	-1,9606
									-1.9224
									-1.9577
-00	0.033	, -0.1050	-0.0134	0.0330	-0.000	0.2019	0.0001	4.1011	-3.0211
									<del></del>
	11 -0. 10.07 -0. 10.07 -0. 10.07 -0. 113 -0. 113 -0. 113 -0. 113 -0. 113 -0. 113 -0. 113 -0. 114 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 115 -0. 1	11 -0.00 4.3974  0.07 -0.00 4.7732  0.07 -0.01 5.1033  13 -0.01 5.4629  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 6.2602  113 -0.01 7.7976  113 -0.02 9.0351  113 -0.02 9.0351  113 -0.02 9.0351  113 -0.02 2.0062	11	11	11	11	11	0.11	0.11   -0.00

TEST	DART M	ACH RELO-	5 PHI	CONF	L OEL	) DELS C	SEL 3 DELA	TRANSITI		
153	150 1.			4±0F32" 0.	O DEL	0 0 -	0 0			
INT ALPHA	ĐĒ TA	<u>CN</u>	CLM	ČÝ	CLN	CLL	CA	CAB	CAF	XCP
1 -0.00	-0.00	0.0028	-0.0319	-0.0322	0.1153	-0.0130	0.5047	0.1516	0,3531	-11.2400
5 5.05	-0.01	0.2817	-0-3972	-0.0323	0-1271	-0.0061	0.5177	0.1645	0.3532	-1.4104
3 4,04	0-01	0.6022	-0.9081	-0.0274	0.1267	-0.0063	0.5348	0.1657		-1.5080
4 6.03 5 A.04	-0.01 -0.01	1.0014	-1.6926 -2.6178	-0.0302 -0.0279	0.1453 0.1377	-0.0062 -0.0049	0.5570 0.5876	0.1729 0.1790	0.3842	-1.6902 -1.8033
6 5.03		1.4611	-2.6878	-0.0326	0.1546	-0.0047	0.5790	0.1953	0.3837	-1.8395
7 10.02		1.9599	-3.7560	-0.0289	0.1645	-0.0030	0.6030	0.2085	0.3945	-1.9164
8 12.06	-0.01	2.4974	-4.0874	-0.0245	0.1538	0.0013	0.6172	0.2165	0.4007	-1.9570
9 14.04	-0.01	3.0517	-6.0065	-0.0270	0.1447	0.0069	0.6304	0.2238	0.4065	-1.968Z
	-0.00	3.6286.		-0.0485	0.1690	0.0213	0.6507	0.2356	0.4151	-1.9765
2 17.08	_	3.9653	<u>-7.6257</u>		0.2355	0.0175	0.6594	0.2486	_0.4106_	-1.9735
	-0.01	4.5979	-6.3480 -6.8601	-0.0694 -0.0700	0.2356	0.0201 0.0270	0.6682	0.2462	0.4220	-1.9509
19.09		4.9330	-9.3715	-0.0633	0.2353	0.0253	0.6768	0.2589	0.4179	-1.9270 -1.8998
5 21.13		5.3155	-9.9719	-0.0499	0.2070	0.0264	0.6763	0.2811	0.3952	-1.8760
	-0.01		-10.4744	-0.0340	0.1975	0.0261	0.6733	0.2896	0.3837	-1.8445
22.19	-0.01	5.7286	-10.4428	-0.0320	0.2415	0.0033	0.6611	0.2816_	0.3795	-1,8229
18 23.19	-0.05	_	-10.8430	-0.0191	0.2203	0.0013	0.6555	0.2911	0.3643	-1.7776
19 24.27			-11-3364	-0.0287	0-2567	-0.0005	0.6550	0.2951	0.3599	-1.7418
25.27			-11.7881	-0.0326	0.2612	-0.0011	0.6471	0.2953	0.3518	-1.7020
<u> 26.30</u> 27.36			-12.2157 -12.5871	0.0315	0.0354	0.0204	0.6223	0.3110 0.3037	0.3291	-1.6696 -1.6275
23 28.39			-12.9370	0.0506	0.0435	0.0224	0.6093	0.2985	0.3108	-1.5848
29.46			-13.2743	0.0536	0.0444	0.0217	-0.5966	0.3016	0.2950	-1.5460
25 30.56		9.0260	-13.5950	-0.0058	0.1669	0.0101	0.5818	0.3029	0.2789	-1.5062
56 . 50-11	-0.01	5.0015	-9.5940	-0.0520	0.2154	0.0198	0.6347	0.3019	0.3328	-1.9102
27 10.03 20 -0.00		1.9943	-3.9051	-0.0277	0.1207	0.0068	0.5749	_0.2716_		-1.9582
	-0.00	0.0056	-0.0364	-0.0207	0.0453	0.0080	0.5099	0.1984	0.3114	-6.5374

28.55

29.60

30.66

-0.00

26 27

85

29

30

-0.01

-0.01

-0.01

0.00

22.27 -0.01

10.05 -0.00

8.2999 -11.9899

8.7298 -12.4024

9.1858 -12.8277

5.8060 -9.5441

1.9548 -3.6408

0.0301

-0.0141

0.1126

0.1359

0.1826

-0.0092

-0.0063

-0.0051

-0.0800

-0.1337

-0.2177

0.1001

0.0422

-0.0125

ARNOLD ENGINEERING DEVELOPMENT CENTER (AEDC) PROPULSION WIND TUNNEL FACILITY(PUT) AERODYNAMIC WIND TUNNEL (4T) PAGE 1 OF 1 MARTIN MISSILE TAIL EFFECTS DATA SHEET 1 OF L DELI DELE DELE DELE TRANSITION TEST PART MACH RX10-6 PHI CONF 0.0 8440F32 0.0 151 1.20 2.3 UNKNOWN ALPHA POINT BETA CLM CY CLN CLL CA CAB CAF ACP -0.0722 0.0138 0.5370 0.1782 0.35FR -2.9578 0.00 0.00 0.0658 -0.0079 0.0016 0.00 0.00 -0.0203 0.0629 -0.0078 0.0032 0-0152 0.5372 0.1839 0.3533 -3.0976 0.00 -0.0223 0.0624 -0.0079 0.0049 0.0180 0.5390 0.3546 -2.8032 0.00 0.1843 2.04 0.00 0.2788 -0.3611 -0.0094 0.0151 0.0191 0.5466 0.1786 0.3660 -1.2951 0.2714 -0.3301 -0.0095 0.0200 0.0192 0.5454 0.3587 -1.2161 2.04 0.00 0.1867 -0.00 0.4190 -0.5500 -0.0106 0.0256 0.0191 0.5480 0.3629 -1.3147 3.00 0.1851 4.05 0.6034 -0.6659 -0.0059 0.0237 0.0204 0.5529 0.1894 -0.00 0.3634 -1.4351 6-06 0.00 1.0042 -1.6441 -0.0157 0.0377 0-0245 0.5779 0.1899 0.3879 -1.6372 -0.00 1-4473 -2.5420 0.0246 0-6008 0.1959 0.4050 -1.7563 8.03 -0.0124 0-0442 10.06 -0.00 1.9376 -3.5626 -0.0047 C.0456 0.0247 0.6175 0.2041 0.4134 -1.8368 -4.6069 -0.06 2.4638 -0.0044 0.0481 0.0260 0-6297 0.2128 0.4169 -1.8696 10 3.0222 -5.6825 -0.0017 0.0523 0.0273 0.6369 0.2211 0.4158 -1.8883 11 14.07 -0.00 16-12 -0.00 3.6305 -6.7589 -0.0130 0.0678 0.0340 0.6464 0.2266 0.4197 -1.8617 13 16.12 -0.00 3.6358 -6.7780 -0.0130 0.0678 0.0340 0.6430 0.2352 0.4078 -1.8642 3-6511 -6-8083 -0-0091 14 16-12 -0-00 0.0640 0.0355 0.6442 0.2393 0.4049 -1.8647 -1.6435 17-11 -0.00 3.9332 -7.2507 -0.0153 0.0734 15 0.0365 0.6475 0.2403 0.4071 18.14 -0.00 4.2773 -7.7749 -0.0259 0.1181 0.0285 0.6525 0.2468 0.4057 -1.6177 16 17 19.15 -0.00 4.6302 -8.2259 -0.0403 0.1538 0.0255 0.6546 0.2485 0.4061 -1.7766 18 20.21 -0.01 5.0144 -8.6718 -0.0296 0.1468 0.0181 0.6547 0.2512 0.4035 -1.7294 19 21.23 -0.01 5.3937 -9.0728 -0.0224 0.1200 0.0228 0.6493 0.2546 0.3947 -1.6621 -9.4694 0.6465 0.3907 -1.6330 20 22.28 -0.01 5.7989 -0-0169 0.1177 0.0234 0.2558 0.3845 -1.5944 23.32 -0.01 6.2101 -9.9137 0.0053 0.0255 21 0.0917 0.6433 0.2589 24.39 6.6145 -10.3545 4950.0 0.0617 0.0289 <u>23</u> -0.01 0.6413 0.2668 0.3745 -1.5654 7.0073 -10.7765 25.38 -0.01 0.0541 0.0235 0.0309 0.6411 0.2721 0.3690 -1.5362 24 26.45 -0.01 7-4468 -11-1804 0.0621 -0.0358 0.0353 0.6333 0.2753 0.3579 -1.5014 25 27.49 -0.01 7.6726 -11.5821 0.1252 -0.1197 0.0395 0.2784 0.6272 0.3486 -1.4712

0.0360

0.0415

0.0456

0.0249

0.0329

0.0317

0.6225

0.6149

0.6233

0.6256

0.6009

0.5323

0.2849

0.2874

0.2895

0.2834

0.2534

0.2045

0.3376 -1.4446

0.3275 -1.4207

0.3338 -1.3965

0.3422 -1.6438

0.3475 -1.8625

0.3278 -2.1353

			ACH RX10-		CONF	L DELI	DELS !	DEL3 DEL4	TRANSITI	ON		
	1		30 2.3		4=0F32 0		0	0 0	UNKNOWN			
NT	ALPHA	BETA	CN	CLM	CŶ	CLN	CLL	CA	CAB	CAF	ACP	
_	2.05	-0.00	0.2748	-0.3240	-0-0134	0.0077	0.0348	0.5245	0.1863		-3,2617	
	4.02	0.00	0.5974	-0.8385	0.0001	0.0161	0.0372	0.5323	0.1877 0.1883	0.3368	-1.1790 -1.4036	
		-0.00		-1.5552	-0.0032	0.0261	0.0372	0.5575	0.1891		-1.5768	
		-0.00		-2.4443		0.0466	0.0360	0.5805	0.1930		-1.7069	
	10.04	-0.00			-0.0131	0.0611	0.0361	0.5963	0.2006		-1.7707	
	12.07	-0.00	2.4277	-4.3571	-0.0033	0.0533	0.0372	0.6052	0.2090		-1.7947	
)	14.10	-0.00	2.9750	-5.3381	-0.0028	0.0516	0.0397	0.6096	0.2163	0.3934	-1.7920	
·	_16.15_			-6.2.02	-0.0031	0.0535	0433_	0.6535	.0.5555		-1.7560	
1	17.15 18.17	0.00		-6.6955 -7.1087	-0.0060 -0.0126	0.0607	0.0457	0.6223	0.5556		-1.7186 -1.6720	
	19.25		4.6408		-0.0114	0.0822	0.0434	0.6277	0.2321		-1.6276	
9		-0.00	5.0026	-7.9370	-0.0142	0.0915	0.0402	0.6284	0.2352	0.3932		
	21.31	-0.01		-8.3552		0.1060	0.0371	0.6287	0.2418		-1,5489	
<u></u> _	55.35	-0.01		-8.7.24	-0.0062	_ 0.1071_	0.0311	0.6302	_0.2470		-1.5136	
5		-6.01		-9-1567	0.0060	0.0973	0.0331	0.6346	0.2549		-1.4817	
<b>7</b>		-0.01		9.531a	_ 0.0258	0.0518	0.0360	0.6337	0.2579		-1.4492	
B		-0.00		-9.8653 -10.2272	0.0474	0.0011 -0.0603	0.0414	0.6317 0.6326	0.2638 0.2684		-1.417 <b>\$</b> -1.3877	
<del>}</del>	27.56	-0.00		-10.6185	0.0967	-G.1056	0.0561	0.6334	0.2738		-1.3613	
ī	28.62	_		-11.010+	0.1075	-0.1166	0.0523	0.6356	0.2781		-1.3399	
<u>-</u>	29.68	-0.01		-11.4377		-0.0740	0.0450	0.6375	SONS.O		-1.3233	
3	30.74	-0.01	9.0605	-11.8701	0.09A0	-0.0646	0.0457	0.6439	0.2857	0.3582	-1.3101	
4	50.26	-0.00		-7.4860		0.0868	0.0429	0,6085	0.2865		-1.5914	
5	10.07			-3.4366		0.0503	0.0385	0.5881	0.2561		-1.7932	
•	0.00	0.00	-0.0121	0.0430	-0.0096	-0,0101	0.0369	0.5207	0.2251	0.2955	-3,5670	
_	-									V,E733	-34 30/4	
				<del></del>	<del></del>					· <del></del>		
_				<del></del>								
_										*		
_								• • • • • • • • • • • • • • • • • • • •	·	<del></del>		

	<u>1 07 1</u>											
			CH RX10-		CONF	ل0قِلِ	1 DEFS	DEL3 DEL4				
	1	154 0.6	0 2.3	0.0 8	4w0f31 0	• 0	0 0	0 0	UNKNOWA			
INT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	
1	-0.00	0.00		-0.0392		0.0018	-0.0170	0.5656	0-1157	0.1469	-2.1841	
Š	0.00	0.00	0.0307	-0.0403	-0.0098	0.0055	-0.0170	0.2644	0.0739	0.1905	-1.3146	•
Ž	2.01_	0.00	0.2A29	-0.3593 -0.8975	-0.0058	G.0053	-0.0210	0.2692 0.2752	0.1083 0.0834		-1.2698	
-	4.01 6.05	0.00				-0.0031		0.2732	0.0996		-1.6757	
¿	8.05	0.00	1.4406	-5-2108	-0.0005	-0.0119	-0.03.2	0.3159	0.1107		-1.0124	<del></del>
7	10.02	0.00	1.9388	-3.6717	0.0067	-0.0380	-0.0309	0.3470	0.1218	0.2252	-1.8938	
8	12.03	0.00	2.4726	-4.8128	0.0076	-0.0750	-0.0294	0.3714	0.1315	0.2399	-1.9463	
9	14.02	0.00	3.0595	-5.9961	0.0042	-0.1058	0.0333	0.3944	0.1430	0.2513	-1.9801	
0	16.04	0.01		-7.2953	0.0038	-0.1288	-0.0209	0.4228	0.1569		-1.9996	
11	17.06	0.01		_7.9708_		-0.1426	-0.0139	0.4364	_0.1736		-5.0100	
5	18.06	0.01		-8.6317	0.0045	-0.1620	-0.0069	0.4528	0.1845	0.2683	-2.0118	
3	19.04	0.01		-9.2894	0.0096	-0.1725	-0.0051	0.4660	0.1776	0.2884	-2.0167	
15	19.04	0.01		-9.3231 -9.9467	0.0020	-0.1603	-0.0050 -0.0033	0.454R	0.2163	_0.2386 1695.0	-2.0195	
6	20.08	0.01		-10.5450	0.0020	-0.1404		0.4836	_0.2218 _0.2252		-2.0079	
17	22.09	0.01		-11.0706	0.0004	-0.1127	-0.0176	0.4912	0.2357		-1.9954	
8	23.10	0.00		-11.5230	0.0107	-0.0719	-0.0190	0.49R0	0.2458		-1.9670	· · · · · · · · · · · · · · · · · · ·
9	24.07	0.00		-11.8285	0.0142	-0.1193	-0.0272	0.5051	0.2603		-1.9388	
20	25.10	0.00	6.3836	-12.2503	0.0811	-0.2193	-0.0548	0.5134	0.2714	0.2420	-1.9192	
21	26.12	-0.00		-12.7820	0.1719	-0.3677	-0.0198	0.5161	0.2796	0.2365	-1 .8979	
5.5	27.14	-0.00		-13.3430	0.2605	-0.5275	-0.0065	0.5108	0.3031		-1.8654	
23	28.17	-0.00		-13.5426	0.4740	-0.9336	0.0337	0.4940	_0.2986		-1,8524	
24	28.17	0.00		-13.5878	0.4609	-0.9104	0.0356	0.4914	0.3084		-1.8534	
? <b>5</b>	28.17	0.00		-13.6051	0.4513	-0-8890	0.0342	0,4849	0.3129		-1.8571	<del></del>
27	29.21 30.21	0.00		-14,1234	0.6268	-0.9551 -1.2002	0.0641	0.4726	0.3167 0.3247	0.1650	-1.8315 -1.7984	
8	\$0.06	0.01		-10.1530			0.0016	0.4036	0.2281		-2.0403	
29	10.02			-3.8142		0.0305	-0.0297	0.2941	0.1438		-1.9458	
30		-0.00		-0.1065			-0.0165	0.2367	0.0872		-3.4464	. ————————————————————————————————————

	TEST	PART MA	CH #X10-		CONF 4#0F31 0		1 DEL20		TRANSITI			
INT	ALPHA	BÉTA	CN	CLH	CY	CLN	CLL	CA	CAB	CAF	кср	
1	-0.00	-0.00	0.0299	-0.0945	-0.0104	0.0252		0.2444	0.0793	0.1651	-3.1655	
Ž	2.01	-0.00	0.2410	-0.4162	-0.0101	0.0281	-0.0217	0.2499	0.0921	0.1577	-1.4274	
3	4.04	-0.00	0.6508	-0.9776	-0.008A		-0.0253	0.2569	0.0964	0.1605		
	6.02	-0.00		-1.7533	-0.0069	0.0279	-0.0273	0.2700	0-1036	0.1664	-1.7296	
<u></u>	10.01	-0.00_	1.9585	-2.6988 -3.7829	-0.0052 -0.0019		-0.0308 -0.0293	0.2942	0.1091	0.1851	-1.8499	
7	12.03	-0.00	2.5132	-4.9A46	0.0021	-0.0191	-0.0295	0.3184 0.3413	0.1230 0.1360	0.1954	-1.9315 -1.9834	
à	14.03	0.00	3.0555	-6-1405	-0.0004	-0.0460	-0.0317	0.3633	0.1456	0.2176	-2.0097	-
9	16.06	0.00	3.6920		-0.0063		-0.0195	0.3861	0.1573		-2.0276	
0	17.05	0.01	4.0125	-8.1555	-0.0064	-0.0763	-0.0126	0.4027	0.1691		-2.0325	
11	16.03	0.01			-0.0048		-0.0058	0.4181	0.1684	0.2497	-2,0320	
12	19.07	0.01		-9.4848	-0.0034	-0.1117	-0.0060	0.4429	0.1860		-2.0323	
13	20.06	0.01		-10.1030	-0.0014	-0.1073	-0.0060	0.4580	0.2087	0.2493	-2.0280	
14	21.03	0.01		-10.6537 -10.7438	0.0009	-0.1052 -0.1051	-0.0079	0.4632	0.2231	10+5.0	-2.0172	
15 16	22.06	0.01		-11.3134	-0.0035	-0.0807	0.0078	0.4582	0.2192	0.2390	-2.0230 -2.0036	
7	23.08	0.00		-11.7055	0.0084		-0.0095	0.4759	0.2408	0.2351	-1.9756	
is —	24.10	0.00		-12.1230	0.0259	-0.0982	-0.0083	0.4845	0.2577	0.2768	-1.9478	
19	24.10	0.00	6.2089	-12-1067	0.0222	-0.0978	-0.0065	0.4783	0.2631	0.2152	-1.9499	
20	25.13	0.00		-12.4977	0.0956	-0.2258	-0.0147	0.4861	0.2767	0.2093	-1,9240	
5 j	26.13	-0.00		-12.9055		-0.2947	0.0004	0.4994	0.2669	0.2325	-1.8938	<del></del>
22	27.14	0.00		-13-306/		-0.7046	0.0358	0.4871	0.2835	0.5036	-1.8710	
<u>23                                    </u>	28.20 28.19	0.01		-13.3616 -13.4605	0.6580_	-1.3295	0.1068	0.4696	_0.2520_	0.1876	-1.8306	
25	29.18	0.01		-13.7594	0.6766	-1.3615	0.1277	0.4718	0.3296	0.1422 0.1365	-1.8337 -1.8099	
26	30.23	0.01		-14.0973		-1.3149	0.1540	0.4614	0.3328	0.1287	-1.7828	
27	20.00	0.01			-0.0053		-0.0035	0.4018	0.2450	0.1568	-2.0459	
26	10.04	-0.00			-0.0064	0.0400		0.2957	0.1774	0.1182	-1.9626	
29	10.04				0.0050		-0.0289	0.2979	0.1521	0.1458	-1.9579	
30	-0-05	-0.00	0.0375	-0-1147	-0.0115	0.0332	-0.0143	0.2388	0.0952	0.1436	-3.0561	

27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8393 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7819 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.8770 0.1255 -1.6583 20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0714		OF 1				EOC) PI			NEL FACILI IL EFFECTS			ODYNAMIC WIND TUNNEL (4T
ALPHA BETA CN CLM CV CLN CLL CA CAB CAF RCP -0.00 -0.00 0.0326 -0.0992 -0.0996 0.0254 -0.0167 0.7039 0.0853 0.1585 -3.0043  2.01 -0.00 0.2869 -0.170 -0.0130 0.0359 -0.0237 0.2592 0.0824 0.1708 -1.5819 6.02 -0.00 1.0280 -1.0029 -0.0077 0.0359 -0.0237 0.2592 0.0824 0.1708 -1.5819 6.02 -0.00 1.0280 -1.0019 -0.0067 0.0284 -0.0273 0.2701 0.1050 0.1643 -1.7529 6.02 -0.00 1.0315 -1.8089 -0.0076 0.0355 -0.0254 0.2709 0.0951 0.1758 -1.7529 6.01 -0.00 1.4915 -2.0064 -0.0079 0.0332 -0.0320 0.2859 0.1103 0.1856 -1.8816 170.05 -0.00 2.0164 -3.9813 0.0005 0.0193 -0.0320 0.2859 0.1103 0.1856 -1.8816 170.05 -0.00 2.0164 -3.9813 0.0005 0.0193 -0.0304 0.3227 0.1175 0.2052 -1.0725 12.01 -0.00 2.5453 -5.1314 0.0033 -0.0177 -0.0306 0.3462 0.1316 0.1464 -2.0162 14.02 0.00 3.1396 -0.0367 0.0012 -0.0284 -0.0356 0.3668 0.1470 0.2174 -2.0582 17.05 0.00 4.0811 -8.3355 -0.0047 -0.0514 -0.0110 0.4519 0.1086 0.2466 -2.0582 17.05 0.00 4.0310 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1868 0.2466 -2.0512 18.04 0.01 4.4310 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1868 0.2466 -2.0512 19.06 0.01 4.7399 -9.7678 -0.0090 -0.0744 -0.0101 0.4519 0.1984 0.2535 -2.0012 20.03 0.01 5.0857 -10.0267 -0.0093 -0.0151 0.0158 0.0955 0.2713 -2.0512 21.00 0.00 5.7224 -11.5312 0.0153 -0.0154 -0.0168 0.4022 0.2176 0.2646 -2.0557 22.06 0.00 5.7224 -11.5312 0.0153 -0.0154 -0.0168 0.4022 0.2176 0.2646 -2.0557 22.10 0.00 6.3695 -12.0342 0.0193 -0.0845 0.0168 0.0422 0.2176 0.2640 -2.0557 22.10 0.00 7.3331 -12.0342 0.0193 -0.0845 0.0168 0.0492 0.2285 0.2649 -2.0573 24.11 0.00 6.3695 -12.0342 0.0193 -0.0845 0.0168 0.0492 0.2285 0.2649 -2.0573 24.11 0.00 6.3695 -12.0342 0.0193 -0.0845 0.0168 0.0492 0.2285 0.2649 -2.0557 25.13 -0.00 7.3331 -13.04540 0.0267 -0.5553 0.0047 0.0973 0.2689 0.2285 0.2649 -1.0843 27.20 0.00 7.3331 -13.04540 0.0553 -0.0575 0.0047 0.0973 0.2689 0.2285 0.2649 -1.0843 27.20 0.00 7.3331 -13.04540 0.0568 -0.0575 0.0047 0.0055 0.0040 0.2062 -1.0838 27.20 0.00 7.3331 -13.04540 0.0056 -0.0575 0.0047 0.0057 0.0057 0.0057 0.0059 0.2285 -1.0059											D=4	
-0.00 -0.00 0.0326 -0.0992 -0.0096 0.0254 -0.0167 0.7239 0.0853 0.1885 -3.0443  2.01 -0.00 0.6300 -1.0029 -0.0077 0.0359 -0.0237 0.2592 0.0024 0.1768 -1.4336  4.03 -0.00 1.0280 -1.0029 -0.0007 0.0284 -0.0273 0.2592 0.0024 0.1768 -1.4939  6.02 -0.00 1.0285 -1.6019 -0.0067 0.0284 -0.0273 0.2701 0.1058 0.1643 -1.7529  6.02 -0.00 1.0315 -1.6009 -0.0076 0.0354 -0.0273 0.2701 0.1058 0.1643 -1.7529  6.02 -0.00 1.0315 -1.6009 -0.0076 0.0354 -0.0273 0.2709 0.0951 0.1754 -1.7536  8.01 -0.00 2.0164 -3.59413 -0.0005 0.0193 -0.0320 0.2959 0.1103 0.1856 -1.0016  10.05 -0.00 2.0164 -3.59413 -0.0005 0.0193 -0.0320 0.2959 0.1103 0.1856 -1.0016  12.01 -0.00 0.5553 -5.1318 0.0033 -0.0127 -0.0306 0.3462 0.1316 0.2146 -2.0162  14.02 0.00 3.1396 -0.0335 -0.0037 -0.0284 -0.0356 0.3462 0.1316 0.2146 -2.0162  14.02 0.00 3.1396 -0.0335 -0.0047 -0.0284 -0.0356 0.3462 0.1316 0.2146 -2.0162  17.05 0.00 4.0811 -8.0335 -0.0047 -0.0561 -0.0178 0.4119 0.1708 0.2411 -2.0865  18.04 0.01 4.310 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1868 0.2401 -2.0865  18.04 0.01 4.309 -9.7678 -0.0090 -0.0744 -0.0101 0.4519 0.1908 0.2535 -2.0612  20.03 0.01 5.0857 -10.0267 -0.0039 -0.0754 -0.0168 0.4022 0.2176 0.2056 -2.0957  21.05 0.00 5.0444 -11.0020 0.0053 -0.0754 -0.0168 0.4022 0.2176 0.2064 -2.0957  22.06 0.00 5.7224 -11.5314 0.0124 -0.0953 -0.0168 0.4022 0.2176 0.2064 -2.0957  23.10 0.00 6.0561 -12.0342 0.0103 -0.0754 -0.0108 0.4022 0.2176 0.2064 -2.0957  24.11 -0.00 6.3695 -12.0342 0.0103 -0.0855 -0.0108 0.4022 0.2176 0.2064 -2.0957  25.13 -0.00 7.3031 -13.4554 0.2655 -0.5875 0.0047 0.4091 0.4086 0.2795 0.2285 0.2284 -1.0087  26.21 0.01 7.6778 -13.6813 0.3521 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.0958  27.20 0.00 7.3031 -13.4554 0.2655 -0.5875 0.0047 0.4097 0.4095 0.2785 0.2284 -1.0025 -1.0019  28.21 0.01 7.6778 -13.6813 0.3521 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.0958  29.28 0.01 7.6877 -10.0202 0.2659 -0.5875 0.0047 0.4095 0.2785 0.2065 -1.0059  20.20 0.00 7.3031 -13.4554 0.2655 -0.5875 0.0047 0.4095 0.2785 0.2065 0.2065 -1.0059  20.20 0.00 7.3031	MT										CAF	200
2.01 -0.00 0.2889 -0.0170 -0.0138 0.0346 -0.0203 0.2490 0.0927 0.1563 -1.0436   4.03 -0.00 0.6300 -1.0029 -0.0077 0.0359 -0.0237 0.2592 0.0024 0.1768 -1.5919   6.02 -0.00 1.0280 -1.8019 -0.0067 0.0284 -0.0273 0.2701 0.1058   6.02 -0.00 1.0315 -1.04089 -0.0076 0.0354 -0.0273 0.2701 0.1058   6.02 -0.00 1.0315 -1.04089 -0.0076 0.0354 -0.0273 0.2701 0.1058   6.01 -0.00 1.0315 -1.04089 -0.0079 0.0322 0.0320 0.2959 0.1103 0.1856 -1.6816   10.05 -0.00 2.0184 -3.9613 -0.0005 0.0193 -0.0304 0.3227 0.1175 0.2052 -1.9725   12.01 -0.00 2.5053 -5.1316 0.0033 -0.0127 -0.0306 0.3062 0.1316 0.2146 -2.0162   14.02 0.00 3.1396 -0.0370 0.0012 -0.0284 -0.0356 0.3062 0.1316 0.2146 -2.0162   17.05 0.00 4.0811 -8.0335 -0.0047 -0.0501 -0.0178 0.4119 0.1708 0.2411 -2.0065   18.04 0.01 4.0310 -9.1333 -0.0115 -0.0627 -0.0833 0.4328 0.1868 0.2466 -2.0612   19.06 0.01 4.7399 -9.7678 -0.0090 -0.0744 -0.0101 0.0519 0.1984 0.2535 -2.0612   20.03 0.01 5.0857 -10.0267 -0.0039 -0.0744 -0.0101 0.0519 0.1984 0.2535 -2.0612   21.00 0.00 5.0044 -11.0020 0.0053 -0.0754 -0.0108 0.0022 0.2176 0.2646 -2.0552   21.00 0.00 5.0044 -11.0020 0.0053 -0.0754 -0.0168 0.0022 0.2176 0.2646 -2.0557   22.06 0.00 5.7024 -11.0310 0.0124 -0.0011 -0.0188 0.0022 0.2176 0.2646 -2.0557   23.10 0.00 6.0561 -12.0332 0.0193 -0.0045 -0.0188 0.0022 0.2176 0.2646 -2.0557   24.11 -0.00 6.3095 -12.0245 0.0193 -0.0045 -0.0188 0.0032 0.2345 0.2646 -2.0551   25.13 -0.00 6.0561 -12.0332 0.0193 -0.0045 -0.0188 0.5016 0.2599 0.2417 -1.0208   25.13 -0.00 6.0501 -12.0345 0.0124 -0.0511 -0.0186 0.00792 0.2284 -1.0071   27.20 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0007 0.0085 0.5016 0.2599 0.2417 -1.0208   25.13 -0.00 6.0059 -1.00592 0.0559 0.05593 0.0085 0.0099 0.2417 -1.0208   25.13 -0.00 6.0087 -1.00892 0.0099 0.0085 0.0085 0.0099 0.2804 -1.0089   27.20 0.00 7.0061 -13.2015 0.1667 0.03475 0.0085 0.0085 0.0099 0.2804 -1.0089   27.20 0.00 7.0061 -13.2015 0.0069 0.0099 0.0085 0.0099 0.1822 0.1107 -1.0954   20.00 0.00 5.0809 -10.0022 0.0593 0.0085 0.0099 0.1822 0.1107 -1.0954	~.	_										
**************************************	7											
6.02 -0.00 1.0280 -1.0019 -0.0067 0.0284 -0.0273 0.2701 0.1058 0.1643 -1.7529 6.02 -0.00 1.0315 -1.8889 -0.0076 0.0354 -0.0254 0.2709 0.0951 0.1758 -1.7538 10.000 1.0315 -1.8889 -0.0079 0.0332 -0.0320 0.2959 0.1103 0.1856 -1.0816 10.05 -0.00 1.0315 -2.0064 -0.0079 0.0332 -0.0320 0.2959 0.1103 0.1856 -1.0816 10.05 -0.00 2.0184 -3.9813 -0.0005 0.0193 -0.0304 0.3227 0.1175 0.2052 -1.9725 12.01 -0.00 2.5553 -5.1316 0.0033 -0.0127 -0.0306 0.3662 0.1316 0.2146 -2.0162 14.02 0.00 3.1396 -0.0367 -0.0284 -0.0356 0.3468 0.1470 0.2178 -2.0582 17.05 0.00 4.0811 -8.0355 -0.0047 -0.0541 -0.0178 0.0179 0.1708 0.2411 -2.0565 18.04 0.01 4.0410 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1860 0.2406 -2.0651 19.06 0.01 4.0410 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1860 0.2460 -2.0612 19.06 0.01 4.7399 -9.7678 -0.0090 -0.0744 -0.0101 0.4519 0.1984 0.2535 -2.0612 19.06 0.01 5.0857 -10.0267 -0.0039 -0.0744 -0.0101 0.4519 0.1984 0.2535 -2.0612 19.06 0.01 5.0857 -10.0267 -0.0039 -0.0754 -0.0101 0.4519 0.1984 0.2535 -2.0612 19.06 0.00 5.4044 -11.0020 0.0053 -0.0754 -0.0168 0.4022 0.2176 0.2646 -2.0357 12.05 0.00 5.7224 -11.5314 0.0124 -0.0011 -0.0186 0.4022 0.2176 0.2646 -2.0357 12.310 0.00 6.0561 -12.0342 0.0193 -0.0845 -0.0189 0.5032 0.2345 0.2649 -2.0151 12.311 0.00 6.0561 -12.0342 0.0193 -0.0845 -0.0189 0.5032 0.2345 0.2649 -2.0151 12.311 0.00 6.0561 -12.0342 0.0193 -0.0845 -0.0189 0.5032 0.2345 0.2649 -2.0551 0.2649 -2.0551 0.2649 -2.0551 0.2649 -2.0551 0.2649 -2.0571 0.0047 0.4973 0.2669 0.2284 -1.0871 0.2665 0.2669 0.2884 -1.0871 0.006 0.007 0.006 -1.0078 0.0077 0.0085 0.0085 0.0085 0.2778 0.1085 0.2884 0.1089 0.2284 0.1089 0.2285 0.2687 0.1089 0.2284 0.1089 0.006 0.0077 0.0085 0.0085 0.0085 0.0085 0.2778 0.1085 0.1085 0.1097 0.0085 0.0085 0.0085 0.2778 0.1085 0.1097 0.0085 0.0085 0.0085 0.0085 0.2778 0.1085 0.1097 0.0085 0.0085 0.0085 0.0085 0.2778 0.1085 0.1097 0.1097 0.0085 0.0085 0.0085 0.2778 0.1085 0.1097 0.1097 0.0085 0.0085 0.0085 0.0087 0.0085 0.0085 0.0087 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0	Á.	_					0.0359					
6.02 -0.00 1.0315 -1.6087 -0.0076 0.0354 -0.0254 0.2709 0.0951 0.1758 -1.7536 10.055 -0.001 0.0951 0.4915 -2.0064 -0.0079 0.0332 0.2959 0.1103 0.1856 -1.0818 0.1758 -1.0818 0.1758 -0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0018 0.0		6.02		1.0280	-1.5019	-0.0067	4850.0			0.1058	0.1643	-1.7529
10.05	8 .		-0.00			-0.0076		-0.0254	0.2709	0.0951	0.1758	_1,7536
12.01		8.01	-0.00	1.4915	-2064	-0.0079	0.0332	-0.0320	0.2959	0.1103	0.1856	-1.0616
14.02 0.00 3.1396 -6.3367 0.0012 -0.0284 -0.0356 0.3668 0.1470 0.2178 -2.9582  17.05 0.00 4.0811 -8.4335 -0.0047 -0.0541 -0.0178 0.4119 0.1708 0.2411 -2.0465  18.04 0.01 4.4310 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1868 0.2460 -2.0612  19.06 0.01 4.7349 9.7678 -0.0090 -0.0744 -0.0101 0.4519 0.1984 0.2535 -2.0612  20.03 0.01 5.0857 -10.4267 -0.0039 -0.0724 -0.0151 0.4768 0.2055 0.2713 -2.0502  21.05 0.00 5.4044 -11.0020 0.0053 -0.0754 -0.0168 0.4022 0.2176 0.2646 -2.0357  22.06 0.00 5.7224 -11.5314 0.0124 -0.0911 -0.0166 0.4934 0.2285 0.2649 -2.0151  23.10 0.00 6.3695 -12.4245 0.0193 -0.0845 -0.0109 0.5032 0.2345 0.2667 -1.0071  24.11 -0.00 6.3695 -12.4245 0.0321 -0.0601 -0.0222 0.5073 0.2412 0.2666 -1.0001  25.13 -0.00 6.3695 -12.4245 0.1039 -0.1927 -0.0085 0.5016 0.2599 0.2417 -1.0205  26.16 0.00 7.0061 -13.2315 0.1667 -0.3475 0.0047 0.4073 0.2689 0.2284 -1.0433  27.20 0.00 7.3031 -13.4594 0.2675 -0.5475 0.0047 0.4073 0.2689 0.2284 -1.0438  27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2066 -1.0393  28.21 0.01 7.6770 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1025 -1.7019  29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177  30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6503  20.04 0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1187 -1.9954												
17.05 0.00 4.0811 -8.4335 -0.0047 -0.0541 -0.0178 0.4119 0.1708 0.2411 -2.0668 18.04 0.01 4.4310 -9.1333 -0.0115 -0.0627 -0.0083 0.4328 0.1868 0.2460 -2.0612 19.06 0.01 4.7349 -9.7678 -0.0090 -0.0744 -0.0101 0.4519 0.1984 0.2535 -2.0612 20.03 0.01 5.0857 -10.4267 -0.0039 -0.0720 -0.0151 0.4769 0.2055 0.2713 -2.0502 21.05 0.00 5.4044 -11.0020 0.0053 -0.0754 -0.0168 0.4022 0.2176 0.2646 -2.0357 22.06 0.00 5.7224 -11.5314 0.0124 -0.0911 -0.0186 0.4934 0.2285 0.2649 -2.8151 23.10 0.00 6.3695 -12.4245 0.0321 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.0571 24.11 -0.00 6.3695 -12.4245 0.0321 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.0508 25.13 -0.00 6.3695 -12.4245 0.1039 -0.1927 -0.0085 0.5016 0.2599 0.2417 -1.0508 25.13 -0.00 6.6301 -12.7467 0.1039 -0.1927 -0.0085 0.5016 0.2599 0.2417 -1.0508 26.16 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0047 0.4973 0.2669 0.2284 -1.0843 27.20 0.00 7.3031 -13.4594 0.2675 -0.5675 0.0491 0.4866 0.2704 0.2662 -1.0843 27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.4085 0.4792 0.2785 0.2006 -1.0838 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1025 -1.7019 29.28 0.01 8.0922 -13.6937 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4558 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1255 -1.6503 20.04 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716			_	_								
18.04												
19.06												
20.03												
21.05								_				
22.06												
23.10 0.00 6.0561 -12.0342 0.0193 -0.0845 -0.0189 0.5032 0.2345 0.2667 -1.9871 24.11 -0.00 6.3695 -12.4245 0.0321 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.9506 25.13 -0.00 6.6361 -12.7467 0.1039 -0.1927 -0.0085 0.5016 0.2599 0.2417 -1.9265 26.16 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0047 0.4973 0.2689 0.2284 -1.8843 27.20 0.00 7.3031 -13.4594 0.2075 -0.5475 0.0491 0.4866 0.2804 0.2062 -1.4848 27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8391 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7019 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2867 0.1255 -1.6583 20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0714												
24.11 -0.00 6.3695 -12.4245 0.0321 -0.0601 -0.0222 0.5073 0.2412 0.2660 -1.9506 25.13 -0.00 6.6381 -12.7487 0.1039 -0.1927 -0.085 0.5016 0.2599 0.2417 -1.9285 26.16 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0047 0.4973 0.2689 0.2884 -1.8843 27.20 0.00 7.3031 -13.4594 0.2675 -0.5475 0.0491 0.4866 0.2804 0.2062 -1.0438 27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.0391 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4003 0.2778 0.1825 -1.7819 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2875 0.1255 -1.6583 20.04 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.423 0.2687 0.1436 -2.0716												
25.13 -0.00 6.6381 -12.7487 0.1039 -0.1927 -0.0085 0.5016 0.2597 0.2417 -1.9265 26.16 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0047 0.4973 0.2689 0.2284 -1.8843  27.20 0.00 7.3031 -13.4594 0.2675 -0.5475 0.0491 0.4866 0.2804 0.2062 -1.8438 27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8393 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7819 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6563 20.04 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716												
26.16 0.00 7.0061 -13.2015 0.1667 -0.3475 0.0047 0.4973 0.2689 0.2284 -1.8843  27.20 0.00 7.3031 -13.4594 0.2675 -0.5475 0.0491 0.4866 0.2804 0.2062 -1.8438  27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8393  28.21 0.01 7.6776 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7819  29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177  30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6563  20.04 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716												
27.20 0.00 7.3031 -13.45% 0.2675 -0.5475 0.0491 0.4866 0.2804 0.2062 -1.8438 27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8391 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7619 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2778 0.1825 -1.7777 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2845 0.1491 -1.7177 20.04 0.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1255 -1.6563 20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0714 10.03 -0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1107 -1.9954												
27.20 0.00 7.2970 -13.4202 0.2692 -0.5583 0.0485 0.4792 0.2785 0.2006 -1.8393 28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7819 29.28 0.01 8.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.8770 0.1255 -1.6583 20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0714												
28.21 0.01 7.6778 -13.6813 0.3521 -0.7692 0.0753 0.4603 0.2778 0.1825 -1.7819 29.28 0.01 8.0922 -13.6947 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177 30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6583 20.04 0.00 5.0889 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716 10.03 -0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1187 -1.9954												
29.28 0.01 0.0922 -13.8997 0.4058 -0.8729 0.0951 0.4336 0.2845 0.1491 -1.7177  30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6563  20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716  10.03 -0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1187 -1.9954												
30.35 0.01 0.4847 -14.0702 0.4313 -0.9238 0.1250 0.4126 0.2870 0.1255 -1.6563 20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716 10.03 -0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1187 -1.9954												
20.04 0.00 5.0869 -10.5422 -0.0069 -0.0290 -0.0110 0.4123 0.2687 0.1436 -2.0716 10.03 -0.00 2.0243 -4.6393 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1187 -1.9954	<u> </u>											
10.03 -0.00 2.0243 -0.0343 -0.0037 0.0433 -0.0300 0.3009 0.1822 0.1107 -1.9954	5		0.00	5.0869	-10-5422	-0.0069						
-0.00 -0.00 0.0374 -0.1185 -0.0084 0.0314 -0.0150 0.2351 0.1055 0.1296 -3.1667		10.03	-0.00	2.0243	-4.6393	-0.0037	0.0433	-0.0300	0.3009	0.1822	0.1187	-1.9954
	7	-0.00	-0.00	0.0374	-0-1185	-0.0084	0.0314	-0.0158	0.2351	0.1055	0.1296	-3,1667
	7	-0.00	-0.00	0.0374	-0-1185	-0.0084	0.0314	-0.0158	0.2351	0.1055	0.1296	-3,1667
												<del></del>
											•	

	1 OF 1 1 OF 1						ISSILE TA	TE EFFECTS				
	TEST	PART MA	ACH RA10-		CONF_		1 DEL2		TRANSITI			-
INT	ALPHA	- eETA	c'n	CLH	CY	CLN	CLL	CA	CAR	CAF	XCP	
1	-0.00	-0.00	0.0336	-0.09AH	-0.0093	0.0763	-0.0146	0.2826	0.1035	0,1791	-2,9432	
2	-0.00	-0.00	0.0313	-0.0954	-0.0082	0.0765	-0-0145	0.2811	0.1056	0.1785	-3.0464	
. 3	-0.00	-0.00	0.0334	-0.0945	-0.0081	0.0228	-0.0145	_ 0.7836	0.0941		-2.8294_	
	7.03	-0.00	0.3028	-0.4416	-0.0086	0.0303	-0.0196	0.2863	0.0985		-1.4585	•
	4.03	-0.00		-1.0596	-0.0091 -0.0048	0.0352	0.0246_	0.2923	0.0973	0.1950_		· <del></del>
6	6.01	-0.00 -0.00	1.0694	-1.0652 -1.9261	-0.0068	0.0353	-0.0214	0.3009 0.3183	0.1026	0.2156	-1.6357 -1.8011	
A	8.02	-0.00	1.5488	-2.7876	-0.0051	0.0317	-0.0309	0.3376	0.1203	0.2173	-1.9290	
9	8.02	-0.00	1.5603	-3.0424	-0.0004	0.0317	-0.0336	0.3518	0.1145		-1.9502	
10	10.03	-0.00	2.0964	-4.2632	0.0015	0.0127	-0.0306	0.3721	0.1321		-2.0336	
11	12.00	-0.00	2.6614	-5.5087	0.0048	-0.0064	-0.0323	0.3944	0.1422		-2.0699	
15	14.03	0.00	3.2733	-6.8535	0.0021	-0.0263	-0.0356	0.4141	0.1533	0.2608	-2.0938	
13	16.01	0.00	3.8858		0.0039	-0.0466	-0.0278	0.4492	0.1660	0.2832		
14	17.04	0.00	4.2156	-8.8434	-0.0022	-0.0457	-0.0248	0.4670	0.1859	0.2811	-2.0979	
_15	18.03	0-00		-9.5171	-0.0060		-0.0505	0.4904	0.1985	0.5919		
16	19.03	0.00	_	-10.1425	-0.0032		-0.0235	0.5100	0.2123		-2.0750	
17	50.06	0.00		-10-7725	0.0203		-0.0302	0.5326	0.2172			<del></del>
16	21.07	0.00		-11.3394 -11.371c	0.0457	-0.1315 -0.1446	-0.0355 -0.0355	0.5349 0.5417	0.2341 0.2356	0.3062	-2.0306 -2.0242	
50	80.55	-0.00		-11.8814	0.0963	-0.2281	-0.0348	0.5441	0.2549	0.3082	-1.9919	
21	23.13	0.00		-12.3240	0.1117	_	-0.0309	0.5502	0.2560		-1.9502	
55	24.14	0.00		-12.7444	0.1222		-0.0221	0.5552	0.2615		-1.9002	
23	25.19	0.00		-13.0847		-0.3114	-0.0181	0.5419	0.2630	0.2789	-1.8497	
24	26.22	0.00	7.4576	-13.3731	0.1455	-0.3309	-0.0190	0.5247	0.2713	0.2534	-1.7932	
25	27.26	0.00		-13.6476	0.1765		-0.0268	0.5003	0.2769	0.2233	-1.7426	
95	27.29	-0.00		-13.6343				0.5114	0.2660	0.2454	-1.7302	
27	26.33	-0.00		-13.7628			0.0386_	0.4833	_ 0.2742_	_0.2091	-1.6619	
28	29.40	-0.01		-13.6951			-0.0367	0.4560	0.2771	0.1789	-1.5924	
59	30.47	-0.00		-13.9931	0.2904		0.0039_	0.4291	0.2642	0.1448	1.5401_	
30	20.05			-10.8756				0.4921	0.2600	0.5355	-2.0661	
31	10.01	-0.00		-4.3515				0.3523	0.1894	0.1629	-2.0563	
32	-0.00	0.00	0.0336	-0.1136	-0.0169	0.0335	-0.0145	0.2770	0.1166	0.1604	-3.1698	

	OF 1	RING DE	AFT OBHE	CENTER(A	EOC)			NEL FACILI		AER	ODANWIC AINO LONNEF (PL
	TEST	PART M.		-6 PH1			1 DEL2_	OEL3 DEL4		Ņ	
OINT	ALPHA	BÉTA	CN -	- CĹ4		CLN	CLL	CA -	CAB	CAF	XCP
1	0.00	-0.00	0.0159	-0.0267	-0.0169	0.0562	-0.0139	0.4924	0.2223		-1.6792
3	5.05	-0.00	0.2991	-0.4262	-0.0193	0.0717	-0.0180	0.4966	0.2052	0.2914	-1.4248
Z	2.02	-0.00	0.2961	-0.4250	-0.0180	0.0674 0.0868	-0.0163 -0.0168	0.4957	0.1962		1·4256
6	4.04	-0.00	0.6536	-1.0728	-0.0149		-0.0200	0.5033	0.1799	0.3234	-1.6414
7	6.01	-0.01	1.0624	-1.9232	-0.0200	0.0960	-0.0212	0.5295	0.1790	0.3505	-1.8102
8	6,01	-0.00	1.0663	-1-4252	-0,0130	0.0668	-0.0230	0.5251	0.1951	0.3299	-1.0022
9	8.02	-0.01	1.5434	-7.9661	-0.0154	0.0515	-0.0301	0.5557	0.2128	0.3429	-1.9210
10	10.01	-0.01	2.0657_		-0.0082		0.0271	0.5858	0.2239		-2.0096
11 12	12.02	-0.00	3.1707	-5.3062 -6.4381	-0.0039 -0.0016	0.0468	-0.0316 -0.0276		0.2369 0.2455	0.3748	-2.0368 -2.0305
13	16.05	0.00		-7.5580	-0.0031	-0.0139	-0.0193	0.6717	0.2572		-2.0066
14	17.04	0.00	4.0652		-0.0057	-0.0220	-0.0137	0.6824	0.2721	0.4103	-1.9917
15	18.06	0.00	4.3832		-0.0083	-0.0125	-0.0183	0.6984	0.2756	0.4227	
16	19.07	0.00	4.7036	-9.12/2	0.0220	_0.0204	-0.0154	0.7112	0.2849	0.4263	-1-9405
17	50-13	-0.00		-9.6111	-0.0022	-0.0090	-0.0217	0.7214	0.2937		-1.9074
18	21.14	-0.00		-10.063	0.0205		-0.0237		0.2983	0.4251	-1-8702
19 20	22.17	-0.01		-10.4957	0.0386 0.0476		-0.0329 -0.0451	0.7130 0.7057	0.2992 0.3022		-1.8229 -1.7689
21	24.25	-0.01		-11.2385	0.0473	-0.02+6	-0.0502		0.3065	0.3930	-1.7203
22	25.30	-0.01		-11.5856	0.0219		-0.0477		0.3078	0.3867	-1.6724
23	26.34	-0.00		-11.9117	0.0878		-0.0234		0.3140	0.3750	-1.6282
24	27.39	-0.00	7.6A30	-12-2102	0.0891	-0.1806	-0.0200	0.6863	0.3212	0.3651	-1 -5893
25	28.43	-0.00		-12-4939	0.1111	-0-5566	-0.0198		0.3218	0.3571	-1-5637
26	29.50	-0.00		-12-7012	0,1285	-0.2708	-0.0137		0.3284	0.3390	
27 28	30.55	0.00		-12.9623 -9.6640	0.2482	-0.5305	0.0171		0.3383	0.3236	-1.4613
29	20.11	-0.00		-4.2512	-0.0145	0.0200	-0.0169 -0.0250		0.3257		-1.9195 -2.0332
30		-0.01		-4.2152			-0.0248		0.2595	0.3099	-5.0335
		-0.00		-0-0412			-0.0062		0.1921	0.2895	

	1 OF 1		<del></del>	-		MARTIN M	TISSILE TA	IL EFFECTS				
_	TEST		ACH PX10-	6 PHI	CONF 84#0F31	L DEL	0 0	DEL3 DEL4				
<b>T</b>	ALPHA	BETA	CN	Cr.₩	CY	CLN	CLL	CA	CAB	CAF	XCP	
	0.00	-0.00	-0.0108	0.0663	-0.0048	0.0154	-0.0080	0.4987	0.1944	0.3044	-6.1241	
	2.01	-0.00	0.7841	-0.3551	-0.0045	0.0209	-0.0082	0.5045	0.1855	0.3190	-1.2498	
	4.02	-0.06	0.6355	-0.9924		0.0258	-0.0123	0.5118	0.1966	0.3252	-1.5615	
	6.04 B.03	-0.00	1.05#0	-1.8675		0.0163	-0.0165 -0.0176	0.5350	0.1930	0.3420	-1.765) -1.8807	
_	8.03	-0.00	1.5371	-7.8927			-0.0161	0.5645	0.2214	0.3430	-1.8819	
	10.05	-0.00	2.0480	-3.9626		· · · · · ·	-0.0168	0.5914	0.2244	0.3670	-1.9349	
_	12.03	-0.00	2.5772	-5.0225			-0.0212	0.6098	0.2321	0.3777	-1.9488	
	14.04	-0.00	3.1291	-6.0844	0.0154	-0.0384	-0.0216	0-6324	0.2396	0.3927	-1.9444	
	16.10	0.00	3.7272	-7.1204	- • - • -		-0.0181	0.6538	0.2430	0.4108	-1.9104	
	_17.10	0.00	4.0303	-7.5868			-0.0143	0.6671	0.2521		-1.8825	
	18.14	0.00	4.3581	-8.0324			-0.0188	0.6794	0.2583	0.4211	-1.8431	,
	19.14	0.00	4.7031	-8.4477			-0.0219	0.6856	0.2636	0.4219	-1.7962	
	20.17	-0.00	5.0574	-0.6116			-0.0307 -0.0329	0.6851 0.6865	0.2673	0.4178	-1.7423 -1.6939	
		-0.00		-9.5736			-0.0324	0.6807	0.2759		-1.6384	<del></del>
	23.31	-0.00		-9.9006			-0.0278	0.6748	2082.0	0.3946	-1.5948	
<del>-</del> ·	24.37	-0.00		-10.1756			-0.0219	0.6676	0.2833		-1.5533	
	25.42			-10-517			-0.0174	0.6649	0.2847		-1.5074	
	26.45	-0.00	7.3849	-10.457	0.1600	-0.3162	-0.0104	0-6647	0.2909	0.3738	-1.4702	
		0.00		-11.1860				0.6638	_0.2968		-1.4344	
		-0.00		-11-4744				0.6584	0.2993		-1.3989	
		0.00		-11.772			0.0065	0.6595	_0.3103_		<u>-1.3694</u>	
	30.66			-12.0491 -A.6901			0.0064	0.6591	0.3194		-1.3411	
	10.33			-4.0164				0.6677	0.3135		-1.7476 -1.9581	
	0.00		0.0012					0.4975	0.2133		18,4869	
									.9 4 2 3 3 5	7,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
_												
			· · · · · · · · · · · · · · · · · · ·									
_												
•				~~·······		<del></del>	• • • • • • • • • • • • • • • • • • • •					

	OF 1	RING DE	VEL OPHENI	CENTER (A	EDÇ)P			NEL FACILIT		AER	DOYNAMIC WIND TUNNEL	(41)
	TEST		ACH RX10-		CONF .	L. DEL			TRANSIT			
	1	162 1.	3v 2.3	0.0 8	4#0F31 0	.0	0 0	0 0	UNKHOW	•		
NT "	ALPHA	BETA	CN	CLH	CA	CLN	CLL	CA	CAB	CAF	XCP	
	0.01	0.00	0.0030	0.0476	0.0009	-0.0059	0.0001	0.4830	0.1828		16.0505	
	2.04 4.02	-0.00	0.7976	-0.3529	0.0022	0.0141	-0.0013 -0.0054	0.4870 0.4933	0.1882	0.2988	-1.2064 -1.51 <b>32</b>	
<del></del>		-0.00	1.0690	-1.8248	-0.0010	0.0347		0.5162	0.1902		-1.7076	
,		-0.00	1.5027		0.0050	0.0289	-0.0134	0.5449	0.1964		-1.8042	
,	10.05	0.00	2.0090		-0.0135	0.0187	-0.0152	0.5646	0.2048	0.3598	-1.6437	
	12.07	-0.00	2.5196	-4.7186	0,0090	-0.0063	-0.0167	0.5860	0.2145	0.3716	-1.8728	
}	14.10	-0.00	3.0255	-5.6194	0.0155	-0.0345	-0.0159	0.6063	0.2226	0.3837	-1.0574	
<u>}</u>	16.15	0.00	3.6527		0.0286	-0.0679	-0.0139	_0.6208	0.2313		-1.8064	
)	17.14	0.00	3.9714		0.0272	-0.0758 -0.0669	-0.0131 -0.0123	0.6285 0.6314	0.2393	0.3892		
	_18.16 19.21	-0.00	4.6781		0.0224	-0.0601	-0.0154	0.6334	0.2492	0.3842	1.7125	
•	20.27	-0.00	5.0470		0.0797	-0.0581	-0.0167	0.6366	0.2532	0.3834	-1.6050	
-	20.27	-0.00	5.0676		0.0233	-0.0473	-0.0174	0.6324	0.2542	0.3782	-1.6041	
5		-0.00	5.4183	-8.4239	0.0314	-0.0643	-0.0208	0.6353	0.2570	0.3783		
		-0.00	5.7900		0.0461	-0.0862	-0.0217	0.6357	0.5635	0.3725	-1.5110	
<u>'</u>	23.43	-0.00	6.1680		0.0646	-0.1184	-0.0227	0.6387	0.2695		-1.4699	
3	24.46	-0.00	6.5433		0.0785	-0.1563	-0.0200	0.6407	0.2749	0.3657		
<u> </u>	25.51	-0.00	6.9295		0.1214	-0.2441	-0.0095	0.6412	0.2806	0.3605	-1.3939	
1	25.51	0.00	6.9093 7.3206		0.1137	-0.2264	0.0094	0.6378	0.2861 0.2902	0.3516	-1.392 <b>6</b> -1.3555	
	27.62	0.00-		-10-2349		-0.3847	0.0152	0.6491	0.2970	0.3521	-1-3227	
	27.63	0.00		-10.7226	0.1620	-0.3615	0.0153	0.6452	0.3091	0.3361		
<u>-</u>	28.67			-10.4909	0.1659		0.0078	0.6522	0.3123		-1.2931	
<u> </u>	29.72	-0.00		-10.8268	0.1566	-0.2820	0.0005	0.6644	0.3205		-1,2710	
5	29.72	-0.00		-10.6192	0.1566		0.0005	0.6619	0.3260	0.3359	-1.2698	
'	30.77			-11.1876		0.2259	0.0042	0.6673	_0.3360		-1-2517	
		-0.00		-8-1125		-0.0369	-0.0132	0.6208	0.3009		-1.6030	
<u> </u>	10.06	-0.01	- 2.0012		-0.0036	0.0267	-0.0106 0.0042	0.5531 0.4840	0.2755		-1.0712	
	V. 00	0.00	0.0010	0.0434	-0.0034	0.0071	0.8042	0.4640	0.2376	0.2443	44,0934	
										<del></del>		
						·						
											•	

12.06 -0.00			17.			ISSILE TAI		<del></del>	<del></del>			<u>i</u> or <u>i</u>	ET
1NT ALPMA BETA CM CLM CY CLM CLL CA CAB CAF XCP 1 -0.00 0.00 0.00 0.00 0.00 0.00 0.00 0						1 DELS (	L DEL						
1 -0.00				_	0 0	<u>.                                    </u>	•0			2.3	166 0.6	-	
3 -0.00 0.00 0.0023 -0.0119 -0.0009 0.0164 -0.0113 0.2551 0.00948 0.1507 -5.1566 1.99 -0.00 0.2193 -0.3096 -0.0089 0.0700 -0.0134 0.2579 0.0948 0.1631 -1.4116 5 4.04 -0.00 0.4668 -0.7056 -0.0063 0.0213 -0.0137 0.2597 0.1105 0.1002 -1.5114 6 4.04 -0.00 0.4667 -0.7146 -0.0075 0.0229 -0.0136 0.2595 0.1090 0.1505 -1.5301 7 0.03 -0.00 0.7566 -1.7357 -0.0091 0.0405 -0.0154 0.2732 0.1047 0.1685 -1.6375 9 8.06 -0.00 1.0714 -1.9538 -0.0102 0.0553 -0.0170 0.2898 0.1256 0.1642 -1.6278 10 10.01 -0.00 1.3346 -2.6412 -0.0099 0.0541 -0.0152 0.3008 0.1356 0.1720 -1.8914 11 12.06 -0.00 1.7332 -3.3119 -0.0039 0.0272 -0.0138 0.3323 0.1464 0.1855 -1.9918 12 14.02 -0.00 2.1346 -4.1662 -0.0118 0.0448 -0.0174 0.3474 0.1618 0.1855 -1.9918 13 16.07 -0.00 2.4821 -4.6669 -0.0333 0.0965 -0.0102 0.3472 0.1753 0.1719 -1.8882 14 18.08 -0.00 2.7404 -4.8125 -0.0355 0.0641 -0.0203 0.3465 0.2115 0.1350 -1.7561 16 19.09 0.00 2.4866 -4.8823 -0.0233 0.0166 -0.0267 0.3517 0.2276 0.1240 -1.6002 17 20.12 0.00 3.0448 -4.9566 -0.0145 -0.0279 -0.0349 0.3586 0.2572 0.1014 -1.6279 18 21.15 0.00 3.1844 -4.9912 -0.0007 -0.0554 -0.0391 0.3665 0.2637 0.0969 -1.5674 19 22.14 0.00 3.5174 -5.0176 0.0181 -0.0866 -0.0349 0.3653 0.2779 0.0874 -1.5124 22 25.24 -0.01 3.6534 -5.0730 0.0440 -0.1355 0.0564 0.3873 0.2779 0.0874 -1.5124 22 25.24 -0.01 3.6534 -5.0730 0.0400 -0.1355 0.0965 0.3998 0.3147 0.0751 -1.3190 23 26.25 -0.01 3.615 -5.0272 -0.0161 0.1276 -0.0054 0.3898 0.3147 0.0751 -1.3190 24 27.28 -0.02 4.6681 -5.6936 0.2499 -0.0265 0.3991 0.3303 0.0616 -1.2764 25 29.33 -0.01 4.6681 -5.6936 0.2479 -0.2205 0.1110 0.3992 0.3740 0.0252 -1.2337 26 29.33 -0.01 4.6681 -5.6936 0.2479 -0.2205 0.1110 0.3993 0.3992 0.3740 0.0252 -1.2337 27 29.32 -0.01 4.6681 -5.6936 0.2479 -0.2205 0.1110 0.3993 0.3992 0.3740 0.0252 -1.2337 28 30.36 -0.00 4.6971 -5.8307 0.0318 -0.0265 0.0151 0.3552 0.3219 0.0336 -1.2063 30 10.03 -0.00 1.2249 -2.8057 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0336 -1.2063 30 10.03 -0.00 1.2249 -2.8057 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0338 -1.2063													THE
1.99													1
5													<u>.</u>
6											-		-š
7 6.03 -0.00 0.7546 -1.2357 -0.0091 0.0405 -0.0156 0.2732 0.1047 0.1685 -1.6278 9 8.06 -0.00 1.0714 -1.4538 -0.0102 0.0543 -0.0170 0.2898 0.1256 0.1642 -1.8236 10 10.01 -0.00 1.3954 -2.6012 -0.0009 0.0541 -0.0152 0.3008 0.1368 0.1720 -1.8914 11 12.06 -0.00 1.7332 -3.3119 -0.0039 0.0272 -0.0138 0.3323 0.1464 0.1859 -1.9108 12 14.02 -0.00 2.1346 -4.1662 -0.0118 0.0408 -0.0174 0.3474 0.1618 0.1855 -1.9516 13 16.07 -0.00 2.4821 -4.6069 -0.0333 0.0905 -0.0102 0.3472 0.1753 0.1719 -1.88082 14 18.08 -0.00 2.7404 -4.6125 -0.0345 0.0641 -0.0203 0.3465 0.2115 0.1350 -1.7561 16 19.09 0.00 2.4846 -4.6823 -0.0233 0.0166 -0.0207 0.3517 0.2276 0.1240 -1.6002 17 20.12 0.00 3.0448 -4.9966 -0.0145 -0.0229 -0.0349 0.3966 0.2572 0.1014 -1.6279 18 21.15 0.00 3.1644 -4.9912 -0.0007 -0.0544 -0.0391 0.3606 0.2637 0.0969 -1.5676 19 22.14 0.00 3.5024 -5.0677 0.0351 -0.0866 -0.0434 0.3653 0.2779 0.0874 -1.5124 22 23.21 -0.00 3.5024 -5.0677 0.0351 -0.0866 -0.0405 0.3723 0.2866 0.0877 -1.4469 22 23.21 -0.00 3.6534 -5.0730 0.0440 -0.1345 -0.0542 0.3817 0.2987 0.0829 -1.3886 23 26.25 -0.01 3.8115 -5.0272 -0.0161 0.1276 -0.0054 0.3898 0.3147 0.0751 -1.3190 24 27.28 -0.02 4.2269 -5.3439 0.0700 0.2333 0.0965 0.3996 0.3611 0.0385 -1.2748 25 28.29 -0.01 4.6357 -5.4725 0.1339 0.0576 0.0943 0.3992 0.3740 0.0252 -1.2337 26 29.33 -0.01 4.6771 -5.6476 0.2361 -0.2055 0.1110 0.3993 0.3992 0.3740 0.0252 -1.2337 28 30.36 -0.00 4.8971 -5.6476 0.2479 -0.2280 0.1186 0.3973 0.4302 -0.0329 -1.2137 28 30.36 -0.00 4.8971 -5.6476 0.2479 -0.2280 0.1186 0.3973 0.4302 -0.0329 -1.2137 28 30.36 -0.00 4.8971 -5.6476 0.2479 -0.2280 0.1186 0.3973 0.4302 -0.0336 -1.1906 29 20.31 -0.00 3.0240 -4.9389 -0.0162 -0.0339 -0.0151 0.25769 0.0336 -1.1906													6
10						-0.0154	0.0405	-0.0091	-1.2357		-0.00	6.03	7
11	· · · · · · · · · · · · · · · · · · ·												9
12													-
13	<del></del>							_					
16													
16													
18													16
19		.6279	0.1014	0.2572	0.3586	-0.0349	-0.0279	-0.0145	-4.9566	3.0448			17
20											0.00_	21.15	
21													_
22 25.24 -0.01 3.4115 -5.0272 -0.0161 0.1276 -0.0054 0.3898 0.3147 0.0751 -1.3190 23 26.25 -0.01 3.9927 -5.0980 -0.0144 0.2615 0.0225 0.3951 0.3334 0.0618 -1.2768 24 27.28 -0.02 4.2269 -5.3439 0.0700 0.2333 0.0965 0.3996 0.3611 0.0385 -1.2643 25 28.29 -0.01 4.4357 -5.4725 0.1339 0.0576 0.0943 0.3992 0.3740 0.0252 -1.2337 26 29.33 -0.01 4.6771 -5.6476 0.2361 -0.2055 0.1110 0.3983 0.3923 0.0060 -1.2075 27 29.32 -0.01 4.6681 -5.6436 0.2479 -0.2880 0.1186 0.3973 0.4032 -0.0329 -1.2197 28 30.36 -0.00 4.8971 -5.8307 0.3183 -0.4263 0.1213 0.3912 0.4249 -0.0336 -1.1906 29 20.11 0.00 3.0240 -4.9389 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0333 -1.6306 30 10.03 -0.00 1.4249 -2.8057 -0.0084 0.0397 -0.0151 0.2769 0.1827 0.0942 -1.9691													
23													
24 27.28 -0.07 4.2269 -5.3439 0.0700 0.2333 0.0965 0.3996 0.3611 0.0385 -1.2643 25 28.29 -0.01 4.4357 -5.4725 0.1339 0.0576 0.0943 0.3992 0.3740 0.0252 -1.2337 26 29.33 -0.01 4.6771 -5.6476 0.2361 -0.2055 0.1110 0.3983 0.3923 0.0060 -1.2075 27 29.32 -0.01 4.6681 -5.6436 0.2479 -0.2280 0.1186 0.3973 0.4302 -0.0329 -1.2197 28 30.36 -0.00 4.8971 -5.8307 0.3183 -0.4263 0.1213 0.3912 0.4269 -0.0339 -1.0196 29 20.11 0.00 3.0240 -4.9389 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0333 -1.6306 30 10.03 -0.00 1.4249 -2.8057 -0.0084 0.0397 -0.0151 0.2769 0.1827 0.0942 -1.9691													
25													_
26						0.0943	0.0576	0.1339	-5.4725				25
28 30.36 -0.00 4.8971 -5.8307 0.3183 -0.4263 0.1213 0.3912 0.4249 -0.0336 -1.1906 29 20.11 0.00 3.0240 -4.9389 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0333 -1.6306 30 10.03 -0.00 1.4249 -2.8057 -0.0084 0.0397 -0.0151 0.2769 0.1827 0.0942 -1.9691		.2075	0.0060_	0.3923_	0.3963	0-1110	-0.2055	0.2361	-5.6476	4.6771		29.33	56
29 20,11 0.00 3.0270 -4.9389 -0.0162 -0.0339 -0.0351 0.3552 0.3219 0.0333 -1.6306 30 10.03 -0.00 1.4249 -2.8057 -0.0084 0.0397 -0.0151 0.2769 0.1827 0.0942 -1.9691	•									_			_
30 10.03 -0.00 1.4249 -2.8057 -0.0084 0.0397 -0.0151 0.2769 0.1827 0.0942 -1.9691													
	-												
		,,,,,,,	441105	001500	4653.0	-040113	0.0003	-0.0110	-011501	0.0213	0.00	-0401	<b>J.</b>
·													
·												<del></del>	
		•											
	···			<u> </u>									
		-				·	····		<del></del>				

INOLD I	OF 1		AFFOHENT.	CENTER (A	EDC)P	HARTIN M	ISSILE T	NNEL FACILI'	DATA	AER	DOANWAIC AIMD TONNE	
	TEST 1		ACH RX10=		CONF 4m0Fl1 0	L DEL	DEL2		TRANS11			
POINT	ALPHA	BFTA	ČN	CLM	C¥	CLN	_ ciī	CA	CAR	CAF	ice	
1	-0.00	0.00	0.0126	-0.0813	-0.0106	0.0086	-0.0126	0.2447	0.0979	0.1468	-6,4352	
2	2.02	0.00	0.7351	-0.3963	-0.0082	0.0101	-0.0128	0.7485	0.0986	0.1499	-1 -6858	
.3	•.00	0.00	0.4777	-0.7796	-0.0068	0.0107	-0.0131	0.2524	0.1046	0.1478	-1.6319	
•	6.05	-0.00	0.7623	-1.3226	-0.0107		-0.0148		0.1132	0.1509	-1.7354	
?		-0.00_	_ 1.0807	2.0014	-0.0011		-0.0168	0.2816	0.1246	0.1570	-1.8519	
7	8.04 10.01	-0.00	1.0830 1.4201	-2.0314 -2.7465	-0.0079 -0.0112		-0.0163 -0.0145		0.1227 0.1378	0.1592 0.1658	-1.8757 -1.9340	
<u> </u>	15.04	-0.00	1.7376	-3.3466	-0.00112	0.0284	-0.0132		0.1463	0.1806	-1.9260	
	14.02	-0.00		-4.1460	-0.0092	0.0337	-0.0151		0.1670		-1.9475	
10	16.05	-0.00	2.4464	-4.5665	-0.0308	0.0893	-0.0080		0.1761		-1.8666	
11	17.04	-0.00	2.5969		-0.0330		-0.0119		0.1841	0.1715	-1.6088	
12	18.09	-0.00	2.7553	-4.8073	-0.0366	0.0628	-0.0197	0.3608	0.1973	0.1634	-1.7429	
13	19.08	0.00	2.9056	-4.8960	-0.0210	0.0163	-0.0240	0.3658	0.2225	0.1433	-1.6850	
14	20.15	0.00	3.0695	-4.9795	-0.0125		-0.0320		0.2425		-1.6223	
_15	20.15	0,00	3.0565_	-4.4618	-0.0258	-0.0211			0.2555		1,6234	
16	21.13	0.00		-5.0023	-0.0005	-0.0419			0.2703		-1.5643	
17		-0.00		5.0637	0.0098	-0.0442			0.2872		1.5028	
18	23.20	-0.00		-5.0912	-0.0135	0.0651	-0.0149		0.3032		-1.4411	
20	25.20	-0.0¢	3.7262	-5.1323 -5.0547	-0.0289	-0.0953 0.3130	0.0259		0.3090	0.0912	-1.3774 -1.3143	
21	26.26	-0.01		-5.1186	-0.0068	0.2515	0.0251		0.3485		-1.2602	
22	27.31	-0.05		-5.3696	0.0670	0.5550	0.0963		-0.3709	0.0434	-1.2457	
23	28.30	-0.02		-5.5663	0.2230	-0.0362	0.1316		0.3946	0.0263	-1.2277	
24	29.36	-0.01		-5.6168	0.2302	-0.1427	-0.1075		0.4086	0.0015	-1.1023	
25	30.39	-0.01		-5.7581	0.3644	-0.4253	0.1304		0.4208	-0.0185	-1.1536	
26	20.12	-0.00		-4.9567		-0.0037	-0.0244		0.3374	0.0352	-1.6247	
27		-0.00		-2.8724	-0.0109	0.0526	0.0145		0.1923	0.0910	-1.9899	
58	-0.01	0.00	0.0230	-0.1348	-0.0080	0.0047	-0.0106	0.2380	0.1190	0.1190	-5.8698	_
			···-		<del></del>	<del></del>						
			<del></del>									
											<del>-</del> :	

	TEST	PART M	NCH RX10-		COMF 4#0F11 0	L DEL	DETS	DEL3 DEL4	TRANSITI	Dir	
INT	ALPHA	BETA			CY	CLN	CLL	CA	CAB	CAF	ACP
1	-0.00	0.00	0.0146	-0.0901	-0.007A		-0.0104	0.2496	0.0927		-6,1674
2	2.02	0.00	0.2412	-0.4031	-0.0049	0.0128	-0.0123	0.2522	0.1043	0.1480	-1.6712
<u>-</u>	6.00	-0.00_	0.4880 0.7734	-0.8236	-0.0061		-0.0141	0.2563 0.2657	0.1085	0.1477	-1.6877 -1.7850
5		-0.00		-2.1009	-0.0089	0.0528	-0.0172	0.2856	0.1210	0.1646	
<u></u> -	10.02	-0.00	1.4648	-2.6594	-0.0126	0.0693	-0.0137	0.2982	0.1302	0.1679	-1.9454
7	12.04	-0.00	1.7614	-3.3677	-0.0119	0.0490	-0.0092	0.3436	0.1427	0,2009	
9	14.01	-0.00	2.1316	-4.1067	-0.0110	0.0395	-0.0160	0.3616	0.1839	0.1777	-1.9266
0		-0.00		4.6847	0.0165_	0.0260	0.0182	0.3789	D.1950_	0.1839	-1.8821
1		-0.00		-4.9611			-0.0235	0.3930	7.005.0	0.1863	-1.8493
<u>?</u>	18.11	_ 0.00		-5-1050		0.0193	-0.0271	0.3949	0.2199		-1.7960
3	19.13	0.00	3.0100 3.1463	-5.2173 -5.2567	-0.0192 -0.0079	-0.0020	-0.0329	0.4014	0.2441		-1.7333
5	21.19	-0.00	3.3493	-5.3840	0.0103	-0.0435	-0.0314	0.4143	0.2617	0.1435	-1.6708 -1.6075
6		-0.01	3.5228		0.0000		0.0038	0.4159	0.3003	0.1155	-1.5336
7	22.21	0.00		-5.4447		-0.0623	-0.0248	0.4163	0.3117	0.1045	
8	23,18	-0.01	3.7196		-0.0214	0.2614	0.0226	0.4265	0.3183		-1.4671
9	24.20	-0.03	3.8933	-5.4270	0.0400	0.3495	0.0464	0.4332	0.3258	0.1074	-1.3939
0	25.22	-0.02	4.0806	-5.4751	-0.0121	0.4354	0.0761	0.4398	0.3462	0.0936	-1.3417
1	25.23	-0.02	4.0923	-5.4607	-0.0173	0.4361	0.0819	0.4394	0.3489	0.0905	
S	26.29	-0.02	4.3366	5.4570	0.0469	0.1927	0.0110	0.4419	_0.3607_	0.0815	
3	27.36	-0.02		-5.3711	0.0743	0.2052	0.0632	0.4377	0.3811		-1.1839
5	29,42	-0.01 -0.00		-5.2461 -5.1379	0.1489	<u>-0.1526</u>	_0.0505	0.4530_	_0.3853_		-1.1002
6	30.51	-0.01		-5.0324	0.2404	-0.2428 -0.3498	-0.0140	0.4523	0.4311	0.0212 0.0017	
7	20.13	-0.00	3.1900	-5.3455	-0.0064	0.0620		0.4102	0.3671	0.0432	
30	10.02	-0.00		-2.9477		0.0681		0.2817	0.1580		-1.9902
11	-0.01	0.00			-0.0088		-0.0087	0.2449	0.1291		-5.6089
1					(21-1)						

TEST PART MACH RRIO-6 1 160 0.50 2.3 0.0 8 mOFF11 0.0 0 0 0 UNKNOWN  T ALPHA 86 TA CN CLM CY CLM CLL CA CA8 CAF XCP  -0.01 0.00 0.0190 -0.1106 -0.0098 0.0078 -0.0086 0.2518 0.0820 0.1998 -5.8219  2.02 0.00 0.2300 -0.0153 -0.0075 0.0091 -0.0121 0.2534 0.0977 0.1557 -1.7351  6.03 -0.00 0.7679 -1.0017 -0.0000 0.0327 -0.0137 0.2672 0.1134 0.1530 -1.7238  6.03 -0.00 0.7679 -1.0017 -0.0000 0.0327 -0.0151 0.2550 0.1041 0.1510 -1.7238  8.02 -0.00 1.2322 -2.1541 -0.0104 0.0556 -0.0151 0.2851 0.1145 0.1706 -1.9379  10.02 -0.00 1.0910 -2.7075 -0.0114 0.0556 -0.0151 0.2851 0.1145 0.1706 -1.9379  12.03 -0.01 1.8506 -3.6877 -0.0230 0.1122 -0.0005 0.3092 0.1605 0.1605 0.1607 -1.0010  12.03 -0.00 2.1322 -0.1614 -0.0007 0.0067 0.0067 0.00151 0.2851 0.100 0.1292 0.1726 -1.9903  14.02 -0.00 2.1322 -0.1614 0.0007 0.0067 0.0067 0.0016 0.3725 0.1736 0.1988 -1.9358  16.04 0.00 2.5228 -0.6012 -0.0183 0.02299 -0.0211 0.3878 0.1957 0.1981 -1.9053  17.05 -0.00 2.7071 -5.0628 -0.0176 0.0763 -0.0230 0.3921 0.2131 0.1791 -1.8702  17.07 -0.00 2.9004 -5.3005 -0.0266 0.0346 -0.0281 0.4006 0.2270 0.1796 -1.8026  19.10 -0.00 3.0767 -5.457 -0.0139 0.0271 -0.0286 0.4155 0.2730 0.1615 1.7026  21.11 -0.01 3.018 -5.5575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1434 -1.6438  22.18 -0.01 3.618 -5.5575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1434 -1.6438  22.18 -0.01 3.6198 -5.5575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1436 -1.6438  22.18 -0.01 3.7079 -5.0169 0.0000 0.1843 0.0184 0.4253 0.4319 0.1115 -1.7026  23.18 -0.01 3.7079 -5.0169 0.0000 0.1843 0.0184 0.4253 0.3137 0.1116 -1.4628  24.25 -0.02 4.0004 -5.5507 0.0000 0.1843 0.0000 0.3798 0.0803 -1.2866  25.30 -0.02 4.0004 -5.5507 0.0266 0.3437 0.0000 0.4830 0.3137 0.1116 -1.6438  25.30 -0.02 4.0004 -5.5507 0.0000 0.1843 0.0000 0.3798 0.0791 -1.0000  27.37 -0.02 4.0004 -5.5507 0.0000 0.1843 0.0000 0.3798 0.0791 -1.0000  27.37 -0.02 4.0004 -5.5507 0.0000 0.1843 0.0000 0.3798 0.0791 -1.0000  27.37 -0.00 3.2906 -5.5507 0.0000 0.1843 0.0000 0.3798 0.0795 -1.3900  20.12 -0.00 3.2906 -5.5507 0.0000 0.1840 0.0000	1 0.01 2.02 4.01 6.03 6.02	8EYA 0.00 0.00 0.00	0.0190 0.23**	0.0 8 CLM -0.1106	4⊌DF11 0	. DEL	DELS-	DEL3 DEL4	TRANSITI	ON	
T ALPHA 6ETA CM CLM CY CLM CLL CA CAB CAF RCP -0.01 0.00 0.0190 -0.1106 -0.0098 0.0078 -0.0086 0.2518 0.0820 0.1698 -5.8219 2.02 0.0 0.2394 -0.4153 -0.0075 0.0091 -0.0121 0.2534 0.0977 0.1557 -1.7351 0.00 0.0091 0.00121 0.2534 0.0977 0.1557 -1.7351 0.00 0.0091 0.00121 0.2534 0.0977 0.1557 -1.7351 0.00 0.0091 0.00 0.00 0.00 0.00 0.00 0	2.02 4.01 6.03	0.00 0.00 0.00	0.0190 0.0190	CLM -0-1106					UNKMOWA		
-0.01 0.00 0.0190 -0.1106 -0.0098	0.01 2.02 4.01 6.03	0.00	0.0190	-0-1106	CI				_		
2.02 0.00 0.23% -0.4153 -0.0075 0.0091 -0.0121 0.2534 0.0097 0.1557 -1.7351   4.01 0.00 0.4907 -0.8465 -0.0081 0.0142 -0.0106 0.2550 0.1041 0.1510 -1.7238   6.03 -0.00 0.7679 -1.4617 -0.0090 0.0387 -0.0137 0.2672 0.1134 0.1539 -1.6299   8.02 -0.00 1.4322 -2.1441 -0.0104 0.0556 -0.0151 0.2851 0.1145 0.1706 -1.9379   10.02 -0.00 1.4910 -2.9675 -0.0141 0.0702 -0.0134 0.3018 0.1292 0.1726 -1.0903   12.03 -0.01 1.8556 -3.6877 -0.0230 0.1122 -0.0065 0.3092 0.1605 0.1847 -1.9663   14.02 -0.00 2.1420 -4.1881 -0.0067 0.0767 -0.0158 0.3725 0.1736 0.1988 -1.9358   16.04 0.00 2.5228 -4.6012 -0.0183 0.0299 -0.0211 0.3874 0.1997 0.1917 -1.0031   17.05 -0.00 2.7071 -5.0628 -0.0176 0.0263 -0.0230 0.3921 0.2131 0.1791 -1.8702   18.07 -0.00 2.9044 -5.3045 -0.0266 0.0346 -0.0261 0.4060 0.2270 0.1796 -1.8264   19.10 -0.00 3.0787 -5.457 -0.0139 0.0271 -0.0286 0.4105 0.2548 0.1561 -1.7488   20.12 -0.00 3.0787 -5.457 -0.0139 0.0271 -0.0286 0.4105 0.2548 0.1561 -1.7488   20.12 -0.00 3.0789 -5.5214 0.0003 0.0333 -0.0222 0.4145 0.2730 0.1415 -1.7026   21.11 -0.01 3.4618 -5.6575 0.0138 0.0526 -0.0019 0.4233 0.2800 0.143 -1.6438   27.16 -0.01 3.4618 -5.6575 0.0138 0.0526 -0.0019 0.4233 0.2800 0.143 -1.6438   27.16 -0.01 3.4618 -5.6577 -0.0280 0.3437 0.0184 0.4253 0.3137 0.1116 -1.4828   23.18 -0.01 3.7679 -5.6169 0.0004 0.0848 0.4263 0.3137 0.1116 -1.4828   24.25 -0.02 4.0004 -5.5879 -0.0280 0.3437 0.0184 0.4253 0.3137 0.1116 -1.4828   25.30 -0.02 4.2109 -5.5105 -0.0183 0.2970 0.6285 0.4388 0.3403 0.0945 -1.3868   26.31 -0.02 4.4640 -5.4777 0.0163 0.2970 0.6285 0.4388 0.3403 0.0945 -1.3868   27.37 -0.02 4.4640 -5.4777 0.0163 0.2970 0.6285 0.4388 0.3403 0.0945 -1.3868   27.37 -0.02 4.4640 -5.5787 0.0288 0.3455 0.0680 0.4364 0.3538 0.0883 -1.2246   27.37 -0.02 4.4640 -5.5797 0.0163 0.2970 0.6285 0.4041 0.3538 0.0883 -1.2246   27.37 -0.02 4.4640 -5.5797 0.0183 0.2970 0.6285 0.4041 0.3538 0.0883 -1.2246   27.37 -0.02 4.4640 -5.5797 0.0183 0.2985 0.00880 0.3798 0.0781 -1.0198   27.37 -0.00 3.3296 -5.7521 -0.0183 0.0897 -0.0185 0.4270 0.3488 0.	2.02 4.0 <u>1</u> 6.03	0.00	0.23%		-0.0098						
4.01 0.00 0.4907 -0.8445 -0.0081 0.0142 -0.0106 0.2550 0.1041 0.1510 -1.7230   6.03 -0.00 0.7679 -1.4417 -0.0090 0.0387 -0.0137 0.2677 0.1134 0.1539 -1.8299   8.02 -0.00 1.1322 -2.1541 -0.0104 0.0556 -0.0151 0.2851 0.1145 0.1706 -1.9379   10.02 -0.00 1.4910 -2.9675 -0.0141 0.0702 -0.0134 0.3018 0.1292 0.1726 -1.9903   12.03 -0.01 1.4556 -3.6877 -0.0230 0.1122 -0.0065 0.3018 0.1292 0.1726 -1.9963   14.02 -0.00 2.1420 -4.1481 -0.0067 0.0267 -0.0158 0.3725 0.1736 0.1988 -1.9358   16.04 0.00 2.5228 -4.6012 -0.0183 0.0209 -0.0211 0.3874 0.1957 0.1917 -1.9031   17.05 -0.00 7.7071 -5.0628 -0.0176 0.0266 0.0346 -0.0230 0.3921 0.2131 0.1791 -1.8702   18.07 -0.00 2.9044 -5.3045 -0.0266 0.0346 -0.0231 0.4066 0.2270 0.1796 -1.0264   19.10 -0.00 3.0787 -5.457 -0.0139 0.0271 -0.0286 0.4105 0.2544 0.1561 -1.7688   20.12 -0.00 3.2429 -5.5214 0.0003 0.0333 -0.0222 0.4145 0.2730 0.1415 -1.7026   21.11 -0.01 3.418 -5.6575 0.0134 0.0526 -0.0109 3.4233 0.2800 0.1434 -1.6438   22.16 -0.01 3.4198 -5.6575 0.0134 0.0526 -0.0109 3.4233 0.2800 0.1434 -1.6438   22.16 -0.01 3.4198 -5.6587 -0.0246 0.3637 0.0184 0.4253 0.3137 0.1116 -1.4628   24.25 -0.02 4.0004 -5.5897 -0.0246 0.3437 0.0184 0.4253 0.3137 0.1116 -1.4628   25.30 -0.02 4.2109 -5.5105 -0.0183 0.2970 0.1286 0.4349 0.3215 0.1135 -1.3973   25.30 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0526 0.4346 0.3317 0.1116 -1.4628   27.37 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0526 0.4346 0.3317 0.1116 -1.4628   27.37 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0526 0.4346 0.3318 0.0668 -1.2346   27.37 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0526 0.4346 0.3318 0.0668 -1.2346   27.37 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0526 0.4346 0.3308 0.0083 -1.2246   27.37 -0.02 4.6400 -5.5897 -0.0246 0.3637 0.0666 0.4366 0.3718 0.0668 -1.1998   27.37 -0.02 4.6400 -5.5897 -0.0246 0.0534 0.2895 0.4866 0.3718 0.0668 -1.1998   27.37 -0.02 4.6400 -5.5897 -0.0246 0.0534 0.2895 0.4866 0.4308 0.0781 -1.0198   27.37 -0.00 5.2794 -0.0033 0.0897 -0.0008 0.4866 0.3798 0.0785 -1.3046   27.37 -0.00 5.2794 -0.0035 0.0057 -0.0057 0	6.03			-0.4153							
8.02 -0.00	8.02	-0.00						0.2550	0.1041	0.1510	-1.7230
10.02 -0.00											
12.03	0.02										
14.02											
16.04											
17.05 -0.00											
18.07 -0.00											
19.10 -0.00 3.0787 -5.4457 -0.0139 0.0271 -0.0286 0.4105 0.2544 0.1561 -1.7488 20.12 -0.00 3.2429 -5.5214 0.0003 0.0393 -0.0222 0.4145 0.2730 0.1415 -1.7026 21.11 -0.01 3.418 -5.6575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1434 -1.6438 27.16 -0.01 3.4198 -5.6347 0.0240 0.0034 -0.0251 0.4253 0.3017 0.1241 -1.5566 23.18 -0.01 3.7579 -5.6169 0.0004 0.1843 0.0184 0.4253 0.3137 0.1116 -1.4628 24.25 -0.02 4.0004 -5.5897 -0.0248 0.3437 0.0448 0.4349 0.3215 0.1135 -1.3973 25.30 -0.02 4.2149 -5.6105 -0.0163 0.2970 0.0285 0.4348 0.3403 0.0945 -1.3648 26.31 -0.02 4.4690 -5.4727 0.0161 0.2475 0.0524 0.4401 0.3538 0.0863 -1.2246 27.37 -0.02 4.6469 -5.3420 0.0434 0.2495 0.0646 0.4386 0.3718 0.0688 -1.1494 28.46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.0108 29.50 -0.00 5.2798 -4.9376 0.1266 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352 30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.0694 20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0867 -0.0168 0.4077 0.3488 0.0209 0.0633 -2.6473											
20.12 -0.00 3.2429 -5.5214 0.0003 0.0393 -0.0222 0.4145 0.2730 0.1415 -1.7026  21.11 -0.01 3.4418 -5.6575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1434 -1.6438  27.16 -0.01 3.4198 -5.6347 0.0240 0.0034 -0.0251 0.4258 0.3017 0.1241 -1.5566  23.18 -0.01 3.7079 -5.6169 0.0004 0.1843 0.4184 0.4253 0.3137 0.1116 -1.4628  24.25 -0.02 4.0004 -5.5897 -0.0248 0.3437 0.0448 0.4349 0.3215 0.1135 -1.3973  25.30 -0.02 4.2109 -5.6105 -0.0163 0.2970 0.1285 0.4348 0.3403 0.0945 -1.3668  26.31 -0.02 4.4690 -5.6727 0.0161 0.2485 0.0524 0.401 0.3538 0.0863 -1.2246  27.37 -0.02 4.6469 -5.3420 0.0434 0.2485 0.0646 0.4386 0.3718 0.0668 -1.1496  28.46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.0108  29.50 -0.00 5.2798 -4.9376 0.1266 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352  30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8696  20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3488 0.0785 -1.7276  20.12 -0.00 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.407 0.3498 0.0599 -1.7114											
21:11 -0.01 3.418 -5.6575 0.0138 0.0526 -0.0109 0.4233 0.2800 0.1434 -1.6438 27:16 -0.01 3.4198 -5.6347 0.0240 0.0034 -0.0251 0.4258 0.3017 0.1241 -1.5566 23:18 -0.01 3.7579 -5.6169 0.0004 0.1843 0.0184 0.4253 0.3137 0.1116 -1.4628 24.25 -0.02 4.0004 -5.5697 -0.0248 0.3437 0.0488 0.4349 0.3215 0.1135 -1.3973 25:30 -0.02 4.2109 -5.6105 -0.0163 0.2970 0.0285 0.4348 0.3403 0.0945 -1.3068 26:31 -0.02 4.4690 -5.4727 0.0161 0.3425 0.0524 0.401 0.3538 0.0863 -1.2246 27:37 -0.02 4.6463 -5.3420 0.0434 0.2485 0.0524 0.401 0.3538 0.0863 -1.2246 27:37 -0.02 4.6463 -5.3420 0.0434 0.2485 0.0646 0.4386 0.3718 0.0668 -1.1496 28:46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.0198 29:50 -0.00 5.2798 -4.9376 0.1266 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352 30.57 -0.01 5.5395 -4.6172 0.1612 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8696 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.4097 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.4097 0.3498 0.0599 -1.7114											
23,18 -0.01 3.7679 -5.6169 0.0004 0.1843 0.0184 0.4253 0.3137 0.1116 -1.4828 24.25 -0.02 4.0004 -5.5697 -0.0248 0.3437 0.0448 0.4349 0.3215 0.1135 -1.3973 25.30 -0.02 4.2109 -5.5105 -0.0163 0.2970 0.0285 0.4346 0.3403 0.0945 -1.3648 26.31 -0.02 4.4690 -5.4727 0.0161 0.3425 0.0524 0.4401 0.3538 0.0863 -1.2246 27.37 -0.02 4.6646 -5.3420 0.0434 0.2485 0.0646 0.4386 0.3718 0.0668 -1.1494 28.46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.6198 29.50 -0.00 5.2798 -4.9376 0.1286 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352 30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8694 20.12 -0.01 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.4097 0.3498 0.0599 -1.7114	21.11	-0.01	3.4418	-5.6575	0.0138	0.0526	-0.0109		0.2800	0.1434	-1.6438
24.25 -0.02					_						-1 <u>-5</u> 56 <u>6</u>
25.30 -0.02 4.2109 -5.5105 -0.0103 0.2970 0.0285 0.4348 0.343 0.0945 -1.3068											- 1 Harris E
26.31 -0.02	_			_							
27.37 -0.02 4.6468 -5.3420 0.0434 0.2485 0.0646 0.4386 0.3718 0.0668 -1.1496 28.46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.0198 29.50 -0.00 5.2798 -4.9376 0.1286 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352 30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8696 20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.4097 0.3498 0.0599 -1.7114											
28.46 -0.01 4.9704 -5.0688 0.1506 -0.1371 0.0168 0.4580 0.3798 0.0781 -1.6198 29.50 -0.00 5.2798 -4.9376 0.1286 -0.2524 -0.0192 0.4517 0.4025 0.4492 -0.9352 30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8694 20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0168 0.4097 0.3498 0.0599 -1.7114 10.21 -0.00 1.5122 -3.0959 -0.0123 0.0687 -0.0147 0.2843 0.2209 0.0633 -2.4473											
29.50 -0.00 5.2798 -4.9376 0.1286 -0.2524 -0.0192 0.4517 0.4025 0.0492 -0.9352 30.57 -0.01 5.5395 -4.8172 0.1812 -0.2405 -0.0201 0.4486 0.4308 0.0178 -0.8696 20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0068 0.4097 0.3498 0.0599 -1.7114 10.21 -0.00 1.5122 -3.0959 -0.0123 0.0687 -0.0147 0.2843 0.2209 0.0633 -2.0473											
30.57 -0.01 5.5395 -4.0172 0.1012 -0.2405 -0.0201 0.4406 0.4300 0.0170 -0.6696 20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3406 0.0705 -1.7270 20.12 -0.01 3.2704 -5.5969 0.0033 0.0092 -0.0068 0.4097 0.3490 0.0599 -1.7114 10.21 -0.00 1.5122 -3.0959 -0.0123 0.0607 -0.0147 0.2043 0.2209 0.0633 -2.0473											
20.12 -0.00 3.3296 -5.7521 -0.0157 0.0791 -0.0135 0.4270 0.3486 0.0785 -1.7276 20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0068 0.4097 0.3498 0.0599 -1.7114 10.21 -0.00 1.5122 -3.0959 -0.0123 0.0687 -0.0147 0.2843 0.2209 0.0633 -2.0473											
20.12 -0.01 3.2704 -5.5969 0.0033 0.0892 -0.0068 0.4097 0.3498 0.0599 -1.7114 10.21 -0.00 1.5122 -3.0959 -0.0123 0.0687 -0.0147 0.2843 0.2209 0.0633 -2.0473											
	20.12	-0.01	3.2704	-5.5969	0.0033	0.0892	-0.0068		0.3498		
-0 01	10.21								0.5509		
-0.01 0.00 0.0169 -D.1270.0076 0.0044 -D.0085 0.2455 0.1164 0.1291 -7.5221	-0.01	0.00	0•0 <u>7</u> ea_	-0.1274	-0.0076	0.004	-0.0085	0.2455	0.1164	0.1291	<u>-7.5221</u>
							-				•
								•			
		7.05 R.07 19.10 20.12 21.11 22.16 23.18 24.25 25.30 26.31 27.37 28.46 29.50 30.57 20.12	7.05		7.05	7.05	7.05	7.05	17.05	17.05	17.05

ALPHA BFTA CN CN CLM CV CLM CLM CLL CA CAB CAF ACP -0.01 0.00 0.0164 -0.1017 -0.0066 0.0080 -0.0120 0.2622 0.0884 0.1739 -6.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19876.19	-0.01
2.03	2 2.03 0.00 0.2448 -0.4443 -0.0045 0.0062 -0.0120 0.2642 0.1049 0.1593 -1.7655 3 3.99 -0.00 0.5055 -0.4196 -0.0032 0.0067 -0.0104 0.2719 0.1037 0.1661 -1.8190 6 6.01 -0.00 0.6243 -1.6362 -0.0037 0.0739 -0.0134 0.2841 0.1038 0.1803 -1.9754 5 8.00 -0.00 1.1640 -2.3866 -0.0096 0.0355 -0.0149 0.2969 0.1215 0.1754 -2.0416 6 10.03 -0.00 1.5423 -3.1869 -0.0166 0.0578 -0.0147 0.3275 0.1262 0.2012 -2.0664 7 12.04 -0.00 1.8650 -3.8658 -0.0187 0.0945 -0.0081 0.3315 0.1429 0.1886 -2.0370 8 14.04 -0.00 2.1567 -4.1275 -0.0050 0.0205 -0.0157 0.3967 0.1665 0.2302 -1.9122 9 16.06 -0.00 2.5513 -4.8709 -0.0084 0.0314 -0.0175 0.4087 0.2081 0.2006 -1.0092 9 17.07 -0.00 2.7596 -5.1870 -0.0128 0.0479 -0.0192 0.4112 0.2264 0.1849 -1.0092 17.07 -0.00 2.9679 -5.4856 -0.0138 0.0656 -0.0225 0.4202 0.2522 0.1680 -1.0403 2 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0060 -0.0251 0.4303 0.2659 0.1644 -1.7778 3 20.09 -0.01 3.3787 -5.8856 0.0017 0.0772 -0.0149 0.4350 0.2808 0.1541 -1.7420 4 21.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0077 0.4325 0.2931 0.1394 -1.6659 5 22.18 -0.01 3.5375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5938 6 23.20 -0.01 3.5375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5938 6 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4341 0.3436 0.0900 -1.1982
3.99 -0.00	3.99 -0.00 0.5055 -0.4196 -0.0032 0.0067 -0.0104 0.2719 0.1037 0.1681 -1.8190   6.01 -0.00 0.8283 -1.6362 -0.0037 0.0239 -0.0134 0.2841 0.1038 0.1803 -1.9754   6.00 -0.00 1.1690 -2.3866 -0.0096 0.0435 -0.0149 0.2969 0.1215 0.1754 -2.0416   7 12.04 -0.00 1.8650 -3.8650 -0.0187 0.0945 -0.0147 0.3275 0.1262 0.2012 -2.0664   7 12.04 -0.00 2.1507 -4.1275 -0.0050 0.0205 -0.0157 0.3957 0.1665 0.2302 -1.9122   7 16.06 -0.00 2.5513 -4.8709 -0.0044 0.0314 -0.0175 0.4087 0.2081 0.2006 -1.9092   9 17.07 -0.00 2.7596 -5.1870 -0.0128 0.0479 -0.0192 0.4112 0.2264 0.1849 -1.8796   18.08 -0.00 2.9679 -5.4850 -0.0139 0.0556 -0.0225 0.4202 0.2552 0.1660 -1.8403   7 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0000 -0.0225 0.4202 0.2552 0.1660 -1.8403   7 19.07 -0.00 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4350 0.2908 0.1541 -1.7720   8 20.09 -0.01 3.5736 -5.9793 0.0050 0.0741 -0.0080 0.4325 0.2931 0.1394 -1.6659   8 23.20 -0.01 3.5735 -5.9743 -0.0067 0.1283 -0.0072 0.433 0.3273 0.3140 0.1187 -1.5938   8 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0085 0.4341 0.3436 0.0904 -1.1982
6.01 -0.00	6.01 -0.00
8.00 -0.00 1.1690 -2.3866 -0.0096 0.0435 -0.0149 0.2969 0.1215 0.1756 -2.0416 10.03 -0.00 1.5423 -3.1869 -0.0187 0.0965 -0.0187 0.3275 0.1762 0.2012 -2.0664 12.04 -0.00 1.8650 -3.8650 -0.0187 0.0965 -0.0081 0.3315 0.1429 0.1866 -2.0379 14.04 -0.00 2.1567 -4.1275 -0.0050 0.0205 -0.0157 0.3967 0.1665 0.2302 -1.9122 16.06 -0.00 2.5513 -4.8709 -0.0084 0.0314 -0.0175 0.0087 0.2081 0.2006 -1.9092 17.07 -0.00 2.7596 -5.8550 -0.0138 0.0679 -0.0192 0.4112 0.2264 0.1849 -1.8796 18.08 -0.00 2.9679 -5.8550 -0.0138 0.0656 -0.0225 0.4202 0.2522 0.1860 -1.8403 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0060 -0.0261 0.4303 0.2659 0.1644 -1.7978 20.09 -0.01 3.3787 -5.8850 0.0017 0.0726 -0.0149 0.4303 0.2659 0.1644 -1.7978 22.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4305 0.2931 0.1394 -1.6659 22.16 -0.01 3.5350 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938 23.20 -0.01 3.7536 -5.9793 0.0063 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5868 24.27 -0.01 4.1517 -5.8743 -0.0067 0.1263 -0.0062 0.4331 0.3233 0.1097 -1.4149 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4341 0.3436 0.0904 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982 27.43 -0.01 5.4581 -4.9607 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9087 29.57 -0.01 5.4581 -4.9607 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9087 29.57 -0.01 5.547 -3.2879 -0.0094 0.0708 -0.0213 0.4576 0.4327 0.0367 -0.6156 20.11 -0.00 1.5547 -3.2879 -0.0094 0.00708 -0.0213 0.4500 0.0307 0.0367 -0.6156	8.00 -0.00 1.1690 -7.3866 -0.0096 0.0435 -0.0149 0.2969 0.1215 0.1754 -2.0416 b 10.03 -0.00 1.5423 -3.1869 -0.0106 0.0578 -0.0147 0.3275 0.1762 0.2012 -2.0664  12.04 -0.00 1.8650 -3.8658 -0.0187 0.0945 -0.0081 0.3315 0.1429 0.1886 -2.0379 b 14.04 -0.00 2.1597 -4.1275 -0.0050 0.0205 -0.0157 0.3967 0.1665 0.2302 -1.9122 9 16.06 -0.00 2.5513 -4.8709 -0.0084 0.0314 -0.0175 0.4087 0.2081 0.2006 -1.9092 0 17.07 -0.00 2.7596 -5.1870 -0.0128 0.0479 -0.0192 0.4112 0.2264 0.1849 -1.0796 1 18.08 -0.00 2.9679 -5.4856 -0.0139 0.0656 -0.0225 0.4202 0.2522 0.1680 -1.0403 2 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0060 -0.0261 0.4303 0.2659 0.1644 -1.7770 3 20.09 -0.01 3.3787 -5.8856 0.0017 0.0726 -0.0149 0.4325 0.2931 0.1394 -1.0659 5 22.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.0659 5 22.16 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938 6 23.20 -0.01 3.6375 -5.6428 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1107 -1.5068 7 24.27 -0.01 4.1517 -5.4743 -0.0067 0.1263 -0.0062 0.4331 0.3233 0.1097 -1.4149 8 25.30 -0.07 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
10.03 = 0.00	10.03 =0.00 1.5423 =3.1869 =0.0106 0.0578 =0.0147 0.3275 0.1262 0.2012 =2.0664 12.04 =0.000 1.8650 =3.8455 =0.0187 0.0945 =0.0081 0.3315 0.1429 0.1886 =2.0379 14.04 =0.00 2.1597 =4.1275 =0.0050 0.0205 =0.0157 0.3967 0.1665 0.2302 =1.9122 16.06 =0.00 2.5513 =4.8709 =0.0084 0.0314 =0.0175 0.4087 0.2081 0.2006 =1.9092 17.07 =0.00 2.7596 =5.1870 =0.0122 0.0479 =0.0192 0.4112 0.2264 0.1849 =1.8796 18.08 =0.00 2.9679 =5.8856 =0.0138 0.0656 =0.0225 0.4202 0.2522 0.1680 =1.8483 19.07 =0.00 3.1753 =5.7061 =0.0172 0.0660 =0.0225 0.4202 0.2522 0.1680 =1.8483 19.07 =0.00 3.1753 =5.7061 =0.0172 0.0660 =0.0261 0.4303 0.2659 0.1644 =1.7978 19.07 =0.00 3.3787 =5.8856 0.0017 0.0726 =0.0149 0.4303 0.2659 0.1644 =1.7978 19.07 =0.01 3.5491 =5.9125 =0.0035 0.0980 =0.0072 0.4325 0.2931 0.1394 =1.6659 19.07 =0.01 3.5491 =5.9125 =0.0035 0.0980 =0.0072 0.4325 0.2931 0.1394 =1.6659 19.07 =0.01 3.5491 =5.9125 =0.0035 0.0980 =0.0072 0.4325 0.3070 0.1310 =1.5938 19.07 =0.01 3.6491 =0.0080 0.0741 =0.0080 0.4380 0.3070 0.1310 =1.5938 19.07 =0.01 3.6491 =0.0080 0.0081 0.0081 0.4327 0.3140 0.1167 =1.5868 19.07 =0.0081 0.4327 0.3140 0.1167 =1.5868 19.07 =0.0081 0.2931 0.0385 0.4341 0.3436 0.0994 =1.1982
12.04 -0.00	
14.04 -0.00 2.1507 -4.1275 -0.0050 0.0205 -0.0157 0.3967 0.1665 0.2302 -1.9122 16.06 -0.00 2.5513 -4.8709 -0.0064 0.0314 -0.0175 0.4087 0.2081 0.2006 -1.4092 17.07 -0.00 2.7596 -5.1870 -0.0122 0.0479 -0.0192 0.4112 0.2264 0.1849 -1.8796 16.08 -0.00 2.9679 -5.4556 -0.0139 0.0656 -0.0225 0.4202 0.2522 0.1880 -1.8483 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0660 -0.0261 0.4303 0.2659 0.1644 -1.7978 20.09 -0.01 3.3787 -5.8856 0.0017 0.0726 -0.0149 0.4350 0.2808 0.1541 -1.7420 21.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6659 22.16 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4325 0.2931 0.1394 -1.6659 23.20 -0.01 3.5375 -5.9288 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1167 -1.5938 24.27 -0.01 4.1517 -5.8743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149 25.30 -0.01 4.4425 -5.6421 -0.0241 0.2423 0.0285 0.4331 0.3233 0.1097 -1.4149 25.30 -0.01 4.4425 -5.6421 -0.0241 0.2423 0.0285 0.4341 0.3436 0.0900 -1.1982 -1.3151 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0900 -1.1982 27.42 -0.01 5.4541 -4.9607 0.1953 -0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9987 29.57 -0.01 5.4541 -4.9607 0.1953 -0.3171 -0.0345 0.4551 0.4576 0.4210 0.0367 -0.8986 20.11 -0.7569 20.11 -0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.0	1
16.06 -0.00	16.06
18.08 -0.00	1 18.08 -0.00 2.9679 -5.855 -0.0138 0.0656 -0.0225 0.4202 0.2522 0.1680 -1.8483 2 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0060 -0.0261 0.4303 0.2659 0.1644 -1.7978 3 20.09 -0.01 3.3787 -5.8855 0.0017 0.0726 -0.0149 0.4350 0.2808 0.1541 -1.7420 4 21.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6559 5 22.16 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4325 0.3070 0.1310 -1.5938 6 23.20 -0.01 3.9375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5968 7 24.27 -0.01 4.1517 -5.8743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149 8 25.30 -0.01 4.4425 -5.6421 -0.0241 0.2423 0.0285 0.4341 0.3436 0.0904 -1.1982
19.07 =0.00 3.1753 =5.7061 =0.0172 0.0060 =0.0261 0.4303 0.2659 0.1644 =1.7978  20.09 =0.01 3.3787 =5.8859 0.0017 0.0726 =0.0149 0.4350 0.2808 0.1541 =1.7429  21.16 =0.01 3.5431 =5.712> =0.0035 0.0980 =0.0072 0.4325 0.2931 0.1394 =1.6659  22.18 =0.01 3.7536 =5.9793 0.0050 0.0741 =0.0080 0.4360 0.3070 0.1310 =1.5938  23.20 =0.01 3.9375 =5.9298 =0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 =1.5068  24.27 =0.01 4.1517 =5.8743 =0.0067 0.1263 =0.0062 0.4330 0.3233 0.1097 =1.4149  25.30 =0.01 4.4425 =5.4421 =0.0241 0.2423 0.0285 0.4330 0.3257 0.1082 =1.3151  26.38 =0.02 4.7025 =5.6344 =0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 =1.1982  27.42 =0.02 4.9182 =5.4433 0.0114 0.3740 0.0651 0.4437 0.3578 0.0860 =1.1072  28.51 =0.01 5.1957 =5.1891 0.0953 0.0102 0.0119 0.4494 0.3744 0.0750 =0.9987  29.57 =0.01 5.4581 =4.9607 0.1953 =0.3171 =0.0345 0.4531 0.3925 0.0607 =0.9987  20.11 =0.01 3.3667 =5.4879 =0.0070 0.0518 =0.0213 0.4302 0.3428 0.0874 =1.7569  10.02 =0.00 1.5547 =3.2879 =0.0070 0.0518 =0.0178 0.3103 0.2178 0.0924 =2.1148	2 19.07 -0.00 3.1753 -5.7061 -0.0172 0.0060 -0.0261 0.4303 0.2659 0.1644 -1.7978 3 20.09 -0.01 3.3787 -5.8856 0.0017 0.0726 -0.0149 0.4350 0.2808 0.1541 -1.7420 4 21.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6659 5 22.18 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938 6 23.20 -0.01 3.9375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5668 7 24.27 -0.01 4.1517 -5.8743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149 8 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151 9 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
20.09 -0.01 3.3787 -5.8856 0.0017 0.0726 -0.0149 0.4350 0.2808 0.1541 -1.7429  21.16 -0.01 3.5471 -5.7125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6659  22.16 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938  23.20 -0.01 3.7535 -5.7248 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5948  24.27 -0.01 4.1517 -5.4743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149  25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151  26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982  27.42 -0.02 4.9182 -5.4423 0.0114 0.3740 0.0651 0.4437 0.3578 0.0860 -1.1072  28.51 -0.01 5.1957 -5.1891 0.0953 0.0102 0.0119 0.4494 0.3744 0.0750 -0.0987  29.57 -0.01 5.4581 -4.4007 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.0987  20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569  10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	20.09 -0.01 3.3787 -5.8856 0.0017 0.0726 -0.0149 0.4350 0.2806 0.1541 -1.7420 21.16 -0.01 3.5471 -5.4125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6659 22.16 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938 23.20 -0.01 3.4375 -5.4248 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5668 24.27 -0.01 4.1517 -5.4743 -0.0067 0.1263 -0.0062 0.4380 0.3233 0.1097 -1.4149 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
21.16 -0.01	21.16 -0.01 3.5491 -5.9125 -0.0035 0.0980 -0.0072 0.4325 0.2931 0.1394 -1.6659 5 22.18 -0.01 3.7536 -5.9793 0.0050 0.0741 -0.0080 0.4380 0.3070 0.1310 -1.5938 6 23.20 -0.01 3.9375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5868 7 24.27 -0.01 4.1517 -5.4743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149 8 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151 9 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
22.16 =0.01	5
23.20 -0.01 3.9375 -5.9248 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5968 24.27 -0.01 4.1517 -5.4743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4149 25.30 -0.01 4.4625 -5.4621 -0.0241 0.2423 0.0265 0.4330 0.3257 0.1082 -1.3151 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982 27.42 -0.02 4.9182 -5.4453 0.0114 0.3740 0.0651 0.4437 0.3578 0.0860 -1.1072 28.51 -0.01 5.1957 -5.1891 0.0953 0.0102 0.0119 0.4494 0.3744 0.0750 -0.9987 29.57 -0.01 5.4581 -4.9607 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9987 30.63 -0.01 5.7743 -4.7096 0.2011 -0.3526 -0.0211 0.4576 0.4210 0.0367 -0.08156 20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	23.20 -0.01 3.9375 -5.9298 -0.0083 0.1920 0.0213 0.4327 0.3140 0.1187 -1.5060 7 24.27 -0.01 6.1517 -5.8743 -0.0067 0.1263 -0.0062 0.4330 0.3233 0.1097 -1.4140 8 25.30 -0.01 4.4425 -5.4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151 9 26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
24.27 -0.01	7
25.30 -0.01	8 25.30 -0.41 4.4425 -5:4421 -0.0241 0.2423 0.0285 0.4339 0.3257 0.1082 -1.3151 9 26.38 -0.62 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982 27.42 -0.02 4.9182 -5.4453 0.0114 0.3740 0.0651 0.4437 0.3578 0.0860 -1.1072 28.51 -0.01 5.1957 -5.1891 0.0953 0.0102 0.0119 0.4494 0.3744 0.0750 -0.0987 29.57 -0.01 5.4581 -4.9607 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.0987 30.63 -0.01 5.7743 -4.7096 0.2011 -0.3526 -0.0211 0.4576 0.4210 0.0367 -0.6156 20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	26.38 -0.02 4.7025 -5.6344 -0.0113 0.2931 0.0385 0.4341 0.3436 0.0904 -1.1982
28.51 -0.01 5.1957 -5.1891 0.0953 0.0102 0.0119 0.4494 0.3744 0.0750 -0.0987 29.57 -0.01 5.4581 -4.9607 0.1953 -0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9089 30.63 -0.01 5.7743 -4.7096 0.2011 -0.3526 -0.0211 0.4576 0.4210 0.0367 -0.8156 20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	
29.57 -0.01 5.4581 -4.9607 0.1953 +0.3171 -0.0345 0.4531 0.3925 0.0607 -0.9089 30.63 -0.01 5.7743 -4.7096 0.2011 -0.3526 -0.0211 0.4576 0.4210 0.0367 -0.8156 20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	
30.63 -0.01 5.7743 -4.7096 0.2011 -0.3526 -0.0211 0.4576 0.4210 0.0367 -0.8156 20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0874 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	
20.11 -0.01 3.3667 -5.9149 -0.0094 0.0708 -0.0213 0.4302 0.3428 0.0074 -1.7569 10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	
10.02 -0.00 1.5547 -3.2879 -0.0070 0.0518 -0.0178 0.3103 0.2178 0.0924 -2.1148	
	-0.01 0.00 0.0213 -0.1287 -0.0041 0.0013 -0.0085 0.2566 0.1318 0.1248 -6.0459

1 ALPHA -0.00 2.02 4.03 6.04 7.99 10.01 12.03 14.03 16.02	171 0.5 BETA 0.00 -0.00 -0.00 -0.00 -0.00 -0.00	CN 0.0160 0.25+2 0.5379 0.6523 1.1952 1.5592	CLM -0.0918 -0.4771 -1.0370 -1.7215 -2.4894	CY -0.0095 -0.0056 -0.0036 -0.0064	CLM 0.0058 0.0121 0.0107	CLL -0.0084 -0.0101 -0.0118	0 0 CA 0.2928 0.2944	TRANSITI UMKNOWN CAB 0.1081	CAF 0.1848	KCP -5,7475	
-0.00 2.02 4.03 6.04 7.99 10.01 12.03 14.03 16.02	0.00 -0.00 -0.00 -0.00 -0.00	0.0160 0.25.2 0.5379 0.6523 -1.1952 1.5592	-0.0918 -0.4771 -1.0370 -1.7215 -2.4894	-0.0095 -0.0058 -0.0036 -0.0064	0.005B 0.0121 0.0107	-0.0084	0.294H	0.1081	0.1848	-5,7475	
2.02 4.03 6.04 7.99 10.01 12.03 14.03 16.02	-0.00 -0.00 -0.00 -0.00	0.2542 0.5379 0.6523 1.1952 1.5592	-0.0918 -0.4771 -1.0370 -1.7215 -2.4894	-0.0056 -0.0036 -0.0064	0.005B 0.0121 0.0107	-0.0084	0.2944		0.1848		
4.03 6.04 7.99 10.01 12.03 14.03 16.02	-0.00 -0.00 -0.00 -0.00	0.5379. 0.8523 _ 1.1952 _ 1.5592	-1.0370 -1.7215 -2.4844	-0.0035 -0.0064	0.0107			0.1086			
6.04 7.99 10.01 12.03 14.03 16.02	-0.00 -0.00 -0.00	0.8523 1.1952 1.5592	-1.7215	-0.0064		-0.0118				-1.8768	
7.99 10.01 12.03 14.03 16.02	-0.00 -0.00	- 1.1952 1.5592	-2.4844		פענט ט		.0.3001	0.1138		-1.9277	
10.01 12.03 14.03 16.02	-0.00	1.5592				-0.0146	0.3183	0.1170		-2.0198	
12.03 14.03 16.02	-0.00		-3-2483	-0.0023		-0.0162 ₋	0.3379 0.3604	0.1207_		<u>-2.0828</u> -2.0873	
14.03		1.9363	-3.9780			-0.0146	0.3811	0.1529	0.2781	-2.0545	
16.02	-0.00	2.1771	-4.1473		0.0396	-0.0092	0.4174	0.1841		-1.9049	
17.05	-0.00	2.5817	-4.8691	-0.0215	0.0578	-0.0155	0.4412	0.2155		-1.8937	
	-0.00	2.8168	-5.2625	-0.0175	0.0636	-0.0187	0.4549	0.2428	0.2120	-1.8754	_
18.09	-0.00	3.0535	-5.6670	0.0392_	0.0940	0.0236_	0.4574	_0.2643	0.1930	-1.8559	
19.12		3.2516	-5.8898	-0.0142	0.0643	-0.0240	0.4597	0.2746	0.1850	-1.8114	
	-0.01	3.4746	-0.1164		0.0645	-0.0215	0.4579	0.2916	0.1663	-1.7603	
21.13	-0.01 -0.01	3.7001 3.7188	-6.7601 -6.3015	0.0054	0.0534	-0.0185	0.4535	0.3051 0.2978	0.1484	-1.6919	
22.17		3.9755	-6.4036	0.0247	0.0629	0.0032	0.4562	0.3052		-1.6945 -1.6108	
23.23		4.2027		0.0323	0.0978	0.0279	0.4498	0.3103		-1.5259	
	-0.0i	4.4697			0.1081	0.0366	0.4440	0.3185		-1.4448	
	-0.01	4.6503	-6.2515		0.1396	0.0131	0.4336	0.3337		-1.3443	
26.37	-0.01	4.9625	-6.2417	0.0214	0.1647	0.0402	0.4376	0.3557	0.0819	-1.2578	
27.43	0.02_	5.1954	-5.9633	0.0048	0.2978	0.0707	0.4407	0.3561_		-1.1478	
28.51	-0.02	5.5071	-5.7768	0.1182	0.1243	0.0490	0.4336	0.3659		-1.0490	
29.57	-0.05	_5.7958	-5.4589	0.1724	0.0555	0.0250	0.4437	0.3779		-0.9419	
30.67 20.12	-0.01	6.0679 3.5190	-5.2137 -6.2248		-0.4083	-0.0148	0.4526	0.3962	0.0564	-0.0592	
10.00	-0.01	1.5988	-3.4528		0.0621	-0.0259	0.4640	0.3521	0.1119	-1.7694 -2.1596	_
		0.0209			0.0049			0.1519			
-0.01	0.00	0.0000				4200 AU	0.2863		m - 1 - 2 - 2	-6.4095	

_1_0/1	<u> </u>	—; <b>-</b>				<del></del>					
TEST	PART MA	CH RX10-	6 PHI	CONF	L OF	1 DEL2	DEL3 DEL4	TRANSITI	<u> </u>	-	
1	172 1.1	10 2.3	0.0	4m0F11 0	•0	0 0	0	UNKNOWN			
ALPHA	- SETA	CN	CLH -	CÝ -	CLN	CLL	CA · · · ·	CAB	CAF	XCP	
-0.00			-0.0610	-0.0215	0.0651	-0.0091	0.4907	0.1774	0.3133	-16.8862	
2.04	-0.00	0.2560		-0.0158	0.0504	-0.0079	0.4996	0.1794	0.3201	-1.7986	
2.04			-0.4763		0.0655	-0.0093	0.4958	0.1857	0.3101	-1.0530	
4.04	-0.00		-0.9981		0.0784	-0.0092	0.4964	0.1976		-1.8739	
	-0.01			-0.0146	0.0810	-0.0123	0.5375	0.2088		-1.9193	
10.01			-3.1665		0.0619	-0.0135	0.5458	0.2138		-5.0292	
12.05			-3.9316	-0.0098	0.0750	-0.0108	0.5555	0.2510		-2.0006	
14.04		2.7506	-4.5926	-0.0194	0.0964	-0.0065	0.5553	0.2266		-1.9536	
16.09	-0.01		-4.6954	-0.0458	0.1785	0.0079	0.5729	0.2336	0.3394	-1.8249	
17.14	-0.01		-5.0672		0.1555	-0.0057	0.5774	0.2469		-1.7577	
18.12		3.1112		-0.0425	0.1553	-0.0118	0.5829	0.2633		-1.7275	
19.14			-5.6720		0.1720		0.5817	0.2729		-1.6925	
20.16	_		-5.4273	-0.0251	0.1434	-0.0198	0.5716	0.2655		-1.6341	
	0.01 -0.01		-6.1793	-0.0103 0.0334	0.1223	-0.0204	0.5624 0.5559	0.2777		-1.5752 -1.5186	
23.27		4.5195	-6.5939	0.0519	0.0131	-0.0095	0.5473	0.2917		-1.4590	
	-0.01		-6.7252	0.0495	0.0348	-0.0252	0.5352	0.2867		-1.3753	
25.36		5.1933	-6.8396	0.0241	0.0497	-0.0202	0.5313	0.3097		-1.3170	
26.43	-0.01	5.4912	-6.4254	0.0271	0.0:96	-0.0113	0.5231	0.3142	0.2088	-1.2607	
	-0.01	5.8216		0.0235	0,1120	-0.0098	0.5131	0.3136		-1.1906	
	-0.01	6.1578	-6.9187	0.0694	0-0145	0.0037	0.5089	0.3221		-1.1236	
S9.66		6.4870	-6.8893	0.1213	-0.0899	0.0157	0.5051	0.3320		-1.0628	
30.70		6.A151	-6.8594	0.0337		-0.0216	0.4999	0.3418		-1.0065	
20.17		3.6731	-5.9958 -3.2877	-0.0071		-0.0093	0.5719	0.3152		-1.6323	<del></del>
-0.01				-0.0176		-0.0049				-2.0636 -19.77 <b>09</b>	
-0141			- 444175				444179	412469	4.5040		
				~ <del>_</del>							<del></del>
										·	
-											

	OF 1	PING DE	VELOPHENT	CENTER(A	EDC)	PROPULSION Martin M	I WIND YUN	MEL FACILI	OATA	AER	ODYNAMIC WIND TUNNE	<u>, (4Y)</u>
								·				
	. IESI		ACH RX10- 20 2.3		CONF 4#0F11 (		0 0	DEL3 DEL4		J		
it	ALPHA	BETA		CL#	Cv	CLN	CLL	CA	CAB	CAF	KCP	
	0.00	0.00	-0.0142	0.0478	-0.0050		-0.0054	0.5010	0.1747	0.3763	-3,3552	
	2.01	0.00	0.2352	-0.3620	-0.0001	-0.0078 -0.0057	-0.0055	0.5046 0.5104	0.1779 0.1790	0.3267	-1.5428 -1.6616	
	6.01	0.00		-1.4257	0.0642		-0.0057	0.5281	0.1849	0.3431	-1.7627	
	8.04	-0.00	1.1436	-2.0931	0.0052	-0.0171	-0.0058	0.5422	0.1907	0.3515	-1.0303	
	10.04	-0.00		-2.7921	0.0123	-0.0124	-0.0045	0.5504	0.2006	0.3497	-1.8492	
	12.07	-0.00	2.2941	-4.0587	0.0099	-0.0101	-0.0061	0.5476	0.2053	0.3423	-1.8243	
		-0.00	2.7244	-4.5887	0.0009	0.0310	-0.0039	0.5468	0.2138	0.3330	-1.7653 -1.6843	
		-0.00	2.9545	-4.9259	-0.0130	0.0640	-0.0027	0.5455	0.2167	0.3247	-1.6334	
	18.16	-0.00	3.1640	-4.8742	-0.0121	0.0719	-0.0088	0.5501	0.2193	0.3306	-1.5421	
		-0.01	3.4392	-5.0419	-0.0171	0.0833		0.5495	0.2259	0.3235	-1.4660	
	20,29	-0.01	3.7437	-5.2280	-0.0092		-0.0187	0,5469	0,2358	0.3112	-1.3965	
	21.31	-0.01 -0.01	4.0510 4.3538	-5.3954 -5.5582	0.0101	0.0521	-0.0198 -0.0161	0.5426	0.2411	0.3015	-1.3319 -1.2766	
	23.44	-0.01	4.7056	-5.7720	0.0452			0.5307	0.2504	0.2802	-1.2566	<del></del>
	24.47	-0.01	5.0244	-5.9327	0.075A			0.5237	0.2535	0.2703	1.1808	
	25.50	-0.01	5.3632	-6.0953	0.0869			0.5185	0.2566	0.2619	-1.1365	
	26,58	-0.01	5.7365	-6.7403	0.1013		0.0051	0.5170	0.2636	0.2533	-1.0878	
	27.61	-0.01 -0.01	6.0542	-6.2955 -6.3590	0.1044			0.5197 0.5156	0.2675 0.2841	0.2522	-1.0399 -0.9937	
	29.76	-0.01	6.7134	-6.4207	0.1565			0.5151	0.2913	0.2237	-0.9564	
	30.84	-0.01	7.0549	-6.4098	0.2034		0.0160	0.5196	0.3071	0.2124	-0.9171	
	30.84	-0.01	7.0657	-6.4696	0.1979			0.5200	0.3139	0.2061	-0.9156	
	20.27	-0.01	3.7330	-5.1899	-0.0043			0.5461	0.2720	0.2741	-1.3903	
	10.03	0.00	1.5157	-2.8431 0.0098	-0-0073	-0.0185 -0.0153	-0.0031 -0.0012	0.5370 0.4964	0.2369	0.3001 0.2887	-1.8757 -0.6252	
	-0,00			00000	-0.0012		-0.0015		082077	015001	-010535	, <del></del>
					-	•						
				_								
					<u> </u>							

					_							
			ACH RELO-		CONF				TRANSIT			
	1	174 1.	30 2.3	V. D	4=0f11 0	••	• •	lie.	) UNKNOW			
Ť	ALPHA	BETA	CN	CLM	CA	CLM	CLL	CA	CAB	CAF	ACP	
	0.00	0.00	-0-0274		-0.0031	-0.0130	0.0027	0.4830	0.1897		-3.0177	
	2.03	0.00	0.2297	-0.3141 -0.7736	-0.0013	-0.0053 0.0053	0.0040	0.4836	0.1887	0.2948	-1.3737	
	6.03	0.00 .	0.5008 0.7863	-1.2798	-0.0029	0.0033_	0.0025	0.5059	0.1853 0.1823		_ <b>-1.544\$</b> -1.62 <b>36</b>	<del></del>
		-0.00	1.1061	-1.5299	-0.0027	0.0122	0.0009	0.5218	0.1926		-1.6544	•
	10.09	-0.00	1.4603	-2.4022	0.0040	0.0129	-0.0006	0.5303	0.1978	0.3325	-1.6450	-
	12.12	-0.00	1.4330	-2.9467	0.0061	0.0110	0.0003	0.5385	0.2026	0.3359	-1,6076	
	14.14	-0.00	5.5198	-3.4254	0.0072	0.0079	0.0011	0.5412	0.2063	0.3350	-1.5438	
		0.00	2.6822	-3-6915	0.0038	0.0207	_ 0.0030	0.5340	0.2168		-1-4509	
	17.24	-0.00	3.2179	-4.0681	-0.0009 -0.0073	0.0396 0.0568	0.0024	0.5356 0.5341	0.2204 0.2248	0.3152 0.3093	-1.3860 -1.3142	
	19.31	-0.01	3.5137	-4.3834	-0.0033	0.0592	-0.0035	0.5339	0.2260	0.3058	-1.2477	
	20.36	-0.01	3.7929	-4.4713	0.0014	0.0560	-0.0045	0.5295	0.2326	0.2969	-1.1842	
	21.41	-0.01	4.0758	-4.5934	0.0106	0.0362	-0-0058	0.5239	0.2358	1885.0	-1.1275	
	25.46	-0.01	4-3907	-4.6872	0.0303	0.0074	-0.0032_	0.5223	0.2377	0.2846	-1.0675	
	23.51	-0.01	4.7037		0.0.74	-0.0212	-0.0033	0.5223	0.2386	0.2837	-1.0150	_
	24.57	0.01_	5.0505		0.0665	_=0.0554	_=0.0022_	0.5250	0.2477	0.2773	-0.9678	
	25.61	-0.01 -0.01	5.7660		0.0835	-0.0909 -0.1156	0.0015	0.5264	0.2550 0.2642	0.2713	-0.93 <b>08</b> -0.8997	
	27.76	-0.01	6.0963	-5.3459	0.0790	-0.1191	0.0106	0.5292	0.2708	0.2584	-0.8766	
	28.82	-0.01	6.4914	-5.5743	0.1013	-0.0928	0.0029	0.5316	0.2770	0.2545	-0.8595	
	29.86	-0.01	6.8606	-5-8172	0.0952	-0.0561	-0-0005	0.5361	0.2543		-0.8479	
	30.91	-0.01		-6. G4 78	0.0970	-0.0578	-0.0003	0.5403	0.2928		-0.8387	<del></del>
	20.34	-0-01	3.7899		-0.0013	0.0602	-0.0033	0.5317	0.2945		-1.1714	
	-0.08	0.00	-0-0195	-2.5058 0.0416	-0.0045	-0.0120	0.0008	0.5168	0.2569	0.2599	-1.6876	
	-0.00	0.00	-000143	0.0410	-0.0040	-0.0120	0.0055	0.4782	0.2168	0.2614	-2.1373	
					· -	·						•
												·
												<del></del>
												<del> </del>
			<del></del>				— —		·			

5.04 -0.00 0.7461 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213  6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.364 1.7199  8.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5868  10.15 -0.00 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4141  17.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2828 0.1622 0.1207 1.2723  15.23 -0.00 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634  18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518  21.42 -0.00 1.7126 1.0518 -0.0732 0.2180 -0.0174 0.2581 0.1986 0.0596 0.9645  24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788  27.58 -0.01 2.6532 2.0620 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7797  30.71 -0.04 3.2946 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832  30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952  5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293		NGINEER OF 1 OF 1	RING DE	VELOPHENT	<u>CENTER (A)</u>	EOC) P			MEL FACILI'		AER	DOYNAMIC WIND TUNNEL (AT
NT ALPHA 8ETA	<u>—</u>							I DEL2	DEL3 DEL4			
-2.04 0.00 -0.0874 -0.1920 -0.0067 -0.0065 -0.0072 0.2343 0.1079 0.1264 2.1965 -1.01 0.00 -0.0371 -0.114 -0.0064 -0.0035 -0.0093 0.2309 0.0999 0.1311 3.0058 0.01 0.00 0.0101 -0.0172 -0.0009 -0.0025 -0.0096 0.7306 0.1025 0.1281 -1.6973 1.01 0.00 0.0544 0.0732 -0.0045 0.0005 -0.0102 0.2324 0.1015 0.1309 1.3445 2.02 0.00 0.1009 0.1597 -0.0053 -0.0008 -0.0109 0.2324 0.1015 0.1309 1.3445 3.03 0.00 0.1495 0.2513 -0.0023 0.0022 -0.0115 0.2384 0.1016 0.1327 1.5017 4.07 0.00 0.1999 0.3384 -0.0042 0.0072 -0.0115 0.2384 0.1041 0.1343 1.6805 5.04 -0.00 0.2681 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 0.5.04 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.1345 1.6933 0.5.05 0.00 0.0065 0.6053 -0.0179 0.0478 -0.0146 0.2736 0.1371 0.1365 1.5666 10.15 -0.00 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4161 10.15 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2808 0.1602 0.1207 1.2723 15.23 -0.00 1.3159 1.4050 -0.0307 0.2452 -0.0151 0.2838 0.1602 0.1207 1.2723 15.24 -0.00 1.7126 1.5518 -0.0037 0.2452 -0.0151 0.2754 0.1938 0.0816 1.0518 18.34 -0.00 1.3359 1.4050 -0.0307 0.2452 -0.0151 0.2754 0.1938 0.0816 1.0518 18.35 -0.00 1.3359 1.4050 -0.0372 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 18.36 -0.00 1.3726 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 18.37 -0.00 1.3359 1.4050 -0.0371 -0.0160 0.2754 0.1938 0.0816 1.0518 18.36 -0.00 1.3726 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.2983 0.2333 -0.0380 0.7707 1.508 -0.00 1.8789 0.0404 -0.0391 -0.0160 0.2316 0.2165 0.0151 0.8788 1.508 -0.00 1.8789 0.0404 -0.0391 -0.0160 0.2754 0.1938 0.0516 0.0516 0.8788 1.508 -0.00 0.9830 1.3580 -0.0030 0.1409 -0.0174 0.1609 0.2441 -0.0739 0.5632 0.5952 0.1520 0.1520 0.2778 0.2264 0.0514 1.3822 0.1522 0.0005 0.0005 0.0005 0.0005 0.0005 0.2778 0.2504 0.0514 1.3822 0.0005 0.2778 0.2506 0.01479 0.1039 2.7723	INT	ALPHA	123	201018			110					ICP
0.01 0.00 0.0101 -0.0172 -0.0049 -0.0025 -0.0096 0.7306 0.1025 0.1281 -1.6973 1.01 0.00 0.0544 0.0732 -0.0045 0.0005 -0.0102 0.2324 0.1015 0.1309 1.3445 2.02 0.00 0.1009 0.1597 -0.0053 -0.0008 -0.0109 0.2344 0.1016 0.1327 1.5617 3.03 0.00 0.1495 0.2513 -0.0023 0.0022 -0.0115 0.2384 0.1041 0.1343 1.6805 4.07 0.00 0.1999 0.3384 -0.0042 0.0072 -0.0103 0.2426 0.1080 0.1345 1.6933 5.04 -0.00 0.2481 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 6.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5868 10.15 -0.00 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4141 12.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2809 0.1509 0.1299 1.4141 12.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2808 0.1622 0.1207 1.2723 1.5.23 -0.00 1.3359 1.4050 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.6344 18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518 21.42 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2561 0.1986 0.0596 0.99645 22.45 -0.00 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7997 3.30.71 -0.04 3.2966 1.9927 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832 3.508 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293				-		_						
1.01 0.00 0.0544 0.0732 -0.0045 0.0005 -0.0102 0.2324 0.1015 0.1309 1.3445 2.02 0.00 0.1009 0.1597 -0.0053 -0.0008 -0.0109 0.2344 0.1016 0.1327 1.5617 3.03 0.06 0.1475 0.2513 -0.0023 0.0022 -0.0115 0.2384 0.1016 0.1343 1.6805 4.07 0.00 0.1949 0.3384 -0.0042 0.0072 -0.0103 0.2426 0.1080 0.1345 1.6933 5.04 -0.00 0.2481 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.00134 0.2594 0.1230 0.1364 1.7199 8.13 -0.00 0.4241 0.4727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5664 10.15 -0.06 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1297 1.4161 12.18 -0.00 0.7351 0.9353 -0.0324 0.6810 -0.0154 0.2809 0.1602 0.1207 1.2723 15.23 -0.06 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634 18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518 21.42 -0.00 1.77126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1906 0.0596 0.9645 24.49 -0.06 2.1400 1.4789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 6.8788 27.58 -0.01 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7797 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293											0.1311	3.0050
2.02 0.00 0.1009 0.1597 -0.0053 -0.0008 -0.0109 0.2344 0.1016 0.1327 1.5817  3.03 0.04 0.1445 0.2513 -0.0023 0.0022 -0.0115 0.2384 0.1041 0.1343 1.6805 4.07 0.00 0.1949 0.3384 -0.0042 0.0072 -0.0103 0.2426 0.1080 0.1345 1.6933  5.04 -0.00 0.7481 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.1364 1.7198  8.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5868 10.15 -0.00 0.5695 0.8053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4141 12.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2808 0.1622 0.1207 1.2723 15.23 -0.00 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634 18.34 -0.00 1.3359 1.4050 -0.0097 0.2452 -0.0161 0.2754 0.1938 0.0810 1.0518 21.42 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.9787 30.71 -0.04 3.2967 1.9227 1.1388 -1.9095 -0.0172 0.1953 0.2333 -0.0380 0.7997 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1069 0.2492 -0.0823 0.5952 15.26 -0.00 0.9830 1.3586 -0.0038 0.1604 -0.0174 0.2536 0.1497 0.1039 2.7293												
3.03 0.06 0.1475 0.2513 -0.0023 0.0022 -0.0115 0.2384 0.1041 0.1343 1.6805 4.07 0.00 0.1979 0.3384 -0.0042 0.0072 -0.0103 0.2426 0.1080 0.1345 1.6933 5.04 -0.00 0.7481 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.1364 1.7213 6.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5866 10.15 -0.00 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4141 12.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2828 0.1622 0.1207 1.2723 15.23 -0.00 1.0106 1.1758 -0.0030 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1034 18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518 18.35 -0.00 1.7126 1.0518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 21.42 -0.00 1.7126 1.0518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 22.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788 27.58 -0.01 2.6332 2.0620 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7997 3 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5932 15.26 -0.00 0.8830 1.3586 -0.0038 0.1046 -0.0176 0.278 0.2264 0.0514 1.3822 5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
4.07 0.00 0.1949 0.3384 -0.0042 0.0072 -0.0103 0.2426 0.1080 0.1345 1.6933 5.04 -0.00 0.2461 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213 6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.1364 1.7198 8.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5866 10.15 -0.00 0.5045 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4161 12.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2828 0.1622 0.1207 1.2723 15.23 -0.00 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634 18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518 18.34 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 21.42 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645 22.49 -0.00 2.100 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788 27.58 -0.01 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7797 3 30.71 -0.04 3.2946 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 1.526 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
5.04 -0.00 0.7461 0.4271 -0.0038 0.0081 -0.0127 0.2499 0.1151 0.1348 1.7213  6.12 -0.00 0.3034 0.5215 -0.0069 0.0175 -0.0134 0.2594 0.1230 0.364 1.7199  8.13 -0.00 0.4241 0.6727 -0.0132 0.0338 -0.0146 0.2736 0.1371 0.1365 1.5868  10.15 -0.00 0.5695 0.6053 -0.0179 0.0478 -0.0141 0.2809 0.1509 0.1299 1.4141  17.18 -0.00 0.7351 0.9353 -0.0324 0.0810 -0.0154 0.2828 0.1622 0.1207 1.2723  15.23 -0.00 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634  18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518  21.42 -0.00 1.7126 1.0518 -0.0732 0.2180 -0.0174 0.2581 0.1986 0.0596 0.9645  22.449 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788  27.58 -0.01 2.6332 2.0620 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7997  30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5832  5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
6.12 -0.00												
						-0.0069						
12.18	0	8.13	-0.00	0.4241	0.6727	-0.0132	0.0338	-0.0146	0.2736	0.1371	0.1365	1.5660
15.23 -0.00 1.0106 1.1758 -0.0630 0.1599 -0.0157 0.2838 0.1801 0.1036 1.1634  18.30 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518  21.42 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645  24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788  27.58 -0.01 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7907  30.71 -0.04 3.2967 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832  30.71 -0.04 3.2966 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952  15.26 -0.00 0.9830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822  5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
18.34 -0.00 1.3359 1.4050 -0.0907 0.2452 -0.0161 0.2754 0.1938 0.0816 1.0518  21.42 -0.00 1.7126 1.6518 -0.0732 0.2160 -0.0174 0.2581 0.1986 0.0596 0.9645  24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788  27.58 -0.01 2.6332 2.0620 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7907  30.71 -0.04 3.2967 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832  30.71 -0.04 3.2966 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952  15.26 -0.00 0.9830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822  5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
21.42 -0.00 1.7126 1.6518 -0.0732 0.2180 -0.0174 0.2581 0.1986 0.0596 0.9645  24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788  27.58 -0.01 2.6532 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7997  3 30.71 -0.04 3.2967 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832  3 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952  3 15.26 -0.00 0.8630 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822  5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
24.49 -0.00 2.1400 1.8789 0.0404 -0.0391 -0.0168 0.2316 0.2165 0.0151 0.8788 7 27.58 -0.01 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7997 8 30.71 -0.04 3.2947 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832 9 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 15.26 -0.00 0.8830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822 15.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
7 27.58 -0.01 2.6332 2.0820 0.3451 -0.7338 -0.0172 0.1953 0.2333 -0.0380 0.7907 3 30.71 -0.04 3.2967 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832 3 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 3 15.26 -0.00 0.9830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822 5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293	<u></u> -											
3 30.71 -0.04 3.2967 1.9227 1.1388 -1.9905 -0.0170 0.1702 0.2441 -0.0739 0.5832 30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 0 15.26 -0.00 0.9830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822 1 5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293												
30.71 -0.04 3.2946 1.9610 1.1217 -2.0079 -0.0174 0.1669 0.2492 -0.0823 0.5952 0 15.26 -0.00 0.9830 1.3586 -0.0038 0.1646 -0.0126 0.2778 0.2264 0.0514 1.3822 1 5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.0095 0.2536 0.1497 0.1039 2.7293	В:											
5.08 -0.00 0.2170 0.5922 -0.0052 0.0115 -0.009 <u>5 0</u> .2536 0.1497 0.1039 <b>2.7293</b>	9		-0.04									
	0		_	-	-					0.2264	0.0514	
2 0.00 0.00 -0.0137 0.0977 -0.0051 0.0028 -0.0062 0.2355 0.1148 0.1206 -7.1365	1											
	2	0.00	0.00	-0.0137	0.0977	-0.0051	0.0028	-0.0062	0.2355	0.1148	0.1206	-7.1365
					•							
					·		<del></del>					
												·
						<del></del>						
<u>.</u>												
				•								

5E	NGINEE OF 1	_	VELOPMENT	CENTERIA	<u>EDC)</u> P	ROPULSION MARTIN M	WIND TUNG	NEL FACILI'	TY(PUT) DATA	AER	ODANVAIC MIN	TUNNEL (41)
	TEST 1		4CH RX10-	6 PHI 0.0 B	COMF ZWOFO 0	L DEL	1 DEL2	OFF OFF	TRANSIT	ION )		
DINT	ALPHA	BETA	CN	CLM		CLN	CLL	Ca	C48	CAF	XCP	
1	-2.03	0.00	-0.0966	-0.1374	-0.0042	-0.0037		0.2409	0.0998	0.1411	1.4231	
2	-1.02	0.00	-0-0463	-0-0558	-0.0075	0.0012	-0.0090	0.2373	0.1032	0.1341	1.1547	
3	0.00	0.00	0.0019	0.0304	-0.0084		-0.0076	0.2344	0.1010	0.1334	15.8332	
•	1.01	0.00	0.0514	0.1223	-0.0055	0.0030	-0.0101	0.2366	0.1141	0.1225	2.3550	
5	2.06	0.00	0.0939		0.0039		-0.0106	0.2382	0.1098	0.1283	2.3230	<del>.</del>
6	3.01	0.00	0.1383	0.3018	-0.0070	0.0087	-0.0112	0.2413	0.1119	0.1294	2.1823	
7	5.09	-0.00	0.1922	0.4846	-0.0053	0.0096	-0.0102	0.2544	0.1145	0.1371	2.0584 1.9950	
9	6.09	-0.00	2962	0.5708	-0.0066	0.0153	-0.0132	0.2618	0.1270	0.1347	1.9269 -	
10		-0.00	0.4172	0.7202	-0.0114	0.0290	-0.0145	0.2765	0.1404	0.1361	1.7263	<del></del>
ii	10.10	-0.00	0.5674	4566.0	-0.0182	0.0489	-0.0140	0.2836	0.1534		1.5199	
iż —	12.21	-0.00	0.7371	1.00-8		0.0772	-0.0154	0.2840	0.1632	0.1208	1.3633	
13	15.27	-0.00	1.0180	1.2334	-0.0654	0.1679	-0.0174	0.2817	0.1775	0.1042	1,2116	
	18.39	-0.00	1.3570	1.4696		0.2432		0.2741	0.1904	0.0837	1.0830	
5	21.45	-0.00	1.7326	_1.7327		0.1278	-0.0183	0+2542	0.5501	0.0341	1.0000	
16	24.51	-0.01	2.1882	1.9849	0.0955	-0.1596	-0.0199	0.2325	4052.0	0.0121	0.9071	
7	27.65	-0.01	2.7294 3.4138	2.1303 2.1658	- 0.5197 0.9671		-0.0192	0.1989 0.1734	0.2351	-0.0363	0.7805	
9	15.27	-0.00	0.9960	1.3539			-0.0160	0.2806	0.1966	0.0840	1.3593	
20	5.08	0.00	0.5510	0.5838			-0.0111	0.2595	0.1496	0.1099	2.6411	
21	0.00	0.00			-0.0074		-0.0078	0.2416	0.1358	0.1058	-5.6652	
					· · · · · · · · · · · · · · · · · · ·		<del></del> -	<del></del>		•		
	· · · · · · · · · · · · · · · · · · ·									<u>-</u>		
							-					
							·			<del></del>		<del></del>

of 1		<del></del> -		<del></del> -	MART		SSILE	AIL EFF	ECTS		<del></del>		
TES1		ACH AX10-			o. L	DEL1 OFF	DEL2_	DEL3	DEL4 OFF	TRANSITI			· <u>·</u>
ALPHA	BETA		CLW	CY	Ci	N	CLL			CAS	CAF	XCP	
0,00	0.00.	-0,0078	0.0693	-0.0069	0.0	0043	-0,0090	0,24	01	0.0802	0.1598	-8,9289	
-5.04	0.00	-0-1007	-0-1303	-0.0040			-0.0098			0.1136	0.1302	1.2936	
-1.00 1.01	0.00	0.0526	0.1272	-0.0083			-0.0102			0.1113	0.1278_	0 • <b>84.95</b>	
2.05	-0.00	0.0913		-0.0013			-0.0112			0.1092	0.1281	2.8814 2.4476	
-3.03	0.00	0.1331	0.3025	-0.0066			-0.0124			0-1111	0.1335	2.2715	
4.05	-0.00	0.1905	0.3941	-0.0038			-0.0131			0.1080	0.1448	2,0688	
5.06		0.2361	0.4599	-0.0055			-0-0137			0.1169	0.1429	2.0577	
_6.11		0.2946		-0.0049			-0.0144			0.1257	0.1442	1.9204	<u></u>
8.11		0.4249	0.7242	-0.0128 -0.0134			-0.0157			0.1438	0.1413	1.7043	
12.24			1.0026	-0.0185		0467 0578	-0.0153 -0.0169			0.1565	0.1353_ 0.1259	1.4659	
15.27		1.0393	1.2353	-0.0473		1340	-0.0206			0.1824	0.1083	1.1886	
18.37		1.3819	1.4922	-0-0711		2128	-0.0214			0.2047	0.0782	1.0798	
	-0.01	1.7917	1-7903	-0.0022		0541	-0-0206			0.2159	0.0534	0.9992	··
24.57	-0.01	5.5955	2.0487	0.1723	-0-		-0.0206			0.2281	0.0242	0.8938	
30.99	-0.03 -0.07		2.5176. 3.3489	0.2856		3110 0567	-0.0265			0.2370	-0.0137 -0.0604	0.845 <u>2</u> 0.8883	
15.31	-0.00		1.3973	-0.0224		0A27	-0.0164			0.2136	0.0737	1.3771	
5.09			0.5994	-0.0000		0168	-0.0124			0.1738	0.0882	2,7423	
0.02	0.00	-0.0221	0-1220	-0.0059	0.	0086	-0.0107			0.1353_		-5.5182	•
							701			-			
											····		
			-										-
						-							
												<del> </del>	
					-				_				
		<del></del>											

				<del></del>				<u> </u>			
	TEST		ACH RX10-	6. PHI	COMF	L DEL		OEL3 DEL4			
INT	ALPHA	BFTA	CN			CLN	CLL	CA -	CAB	CAF	XCP
1	-2.03	0.00	-0.1042		-0.0026	0.0003	-0.0093	0.2698	0.1065	0.1633	1.1051
<del>2</del>	-1.00	0.00	-0.0501	-0.0424	-0.0046	0.0030	-0.0113	0.2692	0.1138	0.1554	0.8462
3	-1.00	0.00	-0.0503	-0.0388	-0.0014	-0.0025	-0.0097		0.1229	0.1454	0.7719
•	-0.01	0.00		0.0547	-0.0044	0.0077	-0.0117	0.2682	0.1196	0.1485	-7.4398
5	1.04	0.00	0.0508	0-1335	-0.0027		-0.0124		_0.1177	0.1514	2.6291
6	2.95	0.00	0.0995	0.552a	-0.0044	0.0056	-0-0130	0.2722	0.1186	0.1534	2.2466
7	3,08	-0,00	0.1478	0.3186	-0.0050	0.0120	-0.0136	0.2807	0,1203	0.1604	2.1555
9	4.06 5.08	-0.00	0.1943	0.4074	-0.0023 -0.0040	0.0125	-0.0127 -0.0150		0.1250	0.1591 0.1634	2.0289 1.9577
10	6.08	-0.00	0.3114		-0.0066		-0.0141		0.1484	0.1653	1.8742
	7.13	-0.00	0.3827	0.6657			-0.0147		0.1535	0.1661	1.7394
<u>1</u>	8.17	-0.00	0.4440	0.7425	-0.0106	0.0362	-0.0154	0.3267	0.1641	0.1626	1.6721
3	10.21	-0.00	0.6017	0.8953	-0.0144	0.0526	-0.0168	0.3376	0.1736	0.1639	1,4879
4	17.26	-0.00	0.7826	1-001-	-0.0200	0-0613	-0.0169	0.3468	0.1811	0.1657	1.3550
<u>5</u>	_15.34_	-0.00	1.7910	<u>1.3212</u>	-0.0311		-0.0194		_0.5050	0.1405	1.2118
6	16.44	-0.01	1.4666	1.6128	-0.0475	0.1574	-0.0191		0.2234	0.1179	1.0997
7	21.56	-0.01	1.9776	1.9578	_ 0.0712		-0.0197		0.2456 _	0.0714_	0.9909
8	21.57	-0.01 -0.01	2.6685	2.0093 2.5145	0.0298		-0.0182 -0.0208		0.2496	0.0546	1.0113
<del>-</del>	27.95	-0.04	3.5066	3.3105	0.1673		-0.0208		0.2670	0.0371	0.9423 0.9441
i	31.23	-0.07	4.4786	4.1750	0.2381	0.2921	-0.0266		0.2777	0.0051	0.9322
ž –	15.33	-0.00	1.0567	1.4974	-0.0271		-0.0136		0.2736	0.0625	
3	5.10	-0.DO	0.5563	0.6113	-0.0064	0.0237	-0.0104	0.3011	0.1956	0.1055	2.7012
24	5.10	-0.00	0.5358	0.5970	-0.0051	0.0238	-0.0104	0.2935	0.1926	0.1009	2,5649
5	0.01	0.00	-0.0166	0-1169	-0.0045	0.0064	-0.0088	5995.0	0.1472	0.1169	-6.9604
						- 177.00 mm					
			<del> </del>								
									<del></del>		
										~ ***	

GE	ENGINEED 1 OF 1 1 OF 1	SIME UE	VEL OPHENT	CENTERIA	<u>EDC)</u> P			NEL FACILII		AER	SHANUT GINE SIMANYOC	<u>L (4T)</u>
	_		ACH RX10-		CONF O	L DEL		DEL3_ DEL4				
TMIO	l Alīpha	102 l. "BETA"	CM		Z#0F0 0	CLN	- CLL	OFF OFF	CAB	CAF	кср	
i	-2.05	-0.00	-0.1169		-0.0155	0.0494	-0.0085	0.4326	0.1452	0.2874	1.0923	
Ž	-1.03	-0.00	-0.0647	-0.0383	-0.0151	0.0535	-0.0073	0.4255	0.1578	0.2678	0.5919	
	0.01		-0.0094		-0.0157		-0.0092		0.1621	2595.0	-6.1700	
	1.04	-0.00	0.0415		-0.0142		-0.0099	0.4245	0.1663	0.2582	3.7401	
<b>,</b>	2.08	-0.00	0.0923		-0.0147	0.0634	-0.0106		0-1714	0.2549	2.0211	
	3.06	-0.00	0.1404	0.3576	-0.0142	0.0576	-0-0112	0.4327	0.1687	0.2640	2.5462	
	4,10	-0.00	0.1968	0.4569	-0.0146		-0.0105	0.4415	0.1723	0.5695	2,3206	
9	5.09	-0.00	0.2487	0.5591	-0.01-1	0.0729	-0.0112	9.4512	0.1807	0.2704	2.2486	
		-0.06_	<u> </u>	0.658A	0.0154		0.0134	0.4651	0.1830	0.5851	_ 2.1161	
Œ.		-0.00	0.4511		-0.0181		-0.0134	0.4827	0.2030	0.2797	1.8758	
	10.24		0.6172		-0.0233	0.1061	-0.0134	0.4909 .	.0.2171	0.2738	_1.6141	
	12.24	-0.01	0.9002	1.1914	-0.0244	0.1130	-0.0137	0.4964	0.2571	\$965.0	1.4896	
<del>-</del>	15.36 18.49	-0.01 -0.01	1.1333	1.7856	-0.0220	0.1124	-0.0138	0.5006	0.2624	0.2382	1.2950	
	21.67		2.1990	2.1947	-0.0286 0.0580	0-1497	-0.0172	0.5009	0.2725	0.2284	1.1403	
5		-0.05	2.9525	2.7719	0.0877	-0.0449_ -0.03F7			0.2867	0.2027	_ 0.9988	
	28.13		3.8609	3.3404	0.1826		_0.0173		0.3033	0.1759	0.8652	
<u>,                                     </u>	31.34		4.7774	3.7016	0.1020		-0.0244		0.3093	0.1770	0.7748	
	15.35	-0.01	1-1046	1.6207	-0.0184		-0.0100		0.3096	0.1880	1.4672	
0	5.13	-0.00	0.2237	0.6776			-0.0071		0.2640	0.1941	3.0289	
Į.		-0.00			-0.0201		-0.0037		0.2189	0.2056	-4.7249	
	•											
								<del></del>	· <del></del> -			
						· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			<del></del>		
											<del></del>	

.6E	ENGINEE 1 OF 1 1 OF 1	BIMB NE	VELOPMENT	CENTEH (4	LEOC) F			NNEL FACILI AIL EFFECTS		AER	ODANAHIC PI	NO TUNNEL (4T)
	TEST	PART M	ACH FX10-		CONF	L OEL		DEL3 DEL4 OFF OFF	TRANSITI UNKNOWN			
INT	ALPHA	HETA	CN -	CLH-		CLN			ČAB	CAF	XCP	
1	-2.03	0.00	-0.1165		-0.0083		-0.0029		0.1933	0.2416	1.1066	
S	-1.03	0.00	-0.0054	-0.020+	-0.0090	0.0174	-0.0033		0.1821	2845.0	0.3116	
_3	0.00 1.05	-0.00-	0.0166 0.0393		-0.0096		-0.0039		0.1744	0.2527	-6,27 <b>62</b> 5,38 <b>35</b>	
5	5.00	-0.00	0.0556		-0.0057	0.0174	-0.0053		0-1754	0.2531	3.9626	
6	3.06	-0.00	0.1369	0.4585	-0.0071	0.0164	-0.0061		0.1699	0.2616	3.3486	
7	4.06	0.00	0.1860	0.5836	-0.0123	0.0725	-0.0055		0.1711	4075.0	3.1284	
	5.12	-0.00	0.5.00	0.7244	-0.0059		-0.0063		0.1721	0.2835	3.0082	
10	6.14	0.00_	0.3005	0.8466	-0.0149 0.0110		-0.0060		0.1762	0.2893		
11	6.13 7.17	0.00	0.3669	0.9585	-0.0248		-0.0068		0.1879	0.2796	2.7699	
įż	8.22	-0.00	0.4458	1.0610	-0.0125		-0.0061		0.1936	0.2930	2.3799	
13	10.24	-0.00	0.6214	1.7454	0.0017	0.0290	-0.0077	0.4882	0.2019	0.2863	2.0042	
14	12.33	-0.00	0.8339	1.4529	-0.0115		-0.0098		0.2069	0.2844	1.7423	
_15	15.45	-0.00	1-2050	1.7757	0.0086		-0.0130		. 0. 2206	0.2777	1.4736	
16 17	21.79	-0.01 -0.01	1.7347	7.1756 2.6557	-0.0249 0.0290		-0.0143 -0.0181		0.2330 0.2491	0.2693	1.2542	
18	25.04	-0.05	3.3638	3.1556	0.0902				-0.262B	0.2371	0.9381	<del></del>
19	28.29	-0.03	4:2870	3.5408	0.1616				0.2731	0.2321	0.8259	
20	31.55	-0.05	5.3749	3.5761	0.1564	0.1947	-0.0260	0.4947	0.2563	0.2084	0.6653	
51	15.43	-0.00	1.1832	1.6949	-0.0127				_0.2915 _	0.2031	1.6015	
53	5.13	-0.00	0.2312	0.7903					0.2499	0.2045	3.4179	
23	-0.00	<u> </u>	- <u>0.0189</u>	0.1545	-0.0068	0.0089	-0.0054	0.4305	0.5065	0.5575	-4.8282	·
												· · · · · · · · · · · · · · · · · · ·
									<del></del>			
									·			
				-								

::	1 OF 1	RING_DI	EVELOPMENT	CENTER	veoc)	PROPULSION MARTIN M	ISSILE TO	NNEL FACILI'S	TY (PWT) DATA	AER	ODYNAMIC WIND TUNNEL (41
	TE5T		ACH RX10-6	_	CONF BZ+0F0	L DEL		DEL3 DEL4 OFF OFF	TRANSITI UNKNOWN		
INT"	ALPHA	DETA	CN	CLM	¢v	CLN	CLL	CA	CAB	CAF	xce
	-7.04	0.00	-0.1079			-0.0049	-0.0056	0.4166	0.1589	0.2577	1.2205
<u> </u>	-1.01 -0.00	0.00		0.1064		-0.0037	-0.0075	0.4130 0.4126	0.1641	0.2490	0.3157
	1.00	-0.00	0.0476	0.2296			-0.0080	0.4128	0.1645	0.2480	-32,799 <u>3</u> -4,8279
	2.03	0.00	0.0940		-0.0110		-0.0095		0.1649	0.2494	3.6393
	3.08	0.00	0.1519	0.4838	-0.0114	0.0104	-0.0090	0.4185	0.1662	0.2523	3.1846
	4,10	-0.00	0.2073	0.6048			-0.0109		0.1677	0.2585	2,9189
	5.10	-0.00	0.2645	0.7240					0.1706	2895.0	2.7371
,  -		-0.00	0.3349	0.8336 1.0313					0.1747	_0,2737_	2.4886 2.9901
ĺ	10.25		0.6724	1.2051					0.1867	0.2874	1.7922
2	12.35	-0.00	0.8864	1.4303					0.1953	0.2895	1.6136
3	15,43	-0.00	1.2853	1.8059	-0-0202	0.0800	-0.0174	0.4914	0,2104	0.2810	1.4050
	18.67	-0.00		2.7647					0.2238	0.2740	1-1950
5		-0.01		_2./833			0.0238		_0.2418	0.5676	1.0303
5 7	28.38	-0.02		3.0881			-0.0270 -0.0308		0.2550 0.2653	0.2550	0.8626 0.7002
B	31.58	-0.02		2.8847			-0.0315		0.2304	0.2445	0.5066
9		-0.02		2.9116			-0.0317		0,2878	0.2308	0.5107
			<del> </del>					· · ·			
										· <u>-</u>	
											· // -
			·····		·_·-						

1 -7.03	CAF XCP 0.1450 1.3796 0.1475 1.3807 0.1536 0.2345 0.1514 1.3686 0.1510 2.2179 0.1521 1.4078 0.1504 1.3710 0.1508 1.3796 0.1498 1.4277 0.1469 1.3668 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
1 -7.03	0.1450 1.3796  0.1475 1.3807  0.1536 0.2345  0.1514 1.3486  0.1510 2.2179  0.1521 1.4078  0.1504 1.3710  0.1508 1.3796  0.1498 1.4277  0.1469 1.3660  0.1464 1.3699  0.1478 1.2621  0.1292 1.0926
1 -7.03	0.1475
3	0.1536 0.2345 0.1514 1.3686 0.1510 2.2179 0.1521 1.4078 0.1504 1.3710 0.1508 1.3796 0.1498 1.4277 0.1469 1.3660 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	0.1514 1.3686 0.1510 2.2179 0.1521 1.4078 0.1504 1.3710 0.1508 1.3796 0.1498 1.4277 0.1469 1.3668 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
5 -0.01 0.00 0.0023 0.0050 -0.0062 0.0041 -0.0078 0.2505 0.0996 0.1 6 2.01 0.00 0.0903 0.1271 -0.0028 0.0032 -0.0088 0.2499 0.0978 0.1 7 2.01 0.00 0.0930 0.1276 -0.0028 0.0053 -0.0048 0.2527 0.1023 0.1 8 3.05 0.00 0.1392 0.1920 -0.0036 0.0059 -0.0075 0.2553 0.1044 0.1 9 4.04 -0.00 0.1801 0.2572 -0.0032 0.0065 -0.0099 0.2578 0.1080 0.1 10 5.07 -0.00 0.2331 0.3185 -0.0014 0.0050 -0.0099 0.2578 0.1080 0.1 11 6.07 -0.00 0.2331 0.3185 -0.0014 0.0050 -0.0104 0.2613 0.1144 0.1 12 8.12 -0.00 0.3899 0.4921 0.0002 0.0109 -0.0100 0.2662 0.1198 0.1 13 10.13 -0.00 0.5204 0.5687 0.0041 0.0096 -0.0113 0.2662 0.1198 0.1 14 12.14 -0.00 0.6755 0.6317 0.0107 0.017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.9486 0.7364 0.0122 0.0072 -0.0126 0.2715 0.1800 0.0 16 18.27 -0.00 1.2690 0.6528 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.8763 -0.4210 1.0292 -0.0095 0.2460 0.1482 0.0	0.1510 2.2179 0.1521 1.4078 0.1504 1.3710 0.1508 1.3796 0.1498 1.4277 0.1469 1.3669 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
7	0.1504 1.3710 0.1508 1.3796 0.1498 1.4277 0.1469 1.3660 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
8 3.05 0.00 0.1342 0.1920 -0.0036 0.0059 -0.0075 0.2553 0.1044 0.1 9 4.04 -0.00 0.1841 0.2572 -0.0032 0.0055 -0.0099 0.2578 0.1080 0.1 10 5.07 -0.00 0.2331 0.3185 -0.0014 0.0050 -0.0104 0.2613 0.1144 0.1 11 6.07 -0.00 0.2804 0.3842 0.0003 0.0035 -0.0110 0.2662 0.1198 0.1 12 8.12 -0.00 0.3899 0.4921 0.0002 0.0109 -0.0102 0.2761 0.1283 0.1 13 10.13 -0.00 0.5704 0.5687 0.0041 0.0096 -0.0113 0.2813 0.1521 0.1 14 12.14 -0.00 0.6755 0.6317 0.0107 0.0017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.9486 0.7364 0.0122 0.0072 -0.0126 0.7715 0.1800 0.0 16 18.27 -0.00 1.2690 0.6528 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.8763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.9999 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	0.1508 1.3796 0.1498 1.4277 0.1469 1.3668 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
9	0.1498 1.4277 0.1469 1.3660 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926
10 5.07 -0.00 0.2331 0.3185 -0.0014 0.0050 -0.0104 0.2613 0.1144 0.1 11 6.07 -0.00 0.2804 0.3882 0.0003 0.0035 -0.0110 0.2662 0.1198 0.1 12 8.12 -0.00 0.3899 0.4921 0.0002 0.0109 -0.0102 0.2761 0.1283 0.1 13 10.13 -0.00 0.5204 0.5687 0.0041 0.0096 -0.0113 0.2813 0.1521 0.1 14 12.14 -0.00 0.6755 0.6317 0.0107 0.0017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.9486 0.7364 0.0122 0.0072 -0.0126 0.2715 0.1800 0.0 16 18.27 -0.00 1.2690 0.6528 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.8763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.9949 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	0.1469 1.3660 0.1464 1.3699 0.1478 1.2621 0.1292 1.0926 -
11 6.07 -0.0U 0.2804 0.3882 0.0003 0.0035 -0.0110 0.2662 0.1198 0.1 12 8.12 -0.00 0.3899 0.4921 0.0002 0.0109 -0.0102 0.2761 0.1283 0.1 13 10.13 -0.00 0.5704 0.5687 0.0041 0.0096 -0.0113 0.2813 0.1521 0.1 14 12.14 -0.00 0.6755 0.6317 0.0107 0.0017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.4948 0.7364 0.0122 0.0072 -0.0126 0.2715 0.1800 0.0 16 18.27 -0.00 1.2690 0.2525 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.8763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.4949 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	0.1464 1.3699 0.1478 1.2621 0.1292 1.0926 -
13 10.13 -0.00 0.5704 0.5687 0.0041 0.0096 -0.0113 0.7813 0.1521 0.1 14 12.14 -0.00 0.6755 0.6317 0.0107 0.0017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.9486 0.7364 0.0122 0.0072 -0.0126 0.7715 0.1800 0.0 16 18.27 -0.00 1.2690 0.6526 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.6763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.9949 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	0.1292 1.0926 .
14 12.14 -0.00 0.6755 0.6317 0.0107 0.0017 -0.0125 0.2823 0.1607 0.1 15 15.22 -0.00 0.9486 0.7364 0.0122 0.0072 -0.0126 0.2715 0.1800 0.0 16 18.27 -0.00 1.2690 0.6526 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.6763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.9949 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	
15	
16 18.27 -0.00 1.2690 0.6528 -0.0108 0.0555 -0.0111 0.2571 0.1948 0.0 17 21.37 -0.00 1.6512 0.6763 -0.4210 1.0292 -0.0095 0.2460 0.1882 0.0 18 21.36 -0.01 1.6191 0.9949 0.0294 0.0317 -0.0079 0.2341 0.2323 0.0	0.1216 0.9352 0.0915 0.7763
_17	0.0623 0.6720
	0.0578 0.5307
19	0.0018 0.6145
	-0.0077 0.4853
	-0.0123 0.0159 -0.1062 0.2504
	0.0551 0.8915
	0.1059 2.0105
24 0.00 0.00 -0.0159 0.0502 -0.0052 -0.0018 0.0011 0.2439 0.1283 0.1	0.1156 -3.6554

1 0,00 2 -2.0 3 -1.0 4 1.0 5 2.0 6 3.0 7 4.0 8 5.0 9 6.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00	-0.0103 -0.0948 -0.0509 0.0396 0.0469	0.0368 -0.1036 -0.0433 0.0667 0-1462	-0.0062 -0.0067 -0.0057 -0.0056	-0.0019 -0.0054 -0.0027 0.0006	0.0010 0.0017 0.0014	Ca 0.2553 0.2617 0.2574	0.069 0.0987	CAF 0.1884 0.1626	ACP -3,7793 1.0929
2 -2.0. 3 -1.00 4 1.00 5 2.00 6 3.0. 7 4.00 8 5.00 9 6.00	0.00 0.00 0.00 0.00 0.00	-0.0948 -0.0509 0.0398 0.0869	-0.1036 -0.0433 0.0667 0.1462	-0.0067 -0.0057 -0.0056	-0.0054 -0.0027	0.0017 0.0014	0.2617	0.0987		
3 -1.00 4 1.00 5 2.00 6 3.00 7 4.00 9 6.00	0.00 2 0.00 5 0.00 3 0.00 5 0.00	-0.0509 0.0396 0.0469	-0.0433 0.0567 0.1482	-0.0057 -0.0056	-0-0027	0.0014				
4 1.00 5 2.00 6 3.00 7 4.00 8 5.00 9 6.00	0.00 0.00 0.00 0.00	0.0396	0-0567	-0.0056				0.1011		0.8502
2.00 5 3.00 7 4.00 8 5.00 9 6.00	0.00 3 0.00 5 0.00			-0-0040		0.0006	0.2533	0.1022	0.1511	2.1500
3.0. 4.0! 5.0' 6.0!	5 0.00	0.1285			0.0012	0.0000	0.2548	0.1025	.0.1523	1.7040
5.0° 6.0°			0.2097	-0.0035	0.0039	-0.0004	0.2577	0.1069	0.1508	1.6310
9 6.00		0.1787	0.2743	-0.0055	0.0045	-0.0010	0.2633	0.1128	0.1505	1,5351
	_	0.2765	0-3365	-0.003A	0.0051	-0.0015	0.2665	0.1155	0.1510	1.4857
		<u> </u>	0•4012 <u>.</u> 0•5027	-0.0009	0.0036	-0.0021	0.2731 0.2825	0.1235	0.1496	1.4816
1 10.14		0.5194	0.5705	0.0016		-0.0024	0.2859	0.1501	0.1358	1.0909
2 10.1		0.5194	0.5786	0.00-1	0.0054	-0.0025	0.2894	0.1587	0.1308	1.1139
	-0.00	0.6795	0.6344	0.0117	-0.0063	-0.0037	0.2883	0.1649	0.1234	0.9337
4 14-2		0.4520	0.7072	0.0158	-0.0117	-0.0050	0.2798	0.1795	0.1003	0.8300
18.3		1.2792	0.8873	0.0838	-0.1578	-0.0055	_0.2605_	0.1962	0.0643_	0.6942
6 21.3			0.9611	0.2013	-0.6026	-0.0002	0.2476	0.2009	0.0466	0.5810
8 27.5		3.0403		0.3552 -1.9947	1.6330	0.0018	0.2155 0.2307	_0.2359 0.2453	-0.0204	0.4947
9 30.7			0.9147		-2.4331	0.0245	0.2177	0.2498	-0.0321	0.2563
0 30.7			0.7474		-3.2399	0.0287	0.2156	0.2878	-0.0722	0.2095
21 15.2		0.9380	0.8456	0.0083	0.0040	0.0046	0.2779	0.2384	0.0395	0.9016
5.0	5 0.00	0.2033	0.4029		-0.0058	0.0070	0.2697	0.1654	0.1042	1.9817
23 -0.0				-0.0015		0.0096	0.2538	0.1109	0 . 1429	-2.7649
-2.0	2 0.40	-0.0958	-0.1059	-0.0041	-0.0149	0.0096	0.2862	0.1038	0.1824	1.1047

TEST PART MAKE RX10-6 PMI COMF L OEL1 DEL2 DEL3 DEL4 TRANSITION  189 u.92 2.3 0.08 650F0 0.0 OFF OFF OFF OFF OFF OFF OFF OFF OFF OF	T ALPMA BETA CN CLM CY CLM CLL CA CAB CAF RCP -2.02 0.00 -0.0955 -0.1096 -0.0052 -0.0149 0.0096 0.2863 0.1082 0.1781 1.1476 -1.01 0.00 -0.0504 -0.0535 -0.0038 -0.0014 0.0111 0.2824 0.1071 0.1753 1.0618 0.01 0.00 -0.0049 0.0162 -0.0036 -0.0078 0.0091 0.2823 0.1041 0.1762 -3.3162 1.03 0.00 0.0423 0.0779 -0.0054 -0.0091 0.0085 0.2808 0.1070 0.1738 1.8402 2.02 0.00 0.0846 0.1405 -0.0027 -0.0046 0.0091 0.2818 0.1057 0.1761 1.6559 3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2867 0.1102 0.1765 1.5799 4.05 0.00 0.2722 0.3339 -0.0024 -0.0025 0.0070 0.2921 0.1115 0.1806 1.5448 5.09 0.00 0.2726 0.3879 -0.0024 -0.0078 0.0044 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2726 0.3879 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0055 0.3253 0.1413 0.1766 1.2882 10.17 -0.00 0.5347 0.5501 0.0020 0.0033 0.0055 0.3253 0.1413 0.1766 1.2282 115.21 -0.00 0.9969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.7958 0.2108 0.0855 0.6618 21.40 -0.00 1.7293 1.0145 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2761 0.2384 0.0287 0.2231 15.25 -0.00 0.9744 0.65300 0.0087 0.0042 0.7671 0.2384 0.0287 0.2231 15.25 -0.00 0.9744 0.65300 0.0087 0.0042 0.7671 0.3381 0.2315 0.0866 0.8518 5.06 0.00 0.00755 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	92 2.3 0.0 45mdF0 0.0 OFF OFF OFF UNKNOWN	
-2.02	-2.02		
-2.02	-2.02	CN CLM CV CLN CLL CA CAB CAF RCP	
0.01 0.00 -0.0049 0.0162 -0.0036 -0.0078 0.0091 0.2823 0.1041 0.1782 -3.3182 1.03 0.00 0.0623 0.0779 -0.0054 -0.0091 0.0085 0.2808 0.1070 0.1738 1.8402 2.02 0.00 0.0866 0.1405 -0.0027 -0.0066 0.0081 0.2818 0.1057 0.1761 1.6559 3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2867 0.1102 0.1765 1.5799 4.05 0.00 0.1750 0.2704 -0.0004 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448 5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4827 6.09 0.00 0.2766 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5357 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 12.17 -0.00 0.6969 0.6127 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 15.21 -0.00 0.9858 0.7460 -0.0033 0.0229 0.0039 0.3109 0.1870 0.1239 0.7579 18.35 -0.00 1.3424 0.8679 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.3242 0.8679 0.0522 -0.0746 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5526 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2248 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	0.01 0.00 -0.0049 0.0162 -0.0036 -0.0078 0.0091 0.2823 0.1041 0.1782 -3.3182 1.03 0.00 0.0623 0.0779 -0.0054 -0.0091 0.0085 0.2808 0.1070 0.1738 1.8402 2.02 0.00 0.0086 0.1405 -0.0027 -0.0004 0.0081 0.2818 0.1057 0.1761 1.6559 3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2887 0.1102 0.1765 1.5799 4.05 0.00 0.1750 0.2704 -0.0004 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448 5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2786 0.3879 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3722 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5357 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 12.17 -0.00 0.5357 0.5501 0.0020 0.0033 0.0055 0.3223 0.1494 0.1759 1.0249 15.21 -0.00 0.9959 0.7460 -0.0033 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3224 0.8879 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.3224 0.8879 0.0522 -0.0746 0.0032 0.2750 0.2108 0.0850 0.6615 21.40 -0.00 1.3224 0.8879 0.0522 -0.0746 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2132 1.3347 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3099 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0022 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.0275 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	-0.0955 -0.1096 -0.0052 -0.0149 0.0096 0.2863 0.1082 0.1781 1.1474	
1.03	1.03		
2.02 0.00 0.0846 0.1405 -0.0027 -0.0066 0.0081 0.2818 0.1057 0.1761 1.6559 3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2867 0.1102 0.1765 1.5799 4.05 0.00 0.1750 0.2704 -0.0060 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448 5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2796 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5347 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9954 0.7460 -0.0003 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.2758 0.2108 0.0850 0.6618 21.40 -0.00 1.7293 1.0145 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5942 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2168 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3099 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0116 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.22075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	2.02 0.00 0.0866 0.1405 -0.0027 -0.0066 0.0081 0.2818 0.1057 0.1761 1.6558  3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2867 0.1102 0.1765 1.5799  4.05 0.00 0.1750 0.2704 -0.0040 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448  5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027  6.09 0.00 0.2796 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908  8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282  10.17 -0.00 0.5357 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249  12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1556 0.8792  15.21 -0.00 0.9854 0.7460 -0.0003 0.0229 0.0039 0.3109 0.1570 0.1239 0.7576  18.35 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615  21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982  24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2511 0.3090 -0.0579 0.2238  30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2238  15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518  5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
3.05	3.05 0.00 0.1317 0.2080 -0.0045 -0.0021 0.0076 0.2867 0.1102 0.1765 1.5799 4.05 0.00 0.1750 0.2704 -0.0000 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448 5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2786 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5347 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 12.17 -0.00 0.6969 0.6127 0.0004 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9954 0.7660 -0.0003 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0145 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0146 0.3021 0.1596 0.1425 1.8691	U.U.C.S U.U.TY -U.U.D.S -U.U.Y.1 U.U.U.S U.Z.505 U.1070 U.1735 1.08402	
4.05 0.00 0.1750 0.2704 -0.0040 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448  5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2786 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908  8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5347 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249  12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9854 0.7460 -0.0033 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4615 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8746 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0051 0.3181 0.2315 0.0866 0.0810 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	4.05 0.00 0.1750 0.2704 -0.0000 -0.0015 0.0070 0.2921 0.1115 0.1806 1.5448  5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0044 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2786 0.3874 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908  8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5347 0.5501 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249  12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9854 0.7460 -0.0003 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3424 0.8879 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0067 0.0042 0.0146 0.3021 0.1596 0.1425 1.8691		<del> </del>
5.09	5.09 0.00 0.2252 0.3339 -0.0024 -0.0028 0.0064 0.2988 0.1195 0.1793 1.4027 6.09 0.00 0.2796 0.3879 -0.0053 0.0016 0.0076 0.3035 0.1268 0.1767 1.3908 8.10 -0.00 0.3922 0.4817 -0.0006 0.0045 0.0050 0.3178 0.1413 0.1766 1.2282 10.17 -0.00 0.5347 0.5550 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 12.17 -0.00 0.6969 0.6127 0.0020 0.0033 0.0055 0.3253 0.1494 0.1759 1.0249 15.21 -0.00 0.9859 0.6127 0.0007 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9859 0.7460 -0.0033 0.0229 0.0039 0.3109 0.1870 0.1239 0.7570 18.35 -0.00 1.3424 0.8879 0.0522 -0.0786 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0455 0.5982 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 0.380 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0067 0.0042 0.002 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
8.10 -0.00	8.10 -0.00		
10.17 -0.00	10.17 -0.00		
12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9654 0.7460 -0.0003 0.0229 0.0039 0.3109 0.1870 0.1239 0.7576 18.35 -0.00 1.3424 0.6679 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0349 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2848 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	12.17 -0.00 0.6969 0.6127 0.0047 0.0020 0.0043 0.3222 0.1672 0.1550 0.8792 15.21 -0.00 0.9654 0.7460 -0.0003 0.0229 0.0039 0.3109 0.1570 0.1239 0.7576 18.35 -0.00 1.3424 0.6679 0.0522 -0.0746 0.0042 0.2958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0145 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2142 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
15.21 -0.00	15.21 -0.00		
18.35 -0.00	18.35 -0.00 1.3424 0.8679 0.0522 -0.0746 0.0042 0.7958 0.2108 0.0850 0.6615 21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2132 1.3947 0.0098 0.7671 0.2384 0.0287 0.2148 30.80 0.33 3.8746 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0067 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	21.40 -0.00 1.7293 1.0345 -0.0156 0.0533 0.0052 0.2704 0.2219 0.0485 0.5982 24.51 0.11 2.4415 0.5226 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
24.51 0.11 2.4415 0.5226 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	24.51 0.11 2.4415 0.5226 -1.2182 1.3947 0.0098 0.2671 0.2384 0.0287 0.2148 30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0262 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0067 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	30.80 0.33 3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.0579 0.2231 15.25 -0.00 0.9744 0.6300 0.0087 0.0042 0.0101 0.3181 0.2315 0.0866 0.8518 5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691		
5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	5.06 0.00 0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	3.8796 0.8654 -0.5346 -3.4675 0.0282 0.2511 0.3090 -0.057 <u>9 0.2231</u>	· ·
		0.2075 0.3879 -0.0026 -0.0082 0.0146 0.3021 0.1596 0.1425 1.8691	
			~
'			
·			
			•

	1 1651		ACH PXIO-		COMF 5=0F0 0	L DEL1		DEL3 DEL4 OFF OFF	TRANSIT			
OINT	ALPHA	BETA	CN	CLM	C4	CLN	CLL	ča	CAR	CAF	ACP	
1	-2.03	0.00	-0.1021	-0-1010	-0.0029	-0.0178	0.0153	0.3287	0.0945	0.2342	0.9894	
5	-1.01	0.00	-0.0555	-0.0392	-0.0027	-0.0134	0.0165	U-330A	3.1023	0.2285	0.6706	
_ 3 _	-0.00	0.00	-0-0040	0-0190	-0.0034	-0-0091	0.0147	0.3269	0.1095		-2.1065	
4	1.02	0.00	0.0378	0.0853	-0.0051	-0.0067	0.0141	0.3299	0.1093	9052.0	2.2579	
6	3.05	0.00	0.1353	_0.2046	-0.0020	-0.0037	0.0147	0.3376	0.1159	0.2216	1.5110	······································
7	4.07	0-00	0.1790	0-2684	-0.0026	-0-0013	0-0142	0.3424	0.1201	0.5553	1.4993	i
8	5.06	0.00	0.2289	0.3249	-0.0032	0.0011	0.0121	0.3476	0.1285	0.2191	1.4196	
10	8.14	0.00	0.2834	0.4673	-0.0015 -0.0025	0.0016	0.0132	0.3571	0.1311	0.2260	1.3370	
ii—	10.19	-0.00	0.5537	0.5334	0.0012	- 0.0044	_0.0121 0.0111	0.3678	0.1465	0.2193_	1.1599 0.9633	
iż	12.20	-0.00	0.7180	0.5967	-0.0014	0.0169	0.0114	0.3793	0.1783	0.2009	0.8311	
i3 ·	15.28	-0.00	1.0230	0.7107	-0.0111	0.0567	0.0094	0.3796	0.1847	0.1949	0.6947	
14	18,36	-0.00	1.3699	0.8371	0.0172	-0.0004	0.0098	0.3564	0.2163	0.1401	0.6023	
15	21.47	-0.0y	1.8426	0.7541	0.0701	-0.1096	0.0109	0.3275	0.2427	0.0848	0.5178	
17	27.74	0.20	3.3086	0.9558	-1.0484	-0.2182	0.0202	0.3046	0.2874	0.0171	0.2889	
18	30.90	0.26	4.1695	1.2255	-0.4314	-2.5332	0.0264	0.2929	0.3026	-0.0097	0.2939	
19	30.92_	0.26	4-2003	1.2247	0.4095		.0-0272	0.2990	0.3137	-0.0147	_0.2916	
50	15.24	-0.00	0.9980	0.7936	-0.0168	0.0649	0.0187	0.3777	0.2750	0.1027	0.7951	
21	5.07	0.00	0.2093	0.0569	0.0010		0.0214	0,3505	0.2105	0.1400	1.8480	
52	-0.00	0.00	-0.0246		-0.0036	-0.0162	0-0223	0.3274	0.1468	0.1805	-2.3176	
					<del> </del>		<del></del>	<del></del>	<del>_</del>	<del></del>		
							-					
_												
			<del></del>								<del></del>	

.6€ <u> </u>	ENGINEE! I OF I I OF I	ING D	EAFFOGHEN!	CENTER (A	E0C) P	ROPULSION MARTIN MI	WIND TUP SSILE TA	NEL FACILI	TY-(PUT)	AERC	DÄWVWIC RIND İMM	<u>•EL (• T)</u>
	TEST		-ACH RX10-	6 PHI		L DEL1	DEL? OFF	DEL3 DEL4 OFF OFF	TRANSIT			
TNIC	AL PHA	BETA		CLM	CY	CLN	CLL	CA	CAB	CAF	ACP	<del></del>
_1	-7.04	0.00		-0.1526	-0.0144	0.0219	0.0271	0.4331	0.1571	0.2760	1.6614	
3	-1.03 -0.01	0.00		-0.0279	-0.0159	0.0321	0.0210	0.4280 0.428I	0.1655	0.2744	2.1823 -3.6193	
	1.03	0.00		0.040	-0.0145	0.0310	0.0262	0.4309	0.1687	2592.0	0.7603	
5	2.03	0.00			-0.0168	0.0399	0.0256	0.4328	0.1687	0.2641	1.0631	
	3.07	-0.00	0.1493	0.1706	-0.0152	0.0366	0.0249	0.4364	0.1704	0.2660	1.1425	
7	4.04	-0.00		0.2-57	-0.0176	0.0459	8550.0	0.4455	0.1787	0.2668	1.2650	
8	5.05	-0.00		0.3067	-0.0141	0.0448	0.0237	0.4532	0.1795	0.2737	1.2436	
. •	_ 6.10	-0.00		0.5056	-0.0157 -0.0154	0.0440	0.0231	0.4644	0.1672	0.2772_	_1.3330	
10 11	8.14	-0.00		0.6007		0.0550	0.0221	0.4613	0.1895	0.2918	1.1893	
5	12.20	-0.00				-0.0409	0.0212	0.4924	0.2167	0.2757	0.8940	
13	15.29	-0.00	_	0.7990	-0.0589	0.1858	0.0198	0.4894	0.2357	0.2537	0.7407	
14	18.40	-0.00	1.4934	5299.0	-0.1599	0.4062	0.0183	0.4809	0.2534	0.2275	0.5908	
15	_21.51	0.01				0.9863	0.0164		0.2758	0.1923	0.4315	
16	24.64	0.05				1.3365	0.0164	0.4508	0.2901	0.1607	0.2177	
17	27.81	0.14			-1.1153	0.8697	0.0179		0.3105	0.1383	0.0210	
18	31.04	-0.00			-0.5073 -0.0746	-1.8727 0.7207	0.0229		0.3434	0.0899	0.1041	
20	5.09	-0.00				0.0440	0.0251		0.2432	0.2198	1.5494	
21	-0.01	0.00			-0.0152	0.0311	0.0283		0.1939	0.2457	-3,6538	
				<del></del>	<del></del>			<del></del>		<del></del>		
						<del></del>						
—-					-							
										·		
										·		

1	OF 1					MARTIN MI	SSILE T	AIL EFFECTS	DATA		ODYNAMIC WIND TUNNEL (4	
	_ TEST	PAPT :	MACH RX10-0		CONF ShoFO	L DEL1		DEL3 DEL4 OFF OFF				
NŤ	ALPHA	BETA		CL#	CA	CLN	CLL		CAB	CAF	XCP	
	-2.03	0.00	-0.10-3	-0.0824	-0.0093		0.0760	0.4227	0.1485	0.2741	0.7906	
	-1.00	0.00		-0-0107	-0.0080	0.0144	0.0743	0-4156	0.1433	0.2723	0.1961	
	0.00	0.00		0.0685			0.0238		0.1421	0.2711	-6.3336	
	1.03	0.00	0.0362	0.1505			0.0232		0.1426	0.2714	4.1509	
	2.05	0.00	0.0619	0.2306	-0.0057		0.0223		0.1544	0.2608	2.8159	
	3.04	0.00	0.12-7	0.3067		_	0-0216	0.4186	0.1595	0.2593	2,4607	
	4.11	-0.00		0.3852	-0.0046		0.0207		0.1620	0.2613	2.1711	
	5.10	-0.00		0.4605	-0.0031		0.0213	0.4309	0.1677	0.2632	2.0221	
	6.09	-0.00		0.5344			0.0195		0.1638	0.2779	1.8945	
	10-19	-0.00		0.7558	0.0000		0.0187	0.4547	0.1816 0.1800	0.2731	1.6852 1.3536	
	12.24	-0.00		-0.8222			0.0179		0.1858	0.2791	1.0986	
	15.33	-0.00		0.5412			0.0156		0.2053	0.2566		
	18.42	-0.00		1.0440			0.0138		0.2126	0.2406	0.6980	
	21.58	0.00			-0.1966		0.0120		0.2355	0.2038	0.5165	
	24.78	0.01			-0.2165		0.0112		0.2464	0.1745	0.3990	
	27.92	0.03		0.6993	-0-4497	0.7533	0.0096		0.2483	0.1593	0.2387	
_	31.07	0.06	4.6952		-0.4592		0.0076	0.3937	0.2589	0.1347	0.1006	
,	15.32	-0.00			-0.0341		0.0187		0.2492	0.2152	0.9435	
	5.08	0.00			-0.0054		0.0218		0.2261	0.2088	2.4266	
	0.00	0.00	-0.0169	0.0991	0.0069	0.0138	0.0225	0.4183	0.1634	0.2549	5.2577	
			<del></del>									
_												
											<del></del>	

TEST		-ACH RX10-		CONF			DEL3 DEL4				
. — . —	_								96		<u> </u>
ALPHA	HETA	CN	CLH	CY	CLN	CLL	CA	CAB	CAF	XCP	
-2.03	0.00	-0.0831	-0.1487		-0.0080	0.0171	0.3837	0.1442	0.2395	1.7801	
-0.99		-0.0373	-0.0503		-0.0197	0.0153	0.3905	0.1655	0.2250	1.3468	
0.01	-0.00		0.0395		- 0.0003	0.0162	0.3871	0.1708	0.2163	4.6336	
1.03	0.00	0.0542	0.1363		-0.0115	0.0142	0.3903	0.1654	0.2249	2.5170	
5.06	0.00	0.1001	0.2319	-0.0075	-0.0076	0.0136	0.3931	0.1587	0.2345	2,3173	
3.08	0.06	0.1484	0.3258		0.0076	0.0145	0.3947	0.1617	0.2330	2,1956	
4.09	0.00	_	0.4145		0.0068	0.0123	0.3967	0.1662	0.2305	2.0994	
5.08	0.00		0.5042		0.0124	0.0133		0.1672	0.2390	2.0482	
6.12	-0.00		0.6065		0.0214	0.0128		0-1711	0.2441	2.0283	
10.20	-0.00		0.8208		0.0326	0.0112		0.1799_	0.2401	1.6902	
12.27	-0.00		0.4981		0.0369	0.0072		0.1956	0.2373	1.1116	
15.36	-0.00		1.0199		0.05.0	0.0046		0.2110	0.2259	0.8561	
18.46	-0.01	1.7111		-0.0013	0.0683	0.0031	0.4350	0.2217	0.2133	0.6307	
21.67	-0.01		1.0836		0.0408	0.0015		0.2377	0.1900	0.4475	
24.86	0.00			-0.1105		-0.0010		_0.2535	0.1706_	0.3255	
27.98	0.01			-0.3062	0.5418	-0.0026		0.2612	0.1664	0.1872	
31.18	0.03			-0.1663	-0.0157	-0.0043		0.2732	0.1452	0.0275	
15.38 5.10	-0.00		1.0713	-0.0068	0.0624	0.0059		0.2683	0.1503	0.8988 2.4014	
0.01	-0.03			-0.0084		0.0067		0.2245		-30.4071	<del></del>
		***************************************	555525				•••••	332235		-2004076	
						<del></del>					
							<del>-</del>				
										,,,,,,,,,,,,	
					<del></del>					<del></del>	<del></del>
										<del></del>	<del></del>
											<del> </del>

	TEST		ACH RX10-0 80 2.3		-	L	OEL1 OFF	OFF	DEL3 DEL	4 TRANSIT	1 1	
	ALPHA"	ĐĒ ŤĀ	CN	ci.	C4	CL		CLL -	- ča	CÁB	CAF	XCP
	-5.05	0.00	-0.0899		-0.0030				0.2444	0.1009		1,8839
	-5.05	0.00	-0.0697	-0.1693	-0.0031			-0.0055	0.2463	0.1021	0.1442	1.8845
	-2.01	0.00	-0.0879	-0.1698	-0.0043	-0.0	157	-0.0055	0.2470	0.1130	0.1340	1.9311
	-1.01	0.00	-0.0425	-0.0864	-0.0041	-0.0	127	-0.0058	0.2443	0.1058	0.1386	2.0428
	0.00	0.00_	0.0024	0.0054	-0.003A			-0.0060	0.7412	0.1026	0.1357	2.2351
	1.02	0.00	0.0441	0.1014	-0.0C21			-0.0085	0.7419	0.1018	0.1401	2.3005
	2.04	0.00	0,0955	0.1626	-0.0004			-0.0073	0.2434	0.1023	0.1411	1.9114
	3.04	0.00	0.1373	0.2767	-0.0ú25			-0.0097		0.1138	0.1321	2.0158
••	5.06	0.0v	0.1839 0.2330	0.3684	-0.0007			-0.0103 -0.0109		0.1165 0.1038	0.1324	2.0029 1.9634
	6.07	0.00	0.5609	0.5494	-0.0010			-0.0114		0.1288	0.1286	I - 12 - 12 - 1
-	8,13	-0.00	0.4001	0.6960	0.0028			-0.0126		0.1415	0.1262	1.7397
	10.14	-0.00	0.5389	0.6165	0.0000			-0.0119		0.1530	0.1180	1.5193
		-0.00	0.6974	0.9.86	6.0096			-0.0133		0.1652	0.1045	1.3602
	15.25	-0.0u	0.9569	1.1568	0.0011	_ C.O		-0.0115		0.1750	0.0847	1.2110
		-0.00	1.2621	1.3797	0.0191			-0.0139		0.1946		1.0932
		-0.00	1.5991	1.6128	0.0363				0.2253	0.2134	_ 0.0150"	1.0086
	24.46	-0.00	2.0261	1.6512	0.0620			-0.0090		0.2289	-0.0377	0.9128
		-0.00	2.4779	2.0301				-0.0059		0.2455	50000	0.8193
	30.61	-0.00	2.4643	2-1477				-0.0040		0.2317	0.0468	0.7197 1.3319
		0.00	0.2139		-0.0016					0.1418	0.1047	
			-0.0082								0.1223_	
		18 - 2-										
		<del></del> ·										
							_					<del></del>

	1 OF 1	B I NG L	EVELOPMENT	CENTER (	AEDC)		HISSILE T	NNEL FACILI		AER	ODÁNYHIC MIMD	YUNNEL (4T)
	TEST		MACH RX10-		CONF		L1 DEL2	DEL3 DEL4 OFF OFF	TRANSIT			
OTNT	ALPHA	0E TA		CL#		CLN -	CLL	CA	CAB	CAF	XCP	
1	0.00	0.00		0.0393					0.1052	0.1781	19.2288	
2	-5.05-		-0.0911	-0.1426	-0.0006	-0.0290	-0.0001	0.2394	0.0917	0-1477	1.5643	
3	-5.05	0.00		-0.1445					0-1157	0.1229	1.5310	
6	-1.03	0.00		-0.0633 0.2067					0.1089	0.1255	1.3839	
<del></del>	- 5.05.	0.00		0.2053					0.1105	0.1164_	2.2944	
ė	3.03	0.00		0.2923					0.1091	0.1268	2.1769	
9	4.04	0.00		0.3760	0.0006	-0.0093			0.1127	0.1271	2.0521	
10	5.06	0.00			-0.0002				0.1200	0.1234	2.0604	
12 11	8.13	0.00		0.5544	-0.000A				0.1235	0.1279	1.9478	
13	10.16	-0.0		0.6316					0.1507	_ 0.1225_ 0.1118	1.5353	
14	12.19	-0.00		0.9674					0.1641	0.0975	1.3752	
15	15.25	-0.00	0.9621	1.1786					0.1811	0.0715	1.2250	
16	18.30	-0-0		1.4050					0-1993	0.0417	1.0978	
17	21.37	-0.00		1.6504					0.2162	0.0041	1.0095	
18	24.45	-0.00		-1.6432			l0.0010 5		0.2352	-0.0365	0.9211	
20	30.64	-0.0		2.3230					0.2435	-0.1459	0.7465	
21		-0.0		1.2573					0.2202	0.0361	1.3312	
22	4.67	0.00		0.5181		-0.0079			0.1453	0.1053_	2.4864	<del></del>
23	-0.01	0.00	-0.0128	0.0608	-0.0014	-0.0143	3 0.0076	0.2339	0.1015	0.1324	-4.7471	
			·					<del> </del>				
								<del></del>				
_							–				_	
-												
							<del></del>					
							<del></del>	<del></del>			<del></del>	

NT AL	TEST P	APT P	ACH 8710-4								
		AB 0.	92 2.3	9 PMI 0.0 E	CONF 04±0F0 (	L DEL1	DEL2 OFF	DEL3 DEL4 OFF OFF	TRANSITI		
-2		BETA	CN	CLM	CA	CLN	CLL		ČA8 -	CAF	ACP
	2.03	0.00	-0.0955	-0.1501	-0.0030	-0.0216	0.0097	0.2378	0.1114	0.1264	1.5708
	1.02 0.01	0.00	-0.0453 0.0021	0.0166	-0.0015	-0.0185 -0.0141	0.0078	0.2312	0.1123 0.1067	0.120 <b>6</b> 0.1246	1.6021 8.0291
	1.02	0.00	0.0515	0.1072	-0.0019	-0.01>2	0.0068	0.2321	0.1106	0.1215	2.0809
	2.04	0.00	0.0413	0.1956	-0.0056	-0.0089	0.0064	0.2345	0.1132	0.1212	2.1427
	3.05	0.00	0.1403	0.2833	-0.0010	-0.0116	0.0057	0.2375	0.1179	0.1195	2.0199
	4,05	0.00	0.1886	0.3666	-0.0005	-0,0108	0.0052	0.2412	0.1161	0.1251	1,9435
	5.08	0.00	0.2359	0.4615	0.0012		0.0046	0-5-66	0.1160	0.1287	1.9564
	6.10	0.00_	0 • Sinne	_ 0.5485	-0.0017	-0.0039	0.0056	0.2548	0.1288	0.1560	1.8987
		-0.00	0.4141 0.5537	0.6954	0.0030	-0.0016 -0.0068	0.0045		0.1410 0.1560	0.1260 0.1145	1.6791
		0.00	0.7209	0.4622	0.0084	-0.0041	0.0019		0.1704	0.1016	1.3347
	_	-0.00	0.9937	1.1882	0.0044	0.0160	0.0015		0.1927	0.0706-	1.1958
		-0.00	1.3087	1.4184	0.0178		0.0023		0.2080	0.0437	1.0838
		-0.00	_1.6971	1.6966	0.0196	0.0754	0.0046		0.2190	_ 0.0134_	0,9997
_		-0.00	2.1881	2.0111	-0.0178	0.0530	0.0060	0.2066	0.2374	-0.0308	0.9191
		-0.01_ -0.02	2.7803	_ 2.4876. 3.3747	0.1121	=0.1241 =0.0379	0.0057		0.2459	-0.0771_	0.8948
	-	-0.02	3.6067 3.5818	3.3391	0.1666		0.0088		0.2493	-0.1123	0.9357 _0.9322
		-0.0u	0.9637	1.2761	0.0030		0.0128		0.2324	0.0373	1.3263
	5.08	0.00	0.2106	0.>331		-0.0019	0.0160		0.1772	0.0757	2.5307
	0.00	0.00	-0.0214	0.0709	-0.0026	-0.0136	0.0172	0.2350	0.1356		-3.3106
							•				
					. <del></del>						
				•							_

Ε	NGINEE OF 1 OF 1	TING UE	VEL OPHENT	CENTER	EDC) 5	PROPULSION MARTIN MI	WIND TUR SSILE TA	NEL FACILI	TY (PUT) DATA	AERO	DÒYNAMIC_#1MD 	TUNNEL (41)
	TEST		ACH RX10-		_	L DEL1	DELZ	DEL3 DEL4 OFF OFF	TRANSIT	ION		
NT	ALPHA	BETA	CN	CLH -	CŸ	CLM -	ĊĹĹ	CA	CAB	CAF	ACP	
	-2.03	0.00	-0.0A48				0.0187	0.5610	0,1236	0.1373	1.9992	
	-1.02	0.00	-0.0411	-0-0424	-0.0014	-0.0160	0.0168	0.2530	0.1249	0.1281	2.2492	
	0.00	0.00	0.0065	0.0015		-0.0170	0.0165	0.2560	0.1274	0.1586	0.2397	
	1.03	0.00	0.0535	0.0916	-0.0028	-0.0111	0.0159	0.7546	0.1223	0.1322	1.7130	
_	2.02 3.06	0.00	0.1019 0.1509	0.2663	-0.0012 -0.0040	-0.0063 -0.0045	0.0153	0.2581 0.2642	0.1269	0.1460.	1.7085	<del></del>
	4.07	0.00	0.2005	0.3575	-0.0056	0.0014	0.0157	0.2695	0.1281	0,1413	1.7829	
	5.10	0.00	0.2516	Ç.4483	0.0003		0.0152	0.2768	0.1387	0.1381	1.7813	
	6.09	0.00	0.3091		-0.0012		0.01-5	0.2906	0.1441	0.1465	1.7153	
		-0.00	0.4292	0.6907	0.0087		0.0149	0.3040	0.1582	0.1458	1.6093	<del></del>
	10.18	-0.00	0.5635	0.8336	0.0177		0.0119	0.3186	0.1695	0.1491	1.4286	
	12.18	-0.00	0.7436	0.9720	0.0150		0.0122	0.3150	0.1871	0.1280	1.3071	
	15.25	-0.00	1.0359	1.2270	0.0137	0.0074	0.0115	0.3157	0.2011	0.11-6	1.1845	
	18.36	-0.00	1.3979	1.4961	-0.0018	0.0699	0.0108	0.3076	0.2290	0.0785	1.0703	
		-0.01	1.8720_	1.6341	0.0491		0.0114		0.2436	0.0440	0,9798	
•		-0.01	2.5038	2.3256	0.0477		0.0096		0.2577	0.0074	0.9288	
33	27.80	-0.01	3.3237	3.0931	0.0876		0.0041	_ 0.2387	_ 0.2723	-0.0337	_0.9306	
i.	31.05	-0.02	4.1508	3.6685	0.1569		0.0068		0.2864	-0.0724	0.9320	
	15.28	-0.00	1:0177	1.2817	0.0168 -0.0041		0.0160	0,3193	0.2433	0.0760	1.2595	
	0.00	0.00	0.0019			0.0122	0.0198		0.1986	0.0850	2.0802 10.6055	
								<u></u>				<del></del>
											_	
<del></del> -								<del></del>				
					~							
											A	
							<del></del>					<del></del>

•

.

<u>}</u> _	OF 1			CEMIEKIA	FOC1	ROPULSION Martin Mi	WIND TU	NNEL FACIL AIL EFFECT	ITY(PWT) S DATA	AER	DOYNAMIC WIND TUNNEL
	TEST	PART M 200 1.	ACH RX10-		CONF O	L DEL1			4 TRANSITI		
u T	LPHĀ .	BETA	CN	CLH	CY	- CLN	CLL	CA	CAB -	CAF	ice
	2.02	0.00	-0.0956	-0.1696	-0.0045	-0.0012	0.0155	0.4267	0.1728	0.2538	1.7730
	-2.02	0.00	-0-0417	-0.1722	-0.0065	0.0000	0.0169	0.4280	0.1790	0.2490	1.8777
	1.03	0.00	-0.0459	-0.0786	-0.0091	0.0171	0.0167		0.1765	0.2496	1.7108
•		-0.00	0.0071	0.016#	-0.0137	0.0337	0.0150	0.4265	0.1774	0.2491	2.3543
	1.00	-0.00	0.0560	0.1216	-0.0093	0.0239	0.0143	0.4261	0.1822	0.2439	2,1729
	2.03	-0.00	0.1023	0.2566	-0.0107	0.0345	0.0137	0.4293	0.1775	0.2518	2.2147
	3.08	-0.00	0.1507	0.3396	-0.0063	0.0230	0.0116	0.4310	0.1A47	0.2464	2,2544
	4.07	-0.00	0.2000	0.4364	-0.0087	0.0384	0.0124		0.1821	0.2591	2.1919
	_5.08	-0.00	0.2546_	_ 0.5447_	.=0.0053	0.0284	0.0117	0.4481	_0.1940	0.2541	2.1394
		-0.00	0.3134	0.650#	-0.0076	0.0405	0.0111	0.4622	0.1970	0.2652	2.0763
-		-0.00	0.4344	0.9972	0.0006	0.0268	0.0097	0.4745	0.2110	0.2635	1.9080
	10.20	-0.00	0.5996 0.7828	1.1503	0.0052	0.0278	0.0047		0.2309	0.2618	1.6630
	17.26	-0.00	0.7864	1.1422	0.0070	0.0303	2800.0		0.2572	8962.0	1.4525
	15.36	-0.00	1-10-7	1.4511	0.0005	0.0536	0.0057		0.2591	0.2238	1.3136
	18.47	-0.01	1.5151	1.7911	0.0037	0.0774	0.0042		0.2756	0.1996	1.1622
	21.61	-0.01	2.0957	2.1521	0.0371	0.0309	0.0042		0.2893	0.1685	1.0269
	24.60	-0.01	2.8632	2.6104	0.0376	0.0344	0.0017		0.2949	0.1460	0.9117
	27.96	-0.01	3.7370	3-0324	0.0514	0.0544	-0.0007		0.3102	0,1168	0.8116
	31.18	-0.01	4.5645	3.3275	0.0209	0.1094	-0.0025	0.4169	0.3190	0.0980	0.7290
	15.35	-0.00	1.0882	1.4797	0.0042	0.0430	0.0085		_0.3118	0.1729	1.359 <u>7</u>
	0.00	-0.00	-0.0032	0.0634	-0.010B	0.0230	0.0133	0.4289	0.2112	0.2177	-19.7511
											<del></del>
			<del></del>	·					<del></del>		

	TEST		MACH RX10-		CONF 4w0f0 0.	L DEL1			EL4_TRANSIT DFF UNKNOW			
uT.	ALPHA	BETA	_	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	
	-2.03	0.00		-0-1195	-0.0054	0.0077	5600.0	0.4340		0.2866	1.2061	er con the control
	-1.03	0.00	-	0.0194	-0.0051 -0.0056	0.0048	0.0089	0.430		0.2795	170.0009	
	0.03	- 0.00	·	0.0982	-0.0056	0.0073	0.0070	0.428			193.5221	
	1.02	0.00		0.7083	-0.0052	0.0067	_0.0077	0.428		0.2731	4.6209	
	2.07	-0.00		0.3226	-0.0037	0.0096	0.0070	0.428		0.2741	3.4696	
	3.06	-0.00		0.4277	-0.0047	0.0120	0.0050	0.433		0.2804	2.9989	
	5.09	-0.00		0.6500	-0.0022	0.0111	0.0050	0.446		0.2825	2.6551	
	6.13	-0.00		0.7569	-0.0016	0.0137	0.0043			0.2869	2.4782	
	- 8.20	-0.00		0.9457	0.0046	0.0087	0.0043	0.469		8.2927	2.125 <u>0</u> _	
	10.22	-0.00		1.1015	0.0081	0.0027	0.0028	0.475	· · ·	0.2899	1.7951	
	15.39	-0.00		1.5661	0.002-	0.0420	0.0000	0.461		0.2646	1.3686	
	18.53	-0.0		1.9397	0.0072		-0.0021			0.2497	1,1813	
	21.71	-0.0		2.3566	0.0308		-0.0031	0.474		7525.0	1.0120	
	24.85	-0.0		2.6913	0.045Z 0.0641	0.0142	-0.0065			0.1983 0.1833	0.6712_ 0.7192	
	31.25	-0.0		2.9238	0.0232		-0.0087			0.1516	0.5923	
	15.37	-0.00		1.6381	0.0003	0.0414	0.0026			0.2053	1.4356	
	_ 1 <u>5.37</u>	-0.00		1.6291	0.0055	0.0190	0.0012			0.2164	1.4277	
	5.10 0.01	0.0		0.1346	-0.0023 -0.0030	0.0097	0.0035			0.2297	2.9282	
	<u> </u>			001340	-0000			0.032	0 001,721		-011511	
				<del></del>	·							
					_ ,							
						<del></del>			<del></del>			·
						<del></del>			<del></del>			

3.06 -0.00 0.1569 0.4517 0.0007 0.0117 0.0008 0.4159 0.1539 0.2621 2.8792 4.12 0.00 0.2072 0.5758 -0.0054 0.0032 -0.0001 0.4210 0.1562 0.2648 2.7799  5.12 -0.00 0.2630 0.6926 0.0018 0.0155 -0.0006 0.4303 0.1662 0.2701 2.6331 6.11 -0.00 0.3203 0.8061 -0.0078 0.0219 -0.0014 0.497 0.1750 0.2745 2.5166  9.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805  10.23 -0.01 0.6393 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702  12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519  15.40 -0.01 1.2699 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862  18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2247 1.1259  21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598  24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882  28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 8.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1933 1.4208  5.12 -0.00 0.2564 0.7293 0.0028 0.0162 -0.0047 0.4342 0.2407 0.1934 2.8443	7 i	OF 1	RING DE	VELOPHENT	CENTERIA	EDC)			NNEL FACILI'		AER	DOYNAMIC WIND TUNNEL (4T)
-2.03		TEST										
-0.9V	NT	ALPHA -	BETA-	CN	CLM		CLN	CLL	CA	CAB	CAF	ACP
-0.00 0.00 0.008+ 0.0787 -0.0018 -0.0095 0.0027 0.4093 0.1473 0.2619 9.4093  1.04 0.00 0.0572 0.2071 0.0015 -0.0044 0.0021 0.4114 0.1541 0.2572 3.6105  2.07 0.00 0.1059 0.3299 -0.0063 0.0057 0.0014 0.4123 0.1541 0.2582 3.1142  3.08 -0.00 0.1569 0.4517 0.0007 0.0117 0.0008 0.4159 0.1539 0.2621 2.8792  4.12 0.00 0.2072 0.5758 -0.0054 0.0032 -0.0001 0.4210 0.1562 0.2648 2.7799  5.12 -0.00 0.2630 0.6926 0.0018 0.0155 -0.0006 0.4303 0.1602 0.2701 2.6331  6.11 -0.00 0.3203 0.8061 -0.0078 0.0719 -0.0014 0.4933 0.1608 0.2745 2.5166  7.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805  10.23 -0.01 0.6393 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702  12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519  15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862  18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259  21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.018 0.4698 0.2561 0.2137 0.7602  28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567  15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1934 2.8443												
1.04 0.00 0.0572 0.2071 0.0015 -0.0044 0.0021 0.4114 0.1541 0.2572 3.6185 2.07 0.00 0.1059 0.3299 -0.0063 0.0057 0.0014 0.4123 0.1541 0.2582 3.1142 3.06 -0.00 0.1569 0.4517 0.0007 0.0117 0.0008 0.4159 0.1539 0.2621 2.6792 4.12 0.00 0.2072 0.5758 -0.0054 0.0032 -0.0001 0.4210 0.1562 0.2648 2.7799 5.12 -0.00 0.2630 0.6926 0.0018 0.0155 -0.0006 0.4303 0.1602 0.2701 2.6331 6.11 -0.00 0.3203 0.8061 -0.0078 0.0219 -0.0014 0.4393 0.1648 0.2745 2.5166  7.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.497 0.1750 0.2746 2.1805 10.23 -0.01 0.6393 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.6702 12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519 15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862 17.5 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0118 0.4698 0.2251 0.2317 0.9598 24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882 27.15 -0.01 5.2780 2.4122 0.0266 0.0375 -0.0145 0.4708 0.2708 0.1934 2.8443												
2.07	!		****				-					
3.06 -0.00 0.1569 0.4517 0.0007 0.0117 0.0008 0.4159 0.1539 0.2621 2.8792 4.12 0.00 0.2072 0.5758 -0.0054 0.0032 -0.0001 0.4210 0.1562 0.2648 2.7799  5.12 -0.00 0.2630 0.4726 0.0018 0.0155 -0.0006 0.4303 0.1602 0.2701 2.6331 6.11 -0.00 0.3203 0.8061 -0.0078 0.0219 -0.0014 0.4393 0.1602 0.2705 2.5166  4.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805  10.23 -0.01 0.6343 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702  12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519  15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862  18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259  21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598  24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882  28.15 -0.01 4.2907 2.7026 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4670 0.2768 0.1933 1.4208  5.12 -0.00 0.2564 0.7293 0.0028 0.0162 -0.0047 0.4342 0.2407 0.1934 2.8443	) E											
4.12	5											
5.12 -0.00 0.2630 0.0426 0.0018 0.0155 -0.0006 0.4303 0.1602 0.2701 2.6331 6.11 -0.00 0.3203 0.8001 -0.0078 0.0219 -0.0014 0.4393 0.1648 0.2745 2.5166 7.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805 10.23 -0.01 0.6343 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702 12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2645 1.6519 15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862 18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259 21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598 24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7842 28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	7											
6.11 -0.00 0.3203 0.8001 -0.0078 0.0719 -0.0014 0.4393 0.1648 0.2745 2.5166  7.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805 10.23 -0.01 0.6393 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702 12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519 15.40 -0.01 1.259 1.7108 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862 18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259 21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598 24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882 28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.00 0.2564 0.7293 0.0028 0.0192 -0.0047 0.4342 0.2407 0.1934 2.8443	6											
7.21 -0.00 0.4655 1.0151 0.0002 0.0192 -0.0015 0.4497 0.1750 0.2746 2.1805 10.23 -0.01 0.6393 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0.2715 1.8702 12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519 15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862 18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259 21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598 24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882 28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0142 -0.0047 0.4342 0.2407 0.1934 2.8443	9											
10.23 -0.01 0.6343 1.1957 0.0141 0.0226 -0.0029 0.4571 0.1856 0,2715 1.6702 12.31 -0.01 0.8446 1.3953 0.0152 0.0276 -0.0033 0.4627 0.1961 0.2665 1.6519 15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862 18.54 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259 21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598 24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7862 28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208	<u> </u>											
15.40 -0.01 1.2269 1.7008 -0.0068 0.0748 -0.0060 0.4679 0.2101 0.2578 1.3862  18.50 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259  21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598  24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882  28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567  15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208  5.12 -0.00 0.2564 0.7293 0.0028 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	i		-0.01	0.6393	1.1957		0.0556	-0.0029	0.4571			
18.50 -0.01 1.8005 2.0272 0.0107 0.0453 -0.0088 0.4723 0.2245 0.2479 1.1259 21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598  24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882  28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567  15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208  5.12 -0.00 0.2564 0.7293 0.0028 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	2	12.31	-0.01	0.8446			0.0276	-0.0033	0.4627		0.2665	1.6519
21.76 -0.01 2.5235 2.4220 0.0262 0.0473 -0.0109 0.4739 0.2421 0.2317 0.9598  24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7882  28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.472 6.2656 0.2066 0.6299  31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567  15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208  5.12 -0.00 0.2564 0.7293 0.0028 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	3											
24.97 -0.01 3.3675 2.6543 0.0297 0.0337 -0.0118 0.4698 0.2561 0.2137 0.7862 28.15 -0.01 4.2907 2.7028 0.0211 0.0741 -0.0147 0.4722 8.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0142 -0.0047 0.4342 0.2407 0.1934 2.8443	•											
28.15 -0.01 4.2907 2.7026 0.0211 0.0741 -0.0147 0.4722 0.2656 0.2066 0.6299 31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0142 -0.0047 0.4342 0.2407 0.1934 2.8443	5	21.76	-0.01				_					
31.32 -0.01 5.2780 2.4102 0.0266 0.0375 -0.0146 0.4630 0.2778 0.1853 0.4567 15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0142 -0.0047 0.4342 0.2407 0.1934 2.8443	6		-0.01									
15.42 -0.01 1.2258 1.7416 -0.0077 0.0797 -0.0061 0.4706 0.2768 0.1938 1.4208 5.12 -0.00 0.2564 0.7293 0.0028 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	7 8											
5.12 -0.00 0.2564 0.7293 0.0024 0.0152 -0.0047 0.4342 0.2407 0.1934 2.8443	9							_	_			
	0											
	ì			-								
	<del>-</del>	- 13.3.3										
										·- <u>-</u>		
											<del></del>	
				<del></del>							<del></del>	
										_		
				-								
								**				
						-				-		
				11								

23.47 -0.00 2.1139 2.0181 0.0745 -0.0311 -0.0728 0.0463 0.2235 -0.1773 0.9547 0.606  23.46 -0.00 1.8167 1.7783 -0.0453 0.1566 -0.0556 0.0707 0.3966 -0.3259 0.9789 0.805  23.48 -0.00 1.8134 1.7742 -0.0194 0.1187 -0.0556 0.0705 0.2964 -0.2259 0.9784 0.808  23.51 -0.00 1.5957 1.4044 -0.0616 0.2557 -0.0186 0.1492 0.2955 -0.1463 0.8801 1.228  23.51 -0.00 1.5744 1.4021 -0.0400 0.2530 -0.0132 0.1479 0.2693 -0.1214 0.8906 1.237  23.56 -0.00 1.6518 1.5020 -0.0361 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634  23.56 -0.00 1.6518 1.5020 -0.0410 0.1580 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637  23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1664 0.2257 -0.0593 0.9577 2.387		OF 1		VELOPHENT			MARTIN M	WIND TUNI	EFFECTS	DATA		~	IND TUNNEL (AT)
ALPHA BETA CN CLM CY CLN CLL CA CAB CAF XCP RX10-6 23.59 -0.00 7.0223 2.045 0.0727 -0.0185 -0.0812 0.1358 0.2672 -0.1314 1.0110 0.631 22.5m -0.00 1.9150 1.8588 0.0781 -0.0533 -0.0803 0.0792 0.1899 -0.1108 0.9700 0.612 23.47 -0.00 2.1139 2.0181 0.0745 -0.0311 -0.0728 0.0463 0.2235 -0.1773 0.9547 0.606 23.46 -0.00 1.8167 1.7783 -0.0453 0.1566 -0.0556 0.0707 0.3966 -0.3259 0.9789 0.805 23.48 -0.00 1.8134 1.7742 -0.0194 0.1187 -0.0556 0.0705 0.2644 -0.2259 0.9784 0.808 23.51 -0.00 1.5957 1.4044 -0.0616 0.2557 -0.0186 0.1492 0.2955 -0.1463 0.8801 1.228 23.51 -0.00 1.5954 1.4021 -0.0400 0.2530 -0.0132 0.1479 0.2693 -0.1214 0.8906 1.237 23.56 -0.00 1.6518 1.5020 -0.0410 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634 23.56 -0.00 1.6518 1.5020 -0.0410 0.1580 0.0119 0.1488 0.2204 -0.0716 0.9093 1.037 23.49 -0.00 1.6518 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9999 1.633 23.59 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.307 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.59 -0.00 1.7790 1.7651 0.0047 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.48 -0.00 1.7790 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2260 -0.0407 0.9689 4.544													
23.59 -0.00	. –		T.A.D. 1107						Desilient Ross				
22.58 -0.00 1.9150 1.8588 0.0781 -0.0533 -0.0803 0.0792 0.1899 -0.1108 0.9706 0.612 23.47 -0.00 2.1139 2.01d1 0.0745 -0.0311 -0.0728 0.0463 0.2235 -0.1773 0.9547 0.606 23.46 -0.00 1.8167 1.7783 -0.0453 0.1566 -0.0556 0.0707 0.3966 -0.3259 0.9789 0.885 23.48 -0.00 1.8134 1.7742 -0.0194 0.1187 -0.0556 0.0705 0.2964 -0.2259 0.9784 0.808 23.51 -0.00 1.5957 1.4044 -0.0616 0.2557 -0.0186 0.1492 0.2955 -0.1463 0.8801 1.228 23.51 -0.00 1.5744 1.4021 -0.0400 0.2530 -0.0132 0.1479 0.2693 -0.1214 0.8906 1.237 23.56 -0.00 1.6518 1.5226 -0.0361 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634 23.49 -0.00 1.6518 1.5020 -0.0410 0.1500 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637 23.49 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7799 1.6612 -0.0463 0.1552 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7762 1.6559 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0161 0.1873 0.2286 -0.0407 0.9689 4.544					_								
23.47 -0.00		27.50											
23.68 -0.00		23.47		2.1139						0.2235		0.9547	0.606
23.51 -0.00 1.5957 1.4044 -0.0616 0.2557 -0.0186 0.1492 0.2955 -0.1463 0.8801 1.228 23.51 -0.00 1.5744 1.4021 -0.0000 0.2530 -0.0132 0.1479 0.2693 -0.1214 0.8906 1.237 23.56 -0.00 1.5431 1.5226 -0.0361 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634 23.56 -0.00 1.6518 1.5020 -0.0410 0.1580 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637 23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9090 1.633 23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.307 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.54 -0.00 1.7531 1.6854 0.0847 -0.1721 0.0168 0.1803 0.2295 -0.0493 0.9613 3.206 23.58 -0.00 1.7704 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2286 -0.0373 0.9613 3.206 23.48 -0.00 1.7709 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544	-	23.46											
23.51 -0.00 1.5744 1.4021 -0.000 0.2530 -0.0132 0.1479 0.2693 -0.1214 0.8906 1.237 23.56 -0.00 1.6431 1.5226 -0.0361 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634 23.56 -0.00 1.6518 1.5020 -0.0410 0.1500 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637 23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9090 1.633 23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0102 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.54 0.00 1.7531 1.6854 0.0047 -0.1721 0.0168 0.1803 0.2295 -0.0493 0.9614 3.206 23.58 -0.00 1.7704 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9614 3.206 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544													
23.56 -0.00 1.6431 1.5226 -0.0361 0.1512 0.0119 0.1517 0.2223 -0.0706 0.9267 1.634 23.56 -0.00 1.6518 1.5020 -0.0410 0.1580 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637 23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9090 1.633 23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.48 0.00 1.7531 1.6854 0.0847 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.54 -0.00 1.7794 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9687 4.544													
23.56 -0.00 1.6518 1.5020 -0.0410 0.1500 0.0119 0.1488 0.2204 -0.0716 0.9093 1.637 23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9090 1.633 23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.48 0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9614 3.206 23.48 -0.00 1.7704 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9689 4.544													
23.49 -0.00 1.6512 1.5009 -0.0206 0.1015 0.0115 0.1451 0.2204 -0.0753 0.9090 1.633 23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.48 0.00 1.7531 1.6854 0.0847 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.54 -0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9637 4.543 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544		23.56		_									
23.58 -0.00 1.7287 1.6555 -0.0515 0.1325 0.0178 0.1664 0.2257 -0.0593 0.9577 2.387 23.49 -0.00 1.7199 1.6612 -0.0463 0.1552 0.0182 0.1693 0.2208 -0.0515 0.9659 2.385 23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.189 23.48 0.00 1.7531 1.6854 0.0847 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.54 -0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9617 4.543 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544										-			
23.59 -0.00 1.7662 1.6959 0.1060 -0.1920 0.0130 0.1779 0.2278 -0.0500 0.9602 3.169 23.48 0.00 1.7531 1.6854 0.0847 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.54 -0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9637 4.543 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544		23.58	-0.00	1.7287	1.6555	-0.0515		0.0178		0.2257	-0.0593	0.9577	2.307
23.48 0.00 1.7531 1.6854 0.0847 -0.1721 0.0148 0.1803 0.2295 -0.0493 0.9614 3.206 23.54 -0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9637 4.543 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544		23.49											
23.54 -0.00 1.7904 1.7253 0.0615 -0.0930 0.0153 0.1873 0.2246 -0.0373 0.9637 4.543 23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544													
23.48 -0.00 1.7739 1.7188 0.0576 -0.0780 0.0141 0.1874 0.2280 -0.0407 0.9689 4.544													
	-												
			MAG.				3,000						
								· · · · · · · · · · · · · · · · · · ·	<del></del>			<del></del>	
	_		_				-						
	_											-	
	_							<del> </del>					
	•								•				
					·····						······································	-	
	_			<del></del>									
							_				-		
													<del></del>

6E	1 OF 1 1 OF 1	- ING DEVI	EFORMENT (		<u> </u>	MARTIN MI	SSILE TA	IL EFFECTS	DATA	AERC	DYNAMIĆ MINO TUNME	LIATI
				<del></del>					<del></del>			
<del></del>	:TEST	207 1.3	CH RX10-6 VARY	0.0 B	CONF.	L . DEL1	OFF	OFF OFF	TRANSITI	ON		
NT 1	ALP4A 9.20	BETA -0.00	CN 0.5245	CLM 1-1011	C7 0.0141	CLM 0.0190	CLL 0.0133	CA 0.4641	CAB 0.2025	CAF 0.2616	ICP RX10-6 2.0991 2.305	
2	9.00	-0.00	0.5046	1.0931	-0.0016	0.0182	0.0147	0.4639	0.2150	0.7489	2.1662 2.300	
<del></del>	8.97	-0.00	0.5162	1-1032	-0.0012	0.0784	0.0131	0.4700	0.2339 0.2273	0.2371	2.1509 3.111 2.1718 3.093	
<u>5</u>		-0.01 -0.00	0.5256		_0.0007	0-0373 _	0.0075		0.2373 0.2383	0.2339_	2.1946 5.807	
7		-0.01	0.5072		-0.0029	0.0310	0.0076	0.4707	0.2359	0.2323	2.2454 5.808 2.2428 5.796	
					-						·	
						<del></del>	•-			<del></del>	· · · · · · · · · · · · · · · · · · ·	<del></del>
_						<del></del>						
<del></del>			-			<del></del>			:			
										•		
		<del></del>	<del></del>								<del></del>	
		·				<del></del>			···			
			-						<del></del> -			
								<del></del>				

----

GE	1 OF 1 1 OF 1		ELOPHENT	CENTERSAE	DC)P	ROPULSION MARTIN HI	SSILE T	NEL FACILI AIL ÉFFECTS	TY (PUT) DATA	AER	DOANWHIC MIND	TUNNEL (4T)
		PART MA	ACH RX10-6	_ PHI 0.0 84	CONF	L DEL1	DELS		TRANSIT			
POINT	1 ALPHA 30.27	BETA -0.00	CN 2.7714	CLM 2.2172	CY 0.3440	CLN -0.6699	CLL 0.0071	CA -0.0290		CAF -0.2764	ACP 0.8000	
3	29.95	-0.00	2.7112 2.7005	2.2030 2.1997	0.3009	-0.5605 -0.5970	0.0051 _0.0072	-0.0233 0.0274	0.2426	-0.2659 -0.2848	0.8126	
	<del></del>	<del></del>	••				<del></del>					
<u> </u>												
· · ·						<del></del>				<u>.                                      </u>		
					<del></del>						<del></del>	
		<del></del>					<del></del> -					
			· · · · · ·				<del></del>					
		<del></del>			<del></del>					<del></del>		

	D ENGINEERING DEVELOPMENT CENTER (AEDC) PROPULSION WIND TUNNEL FACILITY (PWT) AERODYNAMIC WIND TUNNEL  1 OF 1 MARTIN MISSILE TAIL EFFECTS DATA  1 OF 3											
	TEST PART MACH RX10-6 PMI CONF L DELI DELI DELI DELI DELI TRANSITION 1 213 1.00 3.9 0.0 BANDEO 0.0 UFF DFF DFF UNKNOWN											
POINT	ALPHA	BETA	ČN 3.9724	CLM 3.961h	CY 0.0564	CLN 0.0444	CLL 0.0013	CA 0.0011	CAB	CAF -0.2063	XCP 1.0024	
3	30.11	-0.02	4.0463 4.0402 4.0392	3.8652 3.8555 3.8837	0.0953	-0.0147 -0.0162 -0.0107	0.0047	0.255 0.256 0.2157	0.2967 0.3062	-0.0712 -0.0804	0.9548	
	<del></del>	<del></del>	<del></del>			·					•	
			<del></del>	<del></del>								
	•			•		<del></del>			•		· · ·	
·												
	<del></del>											

NGE HEET	1 OF 1 1 OF 1	MING DEA	ELOPMENT					NEL FACILI			 	ind innner(41)
	_ TEST	PART MA 215 1.1	CH RX10-6	PHI 0.0	CONF	L _ DEL1	DEL2 OFF	DEL3 DEL4	THANSIT	710M		
POINT	ALPHA		ČN .	CLM		" CLN		CA .		CAF	XCP	
2 3	29.03	0.00	3.9442	3.3434	-0.0574 -0.0485	0.1353	0.0138	0.2292 0.2260 0.2273	0.3176	-0.1014 -0.0918 -0.0962	0.8471 0.8477 0.8401	
4 5	30.06		4.1667	3.4975	-0.0164 -0.0409	-0.0110	0.0115	0.2172 0.2209		-0.0902 -0.1056	0.8394	
											-1	
	<del></del>	<del>-</del>	· <u>·</u>		<del> </del>	· <del></del>	<del> </del>					·····
					~~ ~~~~~							
						<del></del>		<del></del>				
						-						<b>46</b> —
						<del></del>		·			· • • • • • • • • • • • • • • • • • • •	·

AGE	of 1		YETOBHEH!	CENTER (AI	<u> </u>	ROPULSION MARTIN MI	SSILE T	NMEL FACILI AIL EFFECTS	DATA	AER	DOYNAMIC WIND TUNNEL
-,	TEST	PART MA	ACH RX10-6				DELS	DEL3 DEL4 OFF OFF	TRANSIT UNKNO	ION	
POINT 2 3	29.68 30.01 30.01	-0.00	CN 2.7667 2.8437 2.8523	9-5196	0.1467	CL4 -0.2196 -0.0170 0.0118	0.0178	-0-1174 -0-1163 -0-1150	0.2676	CAF -0.4018 -0.3838 -0.3730	NCP 0,8239 0.8048 0.8052
		<del></del>			·····					,	
		<u>.                                    </u>									
							·	· ·			
						· .		•			·
			- -		•						
	<del></del>										
		<del></del>									· · · · · · · · · · · · · · · · · · ·

3E	ENGINEE 1 OF 1 1 OF 1	P <u>I</u> mg DEV	LLOPMENT	CENTER (A		PROPULSION Martin Mi	WIND TU	NNEL FACILI All EFFECTS	TY(PUT)_ DATA	AERO	DÖÄNYÜLE ÄÏÜÖ LAMMEF(ŸI
	TEST	PADT MA 219 0.4	CH RX10-6	PH1 0.0 H	CONF 440F0	L DEL)	DEL2 OFF	DEL3 DEL4	TRANSIT UNKNOW	ION	
I I 2	ALPHA 29.95 29.95	8ETA 0.00 0.00	2.4230 CN	1.9066 1.6980	0.3185 0.3170	CLN -0.7330 -0.7669	0.0153 0.0116	CA -0.2772 -0.2833	CA8 0.2436 0.2058	CAF -0.5208 -0.4891	XCP 0.7906 0.7833
				- <del></del>							
						4			•		
			•								-
							<del></del>				
											<u> </u>

6É 🗀	ENGINEERING DEVELOPMENT CENTER (AEDC) PROPULSION WIND TUNNEL FACILITY (PWT) AERODYNAMIC WIND TUNN TOF 1 MARTIN MISSILE TAIL EFFECTS DATA												WHIEL (4T)	
EET	l of	<u>.                                    </u>	<del></del>			<del></del>			•					
	TES 1		ACH RX10-6	PHI 0.0	CONF _	0.0	OFF	DELS	DEL3 OFF	DEL4 OFF	TRANSIT	ION		
01NT 1 2	ALPHA 29.93	0.00	2.2269 2.3717	CLM 1.7614 1.8677	0.5730 0.4655	CL -1.3	41B	0.0340	-0.6 -0.7	A 555 064	CAR 0.2958 0.2731	CAF -0.9514 -0.9795	ACP 0.7910 0.7875	
											. <b></b>			
					_				-					<del></del>
								•	~	<del></del>	-			
<u></u>				<u> </u>		·								
			-											-
***			v-											
	<u> </u>				<u> </u>						<del></del>	<del></del>		
				<del></del>			<del></del>			-				
													<del></del>	
		<u>-</u>											<del>-</del>	
~											· <del>-</del>			

223 0.40 3.8		TEST	PART MAC	H RX10-6	PHI	CONF	L _OEL1	OEL2	DEL3 DEL4	TRANSIT	ION		
1 0.00 0.00 0.0128 0.0368 -0.0092 0.0047 0.0108 0.2169 0.0984 0.1165 2.8665 2 0.00 0.00 0.0100 0.0357 -0.0076 0.0050 0.0108 0.2160 0.1048 0.1112 3.5536 3 1.02 0.00 0.0521 0.1247 -0.0102 0.0075 0.0103 0.2176 0.0131 0.1364 2.6679 4 1.02 0.00 0.0569 0.1238 -0.00047 0.0078 0.0121 0.2161 0.1091 0.1070 2.1772 5 2.04 0.00 0.0948 0.2243 -0.0099 0.0108 0.0119 0.2198 0.0920 0.1278 2.3658 0.0000 0.0948 0.2243 -0.0099 0.0108 0.0119 0.2198 0.0920 0.1278 2.3658 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000					0.0		.0 OFF	OFF					
1 0.00 0.00 0.0128 0.0368 -0.0092 0.0047 0.0108 0.2169 0.0984 0.1165 2.8665 2 0.00 0.00 0.0100 0.0357 -0.0076 0.0050 0.0108 0.2160 0.1048 0.1112 3.5536 3 1.02 0.00 0.0521 0.1247 -0.00102 0.0075 0.0103 0.2176 0.0131 0.2161 0.1364 2.4679 4 1.02 0.00 0.0569 0.1238 -0.0007 0.0078 0.0121 0.2161 0.1091 0.1070 2.1772 5 2.04 0.00 0.0948 0.2243 -0.0099 0.0108 0.0119 0.2198 0.0920 0.1278 2.3658 0.00920 0.1381 0.3172 -0.0093 0.0139 0.0131 0.2214 0.1051 0.1163 2.2961 7 4.00 0.00 0.1381 0.3172 -0.0093 0.0145 0.0144 0.2246 0.1111 0.1135 2.3525 0.0093 0.01783 0.4195 -0.0102 0.0145 0.0144 0.2246 0.1111 0.1135 2.3525 0.0093 0.0189 0.0158 0.2306 0.1134 0.1172 2.2539 0.0093 0.0189 0.0158 0.2306 0.1134 0.1172 2.2539 0.0093 0.0185 0.0152 0.2357 0.1165 0.1172 2.2341 0.1172 2.2341 0.0153 0.0093 0.0185 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 0.1111 0.1135 0.1172 2.2539 0.0180 0.2468 0.1319 0.1150 2.0562 0.1211 0.1150 0.1172 0.0093 0.0158 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 0.1211 0.1214 0.1510 0.0093 0.0154 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 0.1214 0.1503 0.0093 0.0094 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 0.1510 0.0093 0.0094 0.0222 0.0180 0.2468 0.1319 0.1505 0.1014 1.7634 0.1214 0.1503 0.0094 0.0222 0.0180 0.2468 0.1319 0.1505 0.1014 1.7634 0.1214 0.1503 0.0094 0.0222 0.0180 0.2468 0.1319 0.1505 0.1014 1.7634 0.1214 0.1214 0.000 0.9004 1.2500 0.0094 0.0222 0.0180 0.2488 0.1994 0.0024 1.2475 0.0000 0.9004 1.2500 0.0094 0.0225 0.0171 0.2489 0.1753 0.0736 1.3866 0.0000 0.2418 0.1994 0.0024 1.2475 0.0000 0.2418 0.01994 0.0024 1.2475 0.0000 0.0000 0.2418 0.01994 0.00255 0.0000 0.0000 0.2216 0.2255 0.0000 0.0000 0.2506 0.2559 0.3741 0.01894 0.00000 0.2506 0.2559 0.3741 0.01894 0.00000 0.2561 0.2559 0.3741 0.01894 0.00000 0.2561 0.2559 0.3741 0.01894 0.00000000000000000000000000000000000	DINT	AL PHA	AFTA.	CM	Ci e	-· ev		. Çı ı	CA		CAF	- xcė	<del></del>
2	1										_		
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	5	0.00			0.0357	-0.0078	0.0050	0.0108		0-10-8	0.1112		
5         2.04         0.00         0.0948         0.2243         -0.0099         0.0108         0.0119         0.2198         0.0920         0.178         2.3658           6         3.04         0.00         0.1381         0.3172         -0.0093         0.0139         0.0131         0.2214         0.1051         0.1163         2.2961           7         4.06         0.00         0.1763         0.4195         -0.0107         0.0145         0.0144         0.2246         0.1111         0.1135         7.3525           8         5.07         0.00         0.2279         0.6052         -0.0093         0.0154         0.0158         0.2306         0.1134         0.1172         2.2534           10         8.10         -0.00         0.2709         0.6052         -0.0055         0.0232         0.0180         0.2468         0.1319         0.1150         2.0562           11         10.13         -0.00         0.5129         0.9045         -0.0041         0.0221         0.0187         0.2519         0.1505         0.1014         1.7634           12         12.16         -0.00         0.6587         1.0357         0.0024         0.0156         0.0155         0.2522         0.1672	3	1.02	0.00	0.0521	0-1767	-0.0102	0.0075	0.0103	0.2176	0.6812	0.1364	2.4679	
6 3.04 0.00 0.1381 0.3172 -0.0093 0.0139 0.0131 0.7214 0.1051 0.1163 2.2961 7 4.00 0.00 0.1783 0.4195 -0.0102 0.0145 0.0144 0.2246 0.1111 0.1135 2.3525 8 5.07 0.00 0.2223 0.5147 -0.0093 0.0154 0.0158 0.2306 0.1134 0.1172 2.2339 9 6.06 0.00 0.2709 0.6052 -0.0093 0.0185 0.0152 0.2357 0.1185 0.1172 2.2341 10 8.10 -0.00 0.3778 0.7765 -0.0055 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 11 10.13 -0.00 0.5129 0.9045 -0.0041 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 12 12.16 -0.00 0.6567 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0850 1.5723 13 15.21 -0.00 0.9044 1.2568 0.0794 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866 14 18.26 -0.00 1.1627 1.4754 0.0016 -0.1356 0.0160 0.2418 0.1994 0.0024 1.2475 15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0048 1.0773 16 24.38 0.01 1.9301 1.6588 0.6980 -1.5148 0.0194 0.2018 0.2477 -0.0400 0.6594 17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.7674 -0.0755 0.5278 18 30.52 -0.10 3.1346 0.0968 2.1726 -2.7427 0.0156 0.2259 0.3741 -0.1882 0.2661 19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2263 0.173 0.1110 2.4878 20 5.07 0.00 0.2138 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4878	•	1.02	0.00	0.0569			0.0078	0.0121	0.2161	0.1091	0.1070		
7 4.06 0.00 0.1763 0.4195 -0.0107 0.0145 0.0144 0.2246 0.1111 0.1135 7.3525  8 5.07 0.00 0.2283 0.5147 -0.0099 0.0154 0.0158 0.2306 0.1134 0.1172 2.2539  9 6.06 0.00 0.2709 0.6052 -0.0093 0.0185 0.0152 0.2357 0.1185 0.1172 2.2341  10 8.10 -0.00 0.3778 0.7765 -0.0055 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562  11 10.13 -0.00 0.5129 0.9045 -0.0041 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634  12 12.16 -0.00 0.6587 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0850 1.5723  13 15.21 -0.00 0.9044 1.2568 0.0294 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866  14 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475  15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0049 1.0775  16 24.38 0.01 1.9301 1.6586 0.6980 -1.5148 0.0194 0.2216 0.2255 -0.0040 1.0775  17 27.44 -0.00 2.4940 1.3143 1.55073 -3.0519 0.0207 0.1919 0.2674 -0.0755 0.5276  18 30.52 -0.10 3.1346 0.8960 2.1726 -2.7427 0.0156 0.2259 0.3741 -0.1482 0.2861  19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2283 0.173 0.1110 2.4878	5								· · · · · · · · · · · · · · · · · · ·	T			
8 5.07 0.00 0.2283 0.5147 -0.0073 0.0154 0.0158 0.2306 0.1134 0.1172 2.2339 9 6.06 0.00 0.2709 0.6052 -0.0093 0.0185 0.0152 0.2357 0.1185 0.1172 2.2341 10 8.10 -0.00 0.3778 0.7765 -0.0055 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 11 10.13 -0.00 0.5129 0.9065 -0.0041 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 12 12.16 -0.00 0.6587 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0851 1.5723 13 15.21 -0.00 0.9064 1.2568 0.0294 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866 14 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475 15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0040 1.0775 16 24.38 0.01 1.9301 1.6586 0.6980 -1.5148 0.0194 0.2078 0.2477 -0.0400 0.8594 17 27.44 -0.00 2.4940 1.3143 1.55073 -3.0519 0.0207 0.1919 0.7674 -0.0755 0.5276 18 30.52 -0.10 3.1346 0.0960 2.1724 -2.7427 0.0156 0.2255 0.1949 0.0556 1.4238 20 5.07 0.00 0.2138 0.5320 -0.0111 0.0126 0.0174 0.2283 0.173 0.1110 2.4878	6	-											
9 6.06 0.00 0.2709 0.6052 -0.0093 0.0185 0.0152 0.2357 0.1185 0.1172 2.2341 10 8.10 -0.00 0.3778 0.7765 -0.0055 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 11 10.13 -0.00 0.5129 0.9045 -0.0041 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 12 12.16 -0.00 0.6587 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0850 1.5723 13 15.21 -0.00 0.9044 1.2568 0.0294 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866 14 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475 15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0040 1.0778 16 24.38 0.01 1.9301 1.6586 0.6980 -1.5148 0.0194 0.2078 0.2477 -0.0400 0.8594 17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.2674 -0.0755 0.5278 18 30.52 -0.10 3.1346 0.0960 2.1724 -2.7427 0.0156 0.2259 0.3741 -0.1482 0.2861 19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2283 0.173 0.1110 2.4878	7												
10 8.10 -0.00 0.3778 0.7765 -0.0055 0.0232 0.0180 0.2468 0.1319 0.1150 2.0562 11 10.13 -0.00 0.5129 0.0045 -0.0041 0.0221 0.0187 0.2519 0.1505 0.1014 1.7634 12 12.16 -0.00 0.6587 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0850 1.5723 13 15.21 -0.00 0.9064 1.2568 0.0294 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866 14 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475 15 21.32 0.00 1.5108 1.6277 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0048 1.0778 16 24.38 0.01 1.9301 1.6588 0.6980 -1.5148 0.0194 0.2078 0.2477 -0.0400 0.6594 17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.2674 -0.0755 0.5278 18 30.52 -0.10 3.1346 0.0968 2.1726 -2.7427 0.0156 0.2259 0.3741 -0.1482 0.2861 19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2505 0.1949 0.0556 1.4238 20 5.07 0.00 0.2138 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4878	5	110											•
11													
12 12.16 -0.00 0.6587 1.0357 0.0028 0.0156 0.0155 0.2522 0.1672 0.0850 1.5723 13 15.21 -0.00 0.9064 1.2568 0.0294 -0.0265 0.0171 0.2489 0.1753 0.0736 1.3866 14 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475 15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.6040 1.0775 16 24.38 0.01 1.9301 1.658h 0.6980 -1.5148 0.0194 0.2778 0.2477 -0.0400 0.8594 17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.2674 -0.0755 0.5278 18 30.52 -0.10 3.1346 0.8960 2.1726 -2.7427 0.0156 0.2259 0.3741 -0.1482 0.2861 19 15.21 -0.00 0.8990 1.2800 0.0264 -0.0336 0.0206 0.2505 0.1949 0.0556 1.4238 20 5.07 0.00 0.2138 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4878	-												
13													
18 18.26 -0.00 1.1827 1.4754 0.0816 -0.1356 0.0160 0.2418 0.1994 0.0424 1.2475 15 21.32 0.00 1.5108 1.6279 0.2565 -0.5374 0.0184 0.2216 0.2255 -0.0040 1.0775 16 24.38 0.01 1.9301 1.6586 0.6980 -1.5148 0.0194 0.2078 0.2477 -0.0400 0.8594 17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.2674 -0.0756 0.5276 18 30.52 -0.10 3.1346 0.0960 2.1726 -2.7427 0.0156 0.2259 0.3741 -0.1462 0.2861 19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2505 0.1949 0.0556 1.4238 20 5.07 0.00 0.2138 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4878	_						-						
15													
16							-						
17 27.44 -0.00 2.4940 1.3143 1.5023 -3.0519 0.0207 0.1919 0.7674 -0.0755 0.5276 18 30.52 -0.10 3.1346 0.0960 2.1724 -2.7427 0.0156 0.2259 0.3741 -0.1482 0.2861 19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2505 0.1949 0.0556 1.4236 20 5.07 0.00 0.2136 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4876													
19 15.21 -0.00 0.4990 1.2800 0.0264 -0.0336 0.0206 0.2505 0.1949 0.0556 1.4238 20 5.07 0.00 0.2136 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4876			-0.00				-3.0519				-0.0755	0.5270	
20 5.07 0.00 0.2130 0.5320 -0.0111 0.0126 0.0174 0.2283 0.1173 0.1110 2.4876	18	30.52	-0.10	3.1346	0.8968	2.1726	-2.7427	0.0156	0.2259	0.3741	-0.1462	0.2861	
			-0.00	0.4990	1.2800	0.0264	-0.0336	0.0206	0.2505	0.1949	0.0556	1,4230	
21 0.00 0.00 0.0047 0.0488 -0.0107 0.0022 0.0166 0.2167 0.0935 0.1232 10.4861		-											
	21	0.00	0.00 .	0.0047	0.0488	<u>-0</u> .0107	2500-0	0.0166	0.2167	0.0935	0.1535	10.4261	
									<del></del>				
											•		
												<del></del>	
				-		•							
				-									
							_						
													~·
									· · · · · · · · · · · · · · · · · · ·	<del></del>			

## APPENDIX B TEST 2

					1_	_						-
	_ <u></u>					الماند		UFF OFF				
INT	ALPHA	#FT.	CN -(.)712	CLW	CY =5.2473	CLN	CLL	CA	C49 0-6241	CAF .	1CP	
<del>-</del> -	=(1.ht	L.J	-0.0.0.3		-0.0346	1.19.4	-1.0015	0.5001	G-6706		-3.0451	
ــــــــــــــــــــــــــــــــــــــ	C.3r_	<u> </u>	الملفضية	_6.c762			-0+001-			0.41.54	-8-8063 .	
•	1.33		+n + 3 ; + 4		-6.230 •		-0.0027	6.5237	0.1126		-43.1114	
<b></b>	3.36						-0.0057	-4-5303 U->230	. 4.1075 . v.1141	_255 <b>4-</b> 0		<del></del>
7	3.30				2006306		-0.01uc	4.5235	2 1235	0.3910	A_8751	
	5.31		7.1-31		-5.6/74		-3.00-1	0.5143	6.1432	0.3761	4.0461	
٠.	06.30		6-6635		_=2263		ـ مدعده .		- 0-1417 -		3-5369	<del></del>
:	7.41	0.6	0.4017			J-2746	0.0011	U-4465	0.1543	0.3421	3.0527	
5	4.30	0.0	11.35		-u.2264-		5-00.c			45EE.u 791E.n	3.0d64 2.9140	
•	17.34	- (	0-1-6-2		23at		5.0042		i 1818	3120	1.9560	16
•	11.30	1.4	C-+c1-	100200	-5-2471		-J.0027	U-4479	0.1753	0.3276	1.6485	
5	12.34		<del></del>		_=4-4110_			6.5002			- 1-4424	· · · · · · · · · · · · · · · · · · ·
	13.37	5.6	0/73		-u.216- <u>-u.221</u>	(-1/-0	0.0034 	0.4440	v.ld51	1.3095	1.1436	
7		<u> </u>	1.147		-0.2137	Lalays	6000.0	2.4813 _ 5.4822	0.1921 0.1921	0.2901	0.9 <u>794</u> 0.7837	
<u> </u>	16.34	المنا	1.37.				-0-0372	- Enda-v	1044	2-2449	9.4052	
٠,٠	17.44	9-4	111		-1.02.00	C.1744	-5-0004	J 7-H	5165.U	0.2676	0.4861	
21	_13.82_				_ <u>=io2214</u>					0.2469.		
<u> </u>	14.43	0.0	1.7523		-0-1024	0.1633	0.0025	·····	0.2111	0.2324	0.50 35	
						· · · · · · · · · · · · · · · · · · ·			- <del></del> -			
					•	· · · · · · · · · · · · · · · · · · ·						

1.33 to 0.657, 0.736n =0.1341 0.0774 =0.0065 0.4374 0.1098 0.3276 4.5950  2.38		5		5v 0.4			.0 UF		DEL3 _ DELA OFF OFF			
-7.67	~1											
1.33   1.0	_											
2-36	<u> </u>											
3.32	•											
### ### ##############################												
6.34 6.4 5.31.33 4.6735 = 4.1674 0.3555 74.6154 0.4384 0.1623 0.2661 2.2203  7.40 6.4 6.3776 0.7444 -0.1167 6.4737 -7.0067 3.4198 0.1495 0.2713 2.0371  M.AU 6.4 6.474 6.4745 -1.1175 0.6534 -4.0124 0.4222 0.1633 0.2569 2.0944  9.36 6.4 6.474 6.4745 -1.1175 0.4225 0.1633 0.2569 2.0944  9.36 6.4 6.474 6.4745 -1.1175 0.4225 0.1633 0.2569 2.0944  1.44 6.4 6.4 6.4 6.4 6.4 6.4 6.4 6.4 6.4										0		<del>-</del>
7.80	4			1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	*** 7137	-1 -1743	0-1.512	-0.0151	U-+359	6-1-18	0.2941	1.7707
######################################	_		The second second second second									
9-36		100 Sept. 2017-2019										
11.46	-							이 아이를 하는 것이 모든 것이 없다면 하지 않는 것이다.	보다 보이 없다고 있다면 하는데 맛있다.			
12.44   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40   1.40	•		0		1-1300	1-06	ححسا		-115441	r-1785		
1.46   1.0   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476   1.476	•											
14-62 C-4 0-5 1-34-4	<u>.</u> .	V. 2										
15-64 0.5 1.7414 7.4551025 4.05.4 -0.0169 0.4003 0.7044 0.1909 0.4007  15-61 1.2244 151.455 0.4651 0.4004 0.4131 0.1874 0.7665  17.67 (.0 1.3444 1427 1427 1427 0.4034 0.3977 0.2227 0.1765 0.4624  18-63 0.5 1.6752 1785 14255 14255 14255 0.3402 0.3402 0.2250 0.1665 0.4944	<u> </u>											
17.47 (.u 1.37	e	15.44	0.5			1000	4005.4	-0.0149	0.4003			0.9007
	<u>-</u>											
	" 1											
	2	- 12.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.00 (1.0										

1	PHANEC HEND TUNNEL (AT)				EFFECTS				*ECUPERI.		1 OF 1	Æ
-1.47							 					
2 -0.4c (.) -0.6c; (.) 574 -0.015 -0.674 -0.0132 0.3eev 0.1523 0.1946 -1.3916 3 0.35 0.0 0.0000 0.2155 -0.077 0.0051 -0.01eb 0.3507 0.1157 0.2358 3.5926 5 2.3a 0.0 0.0000 0.2155 -0.0574 0.0051 -0.01eb 0.3507 0.1157 0.2358 3.5926 6 3.35 0.0 0.1000 0.2155 -0.0577 0.0017 -0.01e7 0.3543 0.1292 0.2751 2.2302 7 4.3a (.) 0.2131 0.667 -0.0136 0.0157 0.0017 0.3543 0.1292 0.2751 2.2302 7 4.3a (.) 0.2131 0.667 -0.0136 0.0157 0.0017 0.3543 0.1292 0.2751 2.2302 8 5.3e (.) 0.2724 0.0000 -0.0000 0.3500 0.3563 0.1522 0.2061 2.7750 9 6.3b (.) 0.2724 0.0000 -0.0000 0.3563 0.1522 0.2061 2.7750 10 7.3e 0.0 0.3650 0.7000 -0.0000 -0.0136 0.3635 0.1528 0.2047 2.3702 10 7.3e 0.0 0.3650 0.7000 -0.0000 -0.0136 0.3740 0.1721 0.2023 2.0656 11 5.4b 0.0 0.3650 0.7000 -0.0000 -0.0133 0.3740 0.1721 0.2023 2.0656 12 9.0 0.0 0.0000 0.9713 -0.0501 0.0007 -0.0156 0.3812 0.1925 0.1866 2.0870 13 16.4c 0.0 0.5000 0.9713 -0.0501 0.0007 -0.0156 0.3812 0.1925 0.1865 0.1891 14 11.45 0.0 0.0000 0.0000 0.5713 -0.0501 0.0007 -0.0156 0.3812 0.1925 0.1866 2.0870 15 12.4b 0.0 0.0000 0.0000 0.0000 0.0000 0.3710 0.1711 0.1920 2.0457 16 13.45 0.0 0.0000 0.0000 0.0000 0.0000 0.3710 0.1711 0.1920 2.0457 17 14.4b 0.0 0.00000 0.7710 0.2017 -0.0140 0.3710 0.1711 0.1920 2.0457 18 13.45 0.0 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0										-		POINT
3 0.35 0.0 C.6[m2 0.277 - u.uvee -u.c[1/5 -0.013]												- 2
5 239	7-0291		_0.2376	0-1095	Ja3471	-0.0131	 	3-127-				3
6 3.35 0.0 0.1045 0.4727 0.0017 0.0107 0.3543 0.1292 0.2751 2.2302 7 4.30 (.1.0017 0.0017 0.0017 0.3543 0.1292 0.2751 2.2302 7 4.30 (.1.0017 0.2131 1.4647 0.2133 0.445 0.4418 0.3623 0.1410 0.2713 2.1811 0.27750 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0.2775 0												•
7							 					6
9 6.30 Cab Carry backs = called = calle						_				-		<u> </u>
10 7.30 6.0 0.3050 0.7007 -0.0103 0.3744 0.1721 0.2023 2.0656 11 8.41 6.0 0.3001 0.3021 0.3021 0.0002 -0.0133 0.3746 0.1721 0.2017 2.4417 12 9.40 0.0 0.4000 0.4713 -0.0501 0.0007 -0.0156 0.3012 0.1025 0.1056 2.0070 13 16.40 6.4 0.51.1 1.0433 -0.1377 -0.0157 -0.0156 0.3012 0.1025 0.1056 2.0070 14 11.45 0.0 0.0 0.700 1.3010 -0.0500 -0.6077 -0.0100 0.3714 0.1719 0.1995 1.0195 15 12.40 0.0 0.7000 1.3010 -0.0100 -0.0100 0.3714 0.1719 0.1995 1.0195 16 13.45 0.0 0.4002 1.4000 -0.6131 -0.6137 -0.6140 0.3561 0.1071 0.1001 1.9401 10 13.45 0.0 0.773.0 1.4570.0137 -0.6137 -0.6142 0.3620 0.1723 0.1707 2.0571 17 14.40 0.0 0.773.0 1.4570.6131 -0.6129 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.773.0 1.4570.6131 -0.6129 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.773.0 1.4570.6131 -0.6129 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.773.0 1.4570.6131 -0.6130 -0.6130 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.773.0 1.4570.6131 -0.6130 -0.6130 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.0 0.773.0 0.4000 -0.6130 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.3560 0.3560 0.3560 0.2018 0.1542 1.9934 10 15.40 0.0 0.3560 0.3560 0.3560 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.3560 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.2018 0.20												٠
11				AN TOTAL STREET	10 mm - 10 mm - 10 mm					911		
12									1 200	2000	0.45.5	12 (42 (42 (42 (42 (42 (42 (42 (42 (42 (4
13 10-ac 6-b C-51-d 1-0433 m(-1377 m-6157 m(-152 0-3700 0-1771 0-1629 2-0457 14 11-a5 0.0 0.000 0.000 1-0514 -0-0500 -0-6007 -0-0104 0-3714 0-1719 0-1995 1-8195 15 12-a5 0.0 6-000 1-6000 -0-6101 -0-6137 -0-6142 0-3561 0-1871 0-1601 1-9401 10 13-a5 6-0 0-6073 1-035 -1-6013 -1-6137 -0-6142 0-3560 0-2018 0-1542 1-934 17 14-a6 0.0 0-73-x 1-a57, m6-37a m-6128 w0-01-6 0-3560 0-2018 0-1542 1-934 18 15-ac 0.0 0-0111 1-0-95 -0-6304 -1-0137 -0-6173 0-3574 0-1048 0-1630 1-8486 19 16-a5 0.0 0-31-x 1-a73 -1-63-x -1-0137 -0-6173 0-3544 0-1401 0-20-8 1-6027 20 17-a9 0.0 1-077 1-3634 -1-0327 1-0070 -0-6148 0-3503 0-1966 0-1537 1-2770 21 18-55 0.0 1-22-x 1-1514 -1-0257 1-0011 -0-0200 0-3512 0-1963 0-1569 1-1021												
15 12.05 0.0 0.00005 1.0000 00.013 0.0149 0.0149 0.3561 0.1671 0.1601 1.9461 10 13.05 0.0 0.0007 1.0135 0.0137 0.0142 0.3620 0.1823 0.1747 2.0571 17 14.06 0.0 0.73.0 1.057. 00.012 0.124 0.3560 0.2018 0.1562 1.9936 18 15.00 0.0 0.7111 1.0495 0.0000 0.157 0.1408 0.1630 1.8488 19 15.00 0.0 0.7112 1.0495 0.0000 0.0000 0.3500 0.1400 0.1630 1.8488 20 17.00 0.0 1.0007 1.3634 0.00070 0.0000 0.3533 0.1966 0.1537 1.2770 21 18.55 0.0 1.2226 1.1514 0.00257 0.00011 0.0020 0.3512 0.1963 0.1569 1.1021					5.3700							
10 13.45 0.0 0.4673 1135 -1.0013 -1.0137 -0.0142 0.3620 0.1823 0.1747 2.0571 17 14.46 0.0 0.73.2 1.4570.232 -0.2125 +0.0126 0.3560 0.2018 0.1542 1.9934 18 15.46 0.0 0.4111 1.445 -0.034 -1.0137 -0.0173 0.3574 0.1448 0.1630 1.8488 19 16.45 0.6 0.312 1.4731 -0.034 -1.0153 -0.0144 0.3534 0.1461 0.2048 1.6027 20 17.45 0.0 1.0277 1.3534 -0.4271 0.0776 -0.0148 0.3533 0.1966 0.1537 1.2770 21 18.55 0.0 1.2252 1.1514 -0.0257 0.0011 -0.0236 0.3512 0.1963 0.1569 1.1021										50000000000		
17												
18 15.00 0.0		100000000000000000000000000000000000000			VIII CONTRACTOR CONTRA					772117		
20 17.49 U.U 1.0077 1.3634 -(.01271 (.0076 -0.0148 U.3533 0.1966 0.1537 1.2770 21 18-55 U.U 1.2256 1.514 -3.0257 (.0011 -0.0256 0.3512 0.1963 0.1569 1.1021			0.1430	0-14-8					^111	0.0		10
21 18-55 4.0 1.22-6 1.1514 -1.0257 1.0111 -0.0200 0.3512 0.1903 0.1569 1.1021	Section Configuration Configuration	Contract to the Contract Contr							U10212 C21100 122100	5-27		- 10 W
	\$₩\$\$\#\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$											

7.1=	4 -(43/ 		-0.0173 -0.0173 -0.0179 -0.0179 -0.0196 -0.0104 -0.0101	0.3237	CAR 0-1274 0-1207 0-1221 0-1221 0-1339 0-1339	CAF 0.1874 0.1903 0.1943 0.1973 .0.1880 0.1868	XCP 1-1781 -1-1017 1-0749 1-6901 2-2946	
7.1=			-0.0173 -0.0173 -0.0179 -0.0179 -0.0196 -0.0104 -0.0101	1858.0 4018.0 4018.0 5-3231 5-3231 5-3241	0.1247 -0.1721 -0.1752 -0.1339 -0.1359	0.1903 6.41.0 6.1973 0.881.0	-1.1017 1.0748 1.6901 2.2946	
		-L.DC=1 -G.O(-20 -L.DC24 	-0.0173. -0.0174. -0.0174. -0.0164. -0.0161.	456.0 ±156.0 1656.0	_0.1721 0.1752 0.1339 0.1369	0.1943 0.1973 .0.1880	1.0748 1.6901 2.2946	
6. ves 1.1944 E-1221	# = ( 43/ = = ( 41/ =	-0.0(20 0.0(20 0.0/72 	-0.0174 -0.0144 -0.0164 -0.0174	0.3146 4.526.0 1.636.0 1.636.0	0.1752 0.1339 0.1359	0.1933 .0.1880	1.6901	
	= = = = = 41	0.00 3 0.00 3 0.00 6	-0.0144 -0.0164 -0.0161 -0.0144	-6-321 × 0-3237	0.1339	-0-13B0_		
7.20/ veniel 7.20/ veniel 7.27// ieilla 7.17// ieilla 7.11// ieilla 7.11// ieilla 7.11// ieilla 7.11// ieilla 7.11// ieilla		0.03 3 0.03 3 0.076	=0-0151 =0-1144	6.3241		0.1868	D.ARGA	
7.207. unital 7.277. unital 7.	1 -0.(31) 2 .mac 3+2 1 -0.0416 2 -0.0324	0.63 3 	-6-1144		_1_1646			
Compa colling	2 -mail3+2 1 -mail3+2 1 -mail3+2 mail3+2 mail3+2					U-1617		
C. 174	-0.0414 0.2324	1.0076		(655.7	0.1722	0.1509	2.5381	
1-411c Jazade 0-41	-u-2324		-4. 01.33	3271_ n.3354	_341583 6.1594	0.1796	2_185\$ 2.1457	
Paster .=11= 	a weather				L.1647		2-1116	
7-335 1-1/6 2-63- 1-1/4/		0141		3.3434	0.1705	0.1424	1.9213	
Danks 100921			=0-6175		41716	0-1643	1.9336	
	1 -5.0253		-0-02-3	1.3542	0.1475	0-1647	1.7904	
Sellai Lales							1.5951	
5.7mel 1.1mm	· -ballees	-1.0.126	-0.0234	J.35-0	0.203Z	0.1508	1.4711	
	<u> </u>			0_3690	4.2040	3-1442	1.5030	
						0.1361	1 • 3885	
							• • • • • • • • • • • • • • • • • • • •	
				11 to 12 to 1				
101445 105346		-0.2445	-00.1518	V•3137	0.5310	U.V049	1.3784	
							•	
· <del>··········</del>								·
	0.00.1 1.330 1.30.00 1.00.1 Cruf 1.1.3 1.761 1.277	0.4m.7 1.43m0.0201 1.5cm 1.m.72	0.5m. / 1.33m0.0201 -0.003m 1.5car 1.m. /	0.5n.7 1.33n0.0201 -0.033n -0.5199 -5cyr 1-ny72 -0.021 -0.053n -0.0211 Cny6 1.7.3n v.01n6 -v.11c0 -v.0233 1.7cf 1.2719 -0.39n -0.17cl -0.023n	0.55.7 1.336.7 -0.0231 -0.0036 -0.5199 0.3522 -5car 1.57.7 -0.0231 -0.0535 -0.0233 0.3365 1.161 1.2719 -0.345 -0.11c0 -0.0233 0.3365 1.161 1.2719 -0.345 -0.11c0 -0.0236 0.3371	0.4m.7 1.33m0.0201 -0.003m -0.5199 0.3522 0.2162 -5cyr 1.m.72 -0.021 -0.053m -0.0211 0.361m 0.235 Cmur 1.7,3m 0.01m2 -0.11cm -0.0233 0.33m5 0.cm2 1.7cf 1.2779 0.34m -0.17m1 -0.023m 0.3371 0.2378	0.44.7 1.334.2 -0.0231 -0.0034 -0.0199 0.3522 0.2162 0.1361 -5.44. 1.472 -0.023 -0.0534 -0.0211 0.3414 6.2345 0.1049 0026 1.7.34 0.0106 -0.1100 -0.0233 0.3365 0.0402 0.0923 1.727 1.2779 -0.346 -0.1701 -0.0234 0.3371 0.2378 0.0993	0.4m.7 1.33m0.0201 -0.003m -0.0199 0.3522 0.2162 0.1361 1.3885  -5cyr 1.my72

		IŁ			TEM HETHER					DEL3 DELA			
	2 -0.00 0.0 -0.07/2 -0.0705 -0.0305 0.0506 p3.0197 0.3003 0.1120 0.1879 1.0074 2 -0.00 0.0 -0.0707 0.1121 -0.0333 0.0175 -0.0216 0.2925 0.1170 0.1600 -0.3911 3 0.13 0.0 0.00 0.0070 0.1127 -0.0333 0.0075 -0.0215 0.2925 0.1170 0.1752 10.7215 4 1.30 0.0 0.0070 0.1127 -0.0300 0.0138 -0.0215 0.2976 0.1306 0.1670 3.2709 5 2.00 0.0 0.0070 0.1127 -0.0300 0.0138 -0.0215 0.2976 0.1306 0.1670 3.2709 5 2.00 0.0 0.0070 0.1127 -0.0326 0.0138 -0.0215 0.3000 0.1376 0.1628 3.0288 6 3.37 0.0 0.1121 -3.160 0.0328 0.0123 -0.0216 0.3055 0.1473 0.1502 2.8597 7 2.17 0.1 0.1221 1.0000 0.0127 0.0326 0.0216 0.3055 0.1473 0.1502 2.8597 8 5.37 0.0 0.0 0.127 0.0117 -0.0322 0.0216 0.3129 0.1501 0.1509 2.3958 9 0.27 0.0 0.0000 0.0000 0.0000 0.0000 0.1571 0.1489 2.3958 10 7.02 0.0 0.127 0.0117 -0.0322 0.0216 0.3129 0.1501 0.1509 2.5320 9 0.27 0.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.00000 0.0000 0.0000 0.00000 0.00000 0.00000 0.0000 0.0000 0.00000 0.00000												
2 -0.00 0.0 -0.00 0.00 0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.	2 -0.00 0.0 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00			_									
1.30 U.O C.UTY J.172 -C.UTSO C.U13R -0.0215 0.2976 0.1306 0.1670 3.2709 5. 2.60 U.O C.LT3164 mis-32A 0.0143 m0.0217 0.3000 U.1376 0.162A 3.028B 6. 3.37 U.O C.LT3164 mis-32A 0.0143 m0.0217 0.3000 U.1376 0.162A 3.028B 7. 3.37 U.O C.LT3164 mis-32A 0.0143 m0.0217 0.3000 U.1376 0.1632 2.8597 7. 4.37 U.O C.LT3164 m.0.0310 0.024A m0.023A 0.3055 0.1673 0.1502 2.305B 8. 5.37 U.O C.ZT3164 m.0.117 -0.0322 0.023A 0.3050 0.1501 0.1569 2.5320 9. 6.42 U.O C.ZT3164 m.0.024A m.0.174 m.0.021A 0.3129 0.1561 0.1569 2.5320 9. 6.42 U.O C.ZT3164 m.0.024A m.0.174 m.0.021A 0.3126 0.3126 0.1632 2.288A 10 7.02 U.O C.ZT3164 m.0.024A m.0.174 m.0.021A 0.3223 0.1593 0.1630 2.2256 11 A.45 U.O C.MT4164 M.0.1174 m.0.021A m.0.0232 0.3262 0.1648 0.1613 2.1396 2 9.40 C.O C.MT4164 M.0.1174 m.0.021A m.0.0232 0.3361 0.1727 0.1614 1.9011 13 1C.AN U.O C.MT4164 M.0.1174 m.0.0274 m.0.0277 m	1.30 U.O C.UPY U.IY -0.0300 C.0138 -0.0215 0.2976 0.1306 0.1670 3.2709 5 2.40 L.O C.10211101 #0.0324 0.0143 #0.0217 0.1000 U.1376 0.1624 3.0248 6 3.37 U.O C.14.												
5 2.60 6.0 1.10233163 min324 0.01-300217 0.3000 0.1376 0.1624 3.0288 4 3.39 0.0 0.14-1	5 2.40 6.0 1.10c1316.1 minus224 0.01 3 m0.0217 0.3000 0.1376 0.1624 3.0288  5 3.39 6.0 0.14 6.470 -0.137 0.6740 -0.0218 0.3355 0.1473 0.1562 2.8597  7 4.37 6.3 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2												
4 3.39 0.0 0.1e+. (700 -0-)337 0.0740 -0-0218 0.3055 0.1e73 0.1602 2.8597  7 2.37 0.3 (-2225 1.2010 -0.216) (-0216 -0.0236 0.3060 0.1571 0.1449 2.3958  8 5.39 0.0 (-2216 0.117 -0.3122 0.0761 -0.0216 0.3129 0.1561 0.1569 2.5320  9 5.20 0.0 (-2216 0.117 -0.3122 0.0761 -0.0216 0.3129 0.1561 0.1569 2.5320  9 5.20 0.0 (-2216 0.1677 0.7022 -0.014 0.0216 0.323 0.1593 0.1632 2.2486  10 7.22 0.0 (-2216 0.0767 0.7022 0.014 0.0216 0.323 0.1593 0.1632 2.2486  11 8.45 0.0 (-2016 0.0767 0.0762 0.0213 -0.0232 0.3262 0.1648 0.1613 2.1396  2 9.40 0.0 (-2016 0.0767 0.001) (0.0761 -0.0232 0.3361 0.1727 0.1614 1.9911  3 10.46 0.0 0.2016 0.441 0.0026 (0.0123 -0.0232 0.3361 0.1727 0.1614 1.9911  3 10.47 0.0 0.2016 0.441 0.0026 0.0122 0.3363 0.1636 0.1636 0.1636  1 10.47 0.0 0.2016 0.441 0.0026 0.0122 0.0732 0.3363 0.1950 0.1613 1.7099  1 12.56 0.0 0.0710 1.1855 0.0027 0.0121 0.3377 0.2017 0.1360 1.5205  14 12.56 0.0 0.0331 1.350 0.0016 0.0027 0.0268 0.3363 0.2072 0.1364 1.5006  15 15.54 0.0 0.0331 1.350 0.0016 0.0027 0.0268 0.3363 0.2072 0.1364 1.5006  15 15.54 0.0 0.0331 1.350 0.0016 0.0027 0.0268 0.3363 0.2072 0.1364 1.5006  15 15.54 0.0 0.0331 1.350 0.0016 0.0027 0.0268 0.3363 0.2072 0.1364 1.5006  15 15.54 0.0 0.0331 1.350 0.0016 0.0027 0.0028 0.3363 0.2072 0.1364 1.5006													
7	7							_			_		
# 5.39	# 5.37			-					_		_		
	10 7.42 0.0 0.7577 0.752 -0.0274 0.0179 -0.0218 0.3723 0.1593 0.1630 2.2254 11 8.45 0.0 0.4048 0.0551 -0.0252 0.4213 -0.0232 0.3262 0.1648 0.1613 2.1398 12 9.46 0.0 0.4743 0.7277 -0.031 0.0261 -0.0220 0.3341 0.1727 0.1614 1.9411 13 10.46 0.0 0.5616 0.7777 0.0017 -0.0228 0.3263 0.3263 0.1950 0.1614 1.9411 14 11.47 0.0 0.5616 0.7777 1.1070 -0.0228 0.0172 -0.0232 0.3363 0.1950 0.1014 0.1694 1.8518 15 12.57 0.0 0.0 0.0017 -0.0227 0.0174 -0.0228 0.3363 0.1950 0.1613 1.7099 16 13.51 0.0 0.0 0.0027 -0.0227 0.0377 0.2017 0.1360 1.5205 17 13.56 0.0 0.0017 -0.0227 0.0174 -0.0228 0.3377 0.2017 0.1360 1.5205 18 15.54 0.0 0.0017 -0.0227 0.0228 0.3377 0.2017 0.1364 1.5008 19 10.56 0.0 0.0017 1.3550 -0.0165 0.0017 -0.0228 0.3300 0.2107 0.1292 1.4581 20 17.53 0.0 1.1107 1.4462 -0.0177 -0.0013 -0.0268 0.3365 0.2315 0.1330 1.3399 21 18.68 0.0 1.107 1.4462 -0.0017 -0.0013 -0.0275 0.3266 0.2018 0.0030 1.4756		_										
	1		<u> </u>			Castal				0.3136_	_4-1544.	0-1632	2.2884
2 9.46 (.0 %.143 C.727 -0.030] 0.0261 -0.0240 0.334] 0.1727 0.1614 1.941] 3 16.46 0.0 0.561. 6.445. 40.6704 -0.0735 0.334] 0.1727 0.1614 1.941] 4 11.47 0.0 7.577- 1.1070 -0.0750 0.0162 -0.0732 0.3600 0.1914 0.1494 1.8518 5 12.57 0.0 6.700 1.1455 -0.0251 0.0169 -0.0732 0.3363 0.1950 0.1613 1.7099 6 13.51 0.0 6.1605 1.1607 -0.0727 0.01-1 -0.0728 0.3377 0.2017 0.1360 1.5205 17 13.56 0.0 0.0007 -0.0727 0.0150 -0.0725 0.3377 0.2017 0.1364 1.5008 18 15.56 0.0 0.930) 1.3550.0725 0.0007 -0.0768 0.3400 0.2107 0.1292 1.4561 19 10.56 0.0 0.930) 1.3550.0725 0.0007 -0.0768 0.3400 0.2106 0.1213 1.3561 10 17.53 0.0 1.1107 1.4402 -0.0777 -0.0737 -0.0739 0.3365 0.2315 0.1030 1.3399 11 15.56 0.0 0.0007 0.0007 -0.0007 -0.0007 0.3365 0.2315 0.1030 1.3399	12	-	_										
10 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	13 10 An												
11.67	14				-								
12.5c   G.u   C.27.0u   1.1255   C.2169   -0.2721   U.3363   0.1950   0.1613   1.7099     6	10 12.5¢ G.v C.o.7uv 1.1050 -0.3251 C.0169 -0.0221 0.3363 0.1950 0.1013 1.7099 1.1050 1.3.51 0.0 0.1013 1.7099 1.0.0217 0.1360 1.5205 1.7 1.0.56 0.0 0.0017 0.1360 1.5205 1.7 1.0.56 0.0 0.0017 0.1360 1.5205 1.7 1.0.56 0.0 0.0017 0.1360 1.5205 1.7 1.0.56 0.0 0.0017 0.1360 1.5205 1.7 1.0.56 0.0 0.0017 0.1360 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5000 1.5												
17 19-56 0.6 0.500 1.2757 -0.0615 0.6155 -0.0253 0.3436 0.2077 0.1364 1.5006 1.5.54 0.0 0.930) 1.3556 -0.0645 0.0097 -0.0268 0.3400 0.2105 0.1297 1.4581 1.4561 1.5.55 0.0 1.213 1.3561 1.5.55 0.0 1.213 1.3561 1.5.55 0.0 1.530 0.2166 0.1213 1.3561 1.5.55 0.0097 -0.0633 -0.0255 0.3399 0.2166 0.1213 1.3561 1.5.55 0.1030 1.3399 1.5.55 0.0097 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000 0.2000	17			ىمى	CasTuu			L_21c9_	-0-0221				
16 15.54 0.0 0.930) 1.3560.0165 0.0092 -0.0268 0.3400 0.2105 7.1292 1.4581  19 12.56 1.0 1.415 1.415 0.0165 0.0160 -2.0255 0.3399 0.2166 0.1213 1.3561  20 17.53 0.0 1.1150 1.4462 -0.0777 -0.0033 -0.0266 0.3345 0.2315 0.1030 1.3399  21 16.68 1.0 1.1674 1.5735 0.0135 -0.0256 -0.3275 0.3266 0.2416 0.0830 1.4756	16 15.54 0.0 0.934) 1.3560.0165 0.0092 -0.0268 0.3400 0.2105 7.1292 1.4581  19 10.56 0.0 1.316 1.402 -0.5155 0.3160 -2.0255 0.3399 0.2166 0.1213 1.3561  20 17.53 0.0 1.1170 1.4462 -0.5077 -0.0133 -0.0266 0.3345 0.2315 0.1030 1.3399  21 15.65 0.0 1.404 1.5435 0.0135 -0.0256 -3.3255 0.3266 0.2416 0.00830 1.4756												
19 10-56 1-4 1-10- 1-400-51-5 0-3160 -3-0255 0-3399 0-2166 0-1213 1-3561 20 17-53 0-4 1-110- 1-40-2 -0-3477 -0-0133 -0-0256 0-3345 0-2315 0-1030 1-3399 21 18-68 1-4 1-14/4 1-5435 0-0135 -0-0236 -3-3275 0-3266 0-2416 0-0830 1-4756	14 10-5h 1-4 1-16c 1-44-2 -0-5145 0-316d -2-0255 0-3399 0-2166 0-1213 1-3561 20 1/-53 0-4 1-110c 1-44-2 -0-1477 -0-0033 -0-0256 0-3345 0-2315 0-1030 1-3399 21 15-54 1-4 1-1474 1-5435 0-0135 -0-0275 0-3266 0-2416 0-00830 1-4756			1411									
20 1/-53 0.0 1.11mc 1.4452 -0.1077 -0.0033 -0.0256 0.3345 0.2315 0.1030 1.3399 21 15.55 1.00 1.16/5 1.5/31 0.0155 -0.0256 -0.3275 0.3266 0.2616 0.0830 1.6756	20 1/-53 0.0 1.11m/ 1.4462 -0.1077 -0.0033 -n.0296 0.3345 0.2315 0.1030 1.3399 21 15-nm 0.0 1.14/4 1.5435 0.0195 -0.0256 -3.0275 0.3266 0.2616 0.00830 1.4756												
			_										
72 14.65 U.U 1.239J 1.7557 0.0555 -0.1523 -0.0282 0.3187 0.2492 0.0695 1.6170	27 14.65 U.U 1.254. 1.755 0.045. 0.155 -0.1523 -0.3167 0.2492 0.0695 1.4170			-		1.544	4-6195	<u> مۇندى . 0</u>	-3-3215	0.3266_	-C-2016	. 0.0830	1.4756
		14.	65	0.6	1.2390	1.7557	ひ・いうつう	-0.1523	-0.0585	0.3197	0.2492	0.0695	1-4170
		<del></del>			<del></del>			<del></del>	<del></del>				<del></del>
·													
				<u> </u>									
		<del></del>			<del></del>		···			<del></del>			
					<del></del>								
									_				

	2 -	-1- <u>-7</u> -0.47	95 T A			3-0-6 0	• O UF	F OFF	UFF UFF	PHEE		
2 -0.47	3 4 5	-6.47								_		
3	4		i U									
1.30					•	_						
5 3.01 0.0 1.171 0.0.0 1.171 0.0.0 0.00 0.0		1.34	G.U									-
7 A.Sh	6											
6 5.60 0.0 1.277	_											
\$\partial \cdots	<del></del>					-						
	-				_		_					
1			_									
12		_										
13 10.51												
10.62 0.0 7.62 0.022 1.7370  15 12.50 0.0 0.723 1.1737 1.0726 0.0426 0.0330 0.3272 0.1947 0.1285 1.5596  16 13.57 0.0 0.722 1.127 -0.0260 0.0339 -0.0310 0.3242 0.2011 0.1231 1.4471  17 14.52 0.0 0.0727 1.257 -0.1170 0.0253 0.320 0.3220 0.2030 0.1137 1.4294  18 15.00 0.0 0.5020 1.3200 -0.175 0.0263 -0.0335 0.3192 0.2141 0.1051 1.3757  19 16.50 0.0 1.102 1.004 -0.0314 -0.0318 0.3192 0.2131 0.2030 0.2090  21 17.70 0.0 1.1027 1.0274 -0.0 0.0 0.0 0.3190 0.2023 0.2030 0.2073 1.2917												
15 12-50 No.			0.6									
17. 14.62 (.u u.m7x/ 1.257a =2.117a u.m2x3 =0.632u u.322a .u.2030 .u.1137 1.4294 10 15.00 0.0 0.5070 1.3205 -0.175 (.u243 =0.0335 0.3192 0.2141 0.1051 1.3757 14 16.55 1.u 1.12x	15	12.50.	Lak	. Lale	lalZ/*_				0.3272	L.1947	0.1785.	1.5594
18 15.50 0.0 0.5055 1.3755175 (.0243 -0.0335 0.3152 0.2141 0.1051 1.3757 .  19 16.50 1.00 1.105 1.00515144 1.6343 -6.5348 0.3197 0.2234 0.6558 1.3424  20 17.70 (.00 1.1557 1.0570) (0 0.013 -0.0340 0.3156 0.2323 0.6673 1.2917  21 16.72 0.00 1.2577 1.5570 1.3042 -2.0224 -2.0342 0.3136 0.2334 0.6799 1.2395			6.0	(./+>	1.1-2-	-0.025-	(.6349	-2.6314	3.3242	0.2011	0.1731	1.4871
14 16-55 1-12 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-12-1 1-												
75 17.70 (.v 1.1777 1.0770) /0 (.0713 -2.0330 0.3190 0.223 0.0673 1.2917 21 16.74 (.u. 1.277 1.2570] -2.0224 -2.0325 0.3136 0.2334 0.6799 1.2395	_		_									
21 16.74 1.u. 1.2377 1.2574												
1317 000 11377 11(000 000000 000000 000000 111311												·
		.,	***	103724		****	-0.0430	-010336	003376	0.5-08	0.0054	101311
										<del></del>		
						<i></i>		-				
					<del></del>		— -		<del></del>			

_
⋗
m
O
C
⇉
33
ż
Č
Ι.
-5
8
•

1	2 17 0.59 2.0	
1.76	1.76	
2 -0.57	2 -0.67	
0.35	1 1.50 to 1 1.50	
1.3e	1.3e	
5 2-61 0-0	5 2.61 0.0 0.135c 6.274a =0.0239 0.0040 =0.0252 0.2585 0.1562 0.1063 2.0308 6 3.44 0.0 0.1727 0.076 =671 0.0048 =0.0264 0.2609 0.1591 0.1018 2.2423 7 4.44 0.0 0.1727 0.076 =671 0.0048 =0.0264 0.2609 0.1591 0.1018 2.2423 8 5.47 0.0 0.2724 0.0044 =0140 0.0446 =0.0251 0.7650 0.1650 0.1695 2.3437 9 6.51 0.0 0.2727 0.004 =0140 0.0446 =0.0251 0.7650 0.1650 0.1695 2.3437 10 7.53 0.0 0.2727 0.010 =0.0191 0.0478 =0.0235 0.2803 0.1647 0.1116 2.2373 11 9.00 0.0 0.2727 0.010 =0.0191 0.0478 =0.0247 0.2677 0.1740 0.1132 2.1908 12 9.03 (.0 0.2745 0.0192 0.0195 0.0486 =0.0250 0.2795 0.1740 0.1132 1.9956 13 10.63 0.1 0.2151 0.0192 0.0486 =0.0269 0.2795 0.1435 0.1120 1.0518 13 10.63 0.1 0.2151 0.000 =0.0192 0.0500 0.2795 0.1435 0.1120 1.0518 14 11.66 0.0 0.4727 0.000 =0.0000 0.0000 0.3072 0.1952 0.1070 0.5008 15 12.72 6.6 0.7427 0.1537 0.0000 =0.0706 0.3072 0.1952 0.1070 0.5008 16 13.77 0.0 0.2512 0.1537 =0.0153 0.0000 0.3033 0.2227 0.1066 0.5508 17 16.75 0.0 0.5121 0.231 0.00135 0.0000 0.3033 0.2036 0.0000 0.0000 0.5005 17 16.75 0.0 0.5121 0.231 0.00135 0.0000 0.3033 0.2036 0.0000 0.3096 0.3096 18 16.92 0.0 0.0000 0.0000 0.0000 0.0000 0.3096 0.3096 19 16.92 0.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.00000 0.00000 0.000	
6 3.44 0.0 7.172/ 7.37/c7cl- 0.0034 -0.024 0.200 0.1531 0.1018 2.2223 7 2.44	0	
9 6.51 C.0 C.215 C.71470140 0.0445 -0.0751 0.7455 0.1450 0.1095 2.3437 9 6.51 C.0 C.215 C.7147 -0.0191 0.0479 -0.0235 0.2803 0.1647 0.1116 2.2373 10 7.53 C.0 0.757 0.0117 -0.0199 0.0474 -0.0247 0.2877 0.1740 0.1132 2.1900 11 8.00 G.0 0.2152 (015 0.0195 0.0245 0.2823 0.2924 0.1790 0.1134 1.9956 12 9.05 (.0 C.214 0.2167 0.0192 0.0445 -0.0246 0.2955 0.1435 0.1120 1.8510 13 10.63 G.1 0.2171 1.0104 -0.0192 0.0445 -0.0246 0.2955 0.1435 0.1120 1.8510 14 11.66 0.0 0.4747 1.0104 -0.0142 0.0070 0.3072 0.1952 0.1070 1.6508 15 12.72 G.0 0.2107 1.1537 -0.0153 0.0446 -0.0233 0.3033 0.227 0.1066 1.5587 16 13.77 0.0 0.215 1.231 -0.0135 0.0446 -0.0233 0.3033 0.2027 0.1066 1.5587 17 14.75 G.0 0.5123 1.221 -0.0135 0.0446 -0.0233 0.3031 0.2008 0.0966 1.5035 17 14.75 G.0 0.5123 1.221 -0.0135 0.0446 -0.0233 0.3031 0.2008 0.0966 1.5035 18 15.63 C.0 1.0 -7 1.3801 -0.0674 0.0446 -0.0250 0.3055 0.2174 0.0881 1.4431 19 15.63 C.0 1.0 -7 1.3801 -0.0674 0.0446 -0.0250 0.3055 0.2255 0.0699 1.3796 19 16.64 0.0 1.271 1.272 0.0015 0.0015 0.2000 0.3005 0.2757 1.3621 27 17.90 0.0 1.271 1.222 0.0010 0.00730 -0.0250 0.3005 0.2753 0.0653 1.2922 28 20.03 G.0 1.0407 1.7005 0.0100 -0.0390 -0.0250 0.2676 0.2440 0.0436 1.1621	9 5.07 U.J 6.7-U 1.00440140 U.0440 -0.0251 U.7/03 0.1450 0.1095 2.3437 9 6.51 C.B 6.315 0.7147 -0.0191 U.0479 -0.0235 D.2833 0.1647 0.1116 2.2373 10 7.53 C.U 0.327 U.01140194 0.0247 0.7872 U.1740 0.1132 2.1900 11 Head Gau 0.4152 (003 -0.0195 0.0243 D.2833 D.2833 D.1647 0.1132 2.1900 12 9.03 (.0 C144 0.4152 (003 -0.0195 0.0243 D.2835 D.1790 D.1134 1.9956 13 10.43 0.1 0.4751 1.11440192 0.0049 0.2955 D.1790 D.1134 1.9956 14 11.60 U.J 0.4701 1.11440124 0.0070 -0.0257 U.3023 0.1914 D.1149 1.7603 15 12.72 0.6 0.7401 1.15110153 0.0070 0.3072 U.1952 0.1070 1.6508 16 13.77 U.O 0.421 1.15110153 0.0070 0.3072 U.1952 0.1070 1.6508 17 14.79 0.4 0.5103 1.2210153 0.0070 0.3031 0.2036 0.0964 1.5587 18 15.03 C.U 1.0701 1.2210137 0.0070 0.0233 0.3031 0.2036 0.0964 1.5035 18 15.03 C.U 1.0701 1.2210137 0.0070 0.0230 0.3055 0.214 0.0881 1.4431 18 15.03 C.U 1.0701 1.12210147 0.0070 -0.0250 U.3005 0.2250 0.0609 1.3796 19 16.97 U.J 1.1221 1.22210153 0.0070 0.0070 0.00757 1.3621 27 17.90 U.U 1.71 1.222  0.0001 -0.0070 -0.0250 U.3005 0.753 0.0063 1.2922 21 10.427  0.0001 1.0005 0.0000 -0.0070 -0.0250 U.2006 0.0005 1.2902 22 20.03 G.U 1.0001 1.7005 0.0000 -0.0030 -0.0050 0.2440 0.0436 1.1821	
9 6.51 (.0 0.215 0.7147 -0.0191 0.0049 -0.0235 0.2033 0.6607 0.1116 2.2373  10 7.53 (.0 0.7457 0610 -0.0195 0.0074 -0.0247 0.7672 0.1740 0.1132 2.1900  11 8.00 0.0 0.457 (.0005 0.00195 0.0044 -0.0243 0.2224 0.1790 0.1134 1.9956  12 9.00 (.0 0.4457 0.0192 0.0045 -0.0245 0.7955 0.1435 0.1120 1.9510  13 10.43 0.1 0.4771 1.0194 -0.0192 0.0045 -0.0245 0.7955 0.1435 0.1120 1.9510  14 11.60 0.0 0.4747 1.0194 -0.0197 0.00735 0.3022 0.1952 0.1070 1.6508  15 12.72 0.0 0.7447 1.0194 -0.0153 0.0044 -0.0233 0.3033 0.2027 0.1066 1.5587  16 13.74 0.0 0.4211 1.231 -0.0134 0.0044 -0.0233 0.3031 0.2036 0.0964 1.5035  17 14.75 0.0 0.0512 1.231 -0.0134 0.0044 -0.0233 0.3055 0.2174 0.0081 1.4431  18 15.03 0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	9 6-51 (-0 0-315 0-7147 -0-0191 0-0249 -0-0235 0-2033 0-1607 0-1116 2-2373 10 7-53 (-0 0-727 0-019 -0-019 0-0247 0-2672 0-1740 0-1132 2-1900 11 9-00 (-0 0-352 (-0-05 -0-0192 0-2445 0-2235 0-1740 0-1132 1-956 12 9-00 (-0 0-744 0-734 -0-0192 0-2444 0-2237 0-2955 0-1835 0-1120 1-9510 13 10-73 0-1 0-771 1-1024 -0-0192 0-2444 0-257 0-3053 0-1610 0-1120 1-7603 14 11-66 0-0 0-747 1-1024 -0-0122 0-00736 0-3072 0-1952 0-1070 1-6508 15 12-72 0-6 0-1202 1-1512 -0-0153 0-00736 0-3072 0-1066 1-5507 16 13-77 0-0 0-721 1-231 -0-0135 0-0074 0-0023 0-3031 0-2036 0-0964 1-5507 17 14-79 0-0 0-714 1-231 -0-0134 0-00736 0-3055 0-2174 0-0081 1-431 18 15-03 0-0 10-7 1-3801 -0-0147 0-0074 0-0023 0-3055 0-2174 0-0881 1-431 18 15-03 0-0 10-7 1-3801 -0-0149 0-0074 0-3055 0-2174 0-0881 1-431 19 15-03 0-0 10-7 1-3801 -0-0149 0-0074 0-3055 0-2174 0-0881 1-431 19 15-03 0-0 10-7 1-3801 -0-0149 0-0074 0-0055 0-3055 0-2174 0-0881 1-431 19 15-03 0-0 10-7 1-3801 -0-0149 0-0074 0-0075 0-3065 0-2757 1-3621 27 17-90 0-0 1-7 1-3801 -0-0149 0-0074 0-0074 0-0075 0-0075 0-0053 1-2022 21 10-77 1-79 0-0 1-79 0-0075 0-0075 0-0075 0-0075 0-0052 1-2022 21 10-77 1-79 0-0 1-79 0-0075 0-0075 0-276 0-276 0-0075 1-2022 22 20-03 0-0 1-90 1-7905 0-0075 0-0075 0-276 0-276 0-276 0-276 0-0075 1-2022	
10 7.53 C.0 0.752/ 0-01/4 -0.01/4 -0.0247 0.7672 0.1740 0.1132 2.1900 11 8.00 0.0 0.452 (-0.05 -0.0145 0.0440 -0.0243 0.2924 0.1790 0.1134 1.9956 12 9.63 (-0 0.444 0.478, -0.0192 0.5446 -0.0240 0.7955 0.1435 0.1120 1.8510 13 10.43 0.1 0.4751 1.0104 -0.0142 0.0444 -0.0257 0.3023 0.1914 0.1109 1.7603 14 11.60 0.0 0.4764 1.000 -7.0142 0.0000 -0.0746 0.3022 0.1952 0.1070 1.6508 15 12.72 0.0 0.4764 1.1504 -0.0153 0.0644 -0.0233 0.3031 0.2066 0.0964 1.5085 16 13.79 0.0 0.4764 1.201 -0.0154 0.0644 -0.0233 0.3031 0.2068 0.0964 1.5035 17 14.79 0.0 0.5164 1.201 -0.0154 0.0644 -0.0250 0.3055 0.2176 0.0881 1.4431 18 15.63 0.0 1.0 -/ 1.3801 -0.0769 0.0448 -0.0250 0.3045 0.2235 0.0699 1.3796 19 16.90 0.0 1.0 -/ 1.3801 -0.0769 0.0000 0.0000 0.0757 1.3621 27 17.90 0.0 1.7 1.1552 0.0000 0.0000 0.0522 0.0533 1.2922 28 20.03 0.0 1.0 407 1.7005 0.0180 -0.0259 0.2676 0.2640 0.0522 1.2606	10 7.53 C.0 0.75=/ 0-01" -0.019 7.0074 -0.0247 0.7672 0.1740 0.1132 2.1900 11 8.00 0.0 0.452 (-0.05 -0.0195 0.0000 -0.0243 0.2924 0.1790 0.1134 1.9956 12 9.00 (.0 0.452 0.0192 0.0192 0.0245 0.7955 0.1435 0.1120 1.9510 13 10.43 0.1 0.455 1.1124 -0.0249 0.755 0.1323 0.1914 0.1104 1.7603 14 11.60 0.0 0.454 1.100 -0.0122 0.0575 0.3022 0.1952 0.1070 1.6506 15 12.72 0.0 0.100 1.100 -0.0125 0.0070 0.3022 0.1952 0.1070 1.6506 15 12.72 0.0 0.100 1.100 -0.0135 0.0070 0.3022 0.1952 0.1070 1.6506 16 13.79 0.0 0215 1.231 -0.0135 0.0070 -0.0233 0.3031 0.2056 0.0064 1.5035 17 14.79 0.0 0.51=1 1.231 -0.0135 0.0070 -0.0233 0.3031 0.2056 0.0064 1.5035 18 15.03 0.0 1.0 -7 1.3001 -0.0700 0.0000 0.3005 0.2235 0.0009 1.3706 19 16.99 0.0 1.0 -7 1.3001 -0.0700 0.0000 0.3005 0.2235 0.0009 1.3706 19 16.99 0.0 1.0 -7 1.3001 -0.0700 0.0000 0.3005 0.235 0.0009 1.3706 19 16.99 0.0 1.0 -7 1.3001 -0.0700 0.0000 0.3005 0.235 0.0000 1.3021 27 17.90 0.0 1.211 1.000 0.000 0.0000 0.2000 0.2000 0.0053 1.2022 28 20.03 0.0 1.0 10 1.1005 0.0100 -0.0390 0.0204 0.2066 0.2040 0.0036 1.1021	
11	11	
12	12	
13	13	
14 11.66 0.0 0.4767 1.705 -7.0152 7.0573 -0.0756 0.3022 0.1952 0.1070 1.6508 15 12.72 0.6 0.1002 1.1532 -0.0153 0.0026 -0.0253 0.3033 0.2027 0.1066 1.5587 16 13.77 0.0 0215 1.2351 -0.0135 0.0026 -0.0253 0.3031 0.2056 0.0966 1.5035 17 16.75 0.0 0.51=1 1.2211 -0.0137 0.0026 0.3055 0.2174 0.0881 1.4431 18 15.63 0.0 1.0 -7 1.3861 -0.0109 0.0046 -0.0250 0.3055 0.2174 0.0881 1.4431 19 16.62 0.0 1.0 -7 1.3861 -0.0109 0.0046 -0.0250 0.3055 0.2255 0.0069 1.3796 19 16.62 0.0 1.0 -7 1.3861 -0.0109 0.0046 0.0250 0.3055 0.2255 0.0069 1.3796 19 16.62 0.0 1.0 -7 1.3861 -0.0109 0.00730 -0.0250 0.3055 0.2757 1.3621 27 17.90 0.0 0.0 1.211 1.525 0.0000 0.00730 -0.0250 0.3005 0.2753 0.0653 1.2922 21 16.62 0.0 1.405 1.3161 1.5256 0.0000 -0.0390 -0.0259 0.2676 0.2440 0.0436 1.1021	14 11.66 0.0 0.4707 1.000 -7.0107 7.60070 0.3022 0.1952 0.1070 1.6508 15 12.72 0.0 0.1002 1.1502 -0.0153 0.4000 -0.0253 0.3033 0.2027 0.1066 1.5507 16 13.77 0.0 0215 1.201 -0.0135 0.4000 -0.0203 0.3031 0.2008 0.0964 1.5035 17 14.79 0.0 0.5100 1.221 -0.0135 0.4000 0.3055 0.2174 0.4001 1.4031 18 15.63 0.0 1.0 -7 1.3001 -0.0700 0.4000 -0.0250 0.3045 0.2255 0.4009 1.3796 19 16.90 0.0 1.0 -7 1.3001 -0.0700 0.4000 -0.0250 0.3005 0.2255 0.4009 1.3796 19 17.00 0.0 1.201 1.202 0.4000 0.4030 0.2030 0.4053 1.2022 21 16.00 0.0 1.201 1.205 0.4000 -0.0700 -0.0250 0.2050 0.2050 0.4053 1.2022 22 20.03 0.0 1.000 1.7005 0.0100 -0.0390 -0.0250 0.2676 0.2440 0.0436 1.1821	
15 12-72 0-16 0-10-22 1-15-32015-3 0-0-260-025-3 0-3033 0-2027 0-1066 1-55-87 16 13-77 0-0 0-215 1-25-10135 0-0-240-025-3 0-3031 0-2066 0-0-066 1-5035 17 14-75 0-16 0-51-1 1-2210107 0-03620-0256 0-3055 0-2176 0-0801 1-4431 18 15-03 0-10 17 1-30610574 0-0-025 0-3065 0-2235 0-0659 1-3796 19 16-92 0-16 1-16-7 1-30610574 0-0-025 0-3065 0-2235 0-0659 1-3796 19 17-90 0-0 1-2-12 1-305 0-0053 0-0-0274 0-3065 0-235 0-0653 1-2922 21 16-02 1	15 12-72 0-4 0-10-7 1-15070153 0-0-6 -0-0253 0-3033 0-2027 0-1066 1-5587 16 13-77 0-0 0-215 1-2351 -0-0135 0-00-70 -0-0253 0-3031 0-2056 0-09-60 1-5035 17 14-79 0-4 0-51-3 1-221 -0-0137 0-0362 -0-0250 0-3055 0-2176 0-0861 1-6031 18 15-83 0-0 1	
16 13.7v v.0 6215 1-231 -0.0135 0.0044 -0.0233 0.3031 0.2038 0.0064 1.5035 17 14.76 0.4 0.51=3 1-3221 -0.0137 6.0362 -0.0269 0.3055 0.2176 0.0881 1.4431 18 15.63 0.0 1.0 -7 1.3661 -0.0349 0.0446 -0.0250 0.3045 0.2235 0.0899 1.3796 19 16.9c 0.0 1.1 1.51 1.515 0.0015 0.0275 0.3065 0.2289 0.0757 1.3621 27 17.9u 0.0 1.21 1.552 0.0010 0.0730 -0.0250 0.3005 0.2353 0.0653 1.2922 21 16.42 1.0 1.3121 1.525 0.0010 -0.0246 -0.0249 0.2440 0.0522 1.2006 22 20.03 0.0 1.0405 1.7005 0.0140 -0.0390 -0.0250 0.2676 0.2440 0.0436 1.1821	16 13.7	
17. 14.75	17. 14-75	
18 15.63 C.U 1.U -/ 1.3mb1 -U.0090 U.0090 U.3045 U.2235 0.0699 1.3796 19 16.97 U.0 1.1 1.5mb1 -U.0015 U.5215 -1.0274 (.3045 U.2235 0.0699 1.3796 20 17.90 U.0 1.271; 1.552 C.0040 U.0730 -0.0250 U.3055 U.2353 0.0653 1.2922 21 16.97 L.U 1.31v1 1.5254 L.U 1.525 C.0040 U.0730 -0.0294 U.2418 0.0522 1.2006 22 20.03 C.U 1.0405 1.7005 C.0100 -0.039U -0.0250 U.2676 0.2440 0.0436 1.1821	16 15.63 C.U 1.U -7 1.3mb1 -0.3694 U.CAVE -0.0250 U.3045 U.2235 0.0609 1.3796 14 16.97 U.J 1.1 1.5 1. 1.5 2. C.00.43 U.JC74 C.30.45 J.2269 0.0757 1.3621 27 17.90 U.U 1.27 1. 1.5 2. C.00.43 U.JC73 -0.0254 U.3055 U.2753 0.0653 1.2922 21 16.42	
10   10   10   10   10   10   10   10	10.92	
21 Iday Lau 1-31-1 1-224 Lauch Catta -0.0249 0-2440 0-0522 1-2406 22 20.03 G.V 1.405 1.7005 C.0180 -0.0390 -0.0254 0.2676 0.2440 0.0436 1.1821	21 Id. x	
22 20.03 G.V 1405 1.7005 G.0180 -0.0390 -0.0250 0.2676 0.2440 0.0436 1.1021	22 20.03 G.V 140- 1.70C5 G.0180 -0.0390 -0.055 0.2676 0.2440 0.0436 1.1821	
·		

1. JP MA 1. JP 1. J9 1. J9 2. 45 3. e7 4. 5 1. 5 1. 5 1. 7 1. 7 1. 7 1. 7 1. 7 1	#ETA	(A -0.101- -0.17.0- -0.20c- -0.707- -111- -0.111- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1- -0.31-1	Coller 	Cv ====================================	0.0533 -0.6515 -0.656 -0.054 -0.0525 -0.0525	CLL 0.0003 -0.0005 0.0005 0.0003 -0.0010 -0.0010 -0.0004	0.2426 0.7457 0.7507 0.2551 0.2545	CAR	0.4970	ACP -2.05A1 0.4960 -2.9404 -2.2867 -2.5257 -2.5257 -2.5252 -2.5224 -2.4573 -2.2956
10.00 10.39 10.39 20.45 30.07 40.50 50.53 40.50 70.62 80.63 90.00 11.77 12.65	0. J 0. U 0. U 0. U 1. J 0. J 0. J 0. J	-0.17.49 0.020c 0.0707 0.1114 1.150. 0.20-1 1.7513 0.3144 0.3054 0.4311 0.5113	coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Coller Co		0.043 0.0345 0.0513 -0.6515 0.656 0.0525 0.0525	-0.00.7 -0.00.9 -0.0005 -0.00.7 -0.00.3 -0.00.0 -0.00.0	0.2378 0.2396 0.2026 0.2457 0.2507 0.2551 0.2545	0.1314 0.1249 0.1655 0.1598 0.1598	0.10% 0.440 0.440 0.0911 - 0.0908 0.0926	0.4966 2.9404 2.2867 2.5257 2.5259 2.5224 2.4573
1.39 2.45 3.47 4.54 5.53 6.56 7.62 8.63 9.69 16.76 11.77	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.020c 0.0797 0.1174 0.1564 0.2057 0.3146 0.3057 0.4311 0.5113	Coller Coller Coller Coller Conjec Coller Coller Coller Coller Coller Coller Coller Coller Coller	-0.01/30.01/30.01/30.01/40.01/50.01/50.01/51.01/51.01/5	0.0345 0.0515 0.0515 0.0506 0.0526 0.0526	0.0005 0.0005 0.0003 0.0003 0.0000 -0.0010	0.2396 0.2457 0.2507 0.2551 0.2595	u.1249 u.1455 -0.1546 0.1548 -0.1664	0.1048 0.0971 0.0908 0.0908 0.0928	2.9404
1.39 2.45 3.47 4.56 5.53 6.56 7.42 8.63 9.69 16.76 11.77 12.65	0.0 0.0 0.0 0.0 0.0 0.0	0.6755 0.1174 0.1564 0.204 4.7513 0.3134 0.3457 0.5431	Coller 	-U.U.D.1 -U.D.174 -U.D.176 -U.U.176 -U.U.176 -U.U.176 -U.U.176 -U.U.176	0.0533 -0.6515 -0.656 -0.054 -0.0525 -0.0525	0.0005 0.0017 -0.0013 0.0000 -0.0010	0.2426 0.7457 0.7507 0.2551 0.2545	0.1556 0.1598 0.1598 6.1639	0.0926 8060°0 160°0 0.0815	2.2867 -2.5257 -2.5759 -2.5224 -2.4573
2.45 3.07 A.50 5.53 5.53 5.56 7.42 8.63 9.60 10.76 11.77	0.0 0.0 0.0 0.0 0.0 0.0	0.117# 0.156** 0.20=7 ************************************		-u.0174. -u.0170 -u.0170 -t.01100 -r.0100	0.0515 0.0506 0.0526 0.0526	-0.0017 -0.0033 -0.0000 -0.0010	0.2507 0.2551 0.2551 0.2545	0.1546 0.1548 6.1639 6.1667	0.0911 - 0.0908 0.0412- 0.0426	-2.5257 2.5959 -2.5224 2.4573
5.53 5.53 7.62 8.63 9.64 11.76 11.77	( . J 0 . J 0 . J 0 . J 1 . L C . V	0.20m/ 0.7519 0.3140 0.3057 0.4311 0.5113	1-5174 1-5175 Geneta Cabble 10-4626		0.052h 0.052h	-0-000t -0-001d	0.2551 0.2595 0.888	6.1607	0-0456	2.5224 2.4573
5.53 5.55 7.62 8.63 9.65 11.77 12.65	0.0 (.0 0.0 0.0	0.3146 0.3146 0.3457 0.4311 0.5(13	1.5174 7145 Geneta Centilo Geneta	-0.0170 -0.0141 -0.0109	0.052b	-0.0010	0.2545 0.2648	6.1607	0.0426	2.4573
7.62 8.63 9.60 11.76 11.77	0.3 0.4 0.3	0.3146 0.3057 0.6311 0.5113	1.2165 5.626- 5.6616 4.4626	-r.::1=1 -r.::10= -0.::157	0.0525	-0-0003	0-S6##_			
7.62 8.63 9.65 16.76 11.77 12.65	0.3	0.5111	Getel- Cebblo Gethen	-F.iilon - <u>-C.iilon</u>	7.5-04					
8.63 9.65 11.76 11.77	0.3	0.511 0.5113	ne then	20_467_			0.7765	0.1778	0.0957	2.2503
16.7A 11.77 12.65	4-U	2-5-11		0144		_0.000a			0.1003	2-0452
11.71 12.65 _	6.0				0.9550	0.0001	0.2045	0.1856	0-0929	1.9205
12.65 _		( T				-1-0041	1-2472	0.1915	0.0958	1.7706
	. Li. a u		1.10-6			-0.0004	6.2915	6.1966	0.0948	1.6727
	0.0		1.0540	-v.0.75		-0.0007 -0.0014	n.2447	2017. 0.2109	0.0915_ 0.0838	1.5162
19.91	C N						0.2934		-0-0754	104714
15.44	6.0	101216	1	6.0664		-0.0004	0.7927	0.22.0	0.0668	1.4100
17.44		1.120	1.513/				J-2044	0.2348	0.4557	1.3491
14-05	b . u	1.725.	_	•			0.2750		0.0463	1.3054
19-15_										
50.56	C.0	1.473#	1.7335	0.0209	-0.0075	-0.0000	0.2722	0.2460	0.0505	1.1762
				•						
				-	<del></del>	•				
						<del></del>				*
1	A.05	9-15 C-4	A.09 b.b 1.7254 9-15 C.u 1.3346	A-09 U-U 1-7254 1-549/ 9-15 C-U 1-3346 1-5614	6.05 0.0 1.7254 1.7254 -0.0047 9.15 0.0 1.3346 1.0614	6.05 0.0 1.7254 1.547 -0.0047 C.0341 9.15 C.0 1.3346 1.6614 0.0041 1.0114 9.0000 -0.0075	9-15 Cou 1-725- 1-746-0-0-25 (0.07) -0.0005 9-15 Cou 1-3346 1-061a	9-15 C-U 1-725- 1-547 -0-0-2 C-071 -0-0005 0-2556 9-15 C-U 1-3346 1-6616	9-15 C.U 1.725-0 1.5450 -0.00-2	0.0463 0.2374 0.00 0.0039 0.0039 0.2374 0.2374 0.0463 0.04 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.0395 0.039

➣
m
O
റ
٠
$\mathbf{z}$
•
2
Ģ
-
~
ចា

	IESI. 2		ALM.ÄILU-E 57 4.3			. 0 Ut	t off 1DELS. i	UFF OFF			. —————————
٩T		PF TA	C+-	Ct 7	CT	CL.	CLL	CA	CAH	CAF	ACP
	-1-71	<u> </u>	- Fedurate					0.2344	C-1431	0.0313	2.3393
	-1.01	U . ··	## 1] = 4		F406.1-	1.03.5		4.2320	C.1357	0.0956	0.7540
	0_3r	<u> </u>					_=f.0019 -0.0015	0.6345	C.1356 C.1405	0.0450	-1.7867. -2.2413
	2.48	0.2							_£.1500 .	. 0.0E18	2.4435
_	3. et	(,,,	1.15				-0.0053	j. 2443	U-1531	0.0512	2.5385
	4.53	lin i					=1-0024	1.2643	u-1661	0.E832	2.5735
	4.45	4.0	(-6247	•-35.			-0.6017	v. 2504	U-1700	0.0056	7.4877
	601_				ـ ـ 1 أ ـ نامنعـــ						_ 2,3670
	7.50	0.0	0. 1777		-2.0675	0.0517	-9.0025	0.2713	0.1799	0.0913	2.1868
	H.7.			حدلعمنا	وولاد بكملاحد	6.25.2_		_0.2767_	3.1841	0.0425	2.0963
	9.7r	0.0	0.51 1	11.4754	-4.0057	1.04.7	-).7031	3.2704	U-1-72	0.0917	1.9130
			Labert				minf 1132		1933	0.0842	1.7862
1	11.24	U . u	1.5772		-0.612-	(.03-1		0.5825	0.1784	0.0568	1.6733
	-4×-51-				_حدىدموح_			283 <i>L</i>	0.2046 .	. 0.0141.	-1-6006
	14.72	4.0	33.4		-6.0000	t-0757	-0-0015	0.2440	0.5105	0.0756	1.5304
<u>-</u>	<u> 15.14.</u>	<u> </u>						0 <u>~2629</u> _		0.0658	_1-4803
	14.15	0.0	1.'31-	1.471.	006135 006135		-0.0615 -3.0311	0.2814	0.2759 	0.0500	1.4256 
	15.66	0.0	1.24~=	1.012-	(-611-		-0.0000	5.2755	J. 2372	0.4344	1.2911
l	19.36		1.3761	Latitya	6-51/9		-1.0000	692ملا		- 0-0274	1.2240
?	20.44	0.0	1.5.10	1.7062	7.0765		-9.0063	9.2626	0.2457	0.0169	1-1741
		i- · · · · ·									
			_ <del></del>				<del></del>	<del></del> -	·_		

	. <u>. 1ESI</u> .		SY 4.4			•0 UF		OFF OFF			
01~1	ALPHA	PF 14	CA.	CLM	CY	CLA	CLL	CA	CAR	CAF	ж¢Р
	-0.67	- U - U	-0.41/3	-0	61. 46	v.u.77m	-0.0030	1.5241 0.5350	0.1353	0.0534	2.019? 0.4827
<u>.</u>	2_3d		0.u32c_					4.2317		-0.0944-	2-3456
•	1.43	0.0	0.0000		-0.0033	0.03-1	-0.0634	0.2335	0.1529	0.0807	2.1951
<u>,                                    </u>		D.U	0-1054		-3.0.35 -3.0.37		<b>alug_ag</b> q_ Elga _e v=	0.2473 0.2473	_0-1601 0-1645	<b>Q.Q774</b> 0.U775	2.4412
_ <u>``</u>	حدمه	<u> </u>	5-24-15-				-0.0033	0.2477	3.1670	0.0407	2.5606
b	5.03	U.U	(	'1 = 0 = U0	-4.6.25	(+0412	-0-0236	0.7551	0.1705	0.0545	2.4221
٠.	6.60		حديدء		. كەنسىنى		2-0032	0.2631_	_0-1772_	-0.0800-	_2,3997
19	7.12	0.U	0.4774 	35. 	-,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		-0.0032 	0 • 2448 <u>4 • 2</u> 734	0.1514 0.1853	0.0045	2.2098 
15	¥.64	C.U	(	C. 7771			-0.003s	0.2771	0.1935	0.7546	1.9122
13_	15.58	ب أُ مُكِ			- History		0.027		6-1944	0.0=50	1.7699
1.	11.4/	0.0	Cone y	1-13-0	-0.3065		-0.0031	6.2412	0.1994	0.0414	1.6632
<u> </u>	- land	Cal	<u>Calely</u>					<del>0.281</del> 4		0.0743	1.6094
16	14.12 <del>15.21</del> -	<b>6.0</b>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1 • 11 0 ··	(.0(∋1 u_0_1_	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-0.0025		u.2115 0.2205_	0.0590 	1.5247 
16	14.24	6.3	1.0555	1.4744	9.2127		-0.0012	6.2768	0.2272	0.0496	1.3971
14-	17.34		1.1450	1.2010				1.2756		0.0413	1,3351
2" 21	14.43 14.55	G a K	1.27~#	1.0310	7.0134		-0.0012	0.2705	0.2390	0.0315	1.2761
25 	20.65	0.0	<u> </u>	<del>1-7444</del> 1-1040	<u> </u>	-0-0253 -0-0451	-0.0017	<del></del>	- 6645.0 9845.0	-0.0062	1.1502
										41000	
			····			<u> </u>		<del></del>			
						<del></del>	<del></del>				

	IESI_ '		ALM RILUM 54 0.3		. CuhF		0 0		TRANSIII FIXEO		
THEO	ALPHA =1.51	eFT-	C'1	CL «	CV ===1:56	CLN	CLL	CA	CAB	CAF	ACP
5	-0.60	<del></del>	-C.UMJD	0-1101	-6.170v		0.0144	<del>0.5572</del> 0.5907	0 <u>.0877</u> 0.0359		-1.2753 -1.3671
_3	C_3B	Late			-uel-el-		40100	_0.5395_	_0.078b		-0.9536
•	1.42	0.0			+0 • 11 u z		0.0053	3.5308	0.6772		-1.3992
<del></del> -	3.3t	<u> </u>			-0-1177			<del>) - 5306</del>	G_0766		-1-3752
7	3.3c	6.6			-4-1-7-		0.0017	0.5334 	0.0792 		-1.5368 -1.4758
b	5.39	Ç.5	4.6455		-(.0000		0.0035	0.4817	0.0550		-1.5512
_9	-6.41	0.4	0-70-7	-1-2374	. ma_uell	-6-0021	0.0046		_ 3-9876	-	-1-6261
16	7.41	0.0					0.0151	0.4977	0-0951		-1-6736
<del>11</del>	<u> </u>				- LaColes		0-0001	0.4851	6-1000		-1-7719
12	10-61	_ N ~ J			-6.0-37		9-01-2	0.4061	0-1005 		-1.7210
1.	11.4¢	6.0			-0-0-7-		0.0051	U. 40F4	0.1150		-1.7921
15	12.44	4.4			-0-0002		0-0071		-C-1310		-1-7943
10	13.45	C . L			-0.0-30		0.01+3	3.4647	6-1333		-1.7904
17	15.44	0-v			-:		2-0450	0.4773	0.1371		-1-6131
15	16.00	6-4			-)A4-		-0.0016	0.003	0-1506		-1.8196 -1.7776
54.	17.47	U. v		+5		-0.1443	0.0193	u-4601	v-1656		-1.7577
.21	16.51	0.1			-1-31-7		0.00-7	0.4629	u-1724		-1-7702
25	19.47	0-0	3.7100	-5.7164	0.0003	-0.2575	0.0016	7.4467	0.1753	C.2714	-1.7246

7 PMA	PETA POUR LOU LOU LOU LOU LOU LOU LOU LOU	C.E.	0.0 m3	Cn) 4 4444 4 4444 5 4444	/CPF1	7CPF1 3.9944 4.9945 3.9993 5.9944	C'-F2 =0.0510 0.0010 	CH2 =0.0134 =0.0017	Cd2 =0.0340 =0.046d =0.0525 0.0079	0.0302	-29.4465 
	P-0 1-3 0-0 0-4 (-6 1-4 (-0 1-3	\$. 44 44 \$.	0.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.	4.444 4.444 4.444 4.444 4.444	6.64-4 6.64-4 6.64-4 6.64-4	9.9949 9.9949 9.9949	0.0016 0.0016 0.0114 0.0352	-0.0717 0.0005 0.0011	-0.0340 6040.0- 2540.0- 0700.0	0-2603 -1.0453 -0-0461 0-0302	-29.4465 4.6256 0.1998
3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3	1.0 1.0 1.0 1.0 1.0 1.0	\$, 4747 \$, 4444 \$, 4447 \$, 4447 \$, 4447 \$, 4447	0,0444 0,1644 3,5444 4,4454 4,4454	4.444 4.444 4.444 4.444 4.444 4.444	6.9944 6.9444 6.9444 6.9444	6.6644 9.6644 9.6644	0.0016 	-0.0017 6.0005 0.0011	-0.0525 -0.0525	-1.0453 -0.0441 0.0302	-29.4465 
1.42 1.40 1.40 1.30 1.41 1.41	1.0 1.0 1.0 1.0 1.0 1.0	G. 4444 G. 4444 G. 4444 G. 4444 G. 4444 G. 4444	0°0444 4°2634 6°1646 3°2434 4°2446	4.444 4.444 4.444	. 3.4444 . 3.4444 . 4.4444	5.9995 ELEG.	0.0352 0.0357	0.00u5 0.0011	0.0079	0.0302	0.1998
1. 10 1. 10 1. 30 1. 37 1. 41 1. 47	(.u (.u (.u (.u (.u	\$,444 \$,444 \$,444 \$,444 \$,444	0.0444 4.4644 6.4444 7.4644 1.46444	**************************************	4.4544 4.4544	_ Eve 9	0.0947.				
3-10 3-3r 3-3y 3-41 7-41	[.u [.u [.u [.u]	\$,4447 \$,4947 \$,4947	4,1444 4,444 4,444	4-444	4.4544			0.6079	-0 0343	4654 4	
7.41 7.42	(.u (.u (.)	9.4947 9.4947	9,5594	4-6444		4.4444					-0.2564
7.41 7.41 7.42	(.U U.2 U.6	4.49.7 	4,444			4.46-4	0-1441	0.6188	-0.0043 -0.0258	0.1303	
7.41 7.47	0.6	5.29.7.7			4.4444	7.5449	0.2254	0.0273	0.0261	0.1213	
•••		9.4446		. 4.4777	_	_2.6924_					- 0-1955
•••	6.6	70 . 77 7	4.4444	7.5544	4.44.4	4.00.44	0.3626	0.0469	0.0775	0.1350	0.2137
		9.4444	7. YYY 7			_9999_مك_	0.4310		0.0563_	_0.12=1	
	0.0	9.5944	7. 7747	7.7477	4.4440	4.0090	(.4354	0.0455	0.1716	0.1068	
l a 3	U . U	7.4444	4.4344 4.4344	A*0440	<u> </u>	4.6644	0.5590	L.JORG	0_137A_	<u>01038</u>	
2.42	Cay	5 5444	5.777¥	4.9544		_ y-9449_		0.4691	0.1325	0.1233 4.1150 -	
3.45		4.444	9.0094	7.777	4.44.4	3.00,0	V.C458	C. 0758			
	4.4	0.4444	3.4944	4.3440	_ V. 93.19_	6.6469	0.7.77	0.0769	0.1810	0.1006	
5.44	6.0	0. 14.4	,	7.444	وا پ د وا و و	7.9979	0.7640	0.0436	0.1976	0.1097	
	<del></del>			-							···
33-	6.0	-		_							
				_	_						
***	<b>V.V</b>	7.14.77	******		76		7.72-0	0.0713	0.20.3	V.077E	. 0.3107
		=	F22		-	•				•	
			<del></del>								
				<del>-</del>							
	•										
										400	
					•						
1 5 E	•44 •44 •67 •51	•• 6.0 •• 7 6.0 •51 4.0	44 6.0 9.79.99 44 1.0 9.79.79 45 1.0 9.79.79 51 0.0 9.79.79 47 0.0 9.79.79	-44 (0.0 Q1444 3.4444 -44 (0.0 Q1444 41444 -44 (1.0 Q1444 41444 -47 (0.0 Q1444 91444 -51 (0.0 Q1444 91444 -67 (0.0 Q1444 91444	-44 (10 Q-444 3-444 4-3449 -44 (10 Q-444 4-4344 4-4444 -44 (10 Q-4444 4-4444 4-4444 -47 (10 Q-4444 4-4444 4-4444 -51 (10 Q-4444 9-4444 4-4444 -51 (10 Q-4444 9-4444 4-4444 -51 (10 Q-4444 9-4444 4-4444	-4 (10 Q.144 Y.434 Y.444	-4 0.0 0.1040 3.4900 9.3440 5.6946 9.6969  -44 0.0 0.1040 9.4947 9.6969 9.6949  -4 1.0 0.0047 9.6969 9.4949 9.6969  -51 0.0 9.6967 9.6969 9.6969 9.6969  -67 0.0 9.6967 9.6969 9.6969 9.6969	44 f. 0 0.14.4 y. 43.4	44 f. 0 Q. 14.4 Y. 13.4 Y. 14.4 Y. 13.4 Y. 14.4 Y. 14.	44 f. 0 Q. 1444 Y. 144	44 C.U Q.444 Y.4344 Y.4444 Y.4

	<del> </del>	IESI		AC- RE1 -		<u></u>	. L UEL	DELZ		TRANSIT			
-1.6	0151		1500				·					XCDEA	YCPF 4
3 0.38	_	-					_Calbab_			_	-		
\$ 1.42 0.0	2	_											-1.7711
5 2.48	_3									_			
## 3.3e	•												-0.8777
7	-												0.4320
# 5.37 0.0	<u>.                                    </u>		_		-		_						0.4320
## 5.41	H								•				0.340R
11	4												
12	10	7.41	0.0	il	-0.2001	-(-1779	9.3461	7.1-32	0-4076	0.0525	9.1007	0.1258	0.2469
15 16-41											0.1866		
1= 11.02													0.4384
15 12-49 Unu =0.1074 = 0.0344 = 0.2047			20 200	10.00		5200 DOM:	100000000000000000000000000000000000000	THE RESERVE OF THE PARTY OF THE					- 1854-0
15 13.45 C.U =0.1151 = C.0355 = -0.1977 C.3370 1.7374 0.6616 0.0496 0.2961 0.0774 0.661 17 14.45 0.U =C.0777 =1.4216 0.1279 0.2652 =1.6060 0.7412 0.0962 0.3546 0.1298 0.61 18 15.46 0.U =C.0777 =1.4216 0.1279 0.2652 =1.6060 0.7412 0.0962 0.3546 0.1298 0.61 18 15.46 0.U =C.0757 =0.0375 = C.3960 1.5867 0.7975 0.3877 0.3272 0.1125 0.61 18 15.46 0.U =C.0757 =0.0367 0.2648 1.2969 0.6718 0.0460 0.3553 0.1067 0.6 20 17.47 (.U =C.01277 =0.0462 1.1753 0.3567 =1.4860 0.6655 0.0934 0.3462 0.1055 0.4 21 18.51 0.1 =0.0567 0.0367 0.0367 0.0368 0.3805 0.1036 0.36										-			
17 14-3 0-4 -0-07/7 -1-1214 0-1274 0-2542 -1-6040 0-7412 0-0962 0-3546 0-1298 0-41 1- 15-44 0-0 -0-0644 0-0945 -0-0945 0-3440 1-5867 0-7975 0-3877 0-3272 0-1125 0-4 1- 15-45 0-4 -5-755 -0-174 -0-69-1 0-22-4 1-2969 0-8218 0-861 0-3553 0-1047 0-4 20 17-47 (-0 -0-17-7 -0-042 1-1-53 0-3547 -1-4800 0-8655 0-934 0-3642 0-1055 0-4 21 18-51 0-1 -0-0567 0-3347 (-1353 -0-5315 0-9527 0-965 0-3845 0-1034 0-3647													0.4617
1- 15.44		-											0.4783
20 17.47 (.0 -0.17-7 -0.042 0.1-53 0.35-7 -1.48-0 0.6455 0.0934 0.3442 0.1055 0.4 21 18-51 0-1 -0.055 -0.0567 0.0347 (.1333 -0.5315 0.5527 0.0985 0.3805 0.1034 0.30	1-		15 12 13 13 13										0.4103
21 19.51 O.J	1.	15.00	Hall	-577:			11.22.14	1.2969	C-821H	Califal	0.3553	0.1067	0.4324
	-	-											0.4113
22 19.47 0.0 -7.129F -7.0423 0.2371 0.3262 -1.8296 0.9935 0.0928 0.3766 0.0944 0.36													0.3994
	52	19.47	0.0	-7-1275	-4.0423	6.2371	0.3262	-1.8296	0.9435	0.0928	0.3766	0.0944	0.3849
<u> </u>	-							<del></del>					
							<del></del>	<del></del> -					
	<del></del>											·	<del></del>
								-					
						_							

	JE51_ ?		ermintini Pa ()••		<u> </u>		1 PEL2	EL3.LUELA	TRANSITI FIRE		
7.111.7	ALPHA	rE TA	<u> </u>	CL4		CLN	CLL		CAH	CAF	ACP
	-1.61					ti3cti		U 740	V-1167		-1.6734
2	-0.46	4.0					-0.0247	4.4474	0.1115		-2.8307
<del></del>	1.42							(.4710	0.1044		-1.4583
-	2.44	(rau		F-10933C.					-0-057#		-1.4629
	3.41	ť. L		· `• o .			-4.02-0	0649	0-0-7y		-1.3889
7		1.25						3-45-0	0.047a		=1.4945
6	5.40	C	3.57 1-	-1. 001	-1.00-5		-0.0355	104527	Ua 942		-1.5733
	6,43	_ن من	-Lat-11	-100026	_=:abscl.	TEXT	-u-0315 -	C.+5Z+	. C. 3943	0.3632	
10	7.45	4.0		-1535			-0.5346	0.4434	0-1001	0.3437	-1.7004
4	-5-41	L <u></u>					-5-654-			_0.3099_	
12	9.46	0.4		-6.6201			-0-0342	0-4191	C-1100		-1.7791
13_	_كهمسل_	-C						u127	-C-116s	-	-1-8263
14	11.44	0.0		-ih/c				0144	9-1264		-1.8276
15 -	11.00	U. U		-1.4707				- 4- <b>-055</b>	-6-1303 1319		-1.8474
12	10000	404		_ =3.=ala_					-4-1419		_=1.8593
10	15.46	()		1+7				0.4.36	0.1479		-1.8795
14	15.51		2.41.		(574	-5-63-2	=0.0397	5500.0	4-1567		-1-8912
51	17.47	0.0	7.44-3	-5. 444		-1.01+2	-3.32-4	3.4059	0.1661	0.2409	-1.8911
21	18.45	6.4		<u>-5.56</u> %3_				0.0030	_C-1741_	-0.230A	1.8668
2ć	14.47	0.0	3-1++1	-5.4265	ーにっぱりつア	0.0745	-0.0157	0099	t.1810	0.2289	-1.8704

	lESI.	FAST	ALE_RAlue6	rnl	CUSE	L VELI	DEL2	DEL DEL	A IPANSIT	I DN		
	5	24 v.	D-4	).0 m	3-0f15 3.	. 0	0	0	O FIXE	D		
DINT	ALWAA	re TA	CLET	C-1	CHI	ACPF 1	YCPF 1	C+F2	CHS	Cas	XCPF 2	YCPF2
	-1-61	_لا _لا	و فقط و	<u> </u>	4.4444	7.9476	4,9999	-a-uala	-6,u116	-0-1116	0.2862	2.6804
2		U . U	4.4444	4	4.4444	6.4346	4.09.3	-3.6144	-0.0136	-0.0A2A	0.9113	5.5315
		0_0	<u> </u>	- KKEKOM -	v-y-y-y-y-y-	-8-8848	-4-3344		ESQ.0.23	-0-5841 -		4.5705
<u> </u>	1.02	0.0	6,4546		وووني. معدد م	4.99-4	9.9999	0.u5h3	0.0068	-0.6577	0.1161	-0.9897
6	2-+4 31	0.0	<u> </u>	7. 7777	4.9494 4.9494		6.664¢ 	<del>0-4-21</del> 9-1347	- 0.0062 - 0.0131		0.0977	0.4549 -0.2283
<u>"</u>		C_U	4.4444		4-4444	5 6000	9.00-0	U-1865	0-0131 u_0202	-9.9306	0.0977	
5	2,00	0.0	6.7977	4.444	7.5754	7.04-9	4.9477	v.2370	0.0752	0.0	0.1062	0.0
<u> </u>	0-43	£-01	9. 4644	4. 4444	- X- X X X X X .		y 9944	_ 502362			_ 0.1099	0.0804
10	7.45	0.0	6.6444	7.5444	4.9	4.4466	4.9449	0.3522	0.0343	1.0545	0-1117	0.1548
ц	- Baal	4-6	<u> </u>		4-3444	2.99:5	A-3322		49479-	C-0641_	-201162	0.1559
12	4.00	ō.u	404640	4-4444	4.9444	4.4344	9.9944	0.4653	0.0495	0.1110	7-1062	0.2361
13	حعمب			4-444	**4444		4.0050	<u> </u>	0-2008	0.1044	0-1134	- 0-2020
14	114	4041	4.64.44	4.6444	4.444	4.04-4	4.9449	0-540-	0.0540	0-1420	0.1031	0.2446
16		0 . J	7.7777	A*****	<u> </u>	9.59x <u>x</u>	4.9943	0.7109	G_0573_ U.0773		D_1436	0.2376
17	19.96	0.0		ילצר אל		9.49.4	4.9949	0.7521	-0.0775	0.1669 	0-1096	0.2382
l H	14.06	0."	4,77.0	4. 7777	4.6357	7.,9.4	4.94.9	0.4233	5640.0	0.1425	0.1083	0.2216
1-	16.51	6.4		4.4444	7.4444	5 66 6	V.9444	(Legal)	0.0063	0.2225	0-0393	0-2560
Sc	17.44	0.0	~, ~, ~, ~	44-	7.3747	4.54+4	4.9944	0.4275	3.4474	0.2374	0.0+47	0.2560
21	1-40	الما الما	4.44.44	+++++	4-6-6-4		9.30-0		0.0885_	0.2519	D-0916.	0.2607
55	1 → • • 7	0.0	**99**	4	4.4444	9.9999	9.9999	4.9945	u.0872	9.2466	0.0877	0.2502
			•									
							<del></del>					
	<del></del>				<u></u>				·	·		

10 11.00 0.0 -1.677301 -0.0000 5.6611 0.0000 0.6144 0.0702 0.3014 0.1143 0.0000 15 12.60 0.0 -0.2000 -0.4141 0.0000 0.6144 0.0702 0.3014 0.1143 0.0000 15 12.60 0.0 -0.2000 -0.4141 0.0000 0.6830 0.6681 0.0732 0.2866 0.1060 0.4194 15 13.60 0.0 -0.50007 -0.1070 0.3783 2.8412 0.7307 0.0749 0.3107 0.1020 0.4232 17 16.60 0.0 -0.1077 -0.1070 0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000 -0.6000		Ė		57 C.4		3-vF15 0.		0 0	DEL3 DEL	o Fixed		<del></del>	
2 -0NU Nob -0Not -0	THIC	_								-			· •
3	<del></del>												
5 2-00 0.4	_ <u>ā</u>		-	_=10-4515_		in2542_		4.5215_				0.0571_	
0	•	-					-						
7													
### 5-40	7										_		
10 7.45 J.U -7.1 27 -0.0457 -0.2031 U.4476 1.9871 U.3937 U.7456 0.1992 0.1158 0.5061 11 0.1 0.0 0.0000 -1.20 0.2036 0.2727 0.3828 0.4526 0.0563 0.1473 0.1199 0.4368 12 -9.42 U.U -0.0467 -0.0204 U.0012 0.3557 -0.4779 0.5050 0.0563 0.2256 0.1085 0.4484 14 10.45 0.0 -7.0727 -0.032 0.0000 0.4611 0.0004 0.6144 U.0702 0.3014 0.1143 0.4904 15 12.46 0.0 -7.0727 -0.032 0.0000 0.4611 0.0004 0.6144 U.0702 0.3014 0.1143 0.4904 15 13.46 0.0 -7.0727 -0.320 0.0000 0.3740 0.0004 0.6144 U.0702 0.3014 0.1143 0.4904 16 13.46 0.0 -7.0727 -0.320 0.0000 0.3740 0.0004 0.6144 0.0732 0.2886 0.1064 0.4194 17 16.46 0.0 -7.0727 -0.0707 0.3010 0.3010 0.0732 0.3010 0.1020 0.4232 17 16.46 0.0 -7.0727 0.0707 0.0707 0.0707 0.3775 0.0709 0.3107 0.1020 0.4232 18 16.46 0.0 -7.072 0.0707 0.0707 0.0707 0.0707 0.3775 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0707 0.0	0		6.3										
11 8-1 0-6 70-1-70 -0-120 0-0-12 0-3557 -0-4779 0-5050 0-0-8 0-2754 0-1085 0-4484 12 -0-0-2 0-0 -0-0-7 -0-0-204 0-0-12 0-3557 -0-4779 0-5050 0-0-8 0-2754 0-1085 0-4484 13 16-5 6-0 -0-12 -0-13 -0-0-23 0-2754 -4-121 0-0-705 0-654 0-247 0-1142 0-4340 14 11-0-0 0-0 -0-0-7 -0-0-13 -0-0-000 0-6-611 0-0-0-6 0-6144 0-0-702 0-3014 0-1143 0-4904 15 12-4-0 0-0 -0-0-24 -0-0-13 -0-0-000 0-3-14 0-0-13 0-0-0-14 0-0-143 0-4904 16 13-4-0 0-0 -0-0-24 -0-0-13 0-0-0-0 0-6-611 0-0-0-6 0-6-14 0-0-702 0-3014 0-1143 0-4904 17 14-0-0 0-0 -0-0-13 -0-0-10-10 0-3-14 0-6-14 0-0-143 0-0-143 0-0-123 0-0-123 1-14-14 0-0-0-0-14 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0-143 0-0		-											
12	_	_											
14 16.65 (.0 = 1.5 = 1.5 = 0.0000			-				-						
10 11.00 0.0 -0.07750.0000 0.6011 0.0000 0.6144 0.0702 0.3014 0.1143 0.4906 15 12.46 0.0 -0.2240 -0.4347 0.0608 0.3740 -0.4580 0.6681 0.6732 0.2686 0.1060 0.4194 16 13.40 0.0 -0.0777 -0.0217 -0.1679 0.3723 2.8412 0.7342 0.0749 0.3107 0.1020 0.4232 17 16.46 0.0 -0.0775 -0.0127 -0.0220 0.2425 0.2621 0.7425 0.0879 0.3736 0.1123 0.4775 18 15.46 0.0 -0.0627 -0.0129 0.2445 0.947 0.0349 0.0752 0.3513 0.1015 0.4188 19 14.51 0.0 -0.0775 -0.024 0.2745 0.94723 0.6417 0.3728 0.0336 0.4232 20 17.47 0.0 -0.021 -0.012 0.2745 0.2744 0.1890 0.9401 0.0476 0.3988 0.0322 0.4221 21 14.46 0.0 -0.0702 -0.0212 -0.0735 0.2744 2.1769 0.9401 0.0476 0.3988 0.0329 0.4888	1		_										· -
16 13.44 0.0 -5.5577 -0.1217 -5.1575	1+	11.44	U. 0	-1.1-71	- • • • • •	-0.0006						0.1143	
17	15.												U.S. C.
10 15.40 CoU =0.050 =0.050 =0.0592 (.2545 0.9447 0.0389 0.0552 0.3513 0.1015 0.4188 19 14.51 (.0 =0.775 =0.284 =0.2124 (.3142 2.7359 0.4723 0.4817 0.3728 0.0936 0.4274 70 17.47 0.0728 0.0936 0.0936 0.4274 70 17.47 0.0708 0.0938 0.0938 0.0932 0.4221 70 14.45 0.0 =0.00 =0.00 =0.00 =0.00 0.00 0.00	_												
19 14-51 6-0 =2-7/5 =1-244 =1-2/26 6-3142 2-7359 0-4723 0-6817 0-3728 0-0936 0-6828 70 17-47 0-0 =1-10 104 -0-0735 0-2744 1-1890 0-9401 0-0476 0-9468 0-0932 0-4228 21 14-44 0-0 =1-752 =1-2/3 -1-1559 (-74/4 2-1769 1-6048 0-0936 0-4040 0-0929 0-4040			_			-							
21 1Haa4 Ual -1-1702 -Carely -lateby (-24/4 201704 latitud 0.0936 0.4040 0.0929 0.4640	19	14-31	6.0	-: 71:	-1	-:-2124							-
		-											
SE 14-01 0-0 -0-1419 -0-1722 -0-0724 0-1411 0-2405 110301 0-0000 0-04051									- :::::::::::::::::::::::::::::::::::::				
	~ ~	17.41	1.00	= 1,5 1,7 %		-0.0357	3-3-17	0.3405	110381	0.0000	0.4140	0.00-0	0.4027
		19.47	n.u	-7-7470	-0-4333	-0.0357	J-3417	5.3982	1.0381	0.0880	0.4140	0.0848	0.4027

	1 OF 3					-A-11- ×	ISSILE TA	IL EFFECTS	OATA		<del></del>	
	IESI	PAUL -L						UEL3. DELA				
-	2	27 0.5	y j.7	J.V n	Bauf 15 U.		Ω 0	0, 0	F PFIAEC			<i>i</i>
INT	ALPHA	ofT-	C~	CLu	CY	CLN	CLL	CA	C 49	CAF	KCP .	,
1	<u>-) -i</u>		795		-1-1-1-3				4-1321		_el_7645	
5	-11.50	0.0	ole /r	-0-00-4		1.6650	-0.0746	0.3414	6.0606		-0.3012	
<del>-</del>	1.41	6.0		_ <u>-54.6.42</u> 			0 <u>0</u>	0.3769 0.3797	. G-0931. U-093U	_AEBS.Q_	-1.3497	<del></del>
5	2.05	U. 5		-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1			-0-00-4				_=1.3788	
6	3	11 . U		-(-1)36			-0.0565	G.3754	6.0941		-1.3831	
7	قعمف	ll a b		-4-6755			-0-0H2		0.1305		-1-5204	
۲	5.45	U . 10	.121e	+1-1006	-11 - 6 - 11 -	3.0357	-0.5629	0. 1697	0.5947		-1.6005	
ـــ جـ	سند و حفظ	<u> </u>					u-0618		4-5997		-1.6600	
l v	7.43	0.0		-1./654			-0.0705	6.3776	0.1056		-1.7155	
11	8.9.7	to u			_=2.2642.			3702		0.2596		<del></del>
14	7.46	0.0		-2.1344		-	-0.0649	6.3764	0.1163		-1.8009	
14	11.56	0.0		-1171		10000	-0.0605	0.3715	0.1217		-1.8323	
15	12.41	U.V		-30.271			-0.Cn23	2-3624	_0.1369		-1.6916	
16	13.51	f U		-3.55.5			-0.0868	U.3543	6.1406		-1.8502	
17 _	14427	_ U . U		THE RESERVE AND THE PARTY OF TH	u_u122		-4-2866	u.355b			-1.8584	
10	15.09	G. U		-4.367-		Pourin	-4.97-6	0.3446	0.1522		-1.6579	
19	10.45	0.0	2.52-1	1931		Cablia	-0-0564	0-3-17	1-1641	6-1676	-1.87A5	
75	17.75	Ú. L		-5-1140	성급하면 하고 하는데 및 모이네		-0.06-4	*.3525	0.1574		-1.6757	
21_	151	0.4		-20175			-u-0613	0.3509	0.1741 -		-1-6721	
26	19.51	6.0	3.0015	->-1421	-3.0756	6.07.55	-0.0456	V.3507	3.1817	0.1690	-1.8599	
											····	
		_										
_	-						=					
				•								
	~			<del></del>	<del></del>							
- 3								<del></del>				

-1 -0	PHA				3.0f15 0.	•0	0	0	A THANSIT			
=0		METM	C··F1	C-1	CHI	ACPF1	YCPF 1	Crof 2	CHS	C45	HCPF2	VCPF2
	1.5e	C.U	0.444	7.7.79		<u> </u>	4.9546 6.6646	7.0239	-0-UCA7	-0.0479	-0.5518 -0.1650	-9-1044
		0.0		VVVVV		9999	7.6576		_=4.4015			1-7593
_	1.41	0.0	4.4077	Y-7777	ب و پ با ن ي	7.4479	9.9999	0.0977	0.0073	-0.05-5	0-0748	-0.5986
	2.42	0.4	_9.55.22_	<u> </u>	_FREEE ET	9,9555	_9_999y_	0.1379		-0-0FOR		_=0-4412
	1.44	0.0	6-4644	7.444 3.444	4.4644	4.40.4	4.9999	0.1A72	0.0230	-0.0453	0-1230	-0.25 <b>8</b> 1
	2.45	0.0	6.4440	6, 77	7. YYY 7	A-464A	6.0044	0.2763	0.0311	-0.0045	G-1125	-0.6161
	5.02	0.4	4 4964	9.4443	verest_	4.66.4	-	4-3-66		_0.0214_		0.0606
, 1	7.43	0.0	9.9444	4.444	4.4499	4.49.4	9.9940	0349	0.0518	6.6419	0.1276	0.1035
	B.47	C.4	4-4644 -				- W-9999	0.4557_	0.0536	0.08ul_	_0.1175	0.1758
	9.46	0.0	4.6394	7. ~ 574	4.6.4.4	4.46.6	4.6444	0.513.	0.0581	0.1001	0.1131	0.1949
	-	<del></del>	<u> </u>		4-6464	C GAAG	9 96-9	-3-553	0.0604	0-1165	-0-1047	0.2034
_	1.50 2.42	( . 0 	4.444	4. 7494 <u>Live</u>		<del>/ / / / / / / / / / / / / / / / / / </del>		0.6366 3.6898	0.0706 <b>0.0765</b> _	3.1279	9.1119	0-2028
	3.51	C. U	4.4.44	7.4771	4.5179	7.54-9	4.0410	U.7641		5.1722	0.1113	0-2224
		Hall					<u> </u>	0.6142_	0.6860			
15	5.49	C-6	6.4512	44	4-4446	4.4444	4.9949	0.F546	0.0544	0.2106	0.1047	0.2467
	<u> </u>	ا ما		7.7477	4-44-	3.40.0	4.6036	3-4145	0.5421	J.2270	0-1507	0.2483
	7.55	0.0	4.46.4	4.4444	7.4144	9.4944	4.4444	U.973F	0.3901	9545.0	0.0926	0.2491
	5.51 9.51	<u> </u>	6.0444 6.4644	4. 7777	4.4544	<u> </u>	9.9999	1.0503	0.0879	. 88 <i>0</i> 5.0	0.0921_ 0.0837	0.2436 0.2514
								1.0503	040017		0.0031	***************************************
	<del></del>											
		-							• •			
						•=						

		<del></del>										<del></del>
							1 DELZ					
	5	27 0.	5y 0.7	0.0	3+0+15 0	<b>+</b> 0	0 0	0	o FIXE	•		
GINT	ALPHE	₽F TA	C1:F 3	Cm)	C-3	XCPF 3	YCPF 3	CNF4	CH4	Cu4	XCPF4	YCPF4
1	-1.61	2-4	Ph. 114-3	-0-2335	-1.41114	1.3472	0.0100	-0-0150	-0-2113	-0-0235	0.7502	1,5618
5	-0-76	0 • U	-0. 4-7	-037-	0.0374	0.30.7	-0.4273	0-0029	-0.6006	0.0238	-2.9487	8.1541
. 3		<u> </u>		-0-4422		_ #-3ncs.		-0-4550	0.0002.		0.0033 _	_ 0-1517
•	1.41	0.0	-0.1014 -(.11a1	-0-64n.	0.0765		-0.7550	0.0H56	6.0043	0.0364	0.0502	0.4489
-	<del>2.</del> *<	<del>!</del> UU	-(allal	-0.13fx				D-1341		Q.Q&¥1_ 0.07C7	0.0996	
7	9.43	5.0		-hat-Zuz	-U. (. 355	C-2m41	0.6633	6-2335	0.0276	0.0912	0-1182	4.3906
8	5.45	17 <b>.</b> U	-5.11-5	-0-0-57	-:.0(1-	6.3-76	0.6117	6.2836	0.0334	2.1135	0.1176	9.4093
ý	5.02	<u> </u>	מעווהנים	حجوبا مناج			-0-6107	U-3361	-0-0344	0.1036	-0-1141	0-4274
11	7.43				-6.0005	0.4045	0.0643	0.3950	0.0457	0.1872	r-1158	0.4613
н	5.97	<u> </u>	-3-6755		29_us29_	0-30-1		0.6435_	24 65 02	0.1938_		0.4370
15	9.46	(· • ·)	10-3-		5.c-17	0.3775		7.5032	0.0549	0.2171	0-1091	0.4315
14	11.50	40 0 0	-111	*C++31n		1.3754				0.2341	0-1086	0.4296
15		0-7		-4.650	0-0-61			0.01nu	0.0474 <u>0.07</u> 25	0.2921 	0.1103	0.4579
10	13.51	(1.9	-1.0mml			(-24-0		0.7427	0.0758	0.3099	0.1021	0.4173
17	14_42_		-201 107		u_63v=_		-5.3196	_0.7964	-0-08-9	_0.3578_	_0.1056	_ 0-4473
3 =	15.44	5.0	-0.1035	-0311	6.11574		-0.596.	0.0444	0.1637	0.3510	0.0766	0.4133
15	10-4-	C . 41		327			0.3352	0-5160	L-CRAB	0.3401	0.0423	0-4140
51	17.55	U . U	-0-1-25		0.0515		-3.3749	0.47.33	0.0076	0.3915	0.0902	0022
<u> </u>	_لمحمد_	<u> </u>					<u>1236.</u>	<del></del>	0-00-7	-0-4118-		
55	19.51	( • 0	-0.1 146	-0.452	3.0740	6.3722	-0.53.0	1.0803	U.0844	0.4177	0.0781	0.3867
							•	10				
						<del></del>						
								-				

	<u> 1851</u> 2		<u>sem 8415-</u> 59 1-1			.0 0		DEL3DELA O O			
1.1	ALPHA	FETA	C× =0-1 191	CLA	CA C25	CL~	CLL	CA 4-3210	CAB 0-0934	CAF	ACP
ž	-:-	0.0	-0.0454	(.0354	-0.0557	n. Cn13	D.0974	0.3210	0.4924		-1.2699
<u>.                                     </u>	0.43			<u>-ual25.</u>	. alaunde.	. 25.75	_ D-0047_	3_3181	-0.094b	1455.0.	-1-4379
•	1.43	0.0		-6-5372		0.0003	0.0052	0.3197	0.0943		-1.3304
6	2.39 3.4¢	<u> </u>		-6.0075 -0.5736		U.U5:2	0.0070 0.0055		_0.0950		-1.4141
i.		0.4		- Contractor		U-6533	6.0.72	_0.3164	0-4965		-1.5429
•	5.43	v.v		-1-0561		1.0450	0.00 19	6.3147	0.0972		-1.6149
4	_خممک_	4.6		-1.304		_C-DALS_	3-0041	0.3191	0.1031		-1.6998
10	7.45			-1-0016		0.0451	6-0117	0.3177	6-1057		-1.7726
15	4.44			-20.3014		0-0463	0.0102.	- <del>0.3516</del>	<del>_0-1126</del> 0-1156		-1.824 <u>0</u> -1.8483
13	_13-51	6-6-		-4.6.22		C-0325	0.0121	0-3224	C-1765		-1-8710
14	11.50	C.U		-30,344		0.0406	0.000	9926.6	0.1325		-1.6816
15	12.5	C.v.		-3-3515		_0.03c4_	C-0082	0.3184	-0-1352-	_0.1832	-1.8459
14	13.50	6.0		-1.474		0.0500	0.0065	0.3167	0.1391		-1.6916
16	_15.53_				-0.(293		0-0095	<del>- 3045</del> -	_C-1437_		-1.8908
10	15.55	0.0		-4.1745 -4.1142		0.61.4	3-01-0	U.3127	0.1524		-1.8d02 -1.8745
20	17,50	C.V				-7.0071	3.0202	0.3043	0-16-5		-1-6709
21	گذمها	U a U		-5-4347		0.01×3_		0-3035	0-1760 -		+1-8705
?2	19.60	0.0	3.1150	-5.75>7	-0.0034	-11-03-4	0.0233	0.3044	0.1868	0-1176	-3.8478
				<del>-</del>							
						-		-			

-0.5	NT ALUMA	Not   Aluma
-0.00	-1.02	-1.02
	2 -0.65	2 -0.65
3	3	3
1.03	1.03	1.03 (.0
2.37	2.3\formal -0.0\formal -0.0\fo	5 23
7	7	7
### 5.03	### 11-50	8
5 6.65 0.0 -0.175 -0.012 -0.0133 '.1352 1.5425 0.3731 0.0522 0.1619 0.1383 0.3865  1 6.65 0.0 -0.175 -0.012 -0.0133 '.1352 1.5425 0.3731 0.0522 0.1619 0.1399 0.3865  1 6.65 0.0 -0.0155 -0.0110 0.0110 0.0110 0.0110 0.0110 0.0516  2 9.67 (.0 -0.0155 -0.0103 -0.0110 0.00110 0.0015 0.4952 0.0510 0.1807 0.1314 0.3650  3 1.51 0.0 -0.0155 -0.0155 0.0170 0.0055 0.4952 0.051 0.1807 0.1314 0.3650  4 11.50 0.0 -0.135 -0.15 -0.0170 0.005 0.0010 0.0744 0.2355 0.1219 0.3878  5 12.54 0.0 -0.0177 -0.0165 0.0165 0.0515 0.0785 0.0833 0.2524 0.1228 0.3728  6 13.50 0.0 -0.0177 -0.0165 0.0103 0.1755 0.5819 0.7325 0.0848 0.2738 0.1111 0.3820  7 18.53 0.0 -0.0177 -0.0165 0.0050 0.0050 0.51609 0.6365 0.7791 0.0867 0.2425 0.1113 0.3754  8 15.55 0.0 -0.0 0.0177 0.005 0.0050 0.0050 0.798 0.3184 0.1099 0.3771  9 15.55 0.0 -0.0177 -0.0165 0.005 0.0050 0.0718 0.0077 0.0867 0.3187 0.1099 0.3771  1 15.55 0.0 -0.0167 0.0074 0.0074 0.0078 0.0078 0.3377 0.1038 0.3577  1 15.55 0.0 -0.0267 -0.0074 0.0074 0.0718 0.0078 0.0978 0.3377 0.1038 0.3577	5 6.45	5 6.45
7.45	0 7.45 0.0 -0.7 -0 -(.012 -0.013	0 7.45 0.0 -0.11-5 -(.0012 -0.0133 1.1352 1.5975 7.3731 0.0522 J.1019 0.1399 0.3805  1 6.00 1.0 -0.11-5 -(.0012 0.0133 0.0016 -0.1009 0.0371 0.0662 0.1500 0.1376 0.3460  2 9.07 (.0 -0.0003 0.0103 -1.7009 0.0015 0.0015 0.0051 0.1807 0.1314 0.3650  3 1.51 1.0 -0.1155 -0.115 -0.1174 0.1520 0.3746 0.5574 0.0659 0.2123 0.1554 0.3800  3 1.50 0.0 -0.1175 -0.170 0.1000 0.1000 0.0100 0.0740 0.2355 0.1219 0.3878  5 12.54 1.0 -0.1175 -0.1024 0.0103 0.0100 0.0100 0.0740 0.2355 0.1219 0.3878  6 13.50 0.0 -0.1175 -0.1024 -1.0103 0.1355 0.5819 0.7325 0.0858 0.2798 0.1171 0.3020  7 12.53 0.0 -0.1175 -0.1024 -1.0103 0.1355 0.5819 0.7325 0.0858 0.2798 0.1171 0.3020  7 12.55 1.0 -0.01175 -0.1024 -1.0103 0.1355 0.0868 0.7791 0.0867 0.2225 0.1113 0.3754  18 15.55 1.0 -0.0115 0.0000 -0.0076 -0.0105 0.0353 0.0998 0.3184 0.1099 0.3771  18 15.55 1.0 -0.0124 -0.0142 0.2353 -1.1339 0.9533 0.9949 0.3377 0.1087 0.3574
1 1-50	1 1-51	1 1-50
7 12-50 1-0 -0.012 -0.012 -0.012 -0.012 0.000 0.0005 0.4952 0.0051 0.1807 0.1314 0.3650 7 12-50 1-0 -0.012 -0.012 0.012 0.1674 0.1620 0.0100 0.0744 0.2305 0.1219 0.3878 8 13-50 0.0 -0.017 -0.012 0.012 0.175 0.5819 0.785 0.0833 0.2524 0.1228 0.3728. 9 13-50 0.0 -0.017 -0.012 0.010 0.175 0.5819 0.7325 0.0058 0.2798 0.1171 0.3820 9 14-53 0.0 -0.012 0.0000 0.0000 0.0000 0.6500 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.7791 0.0007 0.2925 0.1113 0.3754 0.1650 0.0007 0.2925 0.1113 0.3754 0.1650 0.0007 0.2925 0.1113 0.3754 0.1650 0.0007 0.2925 0.1113 0.3754 0.1650 0.0007 0.2925 0.1650 0.3771 0.1650 0.3771 0.1650 0.0007 0.3574 0.1650 0.0007 0.3574 0.1650 0.0007 0.3574 0.1650 0.3577 0.1650 0.3577 0.1650 0.3577 0.1650 0.3577 0.1650 0.3555 0.0000 0.3555 0.3555 0.00000 0.3555 0.3555	2 9.69 (.0 -0.0000 0.0103 -1.2000 -0.0149 0.0005 0.6952 0.0051 0.1807 0.1314 0.3650 3 1.51 -0.0 -0.125 -0.017	2
3 1.51	3 1.51 = 0.125 = 0.3808  - 11.50 = -0.135 = 0.517	3 1.51
12.54 1.0 =0.6[c] =0.00c0 6.6[d] 6.1529 =0.1535 0.6785 0.0833 0.2524 0.1228 0.3728. 6 13.50 0.0 =0.6172 =0.70c4 =0.0103 0.1355 0.5619 0.7325 0.0656 0.2798 0.1171 0.3020 7 18.53 0.0 =0.6135 =0.6115 0.0066 0.1609 0.6366 0.7791 0.0867 0.2925 0.1113 0.3754 8 15.55 0.0 =0.7713 0.006 =0.0076 =0.0176 0.0678 0.0687 0.3184 0.1049 0.3771 9 15.53 0.0 =0.7713 0.006 =0.0076 =0.0176 0.0718 0.0877 0.3257 0.3087 0.3572 17 17.55 0.0 =0.0067 0.0067 0.0067 0.3575 0.3267 0.1087 0.3572 17 17.55 0.0 =0.0067 =0.0062 0.2353 -1.1339 0.0533 0.0449 0.3377 0.1088 0.3537	12.54   1.0	12.5% 1.0 =0.0123 =0.0020 0.013
6 13.50 0.0 -0.172 -0.7024 -1.0103 0.175 0.5819 0.7325 0.0858 0.2798 0.1171 0.3820 7 18.53 0.0 -0.113 -0.1015 mu.0080 0.1689 0.6386 0.7791 0.0867 0.2925 0.1113 0.3756 8 15.55 1.0 -0.7013 0.0000 -0.0076 -0.6156 5.6582 0.5683 0.6928 0.3186 0.1099 0.3771 9 15.53 0.0 -0.702 -0.0042 1.6155 0.0718 0.6928 0.345 0.3227 0.1087 0.3572 17 17.55 0.0 0.0 0.0027 -0.0042 0.2354 -1.1339 0.953 0.9440 0.3372 0.1038 0.3537 17 18.55 0.0 -0.2027 -0.1312 -0.0108 0.1356 1.2220 0.9959 0.3561 0.0963 0.3565	6 13.50 0.0 -0.7172 -0.7024 -0.0103 0.1755 0.5819 0.7325 0.0858 0.2798 0.1171 0.3820 17 12.53 0.0 -0.6135 -0.6615 -0.0086 0.1609 0.6386 0.7791 0.0867 0.2925 0.1113 0.3756 18 15.55 (.0 -0.713 0.000 -0.0079 -0.6156 0.6988 0.6928 0.3184 0.1099 0.3771 19 15.53 0.0 -0.713 0.000 -0.0079 -0.6155 0.6718 0.8776 0.3775 0.3277 0.1087 0.3577 17 17.55 0.0 -0.713 0.00 -0.0042 0.2353 -1.1339 0.953 0.9549 0.3372 0.1038 0.3537 17 17.55 (.0 -0.2021 -0.1312 -0.6106 0.1354 1.2220 0.9959 0.3561 0.0963 0.3555	6 13.50 0.0 -0.6177 -0.3024 -0.0103 0.1355 0.6819 0.7325 0.0858 0.2798 0.1171 0.3020 17 10.53 0.0 -0.6135 -0.6155 50.0085 0.1609 0.6366 0.7791 0.0867 0.2225 0.1113 0.3756 18 15.65 0.0 -0.6715 0.0005 -0.6075 -0.6155 0.6988 0.3186 0.1099 0.3771 18 15.53 0.0 -0.6715 0.0005 -0.6075 -0.6155 0.6718 0.6928 0.3186 0.1099 0.3771 18 15 0.0 -0.6715 0.0005 -0.6075 0.6155 0.6718 0.6928 0.3277 0.1087 0.3574 17 17.55 0.0 -0.6715 -0.6715 -0.6105 0.6353 -1.1339 0.9533 0.9949 0.3377 0.1088 0.3537
7 18-53 0-0 -0.0135 -0.0155 -0.0000 0.1009 0.6366 0.7791 0.0067. 0.2925 0.1113 0.3756  8 15-55 1.0 -0.013 0.0000 -0.0076 -0.0100 5.6582 0.0463 0.0928 0.3186 0.1049 0.3771  9 15-53 0-0 -0.012 -0.0014 1.1655 0.0718 0.0976 0.3207 0.1087 0.3574  17 17-55 0-0 0.0137 0.0137 0.0142 1.2353 -1.1339 0.9533 0.0949 0.3372 0.1038 0.3537  17 18-55 1.0 -0.0017 -0.0142 -0.0140 0.1356 1.2220 0.959 0.0599 0.3561 0.0963 0.3555		
# 15.55 (.0 -0.0013 Decouple -0.0079 -0.6150 5.8582 O.5443 O.6928 O.3184 O.1049 O.3771  - 15.53	15.55	## 15.55 (.0 -0.5713 Decoup -0.0075 -0.413 5.6582 0.443 0.6928 0.3144 0.1099 0.3771
71 17.55 (a) -0.26.7 -0.1312 -0.0105 2.1354 1.2220 0.959 0.059 0.3501 0.0963 0.3555	71 17-55 (a) -0.2021 -0.0142 (-0.0142 (-0.0153 -1.01339 (0.9533 0.01449 0.3377 (0.1038 0.3537 7) 15-55 (a) -0.2021 -0.0142 (-0.0142 (-0.0153 1.2220 0.4959 (0.0154 0.3561 0.0963 0.3555	1 1/-53
71 17-55 (-0 -0-2)-1 -0-1312 -0-1312 (-235.1 -1-1339 (->537 0-)0-0 0-3377 (-1038 0-3537 1-15-55 (-0 -0-2)-1 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0-1312 -0	71 1/-55 (-0 -0.202/ -0.13/ -0.10/ -0.13/ 1.2220 0.959 0.350/ 0.350/ 0.0963 0.3555	71 1/-55 (.0 -0.2) -0.0) -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00
1 15.55 Lab -0.20 -1.112 -0.1105 -1.1304 1.2220 v.4959 -0.4504 0.3541 0.0963 0.3555	21 15-55 tab -0-10-1 -taild -4-6144	71 15-55 Late -Cairel -Carle -
[12] [12] [13] [13] [13] [13] [13] [13] [13] [13		

-	5		59 1-1	ـــــــــــــــــــــــــــــــــــــ	3=0F15 0	·O.	6 0		A THANSIT	_		
UINT	_	FETA	CNF 3	C~3	CA3	ICPF 3	YCPF3	C~F4	CH4	CP+	XCPF4	YCPF4
<del></del>	-1.6c		-0.0261	4.664		-0.1 -74		-0.0226	-0.0015	0.0004	0.0670	-0.0166
<u> </u>	10.03	0.0					_=3.3du4_	G- 4337		0.0036		-0-1061
•	1.+3	6.0	-0.0233	-0.0115	U.0061	6.4435	2611	0.0745	0.0142	0.0127	5+45.0	0.1705
_5	2.39_	0.0		-Phonos	<del>0.0.3d</del> _			0-1130	0.4241_	0.0334	0.2132	0.2953
•	3.00	0.0	-0.6157		0.0032	C.4535	-0.2033	0-1346	0.0245	0.0644	0.1819	0.4784
<del></del> _		<u></u>	-0-141					-0-2045		0.0767	-0-130S	
ė.	5.43 6.45	( • U	-0.60-1	-00".t	-0.0012	-0-14-5	0.2937	0.7610	0.0424	0-1040	0.1640	0.3965
10	7.45	( , J		-7.0107		0:44:0	-v-2140	<del>0.3286</del>	<del>0-0551</del> -	.0.1418 0.1557	0.1676_ 0.1512	0.4316
	9-00-	La U	100	=0167			-0-2094	-0-4415	6.0662	0.2093	0.1512	0.4748
12	9.44	1.0		-6.2065	9.07/3		-0.1139	0.4946	9.0543	0.2368	0.1361	0.4826
13_	10.51	لم		- Maria			-2-1563	£.5417	C 734	0.2572	0.1356	0-4748
1+	11.50	U . U	-3.0177	-6.000	0.0(12	6.27==	-0.0003	0.6947	0.0767	0.2568	0.1266	0.4247
_15	15.50	C- U					-0.1059			-0.3190	-0-1531-	8.4837
16	13.50	0.0	-0.00-5	0.0315	-0.0653	-0.1777	3.5874	G-7138	0.0497	0.2944	0.1520	0.4181
_17		. <del></del>	-				-C-15n2	0.7643.	0907		-0-1167	
14	15.55	(1 <b></b> tr	-0-314} -121-6-	0.79.5	<b>Ψ</b> (+ ₀ ) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	-0.C93P	3.5424	0-82AD	5565.0	0.3357	0.1113	0.4055
- 13 24	17.55	6.0	0.457.5	5.Cv75	-(.uny)		-5.0674	<del></del>	0.6917	<del>0.3665</del> 0.3698	0.1051 0.1033	0.4244
<u>. 21</u>	15.55	0.4		-204192			-0.0005	0.9905	0-0962	0.3457	0.0971	0-3894
45	14.50	V. 0	-0.030-		3.0055		-0.1508	1.0422	0.0981	0.009	0.0942	0.3847

Ε	EN514 1 Of 1 OF	3	ing de	*FT CBREAL	CENTER	AEDC)			MEL FACILI		AER	DUYMAMIC SIND TUNNEL (AT
		SI_		FCH 341"=		CUSE			DEL3 DEL			
	5		37 0.	59 1.3	J.0	53.0F15	0.0	0 0	0 (	D FIXEU		
1 VT			EFTA	CV	CL4	CY	CLA	CLL	CA	CAB	CAF	ACP
1	-1.6		_0_0_			<u> </u>				0.1597		_al-2514
<	-0.6		0 <b>. U</b>	-0-1114	400723				0-3004	0.0800		-1.9587
	1.3		0.0	1991	-0.c+1i	0_ <u>0321</u> -0_028*				0.0962		-1.2736 -1.2746
5	7.5		0.4	0-1541		-4-6311				0.0465		-1.2746
6	3.4		0.0	9-40-21	-: 6025					0.1019		-1.4987
<u>.                                    </u>			ual.	6.557					0.2366	1-0979		-1-5860
el	5.4		0.0		-1-4213					4.0097		-1.6571
9	6.5		المال	iative		-0.0241				0.107A		-1-7432
G	7.0		0.0	6.4561	-1 . 730e	-4.9271	0.01+	0.0054	0.3605	0.1134	0.1670	-1.7975
1_	8.4		C_U	Erlial		2220 0220				_0.1115_		-1.8427
2	9.5		0.9	1-2471	-7.30t1					U-150P	0.1767	
3_	همنا 💶		0.4		-2.7351					u-1277	0-1748	
•	11.4			1.6961		-2-6149				0-13-5		~1.9056
5_	12.5		0.0			-0.015				C-1382		-1-9073
7_	13.7		0.4	1		-u-0121				v-1453		-1.9206
4	15.5		0.0			-0.000	2C.0474 7 -C.0474			6.1513		-1.8945
j	15.5		6.0				-0-03-2			-1591		-1.8903 -1.8858
٠,	17.4		0.0	r.1+35				0 - 10 CO		0.1633		-1.6793
1	15.5		Uest		-5.00		3 -0-4555			0-1762		-1.6709
5	14.6		0.0		-5.144				Control of the contro	0.1877		-1.8545
				<del></del>						20245	7882	
		_							·		·	
•												
					·							
												_
										· · · · · · · · · · · · · · · · · · ·		
											•	-
									·			<del></del>

			<del>Min Pilua.</del> 59 1.3		3-0F15 0		DEL2.		A TRANSIT			<del></del>
INT	ALLHA	+ETA	C of 1	. Cul	C=1	ACPF1	YCPF1	CNF2	C~5	CaS	XCPF2	YCPF2
2	-1-6- -0-53	<u> </u>	-01-1	-0.0010	-u-0147	3.0e15	7.7314	-0.0143	-0.0076	-0.0142	0.5279	0.6485
<u>.</u>	6-34	0.4				-2-15-1		0.6234				-0-1242
•	1.39	n. u	-0.31-1		-0.0117	-6.6345	1.1550	0-05-1	0.0053	0.0146	0.0985	0-2697
<u>-</u> -	7.44	0.W		-6-0003			-0-1004	0-1365	0.0165	0.0274	0-1549	-0-2617
6		1-0	-0.(157	-0.0012	4100.0	- habith	0.0675	0.1558	0.0741	0.0458	0.1545	0.2939
Ħ	5.44	(	-0.00		-0.0140	-(-1.774	1.6135	2.2540	0.4346	0.0957	0.1368	0.3766
.9	6_5	_نوع		- قالداما			0-6527_	0.3177	0.0420	0.1245_	0-1322	0.3919
Ų	7.44			-0.6963	9.9005	0.0775	-0.0307	0.3775	0.0506	0.1443	0.1339	0.3623
15	# <u>##6</u> 9.54	Ç. U		0.0001 0.0001		0.J056	1.0916		0-6574	0.1905	-0-1319- 0-1266	0.3594 0.3852
<u> </u>	13.47	G		=3-,001			1-5615	0.5591	0-4673	0.2080	0-1203	0-3720
4	11.47	C . 0	-0.11/-	-7.0021	-0.617e	v-1193	0.9662	0.e157	0.6723	0.2317	0.1174	0.3763
15	_12.52_	لاحك		<u></u>			1-6413	0.6777	0.u 7.37_	0.2528_		0.3730
16 17	13.50	0.U 		-0-0 <u>0</u> 2]		0-11-0 	0.4913 .0 <u>.0598</u>	0.7325 0.7826	0.0412	0.2753 0.3009_	0.1108 0.1054	0.3758 0-3845
16	15.54	0.0		-0.0012		0.1042	0.4397	U. ~393	0-490	0.3152	7.1060	0.3756
9	12021	سيت	3.2.2.0	حليسمت	-uallian	1-4777	-5-9136	0-9096	4461-0	0.3250	0.1065	.0.3573
شا م	17.66	6.0		+0.00€3		C. J474	0.7332	0.9628	0.0745	0.3450	0.1023	0.3503
21 <u> </u>	19.50	<u></u>			-0.007"		1.2871		0-0551	-0.3665		0.3610
	17.50	0.0	0.7176		-0.0071	J. J. H. J	-v•5549 ————	1.0339	0.0957	0.3641	0.0925	0.3522
			<del></del>		·		<del>-</del>		· <u>-</u>			
		<del></del>				<del></del> -		<u>.</u>	<del></del>			
				<del> </del>				<u>.                                    </u>	<del>- 47.</del>			······································

0.0000  1.020  1.020  1.020  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1	-0.27 <i>c2</i> -0.3805 -0.2527 -0.2525 -0.2937 -0.3304	CNF4 =0.1345 -0.1194 b.0357 0.6715 0.1082 0.1387 0.2332 0.2369 0.3313 0.3797	0.0107 0.0172	Cb4 -0.0337 -0.0042 -0.0025 -0.0104 -0.0329 0.0615 0.0732 0.1056	XCPF4 0-1079 0-0392 0-3001 0-2406 0-1889 0-1755 0-1695	VCPF4 0.9232 0.4217 -0.0686 0.1451 0.3036 0.4436
0.0000  1.020  1.020  1.020  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1.030  1	-0.27c2 -0.3805 -0.2527 -0.2525 -0.2525 -0.3109 -0.1475 -0.2511 -0.1344 -0.2013	-0.J194 0.0357 0.6715 0.1082 0.1387 0.2232 0.2369 0.3313 0.3797	-0.0008 -0.0107 -0.0177 -0.0204 -0.0243 -0.0344	-0.0025 -0.0025 0.0104 0.0329 0.0615	0.0342 0.3001 0.2406 0.1889 0.1755	0.4217 -0.0688 -0.1451 -0.3036
10.004 (1.3412 10.007 (1.3413 10.007 (1.3413 10.007 (1.3413 10.007 (1.3413 10.007 (1.3413 10.007 (1.3413 10.007 (1.3413) 10.007 (1.3413)	-0.2527 -0.2525 -0.2937 -0.3309 -0.1475 -0.2511 -0.1344 -0.2013 -0.1350	0.6715 0.10H2 0.13H7 0.2332 0.2369 0.3313 0.3747	0.0177 - 4.3204 - 0.0743 - 0.0344 - 0.0402	0.0104 0.0329 0.0615 0.0732	0.2406 0.1889 0.1755	0.1451 .0.3036
2.12.0 0.0000000000000000000000000000000	-0.2525 -0.2937 -0.3309 -0.1475 -0.2511 -0.1344 -0.2013 -0.1350	0.10H2 0.13A7 0.2332 0.2569 0.3313 0.3747	0.0204 0.0243 0.0344 0.0402	0.0329 0.0615 0.0782	0.1889	0-3034
0.01/6 0.024  1.02 1.03 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.02 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.03 1.03  1.0	-0.2937 -0.3309 -0.1475 -0.2511 -0.1344 -0.2013 -0.1350	0.2332 0.2332 0.2569 0.2313 0.3747	0.0743	0.0615 0.07a2	0.1755	
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0.3369 -0.1475 -0.2511 -0.1344 -0.2013 -0.1350	0.2332 0.2364 0.3313 0.3747	9450-D	0.6782		
2002 Ca336 2002 Ca30 2002	-0.2511 -0.1344 -0.2013 -0.1350	0-3313 v-3747		0-1056		0.3847
Schen CENTER 16 E E O CENTER 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.1344 -0.2013 -0.1350	U. 3747	0.3523		0.1566	0.4111
0.0022 0.2721 0.0022 0.2721 0.0022 0.2721 0.0022 0.2721	-0.2013 -0.1350				_0.1577_	0.4274
1.6.0.00 (0.373) 0.6.0.00 (0.6.00) 0.2.000 (0.6.00)	-0.1350		0.7554 0.0523_	0.1588	0.1460 -0.1426	0.4161
0.002		0.4979	0.0656	0.2379	0.1317	0.4779
C-3512		0.5483	0.0739	0.2545	0.1293	0.4715
	-0.0943	0.6099	0.0744	G. ee G7	0.1221	2854.0
	<u>0-1817</u> _	56622_	u.u723	_0.3154.	.0-1167-	_0-4763
0.6661	0.058 -0.2272	0.7183 <u>- D.7690</u>	0.0444	0.3384	0.1175 _0.1131	0.4293 
	-0.1944	0.6301	0.0908	0.3411	0.1094	0.4109
		0-6529	4.0914	0.3755	0.1036	
		0.9441	0.3963	0-3767	0.1036	0.1969 .
0.0074 0.3780	-0.1715	1.0340	0.0958	0.4050	0.0936	0.3917
		_ <del></del> .		<del></del>		
						11-2-
U = U	166 0.3554	166 0.3554 -0.1749 172 0.3535 -0.1657	104 0.3554 -0.1749 0.9441 107 0.3554 -0.1749 0.9441 1072 0.3535 -0.1667 0.4891	104 0.3554 -0.1749 0.9441 0.3963 107 0.3554 -0.1749 0.9441 0.3963 1072 0.3535 -0.1667 0.4891 0.4957	100 0.3554 -0.17+9 0.9441 0.3763 0.3767 100 0.3554 -0.17+9 0.9441 0.3963 0.3767 1012 0.3535 -0.1657 0.4891 0.0957 0.3931	100 0.355 -0.107 0.949 0.0963 0.375 0.1036 100 0.3554 -0.1749 0.9491 0.0963 0.3767 0.1036 1012 0.3535 -0.1657 0.4891 0.0957 0.3931 0.0968

2 _P-a	RETA	5× 3.4		3-0f15 0		0 0	0 (	FIXEU		
1.63		C+	CL4	CY	CLV	CLL	C4	CAB	CAF	XCP
	6.0	-C-llei	-		-1.0050		_0.2567_	0-1055		_1.5024
5.4e	U.Ú	-(-0524	100767			-0.0017	0.2605	0.1030		-2.0754
1.35	<u> </u>				-6-00-0		0.2512	0-1017		-1.1636
2.46.	_									
3.49	6.0									-1.5100
50	0.4					0.0000	0.7574	4-10-3		-1.5461
5.51	0.4					0.0013	0.7595	0.1114	0.1450	-1.6762
6.52						-0-0026-	0.7642	_3.1177		-1-7549
										-1.8104
	H700 174 1517									
1.76	System (U.)	The second secon	111/2017/01/2017 15:00							-1.9068
2.56	0.0					_0.000				-1.9114
3.77	0.0			0.3477	-0.0754	0.00-0	0.2624	6.1576		-1.9105
4-A)	<u> </u>					0-0025	0-2588_	3-1631		. =1.8993
111111111111111111111111111111111111111										-1.6847
			resident and the later and the							-1.8687
										-1.7963
					_					
23 45 67 6 4 1 1 2 1 4 5 6 7 4	1.59 1.59 1.61 1.75 1.76		1.46	10   10   10   10   10   10   10   10	10	1	1	A6	A6	A6

. . . . . . .

	I PART =	LLH RALL-	6rnl	CUME		1 VELZ	DEL3_BEL	a_Thansii.	10N		<u></u>
2	37 0.	3.4	3.0 A	3×0F15 0	. 0	0 0	0	O FIXE	Ů		
INT ALPHA	HETA	CNF 1	Cnl	Cal	*CPF1	YCPF 1	C4F2	CHS	CeS	ACPF2	YCPFE
<u> -lab3</u>			10112	10.20	<u> </u>	-0-1648		-0.0099		0-1867	0.5709
2 -0.6e	( v	-0.05-0	0 <b>0 1</b> 0 1	-6-6-155	-0.0047	0.6746	-0.0125	-0.0035	-0.0157	0.2421	1.2546
3 6.35 6 1.45	0.0				5.0224 5.024	3 <u>~2455</u> _ -9.0383		0.6178 0.6178		0.1273	9-0355
5 2.40	9.0	-0-4-125		-0-610n	-3-00-7	0.0047	- 0-1018.	0_01+8_		0.1073 0.1054	0-3256
5 3.49		-0.0130			0.67-5	0.1305	0.1424	8556.0	0.6546	7.1492	0.3572
7 6.54	انمات					e1.1125	4.2061	0.5248	0.0769	0-1444	0.3724
e 5.51			-1 - 66-		0.0-11	0.5747	0-7640	6.3371	0.1034	0.1407	0.3918
<u> 6.57</u>	_ للملا _		<u>13</u>			0.1671_	0-3244	0.3436_		-0-1346	-0-4052
0 7.59 1 8.61	U.U		-0.(26]	9.0906		-9.0777	0.38/1	0.0509	0.1570	0.1314	0.4056
1 <u>- P.61</u> 2 4.63				L.C.17		-0.1299	0.5104	_ <del>- 4564</del> _ 0-4624	0.1830_ 0.2093	<del>0.1264</del> _ 0.1222	0.4191
1 10-62	-		ما شامه			16-4600	0.5163	- C-C6H3	E465-0	0-1142	0-4051
4 11.70			-6.,013		6-11-9	0.08-5	0.6457	0.4736	0.2593	0.1143	0.+016
5 12.64		-Couler	-causes		G-1-36	6-2120	7.7155	-0+4910	0,2813	_0.1133_	0.3934
6 13.77				_	0.0460	0.5879	0.7834	0.5844	0.3050	0.1077	0.3893
7 16-21			_ <del>-</del> 0		0-1151_	D. A. 30		0-0693		0-1058-	-0.3848
6 15.43			-6.156-		V.V613	0.8117	0.907a	0.0944	0,3447 	0.1048	0.3799
17.45			-0.414		0.1435	0.1647	1.0155	0-1016	0.3606	0.1001	0.3747
18.96	_				-7-7956					0.0905_	0-3710
2 20.01		-0.0052			-1.0116	0.2500	1.0956	0.1013	0.3913	.0.0925	0.3571

B BFT.  3		-0.1331 -0.033 -0.0053 -0.0053	C#3 C.ull4 C.ul27 C.0029 J.lu34 U.0039 U.0039	(.3)44 (.4/55 (.44/5 (.4/5/6	YCPF3 -1-2420 -1-2753 -0-2040 -0-2411 -0-2557	CNF6 =0.6347 =0.0064 -0.0329 0.0744	CHA 0.0055 0.0063 0.0060 0.0128	CH- -0.0249 -0.0048 -0.0065	XCPF+ -0.1414 -0.0438 -0.1819	YCPF4 -0-6444 0-6934 -0-2572
2 0.0 2 0.0 3 0.0 4 0.0 4 0.0 4 0.0 6 0.0 6 0.0	-0.46.45 -0.31.77 -0.01.33 -0.01-05 -0.01-05 -0.01-05	-0.1331 -0.0053 -0.0053 -0.1676 -0.1676	\$500.0 \$500.0 \$500.0 \$500.0 \$500.0	(.3)44 (.4/55 (.44/5 (.4/5/6	-1.2753 -0.20d0 -0.2411 -0.2557	-0.0064 0.0329	0.00G3 	-0.0048	-0.0438 -0.1819	0.6934
e 0.0 6 0.0 6 0.0 10 0.0 11 0.0 17 0.0 19 0.0	-0.01-5 -0.01-5 -0.01-5 -0.01-5	-6.6653 -0.6362 -0.676	9560.0 - AEWOL 9600.u 4610.u	0.4635 0.4636 0.464	-0.2411	0.0744	0.0178			4-2577
6 0.0 15 0.0 11 0.0 17 0.0 19 0.0	-0.01-5 -0.01-5 -0.01-5 -0.01-5	-0.167L -0.664D2		G.4655	-0.2557			n_b/n&		
1 0.0 1 0.0 1 0.0 1 0.0	-0.01-0 -0.01-0 -0.01-0	-0.1676	\$600.u 46.da.d	6.404			3.6143.	0.0466	0.1720 	0.3554 0.4115
1 0.0 7 0.0 9 0.0	-0-01-5 e-13-0-				-0.7656	0.1574	0.0246	0.0727	0.1564	0.4618
7 0.0 9 0.0	-0.61	-6-1103			- Ph. 2364			0.0540	0-1535	-0-43 <u>6</u>
9 0.0		-0-6-55	2500-0		-3.1541 -3.1529	0.2712	0.0390 6665	0.1236 . 0.1564	0.1439 0.1391	0.4557
1 0.4	-0-01//	-0-0374	U.UC?b		-0.1493	0.3947	0.0517	0.1837	0.1310	0.4654
	-0.61.2	-0-0055		4.3713	0.1003_	0-4591	0.0569	0.2208.	_0.1242_	0.4808
3 0.0		-0.000-	0.0723		-3.1526	0-5171	0.0655	0.2497	0.1203	0.4829
7 6.0			0.0121		-0-0-59 -0-1108	0.6463	0.0729	0.2727	0-1185 0-1129	0.4723 0.4511
A 0.0			0.0466			-0-7052	-0.0767	_0.3267_	0.1088_	
77 0.0			0.0003			0.7765	0.0423	0.3362	0.1060	0.4329
										0-4346 0-4231
is Cal			3-0.12							0.4234
0.0	-0.0107	-0.0036	U.0605	V.2137	-0.0360	0.4884	0.0940	0.4026	0.0991	0.4073
							_			0.4003
	-0.0745	-0.0107		V+3009	-0.1574	1.0837	0.09/3	0.4246	U.0404	0.3961
								•		
						· · · · · · · · · · · · · · · · · · ·				
							•			
	7 0.0 1 0.0 3 0.0 6 0.0	6 0.0 -0.0172 7 0.0 -0.0172 1 0.0 -0.0175 3 0.0 -0.0175 6 0.0 -0.0175 9 0.0 -0.0197 8 0.0 -0.0225	8 0.0 -0.0172 -0.0057 7 0.0 -0.0172 -0.0057 1 0.0 -0.0175 -0.0057 3 0.0 -0.0175 -0.0057 6 0.0 -0.0175 -0.0057 9 0.0 -0.0177 -0.0058	8 0.0 =0.0172 =0.0253 G.00Gb 7 0.0 =0.0155 =0.0064 0.0003 1 0.0 =0.0355 =0.0123 0.0005 5 0.0 =0.0175 =0.065 0.0000 6 0.0 =0.0525 =0.0557 0.0000 9 0.0 =0.0157 -0.0536 0.0000 8 0.4 =0.0225 =0.0057 0.0025	8 0.0 -0.0172 -0.0050 0.0066 0.2915 7 0.0 -0.0172 -0.0050 0.0003 0.25-1 1 0.0 -0.0175 -0.0124 0.0055 0.6441 3 0.0 -0.0175 -0.065 -0.0000 0.25-6 6 0.0 -0.527 -0.055 0.0000 0.25-7 9 0.0 -0.017 -0.055 0.0000 0.25-7 8 0.0 -0.025 -0.0557 0.0029 0.2523	8 0.0 -0.0172 -0.0050 G.06Gb 0.2915 -0.0372 7 0.0 -0.0173 -0.0064 0.0003 0.25-1 -0.0173 1 0.0 -0.0175 -0.005 0.0000 0.25-4 0.0006 3 0.0 -0.0175 -0.065 -0.000 0.25-4 0.0006 6 0.0 -0.522 -0.057 0.0012 6.29-7 -1.0519 9 0.0 -0.157 -0.058 0.005 0.2521 -0.0360 8 0.0 -0.025 -0.0557 0.0029 0.2521 -0.1279	8 0.0 -0.0172 -0.0050	8 0.0 -0.0172 -0.0000 0.0000 0.2915 -0.0372 0.7052 0.0767 7 0.0 -0.0100 -0.0000 0.0003 0.2501 -0.0173 0.7765 0.0823 1 0.0 -0.0175 -0.0121 0.0000 0.2500 0.0000 0.8312 0.0870 3 0.0 -0.0175 -0.0605 -0.0000 0.2500 0.0000 0.834 0.0690 6 0.0 -0.522 -0.0000 0.2500 0.0000 0.6034 0.0690 9 0.0 -0.0177 -0.0536 0.0500 0.2137 -0.0360 0.9884 0.0980 8 0.0 -0.0255 -0.0057 0.0025 0.2521 -0.1279 1.0298 0.0982	8 0.0 -0.0172 -0.0050 6.0666 0.2915 -0.0372 0.7052 0.0767 0.3267- 7 0.0 -0.0173 0.0765 0.0023 0.3362 1 0.0 -0.0175 -0.025 0.0065 0.4041 -0.1607 0.4312 0.0870 0.3630- 3 0.0 -0.0175 -0.065 -0.0000 0.2594 0.0006 0.6834 0.0954 0.3738 6 0.0 -0.0175 -0.055 0.0012 0.2594 0.0006 0.6834 0.0954 0.3738 9 0.0 -0.0175 -0.055 0.0050 0.2137 -0.0360 0.9884 0.0960 0.4026 8 0.0 -0.025 -0.0557 0.0029 0.2521 -0.01279 1.0298 0.0962 0.4122	8 0.0 -0.0172 -0.0050 G.00G6 G.2915 -0.0372 G.7052 G.0767 G.3267 G.1088 7 U.O -0.0175 -0.0044 G.0030 G.25-1 -0.0173 G.7765 G.0623 G.3362 G.1060 1 0.0 -0.0175 -0.0124 G.0045 G.4041 -0.1607 G.4312 G.0876 G.3636 G.1067 3 U.U -0.0175 -0.0046 G.0000 G.25-4 G.0006 G.4634 G.0494 G.3738 G.1012 6 G.U -0.025 -0.0057 G.0025 G.25-7 W.0519 G.4936 G.0925 G.3938 G.0994 9 G.G -0.0177 -0.0536 U.000 U.2137 -0.0360 G.4984 G.0995 G.3938 G.0994 8 G.G -0.025 G.0057 G.0025 G.2521 -0.1279 L.0298 G.0982 G.4122 G.0953

FAUL 1 OF 3

_ SHEET 1 OF 1

	5	36 v.	PA 0"3	10v.0 b	3-0F15 U	.0	0 0		O FIRED	)		_3
INT	ALPHA	ci la	( =	CLM	CA	CLN	CLL	ÇA	CAR	CAF	ACP	
	-1.55	لاحال	-0-2424		-3.10BZ	1-1176	0.02.2	1-4974	4,3915	C-AC64		
5	-0.7	C-L	-0-7775	しっしちょう		0.1912	0.0167	J070	U-0-34	0.3792	-1.1739	
<u></u>	0_3_	للحائ	<u>-0-0-0-0</u>		u <u>all37</u> _	C-0410	0_0510	0.4.777.			-1.5537	
•	1.44	0.0	けっしゅうち		-0.102n	C.JF34	0.6230	0-4628	N.0045	0.3646	-1.9436	
ــــــــــــــــــــــــــــــــــــــ	2.59	4-4		-Decise		0-6246	0.0052	_ 0.+632_	0915		-1-4229	
•	3. • •	(· • ·	0.3000	-0-5420		6-4-5-1	0.0301	008	0.0954		-1.4829	
	عمعك	1 1.	0-6:-25		عنابرتمات	ملقيت	<u>0.42=3</u>	0-4501	0-7660		-1-6406	
•	5.44	6.0	0.5177		-0.0464	tento2	0.0124	0.4424	6.6663		-1.6131	
<u> </u>		<u> </u>		عتدامات			0.0257	u_a353 .	6.0982			
10	7.43	6. L	C. THE			0.0036	0.0319	0.4301	0.1038		-1.7689	
<del>ii</del>				<del>f+26ÄA</del> -		<del></del>		-0-0115	3-1124			
12	9.45	(· • · ·	1-1510			0.03=5	0.0194	0.4119	v.1179		-1.7637	
	10.43			_ <del>-2.inx2</del>		5.3443	0-0115		0-1198		<u>-1.6271</u>	
15	11.47	C . u	1.7531	-2.4375	-0.0951	0.6544 <u>-0.63</u> 4-	0.0046	0.413~ 	u-1291		-1.8271 -1.8022	
15	13.45	Let	1111			3.07-0	0.0113	0.4174	0-1319 0-1393		-1.8081	
17	1000	G_4							C-1466		=1.7861	
14	15.49	0.0	2.3741			7.7-61	-0.0043	0.3952	0.1644		-1.8026	
19	16.47	( a b			-1-1175	3.1532	C-010A	0-6056	-ú-1000		=1.7847	
20	17.51	(	2.7371			J. 0749	0.0106	0.4045	0.1761		-1.7596	
21	14.49	U - U			-u-0662	4-0541	0.0136	û.3956	0.1757_		-1.7.52	
25	17.50	C. J			-0.0933	0.0767	0.0021	0.4011	G-1852		-1.7230	
												<del> </del>
				<del></del>		<del> </del>						
						•						
		<u>_</u>				<del></del>						<del></del>
						<del></del>	<del> </del>				·····	
				<del></del>			<del></del>					
												···

AEDC-TR-75-125

ANDLE ENGINEERING PENEL CENERAL CENERALATURE PROPERTION - 150 TUNNEE FACILITY PRIL AERODYNAMIC - 180 TUNNEE (ATT

MAPTIN MISSILE TAIL EFFECTS DATA

	TESI				CLNF		1 DEL2	UEL3 DEL				
		36 U.	5+ C+3	140.0 E	3.0f15 0.	.0	0 0	0	0 FIXE	0		<u> </u>
LIMT	* ALPHA	SETA Name	C'F1	C-1	Cb1-	ACEL I	YCPF 1	C4F7	CH2	CH2	2 CPF 2	YCPF2
2	-0.5/	U.U	-0.05-4	-u.v217	V.C33~	0.2306	-0.3751	M050.0	7.0046	0.0369	0.2215	1.6723
3	0.43	D.U.	-Ga: 14=	-6-003-	_حددسه شع_		1.1347_	-0-0011	. 4.0061	-0.0347	-5.4570	31-1962
•	1.44	0.0	-0.0757		0.CO0A		-1.1340		-0.6040	0.00-1	0.1708	-0.0772
6	3,44	0.0	<u> </u>	0-040	0.0347	<u></u>	<del></del>		_ <del>_0</del> _0155 -v.:245		0-1789	0.5764
7	- 4-9/	6.0		-0-6	0.03C1				-0-4199 -0-4199		0.1769	0.5701
H	5.44	0.6	-0.1372		0.0515	3.2540			-0.0425	-0-1152	0.1676	0.4542
4	0.41	Lau	-6-012-		-5.0.3y	_0-2366	A-8825		-0.0435		0-1435	0.4615
10	7.43	0.0	-0.0039		0.0145	6.2375	-0.2268	-0.3317	-0.6374		0.1142	0.4007
11	H-40	-0-4	5-4			<u> </u>			0.564_			
10	9.45	6-0	-6.1709		-0-0617	( - 3925	££80.0		-0.0424 -0.0424		0.1343	0.3750
14	11.07	V.U	0.0	0.L	3.3	5.0	0.0		-U.V693		0.1235	0.3849
15	12.40			-2-6211		0.2366			0.C675		0-1143	0.3546
10	13.45	0.0	0.0254	C-440:	0.0	4.2354	0.0		-0.0+72		9.1284	0.3228
17	_14.67-	0-0	<u> </u>						+0-u710.		0-1056	0.4054
15	15.49 16.47	0.0	-0.02u4	-0.00m2 -0.00m2	6.6271	5-0			-0.6856 		0.1124	0.3345
20	17.51	0.0	-0-271-	-0.6701	0.0465		-3.5401		-0.2585		0.1016	0.3686
21	15.05	0.0	4.017						-0.3600			0.3874
55	14.52	6.0	0.00=1	4-60-7	-0.0509	0-60-9	-6.3127	-6.9115	-0.6797	-0.3318	0.0875	0.3640

	TES1		<u>ьен 9х10-</u> 57 0.3				I VELZ		a iransli O fixe		· <del></del>	·
POINT		BETA	C+F3	C+3	CH3	xCPF3	YCPF3	CNF4	CH4	CB4	#CPF4	YCPF4
2	-0.57	Call.	-C-^1/9	-0-6546	0 <u>-045</u> 0-0165	1.2652	-0.3801	0.072M	0.0171	0.0056	0.3470	0.1573
		_0.4	0.:755				-0.2517			=0.9217_	2.0551	-3.2677
•	1.44	0.0	-0.0334	-0.0292	0.055	0.8750	-0.6709	-0.0426	0.0028	-0.0319	-0.0662	0.7494
	<del></del>	0.0	-9-31 <del>45</del> . 0-7541	-0.0108 0.0321	-0.012?		-0.2146		-0.0094	-0.0564 -0.0871	0.0672_ 0.0748	0.6936
<u> </u>	4-62	0.0		-0.03E1	-0-0127		-0.5663		-0-0155	-0.0071	0.0746	0.6936
8	5.44	0.0	-1.5.	-0.0617	0.0454		-0.4634	-0.2253	-0.0223	-0.1166	0.0986	0.5175
9		_0.0_		-0-6112	62158_		-1.55#1		0_0236		-0-0910-	0.5868
10 11	7.43	U.U	0.4278	0.0008	-0.0010		-0.0535 0.2645		-0.0350	-0.1843	0.1080 0.0921_	0.5679
12	9.45	0.0	-C.u377		0.443		-0.6372		-0.0-84		0.1101	0.5140
13_	10.43	0	0-15/3		-0-6121		-t-2106	-0.4980	=0.0552		0.1108	0.4675
14	11.47	0.0	-0.)+>b D-051b	-0.6376	0.0145		-0.3798	-0.5427	-0.0591		0.1089	0.4667
16	<u> 12.46</u> 13.45	D_0	-6.5362	-0-1235	D-0137		-0.3797 -0.3797		-0.0556 -0.0622	-0.2593	0.0979 0.0995	-0.4958
<u> </u>	14.49	0.4	-0.0011		5550.0		-2.3799				0.0535	0.3641
16	15.49	6.0	5.000]		-0.6175		-).3799		-0.0663	-0.3174	0.0912	0.4368
20	16.67 17.51	0.0	<u>-1-6253</u> 0-6245		-0.0192		-0.3500 -0.3799		-0-0709	-0.3416 -0.3772	0.0899	0.4329
21	18.44	6.0	0-0456				-0-3797			-0.3793	0-0331_	0.4434
55	19.52	0.0	0.01-1		-0.0054		-0.3796				0.0861	0.3577
								•				
							<u> </u>					
								11.0				

7.46 0.0 (.9735 -1.6747 -0.0731 (.0016 -0.0011 0.3911 0.1060 0.2851 -1.7372 0.47 0.0 1.0035 -1.4561 -0.0060 0.6650 0.0108 0.3875 0.1123 0.2756 -1.7879 0.7879 0.1050 0.2851 -1.6280 0.1050 0.2851 0.1050 0.2851 -1.6280 0.1050 0.1050 0.1050 0.1050 0.2851 0.2850 0.1050 0.2851 0.2860 0.1050 0.2851 0.1050 0.2851 0.1050 0.2851 0.1050 0.2851 0.1050 0.2851 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.2850 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1050 0.1		7661	SART N		s 81	CUNE	1	1 1161 2 6	NEL 2 DELA	TOAMETER	<b>^</b>	
1.50 C. =0.15% 1.1n(s =0.0707 0.0517 1.0072 0.416 0.0755 0.255 =1.1001  1.00 C. = -0.0707 0.0007 -1.0007 -1.0007 0.0007 0.0000 0.0032 0.2008 -1.1006  1.02 C. = 0.627 =1.0006 0.0005 0.0005 0.0108 0.0002 0.0005 0.2002 -2.3518  1.02 C. = 0.627 =1.0006 0.0005 0.0002 0.0108 0.0002 0.0001 0.3001 -1.7237  2.40 C. = 0.2567 =1.3008 0.0004 0.0007 0.0002 0.0001 0.3001 -1.7237  2.40 C. = 0.2567 =1.3008 0.0004 0.0001 0.3001 0.3003 0.2003 10.3057 -1.5160  2.40 C. = 0.3576 -1.5023 -0.0004 0.0001 0.3003 0.2003 10.3057 -1.5160  2.40 C. = 0.3576 -1.5023 -0.0004 0.0005 0.3003 0.2003 -1.5160  2.40 C. = 0.3576 -1.5023 -0.0004 0.0005 0.3003 0.2003 0.2003 -1.5003  2.40 C. = 0.3576 -1.5023 -0.0004 0.0005 0.3003 0.0005 0.2003 -1.5003  2.40 C. = 0.0004 0.0005 0.0004 0.3003 0.0005 0.2003 -1.5003  2.40 C. = 0.0004 0.0005 0.0004 0.3003 0.2003 0.2003 -1.5003  2.40 C. = 0.0004 0.0005 0.0004 0.3003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.2003 0.20											-	
	1 47											
1.42 0.0 0.1400 -1.7227 -0.0705 0.0037 0.0032 0.0941 0.3061 -1.7237  2.44 0.0 0.2542 -1.3400 -0.0044 0.0041 0.4564 0.0031 0.3057 -1.5140  3.44 0.0 0.3572 -1.5223 -0.0040 0.0740 0.0003 0.3860 0.2933 0.2934 -1.5162  7.43 1.1 0.474 -0.7405 -0.0171 0.0055 0.0060 0.3091 0.0955 0.7906 -1.6512  8.547 0.0 0.4335 -1.013 -0.0174 0.0715 0.0061 0.3908 0.1021 0.2887 -1.6412  9.547 0.0 0.4335 -1.014 -0.0174 0.0715 0.0061 0.3908 0.1021 0.2887 -1.6412  9.746 0.0 0.5235 -1.014 -0.0174 0.0115 0.0061 0.3908 0.1021 0.2887 -1.6412  9.746 0.0 0.5235 -1.014 -0.0064 0.0116 0.3918 0.1021 0.2887 -1.6412  9.746 0.0 0.0 0.5235 -0.0174 0.0175 0.0061 0.3918 0.2756 -1.7372  9.746 0.0 0.0 0.5235 -0.0174 0.0064 0.0116 0.3918 0.2756 -1.7372  9.746 0.0 0.0 0.0067 -1.0064 0.0064 0.0116 0.3917 0.2065 0.2756 -1.7372  1.547 0.0 0.0 0.0067 -1.0064 0.0067 0.3597 0.1175 0.7417 -1.6280  1.547 0.0 0.0 0.0067 -1.0067 0.0350 0.0350 0.3597 0.1175 0.7417 -1.6280  1.547 0.0 0.0 0.0067 -1.0067 0.0050 0.3650 0.3660 0.313 0.2163 -1.8669  1.549 0.0 0.0067 -3.0060 -0.6071 0.0050 0.3650 0.3660 0.1390 0.2097 -1.8730  1.549 0.0 0.0067 -3.0060 -0.6071 0.0050 0.3650 0.3500 0.1400 0.2097 -1.8730  1.549 0.0 0.0067 -3.0060 0.0050 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0067 -1.0060 0.0060 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1597 0.1995 -1.8777  1.550 0.0 0.0060 0.1065 0.3500 0.1590 0.1597 0.1857 0.18573 0.1652 -1.8573	ė											-
2.44 ( ( 2.302 -0.302 -0.004 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.001 ( 0.00	3											
3.44	•		8.6									
	<del></del>		0 - v									
5.47 L.U U.A3.4 -1.1413 -0.0197 U.U.A23 U.U.A23 U.U.A23 U.U.A23 U.U.A23 U.U.A23 U.A348 U.A23 U.A348 U.A	<u>;                                    </u>											
7.46 (.U (.9735 -1.6*47 -0.0731 (.0516 -0.0011 0.3911 0.1060 0.2851 -1.7372 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.475 0.	6	5.47										
### 10-47	<u>.</u>											
2	ı											
11.47 0.0 · 1vel -7.731 -0.0717 0.0355 0.347 0.1293 0.2264 -1.8368  11.47 0.0 · 1vel -7.731 -0.0717 0.035 0.055 0.3476 0.1313 0.2153 -1.8669  5 12.49 0.0 1vel -3.471 -0.0571 0.6550 -0.0120 0.3425 0.1337 0.2086 -1.8864  5 13.50 0.0 1vel -3.471 -0.0571 0.0572 0.0120 0.3447 0.1390 0.2097 -1.8730  2 12.49 0.0 2.0071 -3.0700 -0.0571 0.00425 0.0120 0.3447 0.1390 0.2097 -1.8730  2 12.49 0.0 2.0071 -3.0700 -0.071 0.0050 0.3508 0.1400 0.2024 -1.8850  3 15.49 0.0 2.4150 -0.3200 -0.0700 0.0125 0.3562 0.1597 0.1965 -1.8777  4 15.50 0.0 2.4151 -0.7227 -0.0707 0.0075 0.3562 0.1597 0.1815 -1.8726  5 17.49 0.0 2.4151 -0.7227 -0.0713 0.0757 -0.0075 0.3562 0.1590 0.1665 -1.8573	5						T					
5 12.49 G.W 1.5947 -3.0/63 -G.G/30 G.G550 -G.G050 0.3425 3.1337 0.2086 -1.8864  5 13.50 G.V 1.5741 -3.4/27 -6.0057 0.0425 G.G014 0.3447 0.1390 0.2097 -1.8730  7 14.49 G.W 2.6671 -3.6/27 -6.0057 0.0425 G.G014 0.3447 0.1390 0.2097 -1.8850  8 15.49 G.W 2.6671 -3.6/27 -0.0769 G.G71 G.G43 -0.0050 0.3508 G.1444 0.2024 -1.8850  9 15.49 G.W 2.4154 -4.3267 -0.0769 G.G1123 -0.0025 0.3562 G.1597 0.1965 -1.8777  16.50 G.W 2.4154 -4.7267 -0.0413 U.0757 -0.0075 0.3501 0.1430 0.1655 -1.8573  1 16.53 G.W 3.0/27 -5.6522 -0.0334 U.0305 -0.0141 0.3552 G.1900 G.1652 -1.8381	3	-	-									
13.50 G.U 1	•											
2 18-44 (-0 2-6671 -3-cine -0.6671 6-68-3 -0.0056 0-3508 6-1486 0-2024 -1-8850  H 15-44 0.0 7-1-50.3265 -0.0764 (-0673 -0.0025 0.3562 0.1547 0.1965 -1-8777  H 16-50 6-0 2-6439 -0.749 -0.0046 6-1123 -0.0050 0.3561 0.1726 0.1815 -1-8726  U 17-44 (-0 2-41-7 -7-7277 -0.013 0.0757 -0.0075 0.3501 0.1436 0.1665 -1-8573  1 16-53 6-0 3-0744 -5-6544 -0.0350 0.0366 -0.0161 0.3552 6-1400 6-1652 -1-8381	5		The second second									
# 15.49 0.0 7.450 -4.3200 -0.0769 (.0673 -0.0025 0.3562 0.1597 0.1965 -1.8777  ** 15.50	10											
15-50 C-1 2-5-10//	*		1 2 2 2 2									
1 16.53 3.2/yc -5.65yy -0.036 u.u366 -0.0161 3552 0.1400 0.1652 -1.8381			100 miles									
	20										0.1405	-1.8573
2 19.52 6.3 3.35:2 -0.0159 -0.0297 0.0275 -0.0055 0.3462 6.1956 0.1533 -1.7941	-1		0.0									
	2	14.52	c.,	3.3524	-401754	-1.0597	F-0275	-0-0055	0.3402	6-1956	0.1533	-1.7941
		_										
		-							-			
					<del></del>					<del>- · · · · · · · · · · · · · · · · · · ·</del>		

TEST	PASI =	ACH REIL-	5 PHI	CONF		1 DF1 2	3-13 DH	a_TRANSIT	10M				
2	37 v.	57 0.4	164.0 0	340F15 U	. 0	0 0	0	O FIRE	Ü				
ALPHA	PETA	CNF1	C+1	CHI	YCPF1	YCPF1	CAFZ	CHS	CBS	XCPF2	YCPF2		
-1.58	4-51			4-05-			0-0494	- 4-636A	0.0169	0-1292	<del></del>		
1.46	0.0			u.u527						0.1717	0.4757		
2.49	4-4			-0.0652		_	-0-0903.	0.61-2	-0.0616_	0.1583			
3.44	0.0												
5.00	0.4									-0-1551	0.011R		
7.40	4.0	-0-11-0	-G. Ce7.	0.9365	0.2356	-0.3149	-n.3573	-0.0495	-0-1527	0.1384	0.4275		
_A.67_	0.0	e0_4557_								0.1317			
	-			_									
		0.41.3											
12.49				0.0012						0.1222	0.4222		
13.50	0.0	0.0005	6-3117	-C-U550						0.1164	0.4265		
												<del></del>	
	D.k.												
17.49	0.0			U. U.65						0.1048	0.3000		
18.53	_0_0_	0.6175		-0-u397		_				0.1038	-0.3632-		
19.52	0.0	St00.0-	0.6613	0.0075	-0291	-2.4637	-0.9697	-0.0945	-0.3568	0.0971	0.3679		
					·				_				
<u>.,</u>			<del></del>				<del>- • • • • • • • • • • • • • • • • • • •</del>	<del></del>			<del></del>		
	2 ALPMA =1.5M =0.5b 0.42 1.42 2.40 3.44 5.47 6.66 7.46 8.47 7.40 10.45 11.47 12.49 13.50 14.49 15.49 15.49 16.50 17.49 18.53	2 37 va  ALPMA PETA  -1.5M PLA  -0.5b V.V  0.42 V.V  1.42 0.V  2.40 V.V  3.44 V.V  5.67 C.V  6.45 V.V  7.40 V.V  11.47 0.V  12.49 0.V  13.50 0.D  13.50 0.D  15.49 0.U  17.49 0.V  17.49 0.V  17.49 0.V  17.49 0.V  18.53 0.0	2 37 v.57 0.4  ALPMA PEIA CMF1  -1.56	2 37 v.59 0.4 10v.0 of  ALPMA PETA CNF1 -1.56 0.9 -0.0017 -0.165 -0.56 0.0 -0.0047 -0.122 0.42 0.0 -0.0047 -0.122 1.42 0.0 -0.007 -0.122 2.44 0.0 -0.007 -0.122 3.44 0.0 -0.04631 -0.126 5.47 C.V -0.1010 -0.266 0.0 -0.0432 -0.116 7.40 0.0 -0.1110 -0.027 4.41 0.0 -0.121 0.007 10.45 0.0 0.0231 0.007 11.47 0.0 0.0163 11.47 0.0 0.0163 11.49 0.0 -0.0331 -0.017 14.49 0.0 -0.0331 -0.017 14.49 0.0 -0.0331 -0.017 14.49 0.0 -0.0231 0.007 15.49 0.0 0.0231 0.007 15.49 0.0 0.0231 0.007 15.49 0.0 0.0031 -0.017 14.49 0.0 -0.0031 -0.0034 15.49 0.0 0.0031 -0.0034 15.49 0.0 0.0031 -0.0031	2 37 v.5v 0.4 100.0 m3s0f15 v  ALPMA PEIA CMF1 CM1 CM1  —1.5h	2 37 v.5v 0.4 10v.0 n3x0f15 v.0  ALPMA REIA CMF1 CM1 CM1 YCPf1  -1.5k 0.4 -0.0b12 mu.la5 0.0km 0.2365  -0.5b 0.4 -0.0cov -0.12v 0.u252 n.2613  0.42 0.0 -0.0m2 -0.0321 0.0033 5.2371  1.42 0.0 -0.0m2 -0.0321 0.0033 5.2371  2.40 0.0 -0.0m2 -0.0221 0.0033 5.2371  3.40 0.0 -0.0m2 -0.0221 0.0033 5.2371  4.43 0.0 -0.0001 -0.0001 0.0325 0.2365  5.47 0.0 -0.101m -0.1202 0.0325 0.2365  5.47 0.0 -0.101m -0.1202 0.0325 0.2371  0.40 0.0 -0.110 -0.027 0.0365 0.2365  7.40 0.0 -0.110 -0.027 0.0365 0.2365  7.40 0.0 -0.110 -0.027 0.0365 0.2365  10.45 0.0 0.0231 0.077 -0.01m 0.3265  11.47 0.0 0.0103 0.077 -0.01m 0.3265  11.49 0.0 0.0103 0.017 -0.050 0.3273  12.49 0.0 0.0103 0.017 -0.050 0.2365  13.50 0.0 0.0231 0.017 0.0050 0.2365  14.49 0.0 -0.0231 0.017 0.0050 0.2365  15.49 0.0 0.0231 0.017 0.0050 0.2365  15.49 0.0 0.0231 0.017 0.0050 0.2365  15.49 0.0 0.0231 0.017 0.0050 0.3265  15.49 0.0 0.0231 0.017 0.0050 0.3265  15.49 0.0 0.0231 0.017 0.0050 0.3265  16.50 0.0 0.0231 0.017 0.0050 0.3265  17.49 0.0 0.0050 0.0125 0.0061 -0.0055 0.2365	2 37 v.5v 0.4 16v.0 r3x0f15 v.0 0 0  ALPMA RETA CMF1 CM1 CM1 YCPF1 YCPF1 -1.5m L.4 -0.0012 -0.165 0.004 0.2365 -1.1341 -0.5c 0.0 -0.6cc -0.220 0.0252 0.2311 -0.3767 1.62 0.0 -0.0023 -0.0120 0.0233 5.2371 -0.3767 2.40 0.0 -0.0023 -0.0120 0.0233 5.2371 -0.3767 2.40 0.0 -0.0023 -0.0120 0.0232 0.1319 0.6621 3.00 0.0 -0.0407 -0.003 0.0703 0.1671 -1.5057 A.A3 0.0 -0.0407 -0.003 0.0703 0.2365 0.2371 -0.3782 5.07 C.0 -0.1010 -0.0202 0.0365 0.2371 -0.3782 5.07 C.0 -0.1010 -0.0202 0.0365 0.2371 -0.3782 7.40 0.0 -0.0110 -0.0202 0.0365 0.2376 -0.3781 7.40 0.0 -0.1100 -0.0270 0.0365 0.2376 -0.3199 A.A7 0.0 -0.0557 -0.0110 -0.0253 0.1991 0.4540 9.00 0.0231 0.0070 -0.010 0.3269 -1.0129 10.45 0.0 0.0231 0.0070 -0.010 0.3269 -1.0129 11.47 0.0 0.0133 -0.0070 -0.010 0.3269 -1.0129 11.49 0.0 0.0133 -0.0071 0.0000 0.3269 -1.0129 12.49 0.0 0.0133 -0.0071 0.0000 0.3269 -1.0129 13.50 0.0 0.0000 0.0117 -0.0550 0.2360 -1.3574 13.60 0.0 0.0000 0.0117 -0.0550 0.2360 -1.3574 15.49 0.0 0.0000 0.0117 -0.0550 0.2360 -1.3574 15.49 0.0 0.00000 0.0117 -0.0550 0.2360 -1.3574 15.49 0.0 0.00000 0.0117 -0.0550 0.2360 0.1955 16.50 0.0 0.00000 0.0117 -0.0550 0.2360 0.1955 16.50 0.0 0.00000 0.0117 -0.0550 0.2360 0.1955 16.50 0.0 0.00000 0.00000 0.3000 0.1955 16.50 0.0 0.00000 0.00000 0.3000 0.1955	2 37 v.5v 0.4 10v.0 r3v0f15 v.0 0 0 0  ALPMA RETA CMF1 CM1 CM1 FCPF1 YCPF1 CM7  -0.50 U.U -0.0017 -0.165 0.002 0.2365 1.13A1 0.049A  -0.50 U.U -0.0047 -0.122 0.0252 0.2613 -0.2947 0.042A  0.42 U.U -0.0007 -0.1021 0.0033 5.2371 -0.3767 0.0036  1.42 0.U -0.0023 -0.124 0.0527 0.2355 -1.0074 -0.0592  2.40 U.U -0.0403 -0.124 0.0527 0.2355 -1.0074 -0.0592  2.40 U.U -0.0407 -0.0231 0.0224 0.119 0.4621 -0.0903  3.40 0.U -0.0407 -0.0232 0.0363 0.2371 -0.3782 -0.2561  5.47 C.U -0.101m -0.1262 0.0325 0.2371 -0.3782 -0.2561  0.40 0.U -0.0437 -0.1100 -0.0235 0.2371 -0.3782 -0.2561  7.40 U.O -0.1100 -0.027 0.0365 0.2371 -0.3781 -0.3231  7.40 U.O -0.1100 -0.027 0.0365 0.2346 -0.3149 -0.3573  8.47 0.0 0.0557 -0.0111 0.2253 0.1991 0.4560 0.4561  9.40 U.O 0.0231 0.0070 -0.01m 0.3265 -1.0129 -0.4901  10.45 0.0 0.0531 0.0070 -0.01m 0.3265 -1.0129 -0.4901  11.47 0.U 0.0113 0.2344 0.027m 0.3223 -0.3743 -0.5020  11.49 0.U 0.0133 -0.017 0.0050 0.2360 -0.314 -0.5020  11.49 0.U 0.0133 -0.017 0.0050 0.2360 -0.314 -0.5020  13.50 0.0 0.0031 0.0070 -0.0500 0.2360 -0.314 -0.5020  15.49 0.U 0.0231 0.0070 -0.0500 0.2260 -1.3574 -0.0857  14.49 0.U 0.0231 0.0070 0.0050 0.2260 -1.3574 -0.0857  14.50 0.U 0.0231 0.0070 0.0050 0.2260 0.1955 -0.7794  15.49 0.U 0.0231 0.0070 0.0050 0.2260 0.1955 -0.7794  15.49 0.U 0.0231 0.0070 0.0050 0.2260 0.1955 -0.7794  15.49 0.U 0.0022 -0.0127 0.0050 0.2260 0.1955 -0.7794  15.49 0.U 0.0022 -0.0127 0.0050 0.2260 0.1955 -0.7794  16.50 0.U 0.0022 -0.0127 0.0050 0.2260 0.1955 -0.7794	2 37 v.5v 0.4 10v.0 n3e0f15 v.0 0 0 0 0 FIRE  ALPMA RETA CMF1 CM1 CM1 YCPF1 YCPF1 CM72 CM7  -1.5m	2 37 v.5v 0.4 16u.0 n3=0f15 u.0 0 0 0 FIREU  ALPMA PETA CMF1 CM1 CM1 YCPF1 YCPF1 CM7 CM2  -1.5M U.0 -0.0012 mu.155 0.00m C.2365 1-1341 0.0494 0.6064 0.0169  -0.56 0.0 -0.5007 -0.220 0.0252 0.2613 -0.2997 0.0028 0.0099 -0.0083  0.42 0.0 -0.0023 -0.012 0.6033 5.2371 -0.3767 0.0036 0.0028 -0.0297  1.42 0.0 -0.0023 -0.012 0.6033 5.2371 -0.3767 0.0036 0.0028 -0.0297  1.42 0.0 -0.0023 -0.012 0.0527 0.2355 -1.0079 -0.0592 -0.0102 -0.0982  2.44 0.0 -0.0023 -0.012 0.0073 0.1621 0.06621 -0.0903 -0.0128 -0.0813  3.40 0.0 -0.0023 -0.012 0.0073 0.1621 0.06621 -0.0903 -0.0122 -0.0816  3.43 0.0 -0.0047 -0.0093 0.0073 0.1621 -0.5057 -0.1447 -0.0250 -0.0616  5.47 0.0 -0.1010 -0.0262 0.0365 0.2371 -0.3782 -0.2561 -0.6390 -0.0982  7.46 0.0 -0.1140 -0.027 0.0365 0.2371 -0.3781 -0.3231 -0.0501 -0.1329  7.46 0.0 -0.1140 -0.027 0.0365 0.2376 -0.3199 -0.3573 -0.0095 -0.1527  8.47 0.0 -0.1140 -0.027 0.0365 0.2376 -0.3199 -0.3573 -0.0095 -0.1527  8.48 0.0 -0.0131 0.0077 -0.014 0.3263 -1.0129 -0.0501 -0.0351 -0.1759  10.45 0.0 0.0133 0.0077 -0.014 0.3263 -1.0129 -0.0502 0.0075 -0.1527  8.48 0.0 0.0103 0.0077 -0.014 0.3263 -0.3783 -0.0075 -0.0152  11.47 0.0 0.0133 0.0077 -0.014 0.3263 -0.3783 -0.0077 -0.0716 -0.2439  12.49 0.0 0.0133 -0.0177 0.0050 0.2260 0.1955 -0.7796 -0.0192  13.50 0.0 0.0103 0.0177 0.0055 0.2260 0.1955 -0.7796 -0.0982 -0.2281  15.60 0.0 0.06231 0.0177 0.0055 0.2260 0.1955 -0.7796 -0.0072 -0.22843  15.60 0.0 0.06231 0.0177 0.0055 0.2260 0.1955 -0.7796 -0.0072 -0.22843  15.60 0.0 0.06231 0.0177 0.0055 0.3260 0.1955 -0.7796 -0.00857 -0.0794 -0.22883  15.60 0.0 0.06231 0.0177 0.0055 0.3260 0.1955 -0.7796 -0.0072 -0.3251  10.50 0.0 0.06231 0.0177 0.0055 0.3260 0.1955 -0.7796 -0.0072 -0.3251  10.50 0.0 0.00621 0.0077 0.0055 0.3260 0.1955 -0.7796 -0.0072 -0.3251  10.50 0.0 0.00631 0.0077 0.0055 0.3260 0.1955 -0.7796 -0.0072 -0.3251  10.50 0.0 0.00631 0.0077 0.0055 0.3260 0.1955 -0.7796 -0.0072 -0.3251	2 37 0.59 0.4 100.0 m3s0f15 0.0 0 0 0 FIREU  ALPMA REIA CMF1 CM1 CM1 YCPF1 YCPF1 CM72 CM2 CM2 XCPF2  -1.5H	2 37 v.5v 0.4 lou.0 n3s0f15 v.0 0 0 0 FIREU  ALPMA REIA CNF1 CN1 CN1 CN1 YCPF1 YCPF1 CNF2 CN2 CN2 XCPF2 YCPF8	2 37 v.5v 0.4 10v.0 r3s0f15 v.0 0 0 0 FIREU  ALPMA RE14 CMF1 CM1 CM1 VCPF1 VCPF1 CM2 CM2 CM2 VCPF2 VCPF2  -1.5m

- 5h	#FT4 6.6. 0.0 0.0 0.0 0.0	6.1-h 6.622 -0.11:1 -0.621	CH3 ====102 (+=102x	Co3 	ACFF3	0 0 1CPF3 =1-2633	C=F+	O FIXE	C84	*CPF+	YCPFA
.5e .46 .45	0.U 0.U 0.U	6.1+h 6.622 -0.11+1 -0.621	(10 10 1 c	V-0.11			0.0750				· · -
• • ¢ • • ¢ • • • • • • • • • • • • • •	0.U 0.U 0.U	-0.11.1 -0.11.1 -0.2-1			しゅしゃコイ			4-0224	0-0175	0.3046	0.2334
• • c • 4.9 • • •	0.U	-0-1101				0.0754 <u>-4.3749</u>	0.0244	U.G117	0.003A 0.0215	0.4772 _ 2.4574	0.15/2
. 4 6 . 4 3	C. U			0.0127			-0.0351		-0.0341	-0.1346	1.1122
							_=u_ud26_		_	- 1	0.6539
	- li - u	j _e naču J _{es} uace	1.0676	-0.076M			-0.1721		-0.0847	0.1015 	0.6938
	0.0	-0.4354		3.6205			-1.2216			0.1199	0.5167
	0.6			GAULE 9_			0.2764			_0.1224_	0.5268
• 4¢	0.0	C.C176	* 13**				-0.3332			0.1266	0.5108
											0.4777
-65	0.4										0.4493
.47	(+.+			6.0115						0-1126	0.4885
-44-	0.4									0.1088	0.4759
											0.4529 
. 69											0.4536
-51	II. li									0.0967	0.4343
. 6 7	0.0		Secot1							0.0091	0.4498
		-0.11.3			. <del>13.2611</del> .	0_3£34_	<u>-0.9.336</u>		.=0.3946.		0.3367
· · · · ·	···			-0.0063	204236	0.3430	-0.4072	-0.0637	-0.3766	0.0007	0.3904
			70000							=======================================	
		<del></del>						<del></del>			<del></del>
		· · · · · · · · · · · · · · · · · · ·									
	47 49 50 49	64 Uev 65 Uev 65 Uev 65 Uev 65 Uev 66 Uev 64 Uev 65 Uev	0.0 0.0 1.0 7  A5 0.0 0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0.0		0.0 - 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.0	0.0 - 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.0 - 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.0 -0.0078 -0.037 -0.037 -0.5830 -0.3024 -0.4663 -0.0578 -0.2199  A5	0.0 - 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.

	TEST PART MALE PAIDES PAI COME 1 DELS DELS DELS DELS TRANSITION											
	è		57 0.7		3-0F15 0		6 0	0 (		.,		
POINT	ALPHA	eFT.	C.	CLM	CY	CL.	CLL	CA	CAF	CAF	ACP	
	-1-50	1		4.2.163			-0-0071	0-3-15	0-1157		-1.5761	
3	-0.50	v. u	-0.0-11		-6.0375	6-6-33		0.3391	0.1136	0.2255		
_3		4.4		-0-1687			-0-0034	0-3423 .	-0-10-1		-1.3925	
•	1.40	0.0		-6.5550			-0.0032	0.3460	0.1059		-1.3950	
6	3.46	6.0		-0.5265			-0.0026	0.3664 5586.0	0-1018 0-0962		*1.4152 -1.4733	
7		G - d		-0.9204			3-0005	0-3332	20402		=1-6142	
6	5.40	0.0		-10 .070			-0-005+	0.3377	6.1705		-1-6577	
9	3.40	1-4		-1-3465			-0.0012		4-1030		-1.7524	
10	7.46	6.0		-1./252			-0.6025	6.3301	0.1070		-1.7625	
.11	B. 9.7	6.4		-2-11220			-0-0026	0.3358	-0-1150		-1-6235	
12	9.47	(·. v		-2.1636		0.6299	0.0000	0.3365	0.1216		-1.8541	
-13	10.64	6-4		-2691			-0-0065	4051-0	201276		-1-4593	
14	11-47	Cot	1.5725	-2. 7545	-0.6-1-	0.0332	-3.0076	0.3389	6.1337	0.2052	-1.8834	
15	12.46	Let.		-3-17ux		Eastual	-4-0042	6.3341	0-1375	0-1967	-1-8974	
16	13.51	6.0	1.0020	-3.5615	-0.6415	0-0217	-0-0063	0.3165	0.1432		-1.9127	
17	14.45	Lak.					-0.0086	0-3450	0-1445		-1.9305	
18	15.50	6.0		1/65	5-11 1-12 1-12 12 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-3.00A6	0.3334	0.1529	0.1506	-1.9421	
19	10.05	1.04		-Serlal			-0.E200	0-3104	0-1421		-1.95A0	
50	17.55	6.0		-5201			-0.0312	0.3133	9-1744		-1.9485	
-21	15-52	_u.u			-w.0375		-0-0-07	3.3179	J-1822		-1.9348	
32	19.53	C. L	3.07.1	+5.4475	-0.01-2	-6-0640	-0.0376	0.3154	0.1916	0.1238	-1.9177	

							<del></del> -					
		4.4.5										
	5		5× 0.7		3-4+15 0		0 0		O FIRE			•
INT	ALPHA -1-5c	of TA	Cr.F1	Cnl	Col	ACPF1	YCPF1	CNF2	CHZ	C+2	XCPFZ	YCPFE
ż	-0.5a	( · v	-0-0547 -0-0511	-5.0^10-j	( • v 1 + 3	1.2111	-0.6317	0.0617	0.0055	-0.0003	0-1874	-0.0544
<u> </u>	0-41	f C	-Cauluy		4.0015	Deut16	-2-1007	_=0_UZ10		_=0.0311	_0.1944	1.4798
•	1.44	0.0		-5-0052	u. 3754				-0-011-		0.1686	0.4663
6	3.40	0.4		-0 <u>-0</u> -1-2	0135 0-3110		-0.5626		-0.0137 -0.0254		0-1556 0-1797	0-7049 0-4288
<u> </u>				-100000	10111		m3-7428				0.1352	0.5390
e	5.48	0.0		-6.5195	6. (131	6-23-6	-0.7m75		-5.3375		0-1465	0.4529
٠		0.6		Corder			1.37ml			-0-1438-	0-1525	
16	7.46	0.0		-0.615		0.2017	0.1170			-0.1499	0.1373	0.4073
11 <u> </u>	B.47_ 9.47				<del></del>		-0.25+0		-0.0454		_0 <u>.1391</u> _ _0.1352	0.4449
13	10-45	0.0 u_u		=127			-0-7343				0-1277	0.4442
14	11.47	+.7		-0-2041		C-1456	7.1941		-5.6746		0-1254	0.4213
15	12.46	<u> </u>		-0.6634	4.04.55	C-1748	-0.0845	-=0.6435	-0.0733	-2.2849	0.1138	0.450\$
16	13.51	G. U	-0-0-4-	3-470-	C.C. 77		-U-A163				n.1188	0-4034
17 15	15.50	0.0	=6-6313.	-0.0071	<del></del>		-u.9722				0-1140 0-1130	0.4100
13	17.50	0.0	-0-1250	_	700 140		+0-3703	-			0-1076	0.3893
50	17.55	0.0	-0.6370	-0-005	6.0431		-1.16+8				0.1037	0.3879
21	18.52	0.4		<u>-0.0361</u>			+0+2656				0.0993	0.3719
2.2	14.53	0-0	-0.0050	0-6325	0.0023	-6.4175	-0-3790	-1.0180	-0.0946	-0.3775	0.0928	0.3706
		<del></del>					<del></del>					
	·											
							······································					
												<u>-</u>
						<del></del>		<del>- · · · · · · · · · · · · · · · · · · ·</del>				<del>.</del>
_				-								
			-									
						-						
						<u> </u>	<del></del>				<del></del>	

<del></del>												
	TEST 2		<u>ALM 8210=</u> 57 0.7	160.0 m	_C_Nt 3+0F15 0		DELZ 0 0	DEL3 DEL	A_IAANSIT O Flxe			
Int	ALPHA	DETA	Cut 3	(×3	C#3	ACPF 3	YCPF	C+F4	CHA	Cd4	XCPF4	YCPFA
	-1.58_	0.0	-5.1113	-0-110-	3 و شائد س	0.9255	-0-3A32	0.0659.	0181	0.4146	0.2582	0.2082
2	-6.50	L.U	-0-4474	-0+,000	4.0050	1.2226	-0.3800	0.0241	0.0116	-0.0079	0.4001	-0.0980
3	0.41	لامنا		-6-111-	-L-0469		-0.3868	0043_		0.0230_	-1.2856	
•	1.44	0.3	-0.6372	-6.314-	0-0115	C-0371	-0.3798	-0.0403	-0.6028	-0.0391	0.0589	0.8104
5	2.44	0 - ¥		-C.LZ13.			-0.3799				_0-1343	
6	3.46	0.0	1150.0	f 1 4 3	-6-05-40	0.6137			-0.6174	-0.0801	0.1326	0.6090
<u> </u>		Call	-0-3-44		i dinga	1.2072			-0-u240		<u> </u>	0.5519
•	56	6.0	-0.121	-( -1 )55		C.7055	-0.3798	-3.2347	-0-0311	-0-1194	0.1323	0.508A
9	- 6-46	0.0	-0-0-20	-6124	O_DCE6_	2.5354		- TG-2852		-0.1495	_0-1256	0.5206
ŭ	7.46 8.47	G . U	3.0125	201102	-0.0946	1-4451	-0.3799	-u.3473 =u-4022	-0.0469	-0.1746	0.1349	0.5027
ž	9.47	C.J	-7.0157		0.0163	6.9210		-0.4605	-0.0589	0-1739	-0-1241	
•	10.44	0-4					-0.3821 -0.3737		0563-0=	-0.2215	1.1279	0.4809
•	11.47	U - U	-1.3270		0103	(.6)77		-0.5656	-0-0661	-3.2706	0.1169	0.4784
5	12.00	6.3	-0-21-3			. Cabala	-			0.2937	3-1124	0.4672
6	13.51	0.0	-0.7/+1		v=0.94	C.4363		-0-6470	-0.0726	-0.3122	0.1040	0.4511
<u>ž                                    </u>	18.85	0.4	0		-0.0007		=0-37+1	0-7361	<u>0660</u>	-0-2996_	0.0897	0.4070
9	15.50	U. v	-6-115-	00 17	J. 1047	v.3332		-0.1254	-0.0A13	-0.3691	0.0985	0.4460
•	10.07	le a le	-0-C6		4.44.37	1-5-12		-4-5912			0.0941	0.4321
Û	17.55	0.6	0.011.	60:012	u.(·	0-16-9	0.0	-0.9347	-0.042A	-0.4071	0.0866	0.4355
1	18.52	0.0	Caldal	0.:01=	-u_uie6	:.2255	-0-1349	-0.9017	-0-0816	-0.4236		0-4284
5	19.53	6.0	0.0143	-4-(460	-6.6013	-0.4261	-0.0674	-1 • v 393	-0.0549	-0.4094	0.0817	0.3729
<del></del> _	<del></del>										·····	
						<del></del>						

					•				•		
	TEST	FART P	ALS RAIGS				10EL20	IEL3 DELA	TRANSITI	04	
	ž	34 5.	57 lel	186.G m	3.0F15 0	. 0	0 G	0 0	FIZEU		
NT	ALPHA -lang	SETA No.U	FC-1256	CLM	CY	CL4	CLL	CA 0-3071	CAH 0-1035	CAF	ACP
	-0.54	<u> </u>	-0.02-4		-0-0266		-0.0132 -0.0132	0.1054	G-1036		-2.2557
	0.04	ـــالامنا .ــ		_26_1452_			-6-0124	0.3081			. =1 -2694
S)	1.46	0.0		-0.2225			-0.0125 -0.0125	0.3056	0.6957 _6.0981		-1.2596 -1.4025
	3.46	0.6		-(456			-C-0035	0.3036	0.1025		-1.4662
		4.4		-12-12-1			-2-0063	4.3006	_0-1015_		-1.5951
•	5.44	0.4		-1.0422 - <u>2186.1-</u>		0-0011	-0.0045 -0.0066	0.244H	0.0969		-1.6496
)	7.45	V . U		-1./504			-0-0042	0.3100	0.107a. 0.1181		-1.724 <del>6</del> -1.7994
	6-51	<u> </u>	1-11-1	-2-456	-2.6313	_0.02:2	-3-0067	4.3654_	_uallāb_	0.1673	-1.8280
?	4.53	C.U		-7.36.2			-0.0086		0-1244	0.1848	-1.8639
<u>.                                    </u>	11.55	<u></u>		-2-7161 -2-7017			-0.0038	0.31AG	C-1300		-1.8761
	12.53				-5-4-03		-0-0005				=1.4904
•	13.54	6.0		-3.700+			-0.0091	0.30=5	U-1444		-1.6915
<u>.                                    </u>	_10 <u>_53</u> _ 15.50	C.u			-0-0200 -0-0200		0.0025	0.2496	0.1544		-1.6999
_	10.56	<u> </u>			-1-4-694		-0.0175	0-1363	1088		-1.8991
u	17.58	0.0	5.6010	-5-113-		0-46		9-3041	6-1754	0.1207	-1.9068
2	<u> 15.57</u> 19.60	U.U			<u></u>				6_190b		-1.9150
- 	17.00		3-0-00	-707480		-0.0332	-0.0317	0.3165	0.1976	0.1154	-1.9116
								<del> </del>		<del> </del>	
											•
									_		
	5000										
											· · · · · · · · · · · · · · · · · · ·
_							·				

10F				<del></del>								
	SI.											
						•0 						
_				Cm]	Ch1	a CPF I	YCHFI	CNF2	CuS	CAZ		YCPF2
												-0.0300
_		<u> </u>			_ ددنامه _							-1-9608
1.4	6	C. U			0.0624	0.1747	5480.0-			-0.G317	0.2138	0.5090
					_=c+0151							0-4478
											0-1041	0.4516
	100	1-000	5 - 1 - 1 - 1 - 1 - 1 - 1	100		10.0						0.4797
		999053			0.00							0.4541
0.000												0.4523
100000000000000000000000000000000000000		4.4										_0.0013
4.5	53		-0.01	-0.000-	3.0456	: - De 17	-2.3775			-0.2127	0.1331	0.4252
		Lou						-0-5565	-0.0712	-0-5351	0.1279	0,4168
0.70											0.1252	0.4230
												-0-4204
												0.4000
												0.4095
				0-0-17	-6-0-13	-2-6441						0.3472
17.5	50	U. U		-0.0052	0.0152	1.1500					0.1039	0.3796
		0.v.						-0.4943	-0.0935	-C-3714	0.0989_	0.3717
19.0	6 u	0.0	-6.0053	0.0022	-9.0172	-6.0144	3.2695	-1.0292	-0.6928	-0.3741	0.0902	0.3634
										······		
	-						<del></del> -					<del></del>
												<del></del>
	11.1 1.0 2.0 3.0 3.0 7.0 6.0 11.1 12.1 13.1 15.1 15.1	VEST.	1FST PAWI 7 2 39 vo  ALPMA BFTA  TLOC GOU  GOAZ GOU  1.46 C.V  2.44 GOU  3.46 GOU  4.40 GOU  5.43 GOU  5.43 GOU  5.43 GOU  11.55 C.V  12.53 GOU  12.53 GOU  13.54 GOU  14.53 GOU  15.54 COU  15.55 COU  17.55 COU	7 39 veby 1:1  ALPHA BFTA CAF1  -0.30 6.0 -0.63e1  -0.30 6.0 -0.63e1  1.46 C.0 -0.62e3  2.44 6.0 -0.62e3  3.46 C.0 -0.62e3  3.46 C.0 -0.62e3  7.44 6.0 -0.63e3  7.44 6.0 -0.63e3  7.45 6.0 -0.63e3  4.53 6.0 -0.63e3  4.53 6.0 -0.63e3  10.53 6.0 -0.63e3  11.55 C.0 -0.62e3  12.53 0.1 -0.62e3  13.54 6.0 -0.62e3  14.53 6.0 -0.62e3  15.55 C.0 -0.62e3  15.56 C.0 -0.62e3  17.50 0.0 -0.633v	TEST PANT FALM RAIGHS PRI  2 39 V-5V 1-1 10V-6 M  ALPMA BETA CAF1 CM  T-0-0V 6-U -0-35M -0-306/  1-46 C-U -0-035M -0-306/  1-46 C-U -0-02M -0-35M  2-44 B-U -0-02M -0-35M  3-46 G-U -0-02M -0-30M  5-44 B-U -0-02M -0-30M  7-44 B-U -0-02M -0-30M  7-44 B-U -0-02M -0-00T  5-51 B-U -0-02M -0-00T  5-51 B-U -0-02M -0-00T  5-51 B-U -0-02M -0-00T  10-53 B-U -0-02M -0-00T  11-55 C-U -0-02M -0-00T  12-53 B-U -0-02M -0-00T  13-54 B-U -0-02M -0-00T  13-55 B-U -0-02M -0-00T  15-56 C-U -0-02M -0-00T  15-56 C-U -0-02M -0-00T  15-56 C-U -0-02M -0-00T  17-56 B-U -0-03M -0-00D  16-57 B-U -0-03M -0-00D	TEST PANT FALM BAIGNED	TEST PANT FALM BAIGES	TEST PANT FALM RAIGNS	TEST PART FALM RAIGHS PRI CORF. 1 DELS DELS DELS DELS CORP.  2 39 voby 1:1 100.0 m340F15 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEST PART FALM EALGED	TEST PART	TEST PART FALM RAIGNS

0.01/3 -0.0101 G. 0.01/3 -0.0101 G. 0.01/7 -0.005 G. 0.01/7 -0.005 G. 0.01/1 -0.005 G.	#3 RCPF3 ##32 C-6AH3 ##32 C-6AH3 ##5000 C-6777 ##600 C-6777 ##600 C-6777 ##600 C-6777 ##600 C-6777 ##600 C-6777	-0.3840 -2.3747 - -0.2233 - -0.2358 - -0.3766 -	CMF4 CM4 0-6027 0-01 0-6301 0-01	102 -0.0032 0340.0200 066 -0.0375		867 056
6.01/3 -0.0101 6. 5.0124 -0.005 0. 6.0177 -0.0085 0. 6.0141 -0.0135 -0. 6.0040 0.0035 -0. 6.014-7 -0.0055 0. 6.014-7 -0.0055 0. 6.014-7 -0.0175 0. 6.014-1 0.0175 0.	030h   5009 0304	-0.3840 -2.3747 - -0.2233 - -0.2358 - -0.3766 -	0.0301 0.01 0.0125 0.00 0.0535 -0.00	02 -0.032 034 -0.0204 066 -0.0375	0.3373 -0.16 -0.26431.55 0.1229 0.76	056 992
0.0124 -0.005 0.00.177 -0.005 0.00.1177 -0.005 0.00.1181 -0.00135 -0.00.1181 -0.0055 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0.00.1175 0	0000 C.6270 0000 C.6777 0005 C.6290 0015 N.6490 0013 C.6290	-0.2233 - -0.2233 - -0.2358 - -0.3766 -	0-0125 - 0-00 0-0535 -0-00	0340.0200. 066 -0.0375	-0-2683 1.56 0.1229 0.76	992
	0040 (.0777 0045 . 2000 0045 . 0015 0045 . 0015 00667 . 00677	-0.2233 - -0.2358 - -0.3766 -	0.0535 -0.00 0.0904 +0.01	066 -0.0375	0.1229 0.7	
Course (confidence of the confidence of the conf	0415 n-8450 4633 6-62-4 0666 6-62-9	-0.376h -		\30 <del>-</del> 0.0528	8.1447 A E	_
00-01-7 #0-035 6-0-017- 0-0-017- 0-0-017- 0-0-017- 0-0-017- 0-0-017- 0-0-017- 0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	0665 6.62±0	-:-3749 -		190 -0.3814		137
0.03.5 -0.1175 0.		-1 77.40 -	Galb57		0-1416 0-5	
9.0413 0.6606 0.	dill65715.		10.0- FOLS.D			997
	U005 -6.4776					967
	11116 un6269					
	360+ -1-1772					762
			-0-5341 -0-46 -0-5637 -0-46			774
				731		744 664
U.A. 0.2304 U.	J. 2? -2.0765	-0.3602 -	16.0- 1.66.0-	746 -0.3151		536
			0.73060.u			252
			-0.7982 -6.06 -0.8854 -0.30			368
			-0.9259 -0.0			350
	504E-1-3402	-4.9101 -	-0-241# -0-CI	6620.4168_		245
-C.v1+7 -A.G095 0.	.0084 G.6450	-0.5669 -	-1.0-63 -0.0	743 -0.4185	0.0852 0.3	3998
	· · ·					
•		· · · · · · · · · · · · · · · · · · ·	<del> </del>	<del></del> -	<del></del>	<del></del>
			<del></del>			
			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		

TEST MART   PALE RALD=6	E	LIGINEE 1 OF 3 1 OF 1	נדעם אנ	<u>eelüPhtiai</u>	- FFFIFKIA	<u> </u>		ISSILE TAI			AER	ODYNAMIC MIND TUNNEL (4)
A												
2			4407	A. D. C. C.	4 5-1	CONE		. DE 3 (	.c. 3 . 051 A	T.) A N. E . T. (	<b>^</b>	
2 -0.46	POINT	ALPHA	6FT &	C*	CLM	CY	CLN	CLL	CA	CAR	CAF	ACP
1 0.64 0.0 0.174 -0.2722 -0.0722 (.0005 -0.0107 0.7900 0.0962 0.1014 -1.2992 0.2992 0.2992 0.1014 -1.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0.2992 0	1											
1.00 U.U 0.1741 -0.2772 -0.0727 (.0005 -0.0107 U.7900 U.0986 0.1018 -1.2992 5 2.63 0.0 U.02709 -0.1313 -0.0400 U.0278 -0.0128 U.2811 0.1005 0.1460 -1.3743 -0.0400 U.0278 -0.0128 U.2811 0.1005 0.1460 -1.3743 -0.0400 U.7860 U.78	_											
6 3.44 0.0 6.3844 -0.075 0.0755 0.0764 -0.0004 0.7866 0.1016 0.1853 -1.5282 7 A.AB 6.0 1.5760 -0.0741 -0.0750 0.0512 -0.0003 0.2867 0.1014 0.1847 -0.6069 8 5.47 0.0 0.6741 -0.074 -0.0306 0.0337 -0.0003 0.2833 0.1008 0.1026 -0.6674 9 5.48 0.0 0.4930 -0.0257 0.0245 -0.0075 0.2879 0.1088 0.1792 -0.7580 10 7.00 0.0 0.9320 -0.0257 0.0257 0.0249 -0.0075 0.2879 0.1119 0.1775 -0.8141 11 8.50 0.0 0.0320 -0.0252 0.0252 -0.0067 0.2879 0.1205 0.1750 -0.8523 12 9.49 0.0 0.2401 -7.3467 -0.024 0.0209 -0.0055 0.2972 0.1244 0.1728 -0.8848 14 10.53 0.0 0.0 0.0000 -0.0000 0.2960 0.1391 0.1603 -0.8848 15 12.55 0.0 0.0 0.0000 -0.0000 0.2900 0.1391 0.1603 -0.9089 16 13.55 0.0 0.0 0.0000 -0.0245 0.0000 0.2956 0.1499 0.1457 -0.9082 17 14.56 0.0 0.0 0.0000 -0.0247 0.0000 0.2956 0.1499 0.1457 -0.9082 18 15.56 0.0 0.0 0.0000 -0.0277 0.0000 0.2956 0.1499 0.1457 -0.9082 18 15.56 0.0 0.0 0.0000 -0.0277 0.0000 0.2956 0.1499 0.1457 -0.9082 18 15.56 0.0 0.0 0.0000 -0.0000 0.2956 0.1499 0.1457 -0.9082 18 15.56 0.0 0.0 0.0000 -0.0000 0.2956 0.1499 0.1457 -0.9082 18 15.56 0.0 0.0 0.0000 -0.0000 0.2956 0.1499 0.1457 -0.9082 19 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1457 -0.9082 19 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1497 -0.9082 19 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1497 -0.9082 19 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1576 0.1391 -0.9058 10 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1576 0.1391 -0.9058 11 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1576 0.1391 -0.9058 12 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1576 0.1391 -0.9058 13 15.50 0.0 0.0000 -0.0000 0.2956 0.1499 0.1576 0.1391 -0.9058	•											
7 A.AB	_5											
# 5.47	6		_									
6         bear         0.0         Outure         -1.0         -1.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.	P				777							
1		0.04		_					D-2874	0-1068	0.1792	-1-7580
12 9.49 0.0 1.2451 -7.3467 -9.0224 0.0209 -9.0255 0.2972 0.1244 0.1778 -1.8844 1.153 ( 1.4270 -2.4751 -0.0215 0.6125 0.6128 0.2481 0.1321 0.1640 -1.8970 1.154 0.0 1.4757 -3.0713 -0.0215 0.6121 -0.0178 0.2494 0.1391 0.1603 -1.9089 1.5255 ( 1.4741 -3.4130 -0.0241 0.0130 -0.0088 0.3024 0.1476 0.1551 -1.9134 1.535 0.0 1.4740 -3.7222 -0.02473 0.6244 -0.0000 0.4956 0.1499 0.1457 -1.9082 1.1 14.55 0.0 1.4740 -1.131 -0.0211 -0.0100 0.2956 0.1499 0.1457 -1.9082 1.1 14.55 0.0 2.1547 -4.3977 -()227 0.0173 -0.0100 0.2908 0.1543 0.1391 -1.9059 1.1 15.50 0.0 2.127 -4.3977 -0.0227 0.0173 -0.0100 0.2908 0.1578 0.1330 -1.9016 1.1 1.501 0.0 2.5231 -0.0006 -0.0151 0.2908 0.1543 0.1314 -1.9008 1.1 15.50 0.0 2.5231 -0.0006 -0.0006 -0.0151 0.2908 0.1578 0.1314 -1.9008 1.1 15.50 0.0 2.7022 -5.6472 -0.0268 -0.0006 -0.0151 0.2912 0.1700 0.1277 -1.8863 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.50 0.1 13.5	1.0											
14 10-53 C.L 1-4210 =2-121 = 0-0212 0-0215 0-0121 0-1321 0-1640 =1-8970  10 11-50 0.U 1-57-7 -3-7713 =0-0215 0-0121 =0-0178 0-2770 0-1391 0-1603 =1-9089  15 12-55 0.U 1-74-1 =1-110 =0-021 0-0120 =1-0008 0-3028 0-1476 0-1551 =1-9134  16 13-55 0.U 1-74-1 =3-722 = 0-0223 0-0224 =0-000 0-2956 0-1499 0-1457 =1-9082  1/ 14-55 0.U 2-15-0 =-1133 =0-021 0-0008 0-2533 0-1543 0-1391 =1-9059  1/ 14-55 0.U 2-15-0 =-1133 =0-0217 0-0100 0-2908 0-1578 0-1391 =1-9059  1/ 15-50 0.U 2-127 =0-0377 =0-0277 0-0100 0-2908 0-1578 0-1330 =1-9016  1/ 15-50 0.U 2-5270 =0-7573 =0-051 =0-0006 0-2059 0-1585 0-1314 =1-9008  2/ 17-61 0-0 2-7023 =5-0101 =0-0173 0-0107 0-2909 0-1866 0-1094 =1-8863			C-									
15 12.55 G.H 1.7ml -3.mlin -4.02ml 3.01m0 -3.02m 0.302m 0.1476 0.1551 -1.9134 10 13.55 G.H 1.47ml -3.7222 -4.0243 0.6244 -0.000m 0.2956 0.1499 0.1457 -1.9082 11 18.55 U.H 2.15mu -8.1134 -4.0221 -1.0237 -9.61652 0.2533 0.1543 0.1543 0.1381 -1.9059 16 15.50 C.H 2.4127 -4.3974 -1.0227 0.0133 -0.0100 0.290m 0.1578 0.1330 -1.9016 19 16.61 C.H 2.5212 -8.7473 -4.0214 -4.0038 -0.0140 0.2852 0.1545 3.1314 -1.9008 26 17.61 0.0 2.7622 -5.6472 -0.0265 -0.0265 0.0151 0.2912 0.1706 0.1207 -1.8863 21 13.60 0.H 2.0734 -5.0101 -1.0173 0.0142 -0.0174 0.2940 0.1846 0.1094 -1.8863			-									
10 13.55												=
1/ 10.56 U.U 2.15#U =0.113/ =0.022/ =0.0062 0.2533 0.1503 0.1391 =1.9059 16 15.50 C.V 2.4[c7 =0.377v =(.3727 0.0133 =0.0100 0.290h 0.1578 0.1330 =1.9016 19 10.01 (.V 2.5210 =0.7573 =0.0151 =0.0100 0.2099 0.1578 0.1314 =1.9006 26 17.61 0.0 2.7(c2 =5.6v/2 =0.0266 =0.0151 0.2912 0.1706 0.1707 =1.8863 21 13.60 0.0 2.6744 =5.0101 =1.61/3 0.01v2 =0.0176 0.2090 0.1866 0.1094 =1.8817	Charles											
16			-									
26 17.41 0.0 2.7022 -5.6472 -0.1224 -0.0066 -0.0151 0.2912 0.1706 0.1207 -1.8863 21 18.60 0.0 2.6724 -5.8101 -0.173 0.01-2 -0.0176 0.2940 0.1846 0.1094 -1.8817	_			7. 11e7	-4.397+	-0.3227						
21 18.60 0.u 2.6724 -5.610i -1.61/3 0.01-2 -0.0176 0.2960 0.1866 0.1094 -1.6817												
			-		-							
											W 1049	
									<del> </del>	· · · · · · · · · · · · · · · · · · ·		
							•					
				•								
			<del></del> -									
				<del></del>		<del></del>						
								_				
	****											
						<u> </u>						

EFI_	1_0F1		-								•	
	TEST		ALP 8410-		CUMF		1 CEL2		A THANSIT			· <del></del>
GINT	ALPHA	PF T A	Chri I	C+1	C=1	a CPF 1	YCPF1	CNF2	CHP	CBS	XCPF2	YCPF2
<del></del> -					7-6-3-	0.1577		0.4513	6.0076	0.005A	-0.1489	0.1723
4	-0.5r	0.0	-0.00-35	-9.0101	4.000m	0.7641	-0.0163	0.0213	££00.6	J.0018	0.1542	0.0836
<u></u>	1,44	0.0	-0.0219 -0.025	-0-0-1-1 -0-0053	U-0151	<u>616.</u> 11=74	-0.4335	_=0.0122 =0.0557	0_0_2p 0_112	-0.0324	_ <b>0.2279</b> _ 0.1972	1.4217 0.5716
	2.63	Soul							-0.018d		- 0-1844	0.4333
6	3.44	U.L	-0-0114	-6.0367	v.0154	1540.0	-1.3032	-0-1546	-0.6250	-0.0697	0.1626	0.4526
<u> </u>		_ بلمان	-u-teta.	V1	1.067-	0-1-122	2369	-0-2GA5	-0-0314		0-1533	0.4505
6	5.47	(.,	-0.03-1		-L.0014	9.19.0	0-2025			-0.1176	0.1511	0.4577
10		F.U					-0.0003				_0.1A38_	0.4710
1	7.46	(, ) 		-6.6367	-5.0(25 	0-19-0	0.0734			-2.1668 	0-1363	0.4449 0.4411
5	4.44	(.)		-0-1050	-7-61-2	(.)356	7.48cb		-v.0681	-0.2166	0.1334	0.4243
<u> </u>	14.53	Lai		-3-311-	فحلياء	Casel	-1-2646		-0.0716	2363	0-1270	0.4228
4	11.50	11.5	-3.4737	-(145	0.0023	0.1441	-6.0976		-0.0774	-0.2612	0.1236	0.4173
15	12.55	Dav.		وحدثهمناهه	<u></u>		≠4.2417				_0-1165_	9-4205
16	13.55	0.0		-6. no17	9-10-0	0.0507			-0.0463		0.1165	0.4067
17	<u>16.5</u> 0 15.50	6.9 t			116_						0-1126	
19	15076	- 4-3		-9-046 	u.ÿ255	0-1519	-0.9600		-0.0968		0-1099	0.3951 0.3925
20	17.41	U. J	-6.02-1		0.0219	0.1657			-0.0967		0-1026	0.3859
21_	19.51	0.4	-0.6050	مبدد من	-U-Guel-	-9-1361			-0.0990		-0-0389	0.3730
25	19.04	0.6	5666.0-	2500.0	0.00e0	-0.4204			-0.0953		0.0922	0.3570
		-										

	CNF3 CN3 -0.01/2 =0.01 -0.21/4 =0.01 -0.21/4 =0.01 -0.02/7 =0.01 -0.02/7 =0.01 -0.01/2 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01 -0.01/4 =0.01	0 03-0F15 0  3	# CPF3	0 0 VCPF3	0 CAF4 0-055H 0-0230 -C-0166 -0-0503 -0-0414 -0-1374 -0-2414 -0-2414 -0-3571 -0-4193 -0-4733 -0-5413 -0-5413 -0-5413 -0-7019	-0.0334 -0.0354 -0.0354 -0.0464 -0.0513 -0.0578	CMA  -0.0116 -0.0146 -0.0199 -0.0379 -0.0797 -0.1621 -0.1757 -0.1550 -0.2765 -0.2765 -0.2765 -0.2765 -0.2775 -0.3045	0.1100 0.1349 0.1396 0.1403 0.1310 0.1299 0.1223 0.1222 0.1123	YCPF4 0.20A2 -0.1951 1.2044 0.7537 0.5773 0.5880 0.5082 0.5291 0.4919 -0.4545 0.4026 0.4775 0.4728
-1.56	-0.0122 -0.01 -0.0122 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01	0m3	7.5174 7.5474 6.2290 0.5474 6.6477 6.6473 2.5271 0.6724 6.5773 0.6925 1.6976 7.3869 C.51 20 6.657 20 6	-0.3611 -0.3749 -0.3749 -0.3749 -0.3800 -0.3800 -0.3751 -0.3750 -0.3600 -0.3600 -0.3600 -0.3600 -0.3747 -0.3749 -0.3749	0-055 0-0230 	0.0144 0.0161 -0.0055 -0.0132 -0.0192 -0.0192 -0.0384 -0.0464 -0.0513 -0.0578 -0.0677 -0.0734	0.0116 -0.0146 -0.0149 -0.0379 -0.0797 -0.1221 -0.1757 -0.1550 -0.1757 -0.2285 -0.2585 -0.2585	0.2583 0.4267 -C.1146 0.1100 0.1849 0.1396 0.1403 0.1310 0.1229 0.1223 0.1223 0.1222 0.1223	0.20A2 -0.1951 1.20AA 0.7537 0.5773 0.5600 0.5A10 0.5082 0.5281 0.4919 0.4545 0.4026 0.4725
-0.5h 0.d C.se 0.d C.	-7.7140 -0.11 -0.1025 -0.11 -0.1025 -0.11 -0.1025 -0.11 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12 -0.1025 -0.12	10# C.0075 Cum U.GQ1J. 12c C.0066 174 G.0116 174 G.0116 175 U.GC25 CYO U.GC25 CYO U.GC25 CYO U.GC25 CYO U.GC25 175 C.0069 175 C.0069 175 C.0069 175 C.0069	7.5474 G.2290 0.54rC 0.54rC 0.54rC 0.54rZ G.6433 2.5371 0.4724 6.5723 0.4925 1.4974 7.3849 C.5727 G.6434 7.3849 C.5728	+0.3749 -U.3748 -0.3749 -0.3846 -0.3745 -0.3746 -0.366 -0.366 -0.366 -0.3676 -0.3747 -0.3747	0.0236 -C.0106 -0.0503 -0.0414 -0.1374 -0.2414 -0.3571 -0.3571 -0.4733 -0.5413 -0.5413 -0.5413 -0.5413	0.0161 	-0.0046 -0.0199 -0.0379 -0.4528 -0.0797 -0.1621 -0.1757 -0.1550 -0.1757 -0.2285 -0.2588 -0.2588	0.4267 -0.1144 0.1100 0.1449 0.1396 0.1403 0.1403 0.1209 0.1223 0.1222 0.1123 0.1145	-0.1951 1.2944 0.7537 0.5773 0.5080 0.5082 0.5082 0.5281 0.4919 0.4565 0.4028 0.4775
C.se U.J.  1.44 U.O.  2.43 G.H.  3.44 U.O.  4.47 U.O.  5.47 O.U.  5.47 O.U.  5.50 U.O.  7.48 U.U.  7.48 U.U.  13.53 U.O.  12.55 U.O.  13.55 U.O.  13.55 U.O.  14.56 U.O.  17.01 C.U.  13.00 U.O.  13.0	-0.6026 -6.66 -0.627 -0.01 -0.642 -0.01 -0.642 -0.01 -0.615 -0.62 -0.615 -0.62 -0.616 -0.62 -0.616 -0.62 -0.616 -0.62 -0.616 -0.62 -0.616 -0.62 -0.616 -0.62	Cub	0.2290 0.5140 0.5141 0.5241 0.6433 0.5371 0.6325 0.6925 0.6925 0.6926 0.5126 0.65126 0.65126 0.65126 0.65126 0.65126 0.65126	-U.3748 -0.3749 -0.3800 -0.3806 -0.3756 -U.3746 -0.3600 -0.3600 -0.3600 -0.3747 -0.2610 -0.3749 -0.3749	-0.0166 -0.0503 -0.0914 -0.1374 -0.1667 -0.2414 -0.3571 -0.4733 -0.4733 -0.5413 -0.5413 -0.7019	-0.0019 -0.0055 -0.0132 -0.0192 -0.0334 -0.0364 -0.0464 -0.0464 -0.0513 -0.0536 -0.0636 -0.0636	-0.0199 -0.0379 -0.0797 -0.1621 -0.1757 -0.1550 -0.1757 -0.275 -0.275		1.2044 0.7537 0.5773 0.5000 0.5010 0.5082 0.5291 0.4919 0.4565 0.4726
1.44 U.0 2.43 GAH 3.44 U.0 4.47 U.0 5.47 U.0 5.47 U.0 5.50 U.0 9.49 U.0 13.53 U.0 13.55 U.0 13.55 U.0 15.50 U.0 15.50 U.0 17.51 U.0 17.51 U.0 17.51 U.0 17.51 U.0	-0.027 -0.01 -0.005 -0.01 -0.005 -0.05 -0.0164 -0.05 -0.0164 -0.05 -0.005 -0.5 -0.025 -0.05 -0.0171 -0.05 -0.0171 -0.05 -0.0171 -0.05 -0.0171 -0.05 -0.0171 -0.05	12c 0.0000 174 0.011a 179 0.0025 180 0.0005 180 0.0055 1721 -0.0701 181 0.0007 181 0.0009 181 0.0009 181 0.0007 181 0.0007	0.54FC 0.5797 0.6477 0.6433 0.5271 0.6724 0.5773 0.6925 1.6494 0.3169 0.5777 0.6925 1.6494 0.5777 0.6925 1.6494 0.5777 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925 0.6925	-0.37 yy -0.3800 -0.3800 -0.3756 -0.3756 -0.3600 -0.3806 -0.3600 -0.3777 -0.2610 -0.3799	-0.0503 -0.0914 -0.1374 -0.2414 -0.2414 -0.3571 -0.4733 -0.4733 -0.5413 -0.5413	-0.0055 -0.0132 -0.0132 -0.0253 -0.0334 +0.0364 +0.0464 -0.0513 -c.0573 -0.0636 -0.0636 -0.0636	-0.0379 -0.0797 -0.1721 -0.1550 -0.1757 -0.1914 -0.2785 -0.2785 -0.2795 -0.3045	0.1100 0.1349 0.1396 0.1403 0.1310 0.1299 0.1223 0.1222 0.1123	0.7537 0.5773 0.5400 0.5410 0.5082 0.5291 0.4919 0.4545 0.4028 0.4775
2-43 Gall 3-44 U-0 4-47 U-0 5-47 U-0 5-49 U-0 5-50 U-0 9-45 U-0 12-53 U-0 12-55 U-0 13-55 U-0 13-55 U-0 13-56 U-0 15-56 U-0 13-61 U-0 13-61 U-0 13-61 U-0		174 0-0114  A29 0-0125  C40 0-0065  A50 0-0655  A51 -c-0701  A51 3-0100  A55 0-065  A51 0-065  A52 0-066	5.5797 6.6433 7.5373 10.6726 6.5773 0.6925 10.6925 10.6926 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925 10.6925	-0.3800 -0.3806 -0.3755 -0.3756 -0.3600 -0.3600 -0.3600 -0.3600 -0.3777 -0.2610 -0.3799	-0.1374 -0.1374 -0.1647 -0.2414 -0.3571 -0.3571 -0.4733 -0.4733 -0.5413 -0.5413	-0.0132 -0.0192 -0.0193 -0.0354 -0.0464 -0.0513 -0.0578 -0.0677 -0.0734	-0.0528 -0.0797 -0.1621 -0.1757 -0.1757 -0.2785 -0.2785 -0.3785 -0.3785	0.1469 0.1396 0.1396 0.1403 0.1310 0.1223 0.1223 0.1222 0.1145	0.5773 0.5600 0.5610 0.5082 0.5291 0.4919 0.4565 0.4028 0.4775
3.44 U.G AAR C.L 5.47 O.V 5.49 U.G 7.48 U.G 4.49 U.G 4.49 U.G 11.53 U.G 12.55 U.G 13.55 U.G 15.50 U.G 17.61 U.G 13.61 U.G 17.61 U.G 13.60 U.G	-0.0004 -0.00 -0.0051 -0.00 -0.0161 -0.00 -0.0003 0.00 -0.0003 0.00 -0.0003 -0.00 -0.0003 -0.00 -0.0161 -0.00 -0.0161 -0.00 -0.0161 -0.00 -0.0161 -0.00 -0.0161 -0.00	0.0025 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005	G.6477 G.6433 J.5371 J.6724 H.5703 D.6925 H.64946 C.5727 G.6450 H.6450 H.6450 H.6450 H.6450 H.6450 H.6450 H.6450	-0.3hii -0.3751 -0.3756 -0.3500 -0.3600 -0.3600 -0.3600 -0.3797 -0.2610 -0.3799	-0.1374 -0.1647 -0.2414 -0.2930 -0.3571 -0.4193 -0.4733 -0.5413 -0.5413 -0.5413	-3.0192 -0.0334 -0.0354 -0.0464 -0.0578 -0.0578 -0.0677 -0.0677	-0.0797 -0.1021 -0.1727 -0.1550 -0.1757 -0.2785 -0.2785 -0.2795 -0.3045	0.1396 0.1394 0.1403 0.1310 0.1223 0.1223 0.1223 0.1103 0.1145	0.5600 0.5082 0.5082 0.5291 0.4919 0.4545 0.4628 0.4775 0.4728
5.47 0.0 5.49 0.0 7.48 C.0 5.50 0.0 9.49 0.0 10.53 6.0 11.54 6.0 12.55 0.0 13.55 1.0 14.56 0.0 15.50 0.0 15.50 0.0 15.50 0.0 15.50 0.0 15.50 0.0 15.50 0.0	-0.(1-F -0.0) -0.0003 0.6/7 -0.0011 -0.00 -0.0011 -0.00 -0.0111 -0.00 -0.0121 -0.00 -0.0121 -0.00 -0.0121 -0.00	CVS	7.5371 	-0.3796 -0.3796 -0.3600 -0.3896 -0.3896 -1.3797 -0.2610 -0.3799 -0.3799	-0.2414 -0.2930 -0.3571 -0.4733 -0.4733 -0.5413 -0.5413	-0.0334 -0.0334 -0.0364 -0.0464 -0.0578 -0.0578 -0.0636 -0.0677 -0.0734	-0.1021 -0.1727 -0.1550 -0.1757 -0.1916 -0.2785 -0.2785 -0.2795	0.1394 0.1403 0.1310 0.1223 0.1223 0.1222 0.1103 0.1145	0.5410 0.5082 0.5291 0.4919 -0.4545 0.4028 0.4775
7.88 (.0 7.88 (.0 5.50 (.0 9.85 (.0 11.53 (.0 11.55 (.0 13.55 (.0 13.55 (.0 15.56 (.0 15.5	-0.01=4 -() 0.0003 0.67 -0.0341 -0.67 -() -0.0240.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01 -0.0124 -0.01	466 0.0655  721 -0.0701  241 2.0031  131 2.0100  235 0.023  091 0.009  115 0.009  115 0.009  115 0.009  107 0.009	0.6724 6.5743 0.6925 1.6926 2.3649 C.5127 1.6934 1.6954 4.6164	-0.3794 -0.3606 -0.3844 -0.3846 -0.3747 -0.3747 -0.3749 -0.3749	-0.2930 -0.3571 -0.4193 -0.4733 -0.5413 -0.5413 -0.7019	-0.0354 -0.0464 -0.0513 -0.0578 -0.0636 -0.0677 -0.0677	-0.1550 -0.1757 -0.1914 -0.2285 -0.2548 -0.2795	0.1310 0.1299 0.1223 0.1222 0.1193 0.1145	0.4919 0.4919 0.4565 0.4628 0.4775 0.4728
7.88 C.U 5.50 U.O 9.89 O.U 11.53 C.U 17.55 U.U 17.55 U.U 17.55 U.U 15.50 U.U 15.50 U.U 15.50 U.U 15.50 U.U	0.0003 0.77 -0.021 -0.021 -0.025 -0.025 -0.025 -0.025 -0.025 -0.025 -0.025 -0.025 -0.025 -0.025	721 -0.0001 383 3.0031 131 3.0100 335 6.0038 391 0.009 1393 6.008 1393 6.008 1393 6.008 1393 6.008 1393 6.008 1393 6.008 1393 6.008 1393 6.008	6.5703 0.6925 1.6976 0.3169 0.5127 0.6836 1.68504 0.6166 0.3800	-0.3600 -0.3844 -0.3840 -0.3866 -1.3747 -0.2610 -0.3749	-0.3571 -0.4193 -0.4733 -0.5413 -0.5413 -0.7019	+0.0464 -0.0513 -0.0578 -0.0636 -0.0677 -0.0734	-0.1757 0.1914. -0.2285 -0.2548 -0.2795	0.123 2521.0 2521.0 2411.0 2411.0	0.4919 
5-50 0.0 9-89 0.0 10-53 0.0 11-55 0.0 13-55 0.0 13-55 0.0 15-56 0.0 15-56 0.0 17-61 0.0 13-60 0.0	-0.00x1 -0.00 -(.00x1 -0.01 -0.01x1 -0.00 -0.01x1 -0.00 -0.02x4 -0.00 -0.02x4 -0.00 -0.01x1 -0.00 -0.01x1 -0.00	343 3.0331 131 3.0100 335 6.6336 391 0.669 1393 6.069 1110 0.669 1674 6.069 1674 0.0661	0.6925 1.6976 7.3869 0.5120 1.6559 1.6559 1.6569 1.6569	-0.3844 -0.3840 -0.3846 -1.3747 -0.2610 -0.3749	-0.4733 -0.4733 -0.5413 -0.5613 -0.7019	-0.0513 -0.0578 -0.0636 -0.0677	-0.1414 -0.2245 -0.2548 -0.2775 -0.3045	-0.1223 -0.1222 -0.1145 -0.1145	0.4545 0.4028 0.4775 0.4728
9.89 0.0 10.53 6.4 11.58 6.6 12.55 6.6 13.55 1.0 18.56 6.0 15.50 6.0 17.01 6.0	-(.0rh(.0) -0.(1r) -(0.6) -0.01rc -0.0 -0.02rc -0.0 -0.02rc -0.0 -0.01vl -0.0 -0.01vl -0.0	131	0.50 20 0.50 20 0.50 20 0.450 4 0.450 4 0.360 0	-0.3806 -1.3747 -0.2610 -0.3749	-0.4733 -0.5413 -0.5413 -0.7019	-0.0578 -0.0636 -0.0677 -0.0734	-0.2285 -0.2568 -0.2795 -0.3045	0.1222 0.1145 0.1145	0.4028 0.4775 0.4728
11.50 C.U 12.55 U.U 13.55 L.O 14.56 U.U 15.5c U.U 15.5c U.U 15.6l U.U 17.6l C.U 13.60 U.U	-0.(1-1 -0.6. -0.(1-1 -0.6. -0.01-6 -01 -0.02-6 -01 -0.02-6 -01 -0.01-1 -0.01 -0.01-1 -0.01	335 4.6.35 	7.3869 C.51 ?e Loania (1.4504 U.4144 C.3640	-0-3606 -0-3747 0-2610 -0-3749 -6-3749	-0.5413 -0.5413 -0.7019	-0-0636 -0-0677 	-0.2548 -0.2735 -4468.8=	0.1193 0.1145 	0.4728
11,50 C.U 12,55 U.U 13,55 C.U 13,55 C.U 15,56 U.U 15,61 U.U 17,61 C.U 13,60 U.U	-0.(1-1 -0.6) -0.0156 -0.5) -0.0254 -5.6) -0.0254 -5.6) -0.0151 -5.6)	1391 (*.0c69 1393 (.0068 115 (.0097 1074 (.0073 1654 (*.0061	0.5126 	-1.37+7 - <del>-0.2610</del> -0.3799 -6.37+9	-0.5413 -0.564 -0.7019	-0.0677 	-0.2795 0.3045	0.1145	0.4728
13.55 t.0 14.56 t.d 15.5e t.u 15.6t t.u 17.6t t.u 17.6t t.u	0.0150 =0.01 0 =0.0250 =0.01 1 =0.0141 =0.01 0 =0.0161 =0.00	115 0.0097 0179 0.0097 059 0.0061	####### ##############################	-0.3799	-0.7019				-0.4678
15-56 0-0 15-5e 0-0 15-61 0-0 17-61 0-0 13-60 0-0	-0-01-1 -0-01	65" 0.0061		-6.3749		-C.0749	-0 3140		
15.5e 0.0 15.61 6.0 17.61 6.0 13.60 0.0	-0.0101 -0.00	05" 0.0061	0.34.0					0.1067	0.4515
17.51 C.U				-U-3630			_	0-5984-	
17.51 C.U			0 . 317			-0.0M44	-0.3660	0.1021	0.4427
بمن بمدد	, <b>-</b> 0.1134 -0.5.	145 0.0373			-0.7364			0.0941	0.4321
19.64 0.0								0.0890	0.4240
						-4.3885		0.0846	0.4052
						-			
						<del></del>			·
		•	<del></del>						
					_				
	<del></del>								

11	PHA 1-50 1-47 1-46 2-53 3-51 4-53 5-57 6-5F	6-1 0-1 0-1 0-1 0-1 0-1 0-1	C% =0.1:57 =0.0:0?7 =0.1:39 =0.2:52 =0.3:51	CLM 1-153- 0-0125 	CY =0.0147 =0.0077 =0.6350 =0.0064	CL4 5.0026 -0.0000	CLL =0.0052 -0.0047	CA 0-2535	CAB -0-1050	0.1445	
1 -1.01	1.65 2.67 1.46 2.53 3.51 4.53 5.57	0 - u 0 - u 0 - u 0 - u 0 - u	-0.0007 -0.007 -0.139 -0.2552 -0.3241 -0.4371	0.000 -0.000 -0.000 -0.000 -0.000 -0.000	-0.0107 -0.0077 -0.6355 -0.0064	0.00.0- 8t+0-d=	-0.0052	0.2535	_C.1050	0.1445	
	0.47 1.46 2.53 3.51 4.53 5.57	0.v 0.v 0.v	0.1.39 0.2052 C.3241	=(+<767 =(-<767 =(-4777	-0-6355			0.7537	0-1071		
1.46 0.6 0.2552 -(.2787 -0.0064 -0.0025 -0.0030 0.2547 0.1089 0.1458 -1.4064 5 2.53 0.6 0.3241 -0.2777 -0.0647 0.0647 0.0643 -0.0038 0.2511 0.1085 0.1426 -1.4745 0.3511 0.0085 0.1426 -1.4745 0.3511 0.0085 0.1426 -1.4745 0.3511 0.0085 0.1426 -1.4745 0.3511 0.0085 0.1426 -1.4745 0.3511 0.0085 0.1426 -1.4745 0.3511 0.0085 0.1615 -1.5682 0.3511 0.0085 0.2511 0.1085 0.1615 -1.5682 0.3511 0.0085 0.2511 0.1085 0.1615 -1.5682 0.3511 0.1085 0.1615 0.2511 0.1085 0.1615 -1.5682 0.3511 0.1085 0.1674 -1.7086 0.3511 0.1085 0.1674 0.1085 0.1674 0.1085 0.1674 0.1085 0.1674 -1.7086 0.1674 0.1085 0.1674 0.1085 0.1674 0.1085 0.1675 0.1676 0.1676 0.1675 0.1676 0.1676 0.1677 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.1687 0.16	1.46 2.53 3.51 4.53 5.57 6.5e	0.u 0.u	0.2552 	=( +< 787 ===773							
5 2.53 U.U	2.53 3.51 4.53 5.57 6.5e	0.U	f-43-1	-:77-		-6.0025					
7	5.57 5.57		7.23			C+043	-0-0038	0.2511	0-1085	J.1426_	-1-4745
8 5.57 U.U (.7(.) -1.7(.) -0.0(.50 0.0)/4 -0.0003 0.7564 0.1045 0.1474 -1.7086 9 5.50 0.0 U.5016 -1.0250.0046 0.0067 0.2636 0.1188 0.1447 -1.7738 10 7.50 U.U 1.012 -1.0504 -0.6(.50 0.0067 0.2636 0.1188 0.1447 -1.7738 11	5.57 6.5e	6.0									
\$ 5.50 0.0											
11	7.5b									-0-1447	-1-7738
12 9.65 N.W 1.30											
14 11.73 0.6 1.7773 =3.3211 =0.633 0.6716 =0.0006 0.2682 C.1490 0.1142 =1.9249 15 12.75 0.0 1.550 =1.6735 =0.0024 0.0013 =0.0005 0.2673 0.1524 0.1146 =1.9285 16 13.76 0.0 2.0445 =0.333 =0.0002 =0.0039 =0.0022 0.2653 0.1577 0.1076 =1.9216 17 14.60 0.0 2.2775 =4.3455 =0.023 =0.0012 =0.0007 0.2624 0.1630 0.0996 =1.9076 18 15.44 0.0 2.4720 =0.0603 0.0025 =0.0123 0.0000 0.2616 0.1630 0.0946 =1.8933 14 15.65 0.0 2.4421 0.0029 =0.0123 0.0000 0.2616 0.1670 0.0946 =1.8933 20 17.93 0.0 2.4421 =0.0720 0.0129 =0.0177 =0.0044 0.2556 0.1755 0.0628 =1.4731 20 17.93 0.0 3.6544 =5.5391 0.0055 =0.0159 =0.0102 0.2636 0.1981 0.0656 =1.8301											
15 12.75 0.0 1.5.50 -1.5735 -0.0024 0.0013 -0.0055 0.2573 0.1524 0.1146 -1.9285 10 13.76 0.0 2.0995 -0.002 -0.0039 -0.0022 0.2653 0.1577 0.1076 -1.9210 17 14.80 0.0 2.2775 -4.3555 -0.025 -0.0027 0.2626 0.1630 0.0996 -1.9078 10 15.44 0.0 2.4720 -4.056. 0.025 -0.0123 0.0000 0.2616 0.1630 0.0946 -1.8933 14 16.86 0.0 2.4420 0.029 -0.0123 0.0000 0.2616 0.1670 0.0948 -1.8933 20 17.93 0.0 2.4420 -4.0720 0.0129 -0.0177 -0.0044 0.2584 0.1755 0.6628 -1.8731 20 17.93 0.0 2.4420 0.0129 -0.0159 -0.0102 0.2601 0.1871 0.0730 -1.6490 21 18.97 0.0 3.6544 -5.5391 0.0055 -0.0159 -0.0102 0.2636 0.1981 0.0656 -1.8301											
10 13.76 0.0 2.0445 -0.333 -0.002 -0.0022 0.2653 0.1577 0.1076 -1.0210 17 10.80 0.0 2.2774 -0.3655 -0.027 -0.012 -0.8007 0.2626 0.1630 0.0995 -1.0078 18 15.40 0.0 2.4720 -0.025 -0.0123 0.0040 0.2018 0.1670 0.0948 -1.8933 14 15.45 0.0 2.4520 -0.0129 -0.0177 -0.0044 0.2584 0.1755 0.0628 -1.8731 20 17.93 0.0 2.4520 -0.0129 -0.0129 -0.0040 0.2010 0.1871 0.0730 -1.6040 21 18.97 0.0 3.654 -5.5391 0.0055 -0.0159 -0.0102 0.2636 0.1981 0.0656 -1.8301											
17											
14 15.06 C.U 2.55.4 -6.477. U.0)29 -U.1)77 -0.0044 J.75n4 J.1755 D.6628 -1.473 20 17.93 0.0 2.55.4 -5.559. U.0)27 -(.6263 -0.0096 0.2601 0.1471 0.0730 -1.6490 21 18.97 D.U. 3.55.4 -5.559. U.0055 -C.0159 -0.0102 0.2636 0.1981 D.6656 -1.8301										0.0936	-1-907#
20 17.93 0.0 />/-> 0.012> -(.0263 -0.0096 0.2601 0.1871 0.0730 -1.6490 21 18.97 0.0 3.53x -5.5391 0.0055 -0.0159 -0.0102 0.2636 0.1981 0.0656 -1.8301											
SS 20.01 0.0 3.74.5 -5.6745 6.0128 -0.0326 -0.0129 0.2632 0.2090 0.6542 -1. <b>6127</b>											
	0.01	0.0	3.24.	-5.0743	0.0159	-0.0326	-0.0159	0.2632	0.5030	0.6542	-1.0127
,			•	<del> </del>		······································	<del></del>	<del></del>			
`											
				<del></del> .	······································						
	2 4 4 4	3.76 3.76 3.60 5.40 5.40 7.93	3.76	1.73 U.U 1.7773 P.74 0.U 1.2759 B.76 0.U 2.0449 B.60 0.U 2.2775 B.40 0.U 2.4750 B.40 0.U 2.451 P.40 0.U 2.451 P.40 0.U 2.451 P.40 0.U 2.451 P.40 0.U 2.451	1.73	1.73	1.73	1.73	1.73	1.73	1.73

<del></del>							1 DEL3				<del></del>	
	5	-1 0.	5v 3.4	180.0 6	3-0F15 0	•0	0 0.	<u> </u>	O FIRE	0	<u> </u>	
POINT	ALPHA Tlack	HETA	Cuf 1	Cn1	C41	ACPF1	YCP+1	CNF2	Cr2	C82	XCPF 2	YCPF2
7	-0-25	0.0	-6.(-11	-6-1132	0.0423		-0.1074		-0.0004	-0.0015	-0.1505	-0.5385
	0_47	0.0	-0-0114		4_4665	_0.0.356			_=0.3071	0.0223	0-1828_	- 0+5791
•	1.45	C . v	-0.6125		0.0023		-0.1815			-0.0361	0.1818	0.4479
<del></del>	<u> </u>	<u></u>					-0.2331			-0.0550		
7	3.51	0.6	=01.50		C.0u32		-0.3013			-0.07d5	0.1627 	0.4418 -0.4520
· ·	5.57	·	-0-6177	-0-1624	-0-0052	0.1356			-0-0445		0.1510	0.4304
<u> </u>	6.58	-1-4	-6.0125									- 0.4380
14	7.58	0.0	-0.211-	-11.7347	-0.0054	0.0670			-0.0573		0.1372	0.4388
11	H.CL.			4.2000							-0+1350-	0-4373
15	4.65	v	-0.7673	6.0635	-0.0037	-6.1530			-0.u7u4		0.1278	0.4327
	10-54		<del></del>	<del></del>	خيتيمت				-0.0743		- 0-1500-	0.4267
14 15	11.73 _12.75	ن. ن	-0.0001	5-4011		-0.1471			-0.0793		0.1164	0.4162
15	13.75	0.0	-0.6022	C-0067	<u>u_6023</u>	-0.1062	-0-162d		-0.3491		0.1125	0.4150
17	19.80	-	=0-4457				0.4625					_ 0.3979
18	15.50	fi e ti	ーりっちょうて	0.0007		-0.10-2			-0.0972		0.1043	0.3939
19	16.84	6.6	-20 ··· 25			-C-2574					0-1036	0.3869
5 tr	17.73	C. A	-0.005	0-1010		-0.2516		-1.0213			0.1024	0.3793
جي	16-47	_لأمث	<u> </u>				13-2571				0_0970	B_3686
55	20.01	6.0	-0.0027	0.3027	-0.0034	-0.5024	1.5841	-1.1004	-0.0994	-0.3957	0.0903	0.3595
					••				·			<del></del> .
			•									
						_						
					_			. 1. 5.		•		
										•		

	TEST.		Air Belom 57 3.4		3 - 0 f 1 5 D		1CEL2		A IRANSII O Flie				
OINT	ALFMA	re TA	CAF 3	Cr3	E+3	>CFF3	YCPF3	CNF4	C+4	C94	XCPF4	YCPF4	•
2	-0.58	0.0	-0-4056	-0-0136	0.0701	0-40-7	-0.0079	0.0110	U-0638	-0.0004	0.3317	-0.0311	
<u>-</u>		_ <u>f-i</u> _			<del></del>	0.4621				-0.0336		-0.6509	
5 _	2-53	G. D		-0.4067	U-0631			-0.1034			0.1520	0.5265	
6	3.51	6.0	-	0.0005	-0.9010	-0.03s7	0.2552	-0.1517	-0.0239	-0.0759	0.1576	0.5007	
<del></del>	5.57	J		-ñ. 1052	V.0536			-0-2047			-0.1539	0.4797	
8	6.78	_G_U_		-0-10-2				-0.7514		-0.1244	0.1477 	0.4761 0.4799	
10	7.50	r. u		-0.0931	6-3462			-0.3816			0.1363	0.4747	
11 -	P.60			-Gad625							0-1300	9-4621	
12	4.65 .10.65	0.0 5.4		=3.3047	23 			-0.5070 -0.5719			0.1257	0.4716	
14	11.73	6.0		-6053	0.0035			-0.6349			0.1149	0.460\$	
15	12.75	C-u		-nlové3c				<del>-0-0498</del>			0.1091	9.4551	
10	13.7t	0.0		-6.5035 -6.3035	0.0033			-0.7618		-0.3403	0.1056	0.4467	
16	15.84	6.4		-6.107+	C.v.31			-0.5667			0.1025	0.4372	
19	16.57			-441.52	3.4552		-4-55/2			-6.3989	0-1001	0.4330	
20 21	17.93	0.0		-0.0012 -100001-	0.3024 0.0627			-0.9710		-0.4165	0.0967	0.4290	
52 21	20.01	U. G		-5.3055	C.0037					-0.4269	0.0469 0.0916	0.4173	

G€	1 OF 1 OF	3	Lei opseni			MARTIY MI	SSILE TA	IL EFFECTS	DATA		ODYMANIC WIND TUNNELL
	IES		59 0.4		CUNF 13a UF 15			DEL3 DELA			
0151	ALPHA		CN	CL=	CY	CL	CLL	CA	CAB	CAF	ACP
1	-1-61		-0-12-14		-6-162	ielala	0.0163	1-4542	_0_1963_		=1-6370
5	-0.00		-0-23		-0.1547	0.1373	0.0076	0.4509	0.0792		-0.7837
					-0-1531		0.00=3	0.500	0.4879		-0.5055
4	1.41			-0.2010		0.14.1	0.0052	0.4439	J. 484		-1.5667
<u>-</u>	2.40				6.153 <u>0</u>		-0143		_0_10-4		-1-4806
6	7.40		0.3720	-(-57+4		0-1372	0.0134	0.4464	0.0956		-1.5455
6	3 5.41			-1.12bt		0.157u	0.0053	0.4345	0.0436		-1.6759
9					-0-1543 -0-1451		_0.0073	3-4=30	_0.0734		-1.0759
lu	7.46				-0-1334	C-1255	0.0067	0.4345	0.0956		-1.7505
ii			_	-1-4004			6.0345		G-10-V		-1-7854
S	9.41				~0.13uc	C-11-9	0.0097	0.3943	0.1118		-1.8142
1.3	_10-45		<u> </u>			C-1140	0-0047	0-3923	6.1127		
1.	11.44			-2.7737			0.0132	0.3H34	0.1550		-1.8611
15 16	13.46			-3 <u>-1415</u>	-0.1145		0-0166 0-0174	0.3614	0-1262 0-1366		-1.8752 -1.8624
17	14.4	_	2-641		-6.1213		4650-0	0-3982	Un1473		-1.8577
) e	15,40				-0.1374		0.01.0	0.3989	0.1523		-1.8761
19	15.00				-0.115.4		0.01-2	7.445	C-1616		-1-88a-1-
20	17.45	0.0			-0.1357		0.0333	0.4057	0.1597		~1.8691
21	18.5				-0901		0.0177	U_3937	G-1717		-1-8535
55	19.5	0.0	7.7454	-5.7617	-4-1071	0.2572	U.0072	0.3958	0.1055	0.2135	-1.8367
									<del></del>		
					·						
											· · · · · · · · · · · · · · · · · · ·
			<del></del>		<del></del> -	•		·····			<del></del>
				<del> </del>							
											-

···

2 4	7 4.57 C.	Ilu-6 Pri								
INT ALPHA		9.0	300r15 0		U O		O FAEL			<del></del>
	ETA CA	+1 CH1	C→1	xCPF1	YCPF1	CHF?	CHS	cas	XCPF2	YCPF2
	<del>۱۵۲ -                                   </del>			23:5	5_0	-4-6478		-0-0221	1.1415	
	0.0			0.1356	-1-0195	-0-6175	0043	0.0673	0.2491	-0.4254
	-5-0				0 <u>-7551</u> _		c.polb		-0.945B	
	0.0- U.(		-0.00by	U.2367	0.3782	0.0414	0.0025 <u>25</u> 4_	0.0380	0.0610	0.9185 0.1352
	-0.0			0.5167	-3.4244	0.130e	u.2179	0.0540	0.1525	0.4131
	104 <b>~</b> 004			6-23-5	-u-6921	0-2066	4-4366	0-0562	0.1673	
	0.0		-1.07276	6.0	-0-6276	0.2554	U-0372	1.0452	0.1534	0.3336
	0.0	Lat	5.3069	0.0	0.0069	0.2940	0.2418_	0.1200	1501.0	24082
10 7.42	i_0 -9-	27n.cco=	-0.0361	0.2345	1.3372	0.3499	0.0501	0.1195	0.1431	0.3416
	-0-0				3_4435_	0-4171			_0-1401	
		1145 110055		r.2312	-4.9714	0.4580	0.0560	0.1974	0.1223	
		<u> 292</u>		<u> </u>		25436		<u>0-1996</u>	0.1363	
	0			2.6113	5.5442	0.5972 3-0451	0.0462	0.2518	0.1342 0.1255	
	D 0			0.2343	1.6902	0.5035	6.0344	0.2507	0.1235	
			0913	0-1617		0.7053		-0.2734	-0.1135	
	6.4 -0.			0.2346	-0.6422	0.7795	6.0252	0.2663	0.1093	
19 16.00	C_UC_E	Line	-1 -569	Lale17	-1.4197	-C-H336	L.GeAl	0.3006	0-1061	0.3619
	_	ups -446014		-6.4276	-4.5758	J.6471	0.0976	0.3079	0.1061	
		124 -0.104			<u>-1.511a</u>	<u> </u>	0.0941	0_35_0_	0.0517	
22 19.50	0.0 0.0	-G.6014	-0.0156	-0.4250	-4.5714	0.9518	0.3834	0.3663	0.0877	0.3849

		PART P	ALC BALLS	hPnl.	CUNE	L. CEL	1 DEL2	DELS. DELA	L. IRANSII	10M			
	2		57 0.4		3+0f15 0		0 0		FAE			•	
O] NT		HETA	CAFi	Cn3	CHI	XCPF3	YCPF3	CNF4	Сн4	C84	XCPF4	YCPF4	
	-0.62	<u> </u>	0-064	1.0717	-1-0107	51000 U	-0.5546	-0.0964	0.UP30	-0.0142	-0.4593		<del></del>
2	Dank	6-0	0-01-52	Count			U-3800_	0-C008:	0.u36a	0-0141		-16-8095	
•	1.41	0.0	-0.0+2u	-0.4850	0.0090		-4.2151	0-1261	0.05	-0.0008	0.4246	-0.0063	
	-2-40-	-6-0		3-0100			0-3801-		u.0244_		-0-2422		
¢.	3.00	6.0	-0.0311	-0-0159	0.0187	0.5120	-0-6028	0.1243	0.0305	0-1086	0.2378	0.8465	
6	_ <del></del>	6.0	-0.0025	-0-1651	G-0-11	1.7354		0.2023	6.7447	0.1426	602500	0.7058	
9	4.37	0.6	1-01-1	6.0575	-4.0:57		_=0.3798_	0_260_		0.1278	0-1470	0.4320	
10	7.42	6 . u	-0.0352	-0.0213	J-0064	0.6059	-0.1822	U.35-8	0.0587	0.1746	0.1654	0.4928	
- 14	_#.42_	0-4	<u>+0-4171</u>	<u></u>	<u>-u-cous</u> .	-6-6166		_0-160_	_0.0612_	0_1797.			
13.	9.41	د و ی	-0.0051 	-0-0012	9erg.a=	0-2301 10E5-0	-1-7505	0.4932	0.0738	0.2056	0.1497	0.4169	
_	11.44	0.9	0.0300	6.(194	-0.01-6			0.5584	0.0750	0.3068	0-1342	0.4406	
	12.46						-0.3796	0.0315_	. 0-1330		0-1923	0-3478	
_	13.46	0.0		-0.C0-1	0.0061	0.5031	-0.3747	0.6642	0.0803	0.2934	n.1199	0.4384	
	4-43-	c_u_		-0-3024	n-tina-		L-0049-		0.C#31_	-0.3008	0-1198	4-4337	
16	15.46 16.85	0.0		-0.J122 -0.J122	Studen Lenned	0.5029	-0.37y7	0.7788 0_8237	7.0555 2.0652	0.32 <b>-3</b>	0-1110	0.4164 	
	17.45	(.0		-0.,151	0.0103	0.55*4	-0.3747	0.2775	C.0846	0.3619	0.1010	0.4124	
21	18.54		-0-61-2	-t-tinal	-J-4076.		0-4621	0-9148.	\$385.0	0.3831	0.0986	a - = =	
55	19.50	U.U	-r.0+>3	-0.0210	0.0037	0.4570	-0.0802	0.9576	0.0915	0.3902	0.0956	0.4074	
							<u> </u>					·	
			·										
	•												

	- <u>IF7I</u>		ST 0.7		CUMF		1:	DELA DELA			
NT	AL	SETA	C~	CL4	CA	CLN	CLL	CA.	CAR	CAF	KCP
<u> </u>	-1.ce	Cau.	-0-13+3 -0-6541		-0.u636 -0.u636	<u> </u>	0.0024	1.3675	J. 1873		-1.6286 -1.3101
	- Ce-U	_0.0		-0.1571		0.07/5	<u> </u>	0.3705			=1.4541
,	1.43	6.0	0.1614	-(-1350		G.0+37	0.0031	0.3656	0.0946		-1.3313
	2.01	No.4	C-25-2	hEcf _0-		0.6731	3_C057	0-3613.	_0.0999.	0.2614	-1.3919
	3.43	Ú <b>.</b> Ú	りゅうちき			6.6.445	0.0029	0.3607	0.1000		-1.5335
<u> </u>		_Leve_				<u> </u>	D-DSAC	0.3606	4958		-1.6510
	5.44 	U.Ü		-1.5036		U-0544	6.3000	0.3563	0.0959		-1.6475
 )	7.42	C.J		-1.0284		0.0674	A-0050	0.3596_ 0.3561	0.1102		-1.7927 -1.7916
Ĺ	8.44	6-4		-l-=64D		2-07-2	4.0076_	_4.3652_	-0-1130		-1-8365
	9.43	0.0		-2.1743		0.0567	0.0042	U.354A	C.1145		-1.5358
	16-00	lind		-2.5324		-0-06-1	3-0355	0.3572	i_12+7		=1-8810
	11.44		1.53	-2214	-9.6767	0.65-3	-0.0005	0-3558	J-1342	0.2715	-1.9089
<u> </u>	12.00	U.u.	NAME OF THE OWNER OWNER OF THE OWNER	-3.11.1.			-0-011v-		c.1353_		-1.8989
•	13.50	0.0		-3-550-		0-04-0	0.0050	0.3239	0.1360		-1.9282
<u>.                                    </u>	15.47	6.0	CONTRACTOR OF THE STATE	-3-a-úa -4-13.12		0.0275	0-0052	0.3185_	1384		-1.9353
	16.45	( , \		-4-13NE		- 0.6545	0.0101	0.3204	0.1477		-1.9491 -1.9732
,	179	C - V		575		0-640-0	0-0167	0.3346	0.1703		-1.9773
Ĺ	18.50	Cav		-5.3502		G-USPB.	9.0107	0.3362			.=1-9777
5	19.52	0.5	5.4100	-5.7602	-0.0330	-0.0034	3-0197	0.3344	0.1876		-1.9748

TEST PART PART PART PART   Color   C	2
-1.60 U.U 0.U15	1.62
-0.60	-0.60
1.43 0.0 0.0035 0.0021 0.0027 0.0021 0.0021 0.0021 0.0029 0.0069 0.0167 0.1000 0.2965  2.41 0.0 0.0035 0.0021 0.0027 0.6104 -2.7403 0.0029 0.0069 0.0167 0.1000 0.2965  2.41 0.0 0.0036 0.0037 0.0021 0.0077 0.6104 -3.7040 0.1012 0.0161 0.0224 0.1590 0.2212  3.43 0.0 0.0096 -0.0015 0.0015 0.0015 0.2774 0.6614 -3.7040 0.1012 0.0161 0.0224 0.1590 0.2212  3.43 0.0 -0.0096 -0.0015 0.0015 0.2730 -1.6863 0.1614 0.0199 0.0533 0.1407 0.3770  4.43 0.0 -0.0096 -0.0015 0.0015 0.0015 0.2017 0.2017 0.2017 0.2017 0.2017  4.44 0.0 -0.0075 -0.0006 0.0017 0.0013 1.2603 0.2601 0.0421 0.0757 0.1618 0.2011  5.44 0.0 -0.0076 -0.0015 0.0017 0.0010 0.0596 0.3566 0.0465 0.1339 0.1361 0.3754  8.44 0.0 -0.0076 -0.0036 0.0037 0.0010 0.0596 0.3566 0.0465 0.1339 0.1361 0.3754  8.44 0.0 0.0013 0.0013 0.0010 0.0010 0.0596 0.3566 0.0465 0.1556 0.1422 0.3568  9.43 0.0 -0.0130 -0.1010 0.0010 0.0010 0.0596 0.3566 0.0465 0.1556 0.1422 0.3568  11.40 0.0 0.0 0.0 0.0 0.0 0.0 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010	0.63
1.43 0.0 0.0035 0.0071 -0.0077 0.6106 -2.7493 0.0629 0.0069 0.0187 0.1898 0.2965 2.41 0.4 0.0075 -0.0075 0.6614 -3.7040 0.1012 0.0161 0.0224 0.1590 0.2212 7.43 0.0 -0.0075 -0.0013 0.0105 0.2303 -1.6883 0.1614 0.0199 0.0533 0.1607 0.3770 4.43 0.4 -0.123 -0.2045 0.697 0.013 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911 5.44 0.4 -0.0075 -0.0075 -0.0077 0.013 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911 6.44 0.4 0.6075 -0.0075 -0.0077 0.013 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911 6.44 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	1.43 0.0 0.0035 0.0021 -0.0077 0.6104 -2.7493 0.0629 0.0069 0.0187 0.1098 0.2965 2.41 0.0 0.0045 -6.0045 -6.0045 0.6614 -3.7040 0.1012 0.0161 0.0224 0.1590 0.2212 7.43 0.0 -0.0056 -7.6013 0.0105 3.2363 -1.6883 0.1414 0.0199 0.0533 0.1407 0.3770 8.43 0.0 -0.0056 -6.005 0.0013 0.0105 3.2363 -1.6883 0.1414 0.0199 0.0533 0.1407 0.3770 8.44 0.0 -0.0075 -6.005 -0.0077 0.0013 1.7663 0.7601 0.0421 0.0757 0.1618 0.2911 8.44 0.0 -0.0075 -6.005 -0.0076 6.3019 -0.3780 0.2947 0.0388 0.1177 0.1317 0.3995 7.62 0.0 -0.0076 -6.005 -0.0307 0.0010 0.0596 0.3566 0.0485 0.1339 0.1361 0.3754 8.44 0.0 -0.0076 -6.005 0.0329 0.3829 -3.6165 0.3566 0.0485 0.1339 0.1361 0.3754 8.44 0.0 -0.0071 0.010 0.0159 0.1359 1.7224 0.675 0.1556 0.1422 0.3560 8.44 0.0 -0.0130 -6.001 0.0035 0.1399 1.7224 0.675 0.0596 0.1844 0.1274 0.3941 8.44 0.0 -0.0071 0.010 0.0159 0.1359 1.7224 0.675 0.0596 0.1844 0.1274 0.3941 8.44 0.0 -0.0071 0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.44 0.0 -0.0071 0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.44 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.45 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.46 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.46 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.46 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.46 0.0 -0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.46 0.0 -0.0071 0.0071 0.0071 0.0071 0.2235 0.1272 0.3646 8.47 0.0 -0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0071 0.0
2-al 0-u =0.0015 =1.01= 1.027= 0.0614 =3.7040 0.1012 0.0161 0.0224 0.1590 0.2212  3-43 0-0 =0.0956 =0.0013 0.0105 3.2363 =1.6863 0.1414 0.0199 0.0533 0.1407 0.3770  4.43 0.u =1.123x =0.0045 0.0013 0.0105 3.2783 =0.3779 0.2047 0.3344 0.0552 0.1422 0.2634  5-4 0.u =0.0075 =0.0077 0.013 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911  6-4 0.0 0.0 0.0 0.0076 =0.0077 0.013 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911  6-4 0.0 0.0 0.0 0.0076 =0.0076 0.0076 0.0077 0.0073 1.7603 0.7601 0.0421 0.0757 0.1618 0.2911  6-4 0.0 0.0 0.0 0.0076 =0.0076 0.0076 0.0076 0.0596 0.3566 0.0485 0.1379 0.1317 0.3995  7.	2-al 0.0 =0.015 = 0.013
7.43 6.0 -0.005h -c.0013 0.0105 3.2363 -1.6883 0.1414 0.0199 0.0533 0.1407 0.3770 6.43 0.4 -1.623 -1.624 0.6 95 0.1421 -0.3779 0.2097 6.534 0.0552 0.1642 0.7634 0.0552 0.1642 0.7634 0.0552 0.1642 0.7634 0.0552 0.1642 0.7634 0.0552 0.1642 0.7634 0.0552 0.1642 0.0757 0.1618 0.2911 0.0646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.1646 0.	7.43
5.44 0.0 -0.0075 -0.0075 -0.0077 0.0013 1.7663 0.7601 0.0421 0.0757 0.1618 0.2011 6.46 0.0 0.0076 -0.0076 -0.0007 0.0010 -0.590 0.3566 0.0485 0.1339 0.1361 0.3754 6.44 0.0 0.0071 0.0035 0.0037 0.0010 -0.590 0.3566 0.0485 0.1339 0.1361 0.3754 6.44 0.0 0.0071 0.0035 0.0037 0.0010 0.0590 0.3566 0.0485 0.1339 0.1361 0.3754 6.45 0.0 0.0071 0.0035 0.0037 0.0010 0.0590 0.3566 0.0485 0.1556 0.1222 0.3560 6.46 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	5.00 0.0 -0.0075 -0.0075 -0.0077 0.0013 1.7663 0.7601 0.0421 0.0757 0.1618 0.2011 6.00 0.0 0.0076 -0.0076 -0.0076 0.3019 -0.3780 0.2447 0.0388 0.1177 0.1317 0.3995 7.00 0.0 -0.0076 -0.0050 -0.0307 0.0010 0.0596 0.3566 0.0485 0.1339 0.1361 0.3756 8.44 0.0 0.0071 0.0035 -0.0327 0.3229 -3.6165 0.3355 0.1556 0.1622 0.3560 9.43 0.0 -0.0130 -0.010 -0.0157 0.1359 1.7224 0.0676 0.1556 0.1222 0.3560 11.44 0.0 -0.0071 0.0071 0.0071 0.0071 0.0071 0.235 0.1222 0.3566 11.44 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0071 0.0071 0.235 0.1222 0.3566 12.44 0.0 0.0030 0.0071 0.0071 0.6075 0.4062 0.0771 0.2235 0.1272 0.3686 12.44 0.0 0.0111 0.0027 -0.0507 0.6075 0.4062 0.0771 0.2235 0.1272 0.3686 13.50 0.0 0.0111 0.0027 -0.0370 0.2305 -3.4056 0.7550 0.0870 0.2849 0.3509 13.50 0.0 0.0111 0.0027 -0.0370 0.6073 0.7550 0.0870 0.2849 0.3509 15.47 0.0 -0.0707 -0.0030 0.6077 0.1350 -0.7550 0.0873 0.3031 0.1096 0.3004 15.47 0.0 -0.0707 -0.0030 0.6057 0.1350 -0.7181 0.505 0.0926 0.3040 0.1089 0.3033 16.48 0.0 -0.0707 -0.0030 0.6057 0.1350 -0.7181 0.505 0.0926 0.3040 0.1089 0.3033 17.49 0.0 -0.0707 -0.0030 -0.0193 0.1350 0.7422 0.9553 0.0583 0.3424 0.1029 0.3504 16.50 0.0 -0.0042 -0.0037 -0.0022 0.1575 0.4640 0.0965 0.3522 0.0974 0.3556
6.64	6.46
7.02 0.0 -0.0076 -0.005 -0.0307 0.0010 0.0596 0.3566 0.0485 0.1339 0.1361 0.3754  8.64 0.0 0.0071 0.0035 -0.0329 0.3529 -3.6165 0.0395 0.0625 0.1556 0.1622 0.3560  9.43 0.0 -0.0130 -0.1010 0.0159 0.1359 1.7276 0.0676 0.0596 0.1844 0.1274 0.3941  10.44 0.0 -0.0020 0.100 0.0151 0.0551 0.0505 0.4062 0.0771 0.2235 0.1272 0.3666  11.00 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0597 0.0597 0.2397 0.1713 0.1014 0.1322 0.3566  12.44 0.0 0.0035 0.0022 0.0597 0.6036 0.46232 0.6751 0.0870 0.2369 0.1269 0.3500  13.50 0.0 0.0111 0.0027 -0.0377 (.2305 -3.4056 0.7556 0.0870 0.2369 0.1269 0.3500  13.50 0.0 0.0111 0.0027 0.0037 0.0137 0.0136 0.7556 0.0873 0.3870 0.2875 0.1171 0.3804  14.45 0.0 0.0111 0.0027 0.0037 0.0157 0.1356 0.7556 0.0873 0.3031 0.1096 0.3808  15.47 0.0 -0.0227 -0.0370 0.0157 0.1356 -0.7181 0.5505 0.0926 0.3090 0.1089 0.3633  15.48 0.0 -0.0275 0.0037 0.0052 0.0052 0.0052 0.0077 0.3560	7.02 0.0 -0.0076 -0.0057 0.00507 0.0010 0.0596 0.3566 0.0485 0.1339 0.1361 0.3756  8.66 0.0 0.0071 0.0035 -0.0329 0.3229 -3.6165 0.0395 0.0625 0.1556 0.122 0.3560  9.43 0.0 -0.0130 -0.016 -0.0159 0.1359 1.7274 0.0676 5.0596 0.1844 0.1274 0.3941  10.46 0.0 -6.0029 0.1000 0.001 0.001 0.001 0.0025 0.500 0.5397 0.713 0.1914 0.1322 0.3566  11.49 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0017 0.0005 0.4062 0.0771 0.2235 0.1272 0.3686  12.46 0.0 0.01035 0.0022 -0.0517 0.6006 0.46232 0.6751 0.0870 0.2369 0.1269 0.3509  13.50 0.0 0.0111 0.0027 -0.0370 (.2305 -3.4056 0.7556 0.0885 0.2875 0.1171 0.3804  14.46 0.0 0.0015 0.0022 0.0033 0.6120 -11.0732 0.7965 0.6873 0.3031 0.1096 0.3808  15.47 0.0 -0.022 -0.030 0.0057 0.1360 0.0575 0.0926 0.3000 0.1089 0.3833  15.47 0.0 -0.022 -0.030 0.0057 0.1360 0.0595 0.0926 0.3000 0.1089 0.3833  17.49 0.0 -0.0270 -0.030 -0.0139 0.1356 0.7422 0.9553 0.0583 0.3424 0.1029 0.3564  16.50 0.0 -0.0502 -0.0370 -0.0223 0.1575 0.4540 0.0965 0.3522 0.0974 0.3556
### ### ##############################	### ### ##############################
9.43 0.0 -0.0130 -0.0100 0.155 0.1359 1.7274 0.4676 9.0596 0.1844 0.1274 0.3941 13.44 0.0 -0.0020 0.1840 0.0031 0.4625 -4.5500 0.5397 0.1713 0.1914 0.1322 0.3546 11.44 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0031 0.46232 0.4662 0.4771 0.2235 0.1272 0.3686 12.44 0.0 0.4033 0.4622 -6.0517 0.6036 -14.6232 0.6751 0.0870 0.2369 0.1269 0.3500 13.50 0.0 0.111 0.7027 -0.5377 (.2705 -3.4056 0.7556 0.0870 0.2875 0.1171 0.3804 14.45 0.6 0.3645 0.4022 0.6373 0.6126 -11.0732 0.7965 0.6873 0.3031 0.1896 0.3806 15.47 0.9 -0.7022 -0.6370 0.6657 0.1350 -0.7181 0.505 0.0926 0.3040 0.1089 0.3833 15.44 0.9 -0.6227 0.1579 0.0622 1.6622 0.4938 0.4977 0.3260 0.1075 0.3637 17.44 0.0 -0.6237 -0.6237 0.3145 0.7422 0.9553 0.0976 0.3624 0.1025 0.3584 16.56 0.0 -0.6262 -0.6277 -0.6227 0.1575 0.4560 0.9988 0.3655 0.3522 0.0974 0.3556	9.43 0.0 -0.0130 -(.:01e -0.0159 0.1359 1.7274 0676 9.0596 0.1644 0.1274 0.3941 13.44 0.0 -6.0020 0.1010 0.0031 0.0031 0.0035 0.4062 0.0771 0.2235 0.1272 0.3666 11.44 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0037 0.0036 0.0036 0.4662 0.0771 0.2235 0.1272 0.3666 12.44 0.0 0.0111 0.0027 -0.0377 (.2765 0.4056 0.7556 0.0870 0.2369 0.1269 0.3506 13.50 0.0 0.0111 0.0027 -0.0377 (.2765 0.4056 0.7556 0.0873 0.2675 0.1171 0.3804 14.40 0.0 0.0111 0.0027 -0.0373 0.6120 0.110732 0.7965 0.6873 0.3031 0.1096 0.3806 15.47 0.0 -0.022 -0.030 0.0057 0.135c -0.7181 0.505 0.0926 0.3040 0.1089 0.3805 15.48 0.0 -0.0277 -0.030 0.0057 0.135c -0.7181 0.505 0.0926 0.3040 0.1089 0.3833 17.49 0.0 -0.0277 -0.0370 -0.0370 -0.0373 0.07422 0.9553 0.0977 0.3260 0.1075 0.3564
11.44 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	11.00 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
12.44	12.66
13.50 U.O 0.0111 0.002 -0.037 (.2765 -3.4056 0.7556 U.URR5 0.2875 0.1171 0.3804 14.46 0.0 0.01171 0.3804 0.0120 -0.6373 0.6120 -0.7965 0.6873 0.3031 0.1896 0.3808 15.47 0.0 -0.022 -0.036 0.6657 0.1356 -0.7181 0.505 0.0926 0.3090 0.1089 0.3633 16.48 0.0 0.0022 0.0026 0.3090 0.1089 0.3633 16.48 0.0 0.0027 0.3260 0.1075 0.3633 17.49 0.0 -0.0227 0.3260 0.1075 0.3584 0.1029 0.3584 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.3638 0.0028 0.3638 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0	13.50 U.O 0.0111 0.0027 -0.0377 (.2705 -3.4056 0.7556 U.URR5 0.2875 0.1171 0.3804 14.40 0.6 0.3635 5.0022 -0.6373 0.6126 -11.0732 U.7965 0.6873 C.3031 0.1096 0.3808 15.47 0.9 -0.022 -0.6030 0.6657 (.1350 -0.7181 0.505 0.0926 0.3040 0.1089 0.3633 16.48 0.0 -0.0175 -0.6637 -0.6139 0.6652 1.6620 0.9089 0.0977 0.3260 0.1075 0.3587 17.49 U.U -0.6270 -(.6035 -0.0193 U.1356 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584 16.50 0.0 -0.0502 -0.6037 -0.6225 0.1575 0.4540 0.9988 0.0965 0.3522 0.0974 0.3554
16.40 0.0 0.30.15 0.0022 m0.63x1 0.6120 m11.0732 0.7965 0.6873 0.3031 0.1096 0.3806 15.47 0.0 -0.4202 -0.6030 0.6057 0.1350 -0.7181 0.5505 0.0926 0.3090 0.1089 0.3633 10.48 0.0 -0.4202 -0.6030 -0.4139 0.6622 1.6420 0.4963 0.4977 0.3260 0.1075 0.3587 17.49 0.0 -0.6200 -0.6030 -0.0193 0.1356 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584 18.50 0.0 -0.4502 -0.6037 -0.6225 0.1575 0.4540 0.4988 0.4965 0.3522 0.4974 0.3554	16.46 0.6 0.3616 0.0622 m0.63*3 0.6120 m11.0732 0.7965 0.6873 0.3031 0.1096 0.3806 15.47 0.9 -0.4272 -0.6030 0.6657 0.1350 -0.7181 0.5505 0.0926 0.3040 0.1089 0.3633 10.48 0.0 -0.075 -0.6030 -0.139 0.0622 1.6626 0.9089 0.0977 0.3260 0.1075 0.3587 17.49 0.0 -0.6270 -(.6030 -0.0193 0.1356 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584 16.50 0.0 -0.0530 -0.6225 0.1575 0.4540 0.9988 0.0965 0.3522 0.0974 0.3554
15.47 0.0 -0.4202 -0.4030 0.6657 6.1350 -0.7181 0.5505 6.0926 0.3090 0.1089 0.3633  10.48 6.0 -0.0175 -0.6045 -0.139 0.6622 1.6420 0.9389 0.0977 0.3260 0.1075 0.3587  17.49 0.0 -0.6200 -(.6035 -0.0193 0.1356 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584  18.50 6.0 -0.0502 -0.6074 -0.6225 0.1575 0.4540 0.9988 0.0965 0.3522 0.0974 0.3554	15.47 0.9 -0.4272 -0.4030 0.6657 6.1350 -0.7181 0.4505 0.0926 0.3040 0.1089 0.3633  10.48 0.9 -0.975 -0.4030 -0.139 0.0622 1.6420 0.9089 0.0977 0.3260 0.1075 0.3587  17.49 0.0 -0.6270 -(.6030 -0.0193 0.1355 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584  16.50 6.0 -0.0542 -1.6437 -0.6225 0.1575 0.4540 0.9988 0.0965 0.3522 0.0974 0.3554
17.49 U.U -0.627 -(.6335 -0.3193 U.1355 0.7422 0.9553 0.0583 0.3474 0.1029 0.3584 18.50 6.0 -0.0574 -(.6375 -0.6225 0.1575 0.4540 U.2988 0.0965 0.3522 0.0974 0.3554	10.4M 0.0 =0.0175 =0.0175 =0.139 0.0622 1.6625 0.9089 0.0977 0.3260 0.1075 0.3587 17.49 0.0 =0.0270 =(.6035 =0.0193 0.1355 0.7422 0.9553 0.0583 0.3424 0.1029 0.3584 16.50 6.0 =0.0502 =1.0074 =0.0225 0.1575 0.4540 0.9908 0.0965 0.3522 0.0974 0.3554
18.50 6.0 -0.054c -1.6470.622- C.1574 0.4540 0.4948 0.4965 0.3522 0.8974 0.3554	16.50 6.0 -C.U
19.52 0.0 -0.0315 -0.00+3 -0.1463 0.1534 1.4714 1.0175 0.0950 0.3582 0.0934 6.3521	19.52 0.0 -0.0315 -0.00-3 -0.1463 0.1534 1.4714 1.0175 0.0950 0.3582 0.0934 0.3521

	1 OF 1											
	TEST		ALE RAILE		CONF		1 DEL2	DEL3 DEL4			·	<del></del>
OINT	ALPHA	rf TA	CNFJ	C+3	C#3	ACPF 3	YCPF3	Crif •	CHA	Cs4	XCPF 4	YCPF4
ــــــــــــــــــــــــــــــــــــــ	-1-64	<u> </u>		1.2154	-6-6123	0.61/1	_el_1947_	-0-0AH3	-0-0057	-0-G31A	0.1390	0.6516
3	-0.50	ر ون <del></del>	()_()]+5 _ <del>=2+1/2</del> _	aleuyne <u>eteu</u> yne	-0.0047	0-5952 0-5503	-0.6643 0.3790-	-0.0092 0.0175	0.0006	0-0059	-0.0666 0.3728	1.6790 
	1.43	11.0	-0.0171	-6-008-	0.0016		-0.1032	0.1026	C. 035A	0.0024	0.3492	0.0234
5	_2.01_		0-6035	55022	-0-6055		-1-5311	0.1393_	0.0255	0.0266	0.2329	0-2630
6	3.43	(· • ·		-0-1152	0.06.23		-0.2523	0.1369	0.0307	0.0848	0.2209	0.6105
<del>.</del> _		<del></del>	<del></del>	-Catilda	<u> </u>	U-2254				0-0750	0-1814	0.3762
ė	5.44	0.6	-0.6155	-0-0101-	0.0062	0.402	-u.3ml? <del>-u.379</del> 7_	0.2359	0.0468	0.1516	0.1986	0.5153
10	7.42	<u> </u>	-0-26-9	-0-010n	0-0441 0-0414	0.4113	-0.0933	0.3637	0.0578	0-1299 0-1657	0-1471 0-1590	0.4252 0.4555
11	Rada	. U. D		-0-0024		O.42EO.	0.6713.		0.0578	0_1765_		-0-4329 
12	4.43	6.0	-0.13.5	-0.0135	0.0374	0.0046	-0.2421	0.4649	0.0701	0.2016	0.1446	0.4159
<u> </u>	10.60		<u>=:</u>	-(4121	i finan	4-5141	-0.2030	ú-52H2	0-0718	0.2265	0-1359	0.4289
1 •	11.44	2.5	-7.6034	#=0001	-0.00063	-0.04-9	1.1266	u.5691	0.0738	0.2814	0.1297	0.4945
15	12.99	Link	-0.05.1	-073	<u> </u>		0 <u>-2955</u>	0-6720	0.1067	0.2653_	_0.1617_	0.3948
16	17.50	U . U	-0.00055 -0.00055	U-001-	-0.0v77 <u>0.0ub3</u>	-0.4755	1.5443 -0.2270	0.77C3 	0.0834 0.0865	0.3104 6.3253	0.1158	0.4308
17	14.46 15.47	D - 11	-C-5534		0.0(44	6.4538		0.6317	0.0496	0.3462	0.1077	0.4162
19	16.96	u a U			-0-30-2	22743		N-1986	6-3923	0.3718	1-1027	0.4136
20	17.49	6.0	-0.01-0	-0.0005	5100.0	0.3240		0.9460	0.0947	0.3727	0.0999	0.3931
21	18.54	0.4		<u></u>	-11-31-23			259840	0.0494	0.3987	0.0905_	0.401A
25	14.52	0.0	-0.02-3	-0.0353	0.000+	0.33a3	-6.0370	1.0459	0.0916	0.4164	0.0476	0.3961
			·	··							<del></del> -	
									- 2			

GE	ENGINEER 1 OF 3 1 OF 1	ING LE	el gpwent	CEPIESTA	DC) PI	MARTI~ MI		EL FACILI		AFR	ODYNAMIC AIND TUNNELIAT
	TEST	PAPT -	ALM RALGE	ins o	Cuse	L. UEL1	OELZ O	DEL3_DEL4	INAMSITI	ON	
	2	49 U.	1.1	6.0 B	3=u+15 0	.0 0	0	0 0	FHEE		
OINT		HETA	C.	CL=	CY	CLN	CLL	C.	CAB	CAF	XCP
<del>'</del>	-0.40	<u> </u>	<u>-9.1242</u> -0.65-4		-0.057n.	U. (146 P	0.0033	0.3505	0.0937		-1.3265 -1.4026
3		_0.4	LE LDail		-4-4551	C.C543	0-0417	_0.3145.	4946	1922-0	-0.7931
•	1.43	0.0		-0-17/6		0.0005	0.0046	0.3202	0.0974		-1.3602
-	3.44	0.0		-v•-c-1		<u></u>	0.0013	<del>_0.3185</del> 0.3153	0.0950		-1.4093 -1.5028
<u> </u>	6.46	0.4	5.5.mc	-101147	Phous57	2-0413	2.0016	4-3124	C 0945	0-2140	-1.5979
K G	5.39	G.u		-1.0320		0-400	0.0023	0.3117	0.3975		-1.6719
10	7.47	0.0		-1.4320 -1.4320		0.03/3	0-0357 0-0051	0.3143 0.3156	0-1111		-1.7271 -1.7890
<u>ii                                    </u>	9.47			10041		C-041/	-0-0023	0.3192	_0.1173		-1-4519
12	9.46	U. U		-1-121		6.6336	0.0050	U.3176	0.1727	0.1954	-1.8849
13				-2.57-3			C057	0.3259	-1280		-1-9032
14	11.50 12.51	U . U		ct 5 t • 5 -		0.0210	0.0100 	0-3195 0-3193 -	0.1734 		-1.9099 -1.9148
10	13.46	6.3		-3.4662		0.0234	0.0055	0.3183	0.1476		-1.9202
17_	_leey_	0.4		-3.4624		0-0193	0-002	-0-3118	G_1531_		-1-9143
16	15.54	0.0		-4.344/		0.0154	1.0056	0.3040	0.1404		-1.9086
<u> 20</u>	17.50	6.0		-4.7141 -4.704		0.0034	0.0035	0.2400	J.1467		-1.9211 -1.9253
ži_	13.57			-5-2262		-4-(2-2	0-0126	0.2497	1.1737		-1.9315
22	19.56	0.0	2.5765	-5.6514	6.0376	-0-17-6	0.0117	0.2843	0.1865	0.0976	-1.9510
									<u> </u>		
				<del></del>				<del> </del>			
		•									
											-
				<del> </del>					<del></del>		
					· ~ .						

									4_TRANSII			
<del>-</del>	<u> </u>		<u> </u>		3+0f15 0		0 •		O FRE			
JINT	-labl	EFTA Call	CAF1 -C-3563	6nl 6a2013	Col 	XCPF]	YCPF1 3-127h	CNF2 -0-0439	-(~)04P CHS	-2-0550 -2-0550	XCPF2 0-1956	YCPF2 0-5008
4	-0.6u	6.0	-00077	-0.0033	-(.0067	r.1355	1595.0	-0.0155	-0.0044	-0.0056.	0.2019	0.3502
3	1.63			_=C • 0 ula_		0-10-5				_0.002A	0.0610	_0-1261
5	2.94	0.0 Cay		-0.0015			1.2459	0-0571	0.0073	0.0190 	0.1271	0.3327
6	3.44	0.0		-3.061e		0.1355	0.7614	0.1499	6.0235	0.0-95	0.1590	0.3303
		سلميا		-5-:321		(-1124	- 1-11mm	0.1990	1050-0	0.0722	0.151	0.3627
	5.35	0.0		-0.0036		5.1535	6.6790	0.2515	0.7301	0.0940	0.151	0.3737
<u></u>	7.47	0.0	-0.5047		-3.9c66	-0.0144	10.037/	.0.3089. 0.3736	0-0435 0529	3.1242_ 0.1448	0 <u>-1410</u> 0.1415	- 0.4020 0.3874
ii	5.47			3.632.		(T) (T) (T)	-5-6704	0040	0-0615	0-1672_		0.3766
12	4.46	C.0		-6.6315		0.1674	0.2312	0.4906	0.00+D	C.1917	0.1304	0.3907
13	17-60						-2-6029	<u>0_5648</u> .		0.2007	_0-1324	0.3522
15	12.51	0.0	-6-1164	-0-(00)	-4-3300	0.7620 	4.0605	0.6172 	0.0796 <u>0.0796</u>	7-2569 	0.1274	0.3816 
16	13.44	0.0	0.0164		-0.0144	4.0111		0.7349	C.0474	0.2740	0.1189	0.3729
17	_14.49_	<u> </u>				-0.4254		0.7814	0.0879		0.1125_	0.3759
14	15.54 10.54	0.3		-0.066	C.0010		-6-1007	0.9494	0.0930	0.3205	0.1345	0.3773
<u> </u>	17.50	0.3		-U-662t		0.1192	-0-0255 0-6157	0.4750	0-1959. 0-1017	0.3551	0.1065	0.3794
<u> 21 </u>	16.57	0.4		-6-1030			-0-10-8	1-0143	0.0969	-0.3510-		0-3461
?<	19.56	0.0	0.6064	0.10.2	-0.0410	6.6106	-5.9191	1.0568	0.0866	0.3770	0.0839	0.3567
					·							

	IEST_		ulm malim Sv 1.1				) . DELZ_		A_IRANSIT 0 FPE			
INT	-	mF TA	C . F s	(43	Cr3	1CFF3	YCPF3	CAFA	CH4	CB+	ACPF4	YCPF4
2	-0.50	<u> </u>			<u> </u>	V.5476	-0-173A -0-236u	-0.0045	<u>=6-1043</u> −0-6004	-0.0155	0.0389	1.6243
<u> </u>	C.43	0.6		وبالساء	-u-Cuch	CANGER			G_0C73.	_0.0040_		
•	1.43	0.0	-r.1334	-01=3	5.007.	0.5369	-0.2173	0.0907	3.0295	0.0091	0.3259	0.1006
<u> </u>	. <u>_2</u> _42_	0_1_			-0.0029	2.5977		0_1_058_	0-6225		-0-2127	0.3140
6	7,44	( u	-0-:-3~	-1-1-10/	0.0y52	C+4516	-0-2632	0.144H	0.0285 4.5358	0.0731	0.1970 	0.5048
8	5.34	٥.٥		.5261	-0.6015	-0.4374	7.4563	0.23F1	0.0430	0.1172	0.1807	0.4922
ç	-5.45	- trail		-La.177			0-3006_	0-3136		0.139A_		0-4171
G	7.47	t . u	پوځي. ۴⊷	-6.5047	0.003?	3.4711	-0.1324	0.3759	0.756	0.1672	0.1512	0.4448
1	9.47	_0_ <u>u</u> _	-:-:-1		-11-11-12	الحطن منا		_0.0373	0.3625_	0-1256_	_D-1429 .	-0.4243
3	4.46	0.0	-7-5:7-	-20-4125	0.0055	0.4510		0.496A	0.0579	0.2141	0.1366	0.4309
•	11.50	( , ii	7.6.7		-0.0000		-11.8849	0.5694	0.07-6	0.2764	0.1264	0.4686
5	12.71			-6-6121			-0-1681	0.67u2	0.5405	0.2718_	_0-1471_	0.4055
10	13.40	0.6		-4021	-3.0020	0.2290	0.2147	0-7691	0-0824	0.3005	0.1169	0.4237
17		0.0		<u>-1-1002</u>	<u> </u>		-0-1157	_ 4-7524		0.3195	0.1129_	-0.4249
[8 [5	15.54 lp.54	0.0	-( .( 23- -( .): 77	-(.)692	0.0035	0.3770		8656.0 2062.0	0.0929	0.3432	0.1091	0.4151 
20	17.50	C.u		-0.(042	6.0007	0.3676		0.9543	9-0462	0.3874	0.1008	0.4060
21	15.57	4.4		-1.00002	DeuC22		-0-1101	0.9446	6.2939		0.0939	0.3963
25	19.50	V. 0	-0.6372	-0.0164	0.0056	0.4406	-0.2317	1.0617	0.0933	0.4215	C-0878	0.3970

E	t	Charles Access	LEL OPSE's	CENTERLA	EOC) &			IL EFFECTS		AEG	ODYNAMIC #IND TUNNELIATI
		_			-						
			MACH FALLS 50 3.4		3-0F15 0		DELZ.	DEL3 DELA		DM	
TAL	ALPHA	BETA	-0-13-4	CL*	C1	C[4	CLL	C4 0-2630	CAR C-10A6	CAF	ACP -1-5114
2	-0.58	6.0	-0.0257		-0-0114	0.0101	0.0005	6.7611	U-10+0	0.1571	-1.9956
<u>. 3</u>	0.00	0.0	0-1742	- Undar		O.Jlan	1500-0	0.26Ub	-0-1076		
•	1.45	6.0	1.1565	-0-241-		J-000C	0.0035	0.7576	0.1059	0.1517	
5	2.47	0-0	Cocaou Cocaou			0.0127_	0-0027		_0-1055		-1.3888
6	3.50	0.0				0.0077	0.0029	0.2545	0.1794		-1.5126 -1.5945
e	5.52	Ú. v	100772		-1.0062	f = G(r+	0.0041	0.2595	6-1109		-1.6619
ų į	8.57	0.0			-4-0466	C.0074	0.0056	4.2620			-1-7457
10	7,59	0.0	0.944.		-0.6000	0.0130	0.0072	9.7661	0-1244		-1.6075
11	3.62	0_0_		-241942		£400±1	- 0-0052	0.2660			
15	9.03	0.0	1-32-0	_		C.0626	0.0001	1.7654	0.1732		-1.6660
13	11.67	0 - '1	<u>1-5-1-7</u> 1-69.0		-0.06-1	-0-0061	6 10 0 0 S	0.2649 0.2650	0-1457		-1.9033 -1.9196
15	12-47	0.0		-3-5-23		0.0107	0.0091	0.2599	0-1441		-1.9264
16	13.75	0.0	2.1954			1500-1	0.0061	0.25A1	6.1578		-1.9146
12	14.71	0.0		فلفغمو		4-0016	- 0-0364	0.2546			-1.9066
18	15. "3	0.0	2.4524	-4.0513	0.0.20	-0-0030	0.6044	0.2542	6-1686		-1.8962
19	هتمول	0_0					-0-60-1	3-2-9-	-1737		-1.8424
ŞC	17.47			-5.539.	0.0044	-0-0000	0.0074	0.2-70	0.1420		-1.8584
55	<u> 19.93</u> 19.75	0.0		-5013	1910-0		0.0061	0-24H7	0-1499		-1-8297
~~	17.73	0.0	3./1	-20013	0.0201	-0.0416	0.0133	0.2479	0.2031	U. 0448	-1.8046
											·
						*			••		
		_									
							<del>,</del>		<del></del>		
								-			
											. <del> </del>

•

<u></u>	1_0+_1	<del>,</del>										
	1651	PART -	ain kalu-	e e e	COME	4 754	T -0EL2	DEL 3 DEL	A THANGIT	7.004		
	S		57 3.4		3-0f15 0		0 0		O FHE			
7~10	ALPHA	#FTA	CNF1	Cri	CHI	- Cef I	YCPF1	CNFZ	C45	C85	FCPFZ	YCPF2
	-1453	_نيـــ	-1-119	Compe	ـ دهبينيونيو		0-8851	-B-CASH-	-6-0093		-0.1866	0-4514
4	-0.54	0.0	-0.0043	6.0011	-0.0342	-4.25/1	L. 97HH	-0.0124	-0.0036	-0.0022	0.2897	0.1728
•	1.45	<u> </u>	-0-7484 -0-7053	0. úu0-	-0-054 	-0-1530	0.5472	0.0272 0.0615	- 0.0096 - 0.0096	0.02 <b>6</b> 1	D.1464 0.1390	0.3914
5	2.67	Cou	-0-3035	0.3015			102401	-0-1043	0-0163	-0-0-11	0.1560	0.3939
6	3.50	0.0	-0-0045	6.0000	-6-0047		0.9554	0.1510	1550.0	0.0662	0.1466	0.4387
7	651	11-11	PE-CSAR			THEORY SHOULD TOURS	0.2472	0.2076		0.0425	0.1515	0.3968
A	5.50	( • ù	-0.36.35	0.0567	-0.0574	-0.21-1	5.5344	J. 2640	u.3379	0.1096	0.1434	0.4152
<del></del>	<u> </u>	4.0	<u>-c-oc13</u>		-4.0012		0-9063			0.1364		-0.4192
1¢	7.54	6.0	-0.5034 -0.5034	0.6064		-1 -23-0	1.5424	0.4530	0.0530	0.1632 0.1914 .	0.1361	7814.0 —— <del>4554.0</del>
12	9.03	0.9	-0.0024	0.0010		-^	4.1314	J.5134	0.0643	0.2174	0.1252	0.4234
<u> </u>	1:-60	6-4	0.0320	417	ed-637#	مدامه	-2.7533	2-5777	56602	0.2410	-0-1198-	0.4183
1•	11.67	0.0	-0.0012	0.000=	-0-0114		10.06+7	0.0091	0.0752	0.2674	0.1159	0.4120
15	12.67_	0.4	-6-6052	20021		-2-0115		0.7375		0-2913_	0.1107	-0.4117
14	13.75	v.u	-0.1071		-6.6377	0-44-36	1.0236	0.7013	C.0543	0.3135	0.1079	0.4018
<del>17</del>	<u> 14.77</u>		R-7un5				leee15-	- 4-n361	0.0678	-	0-1050	0.3957
14	15.63	U . U	14.05-1		-0.H355		-0.3797 -0.3796	0.4005 0.4561	0.0923	0.3499	0.1025	0.3886
51,	177	U.U	14.0435		-0.7551	3.2356		0.9971	0.0945	0.3F55	0.0997	0.3866
نغ	10.33	0_0	15.35.35		-0.5503		-0-3786	legelA		0.3951	-0-0966	0.3802
Pè	19.45	6.0	16-0603		-0.6455		-0.3790	1.0731	0.1003	0.3972	0.0935	0.3702
					•				•			
					20					*		
							_					
			-									
										<del></del>		
												· · · · · · · · · · · · · · · · · · ·

	2		PA 3"W	rnl 6.0 b	3 = 6 + 15 0 .		DELS.	DEL3-DELA	The second secon			
OINT	AI PHA	bt TA	C++ 3	Cr3	C63	#CPF3	YCPF 3	C-ıF4	CHA	C84	XCPF 4	·YCPF4
1	-1.64		-2-20-	26		1. 22 -		-0-4433	-6-6060	-0.0237	Calasa	0.5725
5	-0.56	6.0	6.0034	6.0030	-0.6607	0.7637	-0.1054	-0-00-4	0.0006	-0.00m2	-0.1346	1.0589
_3	- 0.02	<u> </u>		-0114	ــ بدانانامنا			_D.0303.	0-0067		0.2208_	0.3199
•	1.45	0.0	-0-01-4	-0.0016	0.0065	0.5073	-0.4348	0.0765	0.0171	0.0238	0.2177	0.3035
÷	3.50	U.U	-0.15-	-U-1170	1.0007	v.41.11		0.1627	<b></b> 	0.0764	0.1680	0.4030
7			-2.067	-101055	4-9417	(-Al35	-2622	0-2123		0.0932	0-1575	0.4700
8	5.50	0.0	-0.31,3	-0	1.01 31	43-3		0.2641	U.0414	0-1205	0.1588	0.4564
¥	6.57	0.0	-3-0:		u-0025		-0.283y	4-3305	0-2463	4.1.91	0.1400	0.4510
10	7.59	0 . u	-0.064-	-( - 1036	0.6917	0.4056	-0.1935	0-3919	0.0535	0-1804	0.1366	0.4604
11	8.62	C. U	-3-7046		-0-017A		0-1964	0.4545 .	0.4589.	C.209Z.	0.1296	0.4592
15	9.53	0.0	-0.0135		0.05.	0.3-27		0.5171	0.0650	0.2354	0.1258	0.4552
13	10-02	_0_4_		-0-0333	0.0154	0.3351	-0.2961	<u> </u>	<u> </u>	8445-0-	0.1195	-0.4585
15	11.57	0.0	-0.00-	-0-0307	5.0°01	6.1151	-0-0217 -0-3240	3-6472	0.0734	0.2991	0.1143	0.4657
16	200000000000000000000000000000000000000	. 0.U	-0.00/2		C.C.14	0.2450		0.7086 0.7631	0.0629	0.3127	0.1065	0.4424
17	19.77	0.0					-0-375		D-0844 .	-0-3588	0.1033	-0.4392
16	15,93	10		-0.033-	0.0035		-0.3067	0.4845	D.0845	0.3798	0-1012	0.4294
19	15.50	L-U	-5.: -1.	-4-1314	4-0:03		G. 277H	7-4347	0.0927	4.3967.	0.0392	0.4264
20	17.47	0.0	-0.01-3	-0-134-	u - 1( +6	6.33.3	-0.3272	0.9794	0.0461	0.4107	0.0481	0.4191
21	15-43	0.4		ـ عدندمنات.	6.003-		0.31	1.0256	-0-0971	0.4166	0.0947	5002
22	14.95	0.0	-0.0153	-0.0055	0.0052	0.3449	-0.3241	1.0677	0.0954	0.4300	0.0894	0.4028

E	ENGINE 1 OF	3	BELSPEE A	CENTERIA	NEUC) P	M PITHAM	STATE TA	LEL FACILITY	DATA	AERI	MIK_SIMAMYGG	D JUNNELLAT)
	1ES		MACH EXLIP		COME.		1. DEL2	DEL3 - DELA				
TAIG	ALPHA		C.	CLH	CY	CLN	CLL	CA	CAB	CAF	ACP	
<del></del>							7-0030	0.540#	0-1171		-4.5741	
5	-0.64		-0.03.7		-0.01-	0.01.0	0.0011	0.7894	3-115-		-1.8748	
4	1.44	_	U-171-		-0.0102 -0.0115	<u></u>	0.0032	<del></del>	C-1156		-1.0897 -1.3276	
<u>.</u>	1.00 [ <u>4.5</u>				-0.0117			0_2437	G-1174		-1-4917	
6	3.40		7.4174		-v.0151	(.0146	0.0036	0.7427	9.1164		-1.5839	
7	5.4	3.4	C.P.S.		20.4117	0.01/1	3-00aH	0.2836	_u_llab_	C-1652	-1-7606	
F	9.50				-4.662-		0.0052	3.23.6	0.1.54		-1.9742	
<u> </u>	_13-20						0-0099	G.2817	_0.16.7.		-1-9850	· · · · · · · · · · · · · · · · · · ·
10	17.84			-5.5791	ن/ ۵۰۱۱ خملک و س	-0.0563	0-0041	0.2544	U-1765 3-1935		-1.9025 -1.4364	
11 12	19.45 25.2			-5.726A		-0.0252		0.2645	0.5594		-1-5905	**************************************
13	27.4			-7-7133		-C-1735		0.2643	3-2545	0-0008	-1-AQ19	
												·
							•					

ARYOLU ENGLUPERING MENEL GENERAL CENTERINEUC) PROPOUSION WIND TUNNEL FACILITY (PAT) AFRODYMANIC SIND TUNNEL (AT)

MANTI I MISSILE TAIL EFFECTS DATA

PASE 2 OF 3

SMEET 1 OF 1

ůŁ .	3 OF 3		AEL UPPE-1	LENIER (A			ISSILE TA			AERO	UYRANIC I	INO TUNNEL (AT)
	1F51.		<u>alm °Il</u> bu 2.5		CONF		1 0ETS		A TRANSIT		·	
CINT	ALPHA	DETA	CNF 3	C⊬3	Ch3	#CFF3	YCPF3	CNFA	CH4	CA◆	XCPF 4	YCPF4
	_1_4	<u></u>	<u></u>	-1-:052	<u> </u>	Co 3F 2E	<del>-0-0253</del>		-0-0070	-0-026A	<del>-o-iojo</del> -	
2	-0.56	0 = n (ı = u	-0.612y	-0.0004/	1.0203	(·•35¤7 0.35¤7	-0-022 <b>6</b> 0-0281	-0.0091	-0.0006	-0.0102	0.0526	1.1184
<del></del> -	1.42	0.0	-0.01.1	-0.0055	-0.000-	<u></u>	7-0121	0-0316 0-0661	0-0079 0-0117	0.026B	_ <del>0.2211</del> _ 0.1770	0.4053
5	2.47	C = 0		-0.0053 -0.0052			1-0202		C.G192_	0_0_659		-4-4144
6	3.40	0.0	-0.61	-0.0055	-0.0009	0.35-1	U-6572	0.1642	0.0269	0.0658	0.1640	0.4192
7	5.66	<u> </u>	-6-41			0.36-5	6-1195	4.2764	3_0A0H	0-1224	0-1-77	
6	9.40	6.0	-0-917-		-0.0015	4.3279	9-66-1	0.5204	0.0527	0.2442	0.1191	0.4638
4	13.76_	<u>u.t.</u>		_=0.4063		0.31=1	0.0348		0.0734_	6546.0	_0.0949_	0.4424
10	17.44	C.U		-0.0061		0.30.7	7.0501	0.9801	0.0771	0.4046	0.0786	0169
11	<u> </u>	<u> </u>		-6.537+				1-0804	<del>0.071</del> 4_	0.4365		
12	25.21 27.47	6.U		-6.0074 -6.0074	\$100.0 \$30u_0	4.55.g	-1-0464	1-1105	0.0380	0.4311	0.0342	0,3681
							•					

1 =1.53 G.U =G.13nV 0.213A =0.0002 =C.003A =0.0002 0.2436 0.1131 0.1805 =1.5369 2 =0.5V 0.V =C.0350 0.0704 =V.0077 0.0nc3 =G.0010 0.2914 0.1100 0.1818 =1.9748 3 0.42 G.U 0.4555 =6.0125 0.4120 =0.0005 0.2931 0.1131 0.1800 =0.9126 4 1.44 0.0 C.1655 =0.0207 =0.0056 G.0013 0.0003 0.2900 0.1114 0.1702 =1.3102 5 2.47 0.4 0.2207 =C.4263 =0.0056 0.0020 0.0013 0.2914 0.1131 0.1771 =1.4564 6 3.47 0.0 0.4112 =0.0405 =0.0056 0.0013 0.2914 0.1131 0.1771 =1.4564 7 5.44 0.4 0.722 =1.2537 0.411 =0.0161 0.0033 0.2915 0.1123 0.1772 =1.7849 8 9.60 0.0 1.5776 =7.7725 0.0055 =0.0130 0.0053 0.3027 0.1414 0.1613 =2.0125 9 13.70 0.0 2.1775 =4.4465 0.0055 =0.0146 0.0056 0.3027 0.1414 0.1613 =2.0125 10 17.57 0.0 2.7455 =0.0155 0.0055 0.0056 0.2435 0.1651 0.1336 =2.0418 11 19.97 0.0 2.7455 0.0055 =0.0146 0.0056 0.2437 0.1628 0.1109 =1.9198 11 19.97 0.0 3.4455 0.0228 =3.0347 0.0161 0.2928 0.1953 0.0972 =1.8372	θE	ENGINEED 1 OF 3 1 OF 1		vel Graeni	_CENIERIA	<u> </u>		ISSILE TA			AEX	Jannet Dale 31 MAY CO	(AT)
1 =1.53 G.U =G.13nV 0.213A =0.0002 =C.003A =0.0002 0.2436 0.1131 0.1805 =1.5369 2 =0.5V 0.V =C.0350 0.0704 =V.0077 0.0nc3 =G.0010 0.2914 0.1100 0.1818 =1.9748 3 0.42 G.U 0.4555 =6.0125 0.4120 =0.0005 0.2931 0.1131 0.1800 =0.9126 4 1.44 0.0 C.1655 =0.0207 =0.0056 G.0013 0.0003 0.2900 0.1114 0.1702 =1.3102 5 2.47 0.4 0.2207 =C.4263 =0.0056 0.0020 0.0013 0.2914 0.1131 0.1771 =1.4564 6 3.47 0.0 0.4112 =0.0405 =0.0056 0.0013 0.2914 0.1131 0.1771 =1.4564 7 5.44 0.4 0.722 =1.2537 0.411 =0.0161 0.0033 0.2915 0.1123 0.1772 =1.7849 8 9.60 0.0 1.5776 =7.7725 0.0055 =0.0130 0.0053 0.3027 0.1414 0.1613 =2.0125 9 13.70 0.0 2.1775 =4.4465 0.0055 =0.0146 0.0056 0.3027 0.1414 0.1613 =2.0125 10 17.57 0.0 2.7455 =0.0155 0.0055 0.0056 0.2435 0.1651 0.1336 =2.0418 11 19.97 0.0 2.7455 0.0055 =0.0146 0.0056 0.2437 0.1628 0.1109 =1.9198 11 19.97 0.0 3.4455 0.0228 =3.0347 0.0161 0.2928 0.1953 0.0972 =1.8372													
2 -0.59	OINT			•							• • • • • • • • • • • • • • • • • • • •	· · · · · · · · · · · · · · · · · · ·	·
3 0.22 G.u 0.0533 =0.0134 =0.0125 0.0120 =0.0005 0.2931 0.1131 0.1000 =0.9128  6 1.44 C.U 0.1655 =0.2026 =0.0056 C.0713 0.0003 0.2900 0.1114 0.1762 =1.3102  5 2.47 0.0 5.2427 =0.4263 =0.0075 0.0020 0.0013 0.2914 0.1131 0.1771 =1.4564  6 3.47 0.0 0.4112 =0.5046 =0.0045 =0.0020 0.0013 0.2914 0.1131 0.1771 =1.5564  7 5.49 0.0 0.70 1.576 =1.2537 0.0011 0.0031 0.2915 0.1143 0.1772 =1.7849  8 9.60 0.0 1.576 =2.772 0.0055 =0.0150 0.0053 0.3027 0.1414 0.1613 +2.0125  9 13.70 0.0 2.1775 =4.4465 0.0055 =0.0156 0.0064 0.2485 0.1651 0.1334 =2.0418  10 17.57 0.0 2.445 0.025 =0.0156 0.0064 0.2485 0.1651 0.1334 =2.0418  11 14.97 0.0 3.4045 =6.2554 0.0250 =0.0347 0.0161 0.2924 0.1933 0.0972 =1.8372  12 25.26 0.0 4.4234 =0.0211 0.0459 =0.1527 =0.0541 0.2918 0.2549 0.0369 =1.8372	2												
5 2.87 0.0 5.2427 - C.4263 - G.0075 0.0020 0.0013 0.2914 0.1141 0.1771 - 1.4564 6 3.47 0.0 0.4112 - 0.5466 - 0.0045 - 0.0016 0.9017 0.2907 G.1171 0.1736 - 1.5739 7 5.44 0.0 0.7124 - 1.2537 0.0011 - 0.2161 0.0033 0.2915 0.1143 0.1772 - 1.7849 8 9.60 0.0 1.3476 - 7.7424 0.0055 - 0.0150 0.0053 0.3027 0.1414 0.1613 - 7.0125 9 13.70 0.0 2.1774 - 6.4864 0.0055 - 0.0150 0.0053 0.3027 0.1414 0.1613 - 7.0125 10 17.57 0.0 2.4775 0.0750 - 0.0255 - 0.0140 0.2435 0.1651 0.1334 - 7.0418 11 14.97 0.0 3.4045 - 6.2554 0.0226 - 7.0347 0.0161 0.2924 0.1953 0.0972 - 1.8372 12 25.26 0.0 4.4234 - 0.0211 0.0459 - 7.1527 - 0.0541 0.2918 0.2549 0.0369 - 1.5419		0.05		ــددخه.م.ـــ	-6-0534	-0-0125	0-3120	-0-0005	_4.2931	4-1131	0-1800-	-0-9126	
5 3.47 0.0 0.4112 -0.5450 -0.0045 -0.0016 0.0017 0.2907 0.1171 0.1736 -1.5730 7 5.49 0.0 0.7124 -1.2537 0.0011 -0.0161 0.0033 0.2915 0.1143 0.1772 -1.7849 8 9.60 0.0 1.3476 -2.7724 0.0055 -0.0150 0.0053 0.3027 0.1414 0.1613 -2.0125 9 13.70 0.0 2.1774 -4.4450 0.0055 -0.0146 0.0054 0.2435 0.1651 0.1334 -2.0418 10 17.57 0.0 2.99-0 -5.7375 0.0256 -0.035 0.0014 0.2937 0.1628 0.1109 -1.9198 11 19.97 0.0 3.4045 -6.2554 0.0228 -3.0367 0.0161 0.2924 0.1953 0.0972 -1.8372 12 25.25 0.0 4.4239 -0.0211 0.0459 -0.1527 -0.0541 0.2918 0.2549 0.0369 -1.5419	<u>•</u>												
7 5-4 0.0 0.7324 =1-2537 0.0411 =0.0161 0.0633 0.2015 0.1143 0.772 =1.7849  8 9.60 0.0 1.376 =2.7725 0.6055 =0.0150 0.0053 0.3027 0.1414 0.1613 =2.0125  9 13.70 0.0 2.1775 =4.4455 0.0155 =0.0146 0.0054 0.2745 0.1651 0.1334 =2.0418  10 17.57 0.0 2.945 0.0750 =0.0835 0.0014 0.2937 0.1628 0.1109 =1.9198  11 19.97 0.0 3.445 -6.2554 0.0228 =3.0347 0.0161 0.2928 0.1953 0.0972 =1.8372  12 25.25 0.0 4.4239 =0.0211 0.0459 =3.1527 =0.0541 0.2918 0.2549 0.0369 =1.5419	<del>-</del>												
9 13.76 0.0 2.1777 =4.4467 0.055 =0.0146 0.0064 0.2485 0.1651 0.1334 =2.0618 10 17.57 0.6 2.545 =5.7375 0.0750 =0.0835 0.0014 0.2437 0.1628 0.1109 =1.9198 11 14.97 0.0 3.465 =6.2554 0.0228 =3.0357 3.0161 0.2924 0.1953 0.0972 =1.8372 12 25.26 0.0 4.5237 =6.8211 0.0559 =3.1527 =0.0541 0.2918 0.2549 0.0369 =1.5419	<u>.ž</u>		-										
10 17.57 C.U 2.54-c -5.7375 U.0250 -C.0835 0.0014 0.2937 0.1628 0.1109 -1.9198 11 14.97 C.U 3.445 -6.2554 0.0222 -0.0357 0.0161 0.2924 0.1953 0.0972 -1.8372 12 25.25 C.U 4.4234 -5.8211 C.0459 -0.1527 -0.0541 0.2918 0.2549 0.0369 -1.5419													
11 14.97 0.0 3.4044 -6.2554 3.0222 -3.0347 3.0161 0.2924 0.1953 0.0972 -1.8372 12 25.26 0.0 4.4234 -6.8211 0.8459 -3.1527 -0.0541 0.2918 0.2549 0.0369 -1.5419													
2 25.26 C.U 4.4237 -4.0211 C.0459 -3.1527 -0.0541 0.2918 0.2549 0.0369 -1.5410	_												
13 27.57 p.0	12												
	13			42.47	-7.43×								

7. TEST PART HACK RAIGHT PRIL COME 1. DELL DEL2 DEL3 DELA IRANSITION  2 54 0.00 2.5 0.0 M3-0615 0.0 0 0 0 FREE  T ALPHA -FT - CAF1 CA1 CA1 CA1 CA1 ACP1 VCPF1 CAP2 CAP2 KUPF2 VCPF2  -1.A3 M. U. 0-1151 -3-1.10 0.110 1.27-1 VCPF1 CAP2 -1.111 0.0345 0.2111 0.6040  -0.44 U. U0.2143 - 0.134 U. 0.110 1.27-1 V.	2 5F U-P2 2-5 U-D W3-DF15 0.0 0 0 0 FREE  I ALPMA -FT CMF1 CM1 CM1 CM1 KCPF1 VCPF1 CMF2 CM7 CM7 KCPF2 VCPF2 -1-53 MUN -0-0-11-1 -0-0-16-0 CM10-1 (-273 *6-570A *0-0-16-1 -0-0-10-3 -0-211-1 (-650A *0-11-1 -0-0-16-0 CM10-1 -0-0-0-16-0 CM10-1 -0-0-0-16-0 CM10-1 -0-0-0-16-0 CM10-1 -0-0-0-16-0 CM10-1 -0-0-0-0-16-0 CM10-1 -0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	2 5+ 0.ep 2.5	7 ALPMA -FTN CMF1 CM1 CM1 FCPF1 VCPF1 CM2 CM2 CM2 RCPF2 VCPF2 -1.63 NEW -0.0112 -0.0146 CM10m (.2703 VG.570A v0.065 -0.0163 0.0385 0.2111 0.8860 -1.64 N.0 -1.2163 -0.0146 CM10m (.2703 VG.570A v0.065 -0.0162 0.0385 0.2111 0.8860 -1.64 N.0 -1.2163 -0.0166 -0.0167 -0.0162 0.0162 0.0231 1.5669 -1.64 N.0 -1.0166 -0.0166 -0.0322 0.0063 0.0083 0.0083 0.0083 0.0081 0.010 0.1669 0.1760 -2.64 N.0 -1.0168 -0.0322 0.0065 0.2217 -0.4330 0.0831 0.0081 0.010 0.1669 0.1760 -2.64 N.0 -1.0168 -0.0322 0.0065 0.2221 -0.0430 0.0831 0.0081 0.0010 0.1669 0.1760 -2.64 N.0 -1.0168 -0.0322 0.0565 0.2227 -0.02475 0.1089 0.0831 0.0084 0.1568 0.2288 0.0065 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0067 0.0	E	ENGINES 2 OF 3 1 OF J	3	<u> </u>	CENTERIA	EDC1 PI	Martie 4	LAIND TUN	NEL FACIL	ITY(P=1) S uata	AERO	 INO TUMMEL (AT)
-1.43 val =0.4113 =0.4146	-1.43	-1.63	-1.43												 ha
-0.47 0.0 0 0.0 0.032 0.032 0.032 0.032 0.032 0.032 0.033 0.0025 0.0033 0.003 0.032 0.032 0.032 0.032 0.032 0.032 0.002 0.002 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003	-0.49 0.0 -0.2163 - 0.036 0.027 0.027 0.0276 -0.0116 -0.0737 -0.0162 0.3231 1.5669  1.44 0.0 -0.6164 -0.0332 0.0369 0.2017 -0.6330 0.0431 0.0010 0.110 0.1409 0.1746  2.47 0.0 -0.2124 -0.0364 0.0393 0.0369 0.2017 -0.6330 0.0431 0.0011 0.110 0.1409 0.1746  2.48 0.0 -0.2224 -0.0245 0.0393 0.0369 0.2017 0.2265 0.1049 0.0175 0.0281 0.1608 0.2584  3.47 0.0 -0.0224 -0.0245 0.0392 0.0369 0.1565 0.0555 0.0251 0.0448 0.1583 0.3000  5.40 0.0 -0.124 -0.024 0.0392 0.0393 0.0393 0.0048 0.1583 0.3000  5.40 0.0 -0.124 -0.024 0.0392 0.0393 0.0393 0.0393 0.0393 0.0393 0.3000  13.70 0.0 -0.124 -0.024 0.0392 0.0593 0.0593 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0.0393 0	-0.44 0.0 -0.213 -0.037 0.017 0.076 -0.016 -0.0737 -0.0162 0.3231 1.5669  1.44 0.0 -0.6166 -0.0322 0.0063 0.2017 -0.4330 0.00631 0.0110 0.1100 0.1409 0.1706  2.47 0.0 -0.2242 -0.0165 0.0055 0.2217 -0.4330 0.00631 0.0110 0.1409 0.1706  2.48 0.0 -0.0224 -0.0245 0.0055 0.2217 -0.4330 0.00631 0.0064 0.1503 0.0064 0.3435  2.49 0.0 -0.0224 -0.0245 0.0055 0.2217 -0.2415 0.1555 0.0251 0.0446 0.1503 0.3000  5.40 0.0 -0.0224 -0.0245 0.0057 0.2027 0.1650 0.1555 0.0251 0.0446 0.1503 0.3000  5.40 0.0 -0.0163 -0.032 0.0050 0.0050 0.0050 0.0050 0.0251 0.0446 0.1503 0.3000  5.40 0.0 -0.0163 -0.032 0.0050 0.0050 0.0050 0.0050 0.0050 0.2105 0.1610 0.3844  13.70 0.0 -0.0163 -0.032 0.0057 0.0557 0.0558 0.0057 0.0563 0.2105 0.1610 0.3844  13.70 0.0 -0.0177 -0.0057 0.0559 0.3150 0.0155 0.0077 0.0563 0.2105 0.1610 0.3844  17.67 0.0 -0.0177 -0.0057 0.0559 0.3150 0.0155 0.0077 0.0563 0.0077 0.0008 0.3785  17.67 0.0 -0.0177 -0.0057 0.0559 0.3150 0.03780 0.03780 0.03780 0.3732 0.0761 0.3609  25.26 0.0 -0.0320 -0.0070 0.0100 0.0100 0.2556 -0.3260 0.2515 0.0008 0.3785  27.57 0.0 -0.0324 -0.0074 0.0050 0.2555 0.0193 0.0557 0.4231 0.0044 0.3435  27.57 0.0 -0.0324 -0.0074 0.0050 0.2755 0.0193 0.2272 0.0375 0.4064 0.3435	-0.44	INT											
1.44	1-46	1.44	1.44 6.0 -0.6106 -0.0332 0.0000 0.2017 -0.4330 0.00631 0.010 0.1000 0.1400 0.1700 0.241 0.0051 0.241 -0.6106 -0.0332 0.0000 0.00631 0.0001 0.0110 0.1400 0.1700 0.241 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.00510 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.0051 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2510 0.2	<del></del>											
1.44	1.44	1.44 G.U =0.6186 = 0.0332 U.0367 0.2017 -0.4330 0.0031 0.0031 0.1040 0.1440 0.1740 2.21 0.0031 0.0031 0.0031 0.0031 0.1040 0.1740 2.21 0.0031 0.0031 0.0031 0.0031 0.1040 0.1740 2.21 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.	1.44	2											
2.47 0.0 -0.32.3 -0.3162 0.005. 0.22.7 -0.24.5 0.104.9 0.015. 0.0281 0.1608 0.2586  3.47 0.0 -0.52.2 -0.52.5 0.005.0 0.37.4 0.27.4 0.165.0 0.155.5 0.0251 0.0448 0.1602 0.165.7 0.3612  v.b. 6.0 -0.51.3 -0.73.5 0.010.7 0.27.5 -0.747.0 0.467.7 0.065.0 0.210.5 0.3612  v.b. 6.0 -0.51.3 -0.73.5 0.010.7 0.27.5 -0.747.0 0.467.0 0.265.0 0.210.5 0.1210 0.3844  13.70 0.0 -0.015.7 -0.005.7 0.005.7 0.37.5 0.37.6 0.015.0 0.015.0 0.27.2 0.306.7 0.0948 0.37.6  17.87 0.0 -0.015.7 -0.005.7 0.005.7 0.37.6 -0.37.80 1.03.9 0.07.9 0.37.2 0.004.8 0.37.8  17.89 0.0 -0.015.7 -0.005.7 0.005.7 0.37.6 0.37.80 1.03.9 0.07.9 0.37.2 0.004.7 0.3609  19.37 0.0 -0.015.7 -0.005.7 0.005.7 0.37.6 0.37.80 1.00.8 0.065.9 0.37.2 0.004.7 0.34.9 0.37.8  25.26 0.0 -0.03.0 -0.007.0 0.010.5 0.27.5 -0.32.4 1.23.1 0.004.0 0.34.5 0.37.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.33.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.34.5 0.004.0 0.004.0 0.34.5 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0 0.004.0	2.47 0.0 -0.32.3 -0.3100 0.005.	2.47 0.0 -0.32.3 -0.1645 0.005, 0.22.7 -0.24.5 3.1349 3.0175 0.0241 0.1648 2.2584 3.47 0.0 -0.32.2 -0.02.5 0.03.5 0.27.4 -0.165 0.1555 0.251 0.0448 0.1603 0.3000 5.27 0.0 -0.167 -0.02.3 0.002 0.27.5 0.1621 0.2774 0.0404 0.1602 0.1457 0.3612 9.00 0.0 -0.51.3 -0.737 0.0107 0.27.5 -0.7475 0.4477 0.0563 0.2105 0.1210 0.3844 13.70 0.0 -0.0157 -0.0057 0.0057 0.3016 -0.3780 0.0165 0.0075 0.3067 0.0988 0.3765 17.07 0.0 -0.0157 -0.0057 0.0057 0.3016 -0.3780 0.0316 0.00165 0.0075 0.3732 0.0761 0.3609 19.37 0.0 -0.032.2 -0.0057 0.0057 0.3016 -0.3780 0.0059 0.3772 0.3067 0.0988 25.26 0.0 -0.032.6 -0.0070 0.0105 0.2276 -0.0479 1.0000 0.0059 0.3772 0.00647 0.3609 25.26 0.0 -0.032.6 -0.0070 0.0105 0.2240 1.2316 0.0659 0.3772 0.00647 0.3435 27.57 0.0 -0.0265 -0.0071 0.0055 0.2755 -0.1930 1.2272 0.0375 0.4164 0.0306 0.3383	2.ef 0.0 -0.32.3 -0.1625 0.005; G.22/I -0.24/S 0.132/ 0.0281 0.0088 0.3584 3.e7 0.0 -0.32.2 -0.0525 0.0325 0.3251 0.0088 0.1583 0.3000 5.ex 6.p -0.112/ -0.112 -0.112 -0.112/ 0.121/ 0.121/ 0.1628 0.1533 0.3000 9.ex 6.p -0.112/ -0.112/ -0.112/ 0.2725 -0.142/ 0.2718 0.1628 0.2105 0.1617 0.3621 9.ex 6.p -0.112/ -0.112/ 0.101/ 0.2725 -0.747* 0.4477 0.0663 0.2105 0.1210 0.3844 13.70 0.p -0.012/ -0.0540 -0.0524 0.2520 0.1536 0.815. 0.815. 0.8072 0.3067 0.8988 0.3725 17.87 0.p -0.012/ -0.057 0.005* 0.3010 -0.3780 1.0339 0.0796 0.33732 0.0761 0.3609 19.ex 6.p -0.012/ -0.0067 0.005* 0.3010 -0.3780 1.0339 0.0796 0.3772 0.0667 0.3609 19.ex 6.p -0.012/ -0.0067 0.005* 0.0069* 0.3722 0.0667 0.3498 25.ex 6.p -0.0326 -0.0070 0.010 0.2644 -0.3240 1.2316 0.6597 0.4231 0.0644 0.3435 27.57 0.0 -0.0326 -0.0074 0.0055 0.2755 -0.1930 1.2272 0.0376 0.4040 0.3393												
3.47 0.0 -0.22.2 -0.0245	3.47 0.0 -0.72/2 -0.0245	3.47 0.0 -0.72.2 -0.0245 0.3024 0.2746 -7.1165 0.1555 0.0251 0.0449 0.1583 0.3060 5.44 0.0 ministry mi	3.47 0.0 =0.07.2 = 0.0024												
Vanc 6.0 -0.5143 -0.737 0.6107 0.2755 -0.747 0.5463 0.2105 0.1210 0.3844 13-14 0.4 -0.4102 -1.6104 -1.6124 0.2524 0.41536 0.4145 0.4577 0.3067 0.4988 0.3765 0.4988 0.3765 0.4988 0.3765 0.4988 0.3765 0.4988 0.3765 0.4988 0.3765 0.4988 0.3765 0.4988 0.3761 0.3669 19.37 0.4 -0.4022 -0.4040 0.4044 0.2766 -0.4879 1.6040 0.4649 0.3772 0.4067 0.3669 25.766 0.4 -0.3265 -0.0076 0.4104 0.2766 -0.4879 1.6040 0.4649 0.3772 0.4067 0.3669 25.766 0.4 -0.3265 -0.0076 0.4104 0.3655 0.6567 0.4231 0.4067 0.3668 27.57 0.4 -0.3265 -0.0076 0.4105 0.6567 0.4231 0.4064 0.3435 27.57 0.4 -0.3265 -0.4074 0.4055 0.2755 -0.1936 1.2272 0.4067 0.4231 0.4064 0.3435 0.4 -0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067 0.4067	Vanc Cau -0.5143 -0.737 0.6167 0.2755 -0.7476 0.4477 0.6663 0.2105 0.1210 0.3864 0.3745 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	### ### ##############################	4.00       6.0       -0.5163       -0.7187       0.6107       0.2755       -0.7476       0.6063       0.2105       0.1210       0.3866         13.70       0.0       -0.0162       76.0162       0.2520       0.01536       0.0165       0.0177       0.3067       0.0948       0.3785         17.87       0.0       -0.0177       -0.0067       0.0054       0.3166       0.3796       1.2319       0.0796       0.3772       0.0067       0.3609         19.97       0.0       -0.0221       -0.0221       -0.0102       -0.0102       0.0479       1.0087       0.0479       0.0479       0.0067       0.3609         19.97       0.0       -0.0221       -0.0221       -0.0479       0.0479       1.0087       0.0487       0.0488       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0668       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667       0.0667 <td></td> <td>3.47</td> <td>0.0</td> <td>-0-2203</td> <td>-0.0045</td> <td>U.397.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		3.47	0.0	-0-2203	-0.0045	U.397.						
13.76 0.6 =0.0122 = 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0	13.74	13-74 0-4 -0-41ex -1-0-15h -1-0-15h 0-30-15 0-31536 0-41e5 4-0-1772 0-30-7 0-0-488 0-3765 17-97 0-4 -0-41ex -1-0-40-7 0-30-15 0-39-16 1-0-33-9 0-0-1796 1-33-32 0-0761 0-3609 19-97 4-4 -1-0-12-1 -4-4-10-4 4-41144 (-2-746 -10-4879 1-1-0-48 0-0-49-9 0-3772 0-0-4647 9-3-469 25-26 0-4 -0-32-16 -0-0-17-0 4-4-10-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-16 1-2-2-2-16 1-2-2-2-16 1-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2	13.70 0.0 -0.0102 -0.0057 0.0054 0.3105 0.01536 0.0155 0.0772 0.3067 0.0988 0.3785 17.87 0.0 -0.0157 -0.0057 0.0054 0.310 -0.3780 1.0339 0.0796 0.3732 0.0761 0.3609 19.97 0.0 -0.0224 -0.0050 0.0050 0.0050 0.3780 1.02316 0.3772 0.0667 0.3435 25.26 0.0 -0.0320 -0.0070 0.0000 0.0000 0.3231 0.0000 0.3435 27.57 0.0 -0.0324 -0.0074 0.0055 0.2755 -0.1930 1.2272 0.9376 0.4104 0.0306 0.3393	_											
17.87	17.87	17.97 C.U -0.157 -C.UC57 0.054 0.3716 -0.3716 1.0339 0.0796 0.3732 C.0761 0.3609 19.97 U.U -0.0227 -U.000 U.UUU -0.2764 -0.3749 1.000 0.0649 0.3772 0.0667 0.3688 25.26 C.U -0.0328 -0.0700 U.UU0 0.2664 -0.3240 1.2316 0.6231 0.000 0.3435 27.57 C.U -0.0326 -0.0014 0.0055 C.2755 -0.1938 1.2272 0.0376 0.0104 0.3383	17.97			-									
19.97 0.0 -0.322) -0.300 0.0109	19.97 u.u =0.322) =u300 u.ulud f.2766 =0.4979 1.000 0.0699 0.3772 0.0667 0.3698 25.26 C.u =0325 =0.0740 u.ulub 0.2574 =0.3240 1.2316 0.0557 0.4231 0.044 0.3435 27.57 0.u =0.7245 =0.1)14 0.0055 0.2755 =0.193a 1.2272 0.9376 0.4164 0.0306 0.3393	19.97 u.u =0.0222 -u.o.000 u.ulud	19.97 u.u =0.0221 =u200 u.u105 0.2546 =0.4979 1.6008 0.0699 0.3772 0.0667 0.3698 25.26 C.u =0.03c6 =0.0760 u.u106 0.2546 =0.3240 1.2315 0.0557 0.4231 0.0446 0.3435 27.57									_			
25.26 C.v -0.03cb -0.00cb u.010b 0.25c4 -0.32ch 1.2316 0.05c7 0.4231 0.0cc4 0.3435 27.57 0.4 -0.02d6 -0.00cc 0.20cc 0.2755 -0.1932 1.2272 6.9376 0.41c4 0.0306 0.3303	25.26 C.u -0.03cb -0.00cb u.010c 0.25c4 -0.32ch 1.2316 0.05c7 0.4231 0.06c4 0.3435 27.57 C.u -0.02d5 -0.00fd 0.06c5 C.2755 -0.193c 1.2272 0.9376 0.41c4 0.0306 0.3393	25.26 C.w — C.w326 — C.0040 W.W30	25.26 C.u =0.03cb =0.0740 u.010b 7.25cb =0.3260 1.2316 0.05c7 0.6231 0.00c6 0.3435 27.57 0.u =0.0245 =0.074 2.6055 0.2755 =0.193c 1.2272 6.9376 0.41c4 0.0306 0.3393												 
27.57 0.ú -ù.1245 -ù.1)/+ 3.ú.55 (.2155 -ù.193 1.2272 6.5376 (.4164 0.4364 6.3383	27.57 0.ú -0.7245 -0.174 3.ú.55 C.2755 -0.1930 1.2272 6.9376 0.4164 0.0306 9.3393	77.57 0.6 -0.3245 -6.3314 3.6.55 F.2755 -6.1930 1.2272 6.9376 0.4364 0.3304 9.3383	27.57 0.4 -0.0244 -0.1014 2.60.54 C.2755 -0.193 1.2272 6.9376 0.4164 0.0306 9.3393												
		·													
				_			<del></del>								 
				_			<del>,</del>				· · · · · · · · · · · · · · · · · · ·				 <del></del>

. 1	OF 3		**LGPMESI		P.UC1 #			L EFFECTS		AER	ODYNAMIC - IND TUNNEL (AT)
	IESI		*CH_3X1#=		.cu.E.	L VEL	1 DELZ	UEL3 DELA			
INT	ALPHA	tela	C+	CL=	CA O	CL~	CLL	CA CA	CAR	CAF	ACP
	-1.63	بيونا	<u>-1-1-15u</u>					0-3206	6-1090		-1.3587
	-0.61	0.0	-0-0540	100001	-6.0055			0.3201	0.1114		-1.5757
	1.46	0.0		-0.1924		=:_0113	0-00 <b>36</b>	0.3209_ 0.3186	-4-1105 . 0-1057	- 0-2105	-1.1387
	2.07	C-u				-1-0114		0-3176	2-1116_		-1.1367 -1.3638
	7.47	4.6	(-41-6			7	-0.0012	0.3163	6.1131		-1.5176
	5.53	0.0		-: -2044	3.002	جناسات	-0-0003	6-3243	0-1120	0.2077	-1.7753
4	9.59	n v		-2.4-32		-4.0074	0.0036	0.332H	0.1416		-2.0772
<b>.</b>	17.50	<del>0.0</del>		-5.33e7		=0.6025	-0.0007	0.3333	_4-1637_		-2.1231
υ 1	17.30	D. Ú		-5.3307 -6.714a		-1-0195		0.320U 0.3259	0.1740		-2.0016 
	25.40	U. Ú	4.0501			-0.27-3		0.3396	0.2714		-1.4905
3	27.75	سم	5.15/1	-6.6411		-C. C+211		0-3433	0.3114		-1.2075

sŁ.	ENGLIELE 3 Or 3 1 OF 1	21 NG_4E	YEL DEMEIST	CENTERIA	EOC) P	MANTIN MI				AERO	DINAMIC	IND TUNNEL (AT)
	1651 2		<u>sem #Xlu-</u> 72 7.4		CJMF				A TRANSIT			
TALC	-	HF TA	CNES	(=3	C+3	rCPF 3	YCPF3	CNF4	CH4	CB4	XCPF4	YCP#4
1	-1.64	leale		-7-005-	-1-4-53	Caa37U	1.2736_	0_u373_	460000	-0.0246	0-2561	0.6660
Ž	-6.51	1.0	-6.526	-0.0007	-0-3944	0.4256	0-53-0	-0-0324	-0.0009	-0-0098	9.3135	3.4733
	46.00	_ <u> </u>	-0.52v4 -0.623v				0.2345		2_2075_	0.00eT	0.2568	0.1586
	2.47	0.0 		-0.0099 -1.093	-0.0(35 -0.005)	0.4?5H 0.4124	0.1659 	0.0659	0.0146	0.0239	0.2209	0.3626
	3.49	(.0	-0.000 -0.00	-1.00373	-0.01.53	(.3465	-305341-	0.1632	0.6313	0.0006	7-1916	0.4078
	5.53	Law		- 115		6-6163	0-2522	0.2545	0-4472	0-1219	0-1659	0.4283
,	4,59	r. u	-^.5207		-6.01.59	u . 361:0	0.2212	U-553A	0.0665	0.2523	0.1201	0.4556
	13.07	<u> </u>		-1.41117	-2-4-50	3.3003	3.1593	J. 5250_	0.4614	0.3577_	0.0745_	0.4336
1	17.46	(.0	-C. [277	-6.304-	-9-9666	U-3274	2-1541	1-0323	0.0599	0.4307	0.0560	0.4172
L	14.95	<u> 0-n</u>		-0-5105		6.31c 6	U-1249	1.0977		_0.4433_	£0494_	0.4039
?	25.40	0.0		-vec115		6.3767	U-05h4	1.7446	0.0240	0.1963	0.0230	0.3813
3	27.76	للجنا	<u>-1341352</u>	e toul 25	<u>-û.Lu25</u>	<u> </u>	9-0711	1.1083	<u> </u>	0.4253	C_017A_	0.3838
					· · · · · · · · · · · · · · · · · · ·							
						<del></del>					<del></del>	
							<del></del>		<del></del>			
							<del></del>		<del></del>		<del></del>	<del>,</del>
					·						<del>~</del>	
			· · · · · · · · · · · · · · · · · · ·			<del></del>	<del></del>	<del></del>				
												_

2 4

E	EmG14Frs 1 OF 3 1 OF 1	Ring ut	<u>weldement</u>	CENTERIA	EUC) P	MOPULSION MARTIN	ISSILE TA	EL FACILI	TY(PAT)	<b>A</b> ER	DDANWAIC PI	ND TUNNEL CATS
	IESI.		ACH - A110-					DEL3 - DELA				/4.
I 14T	ALPHA	HETA	C+,	CLM	CA .	CL+	CLL	0 0 C4	CAH	CAF	KCP	
<u> </u>	-1.53	0	*** 10.44	<u> </u>	حميات ت ـ			-0-0171-	0-1344	2722		
è	-0.54	0.4	-0.0465		-0.0477	0.01e3	-0.0044	56000	0-1-17		-2.0483	
3		<u> </u>		_=5-152-			-0-0065		4-1-00		1.3994	
2	1.45	0.0	0.173.		-0.0064	0.0153		0.4173	0.1440	0.2453		
<b></b>	2,85 3.98	(, , t	0.4545			0.0>00		0.4021	0.1442	0.2669	-1.6609	
ì	5.52	المناب	n. A./Anl	=1-5-5	وهساءا	4250-0	=3-0336	0-4021	0-1568		-2-0434	
8	9.56	6,0	1346		0.0051	-0.0002	0.0619	0.4354	3.1774		-2-1665	
<u> </u>	13.73	<u> </u>	2-1216	-5.02.	2.0033		-0.0037	0_+08			2-1375	
Ĺ	17.72	6.7	3.27-1		0.0171	-C.C1+7		ŭ.+325	0.2109		-1-9656	
	20.09	1-4			3.0137		-0-0013	0.4275	_u_2370		-1-8287	
2	25.56	6.0		-7.1545	6-0347	-0.033-	-3-0101	0.4317	0.2946		-1.4066	
1	26.01		5,7755	-6.5374	<u> </u>	<del>_=0.016l</del>		0.3 <del>878</del>	0.3130	0-0679	-1-5015	<del></del>
												<del></del>
				· <u> </u>								
												_
					<del></del>			<del></del>			<del></del>	
											· · · · · · · · · · · · · · · · · · ·	
	•											
								<del></del>	<del></del>			
						<del></del>		<del></del>				<del></del>
							•			•		
									<del></del>			·····
												<u> </u>
							<del></del>					<del></del>

											·····	
ARNOLU PAGE SHEET	2 04 3	ING LE	y cl_gomeT.	CEILLEMENT	C)		NIND TUN 155ILE TA			AERC	DYNAMIC	IND. TUNNEL (AT)
	1E\$1.	PARI M	ALH PX13-	6PmI	<u>:::::::::::::::::::::::::::::::::::::</u>		1 1115		A TRANSLY O FHE			
POINT	ALPHA	BETA	CNF1	Ch1	Cu)	#CPF]	VCPF1	CNF2	CH7	C82	xCPF2	ACOLS
2	-3.60	( , ()		-1.00	6.0071	6.1471		-0.0112	-0.0000	-0.0254	0.4284	2.2766 ·
	1.45	¢.0		-0-0045 -0-0047			-0.2164 -0.1677	0.0323	0.0011	0.0116 0.0049	0-1044 0.1446	-0.3588
5	2.05	0.4	-0.02.7	-Catalan	6.0653	(-1749	-4-2151	0.1255	0.0174.	_ 0.4278_	4.1388	0.2217
6	3.48	U . U		-0.0047	0 <b>-</b> 00 € •		-0-2321 -0-2074	0.1789	0.0745	0.0494	0.1368	0.2764
6	9.50	0.0		-6.1345	0.0123	6.2175	-5.5698	0.5412	0-0519	0.2235	0.0912	0.3780
10	17.92	C.U		-0.0355 -0.0355			-0-1760 -0-1454	0-8721- 1-1014	<u>0-0552</u> 0-0517	0.3248_ 0.4115		<del>0.3782</del> 0.3736
_11_	20,64	0.4	-0.v3ln	-0-00-3	c_outo	1967	-2-2766	l.1#3#	0+44db_	0.4333_	_0.0412_	0.3660
13	25.55 28.01	U_U_		-0-2362	0.0000		-0.1956 -0.0563	1.3157	78E0.0	0.4540	0.0293	0.3519
						-						
							<del></del>					
												···
		•										
							<del></del>		<del></del>			
									· · · · · · · · · · · · · · · · · · ·			
··			<del></del>	*****					<del></del>			
				· · · · · · · · · · · · · · · · · · ·						****		· · · · · · · · · · · · · · · · · · ·
			_									
			<del></del>					<del></del>				

٠,

:

E .	OF 3	TING LE	VEL OP-E.I	CENTERIA	EGC) P	MANTIN MI		NEL FACILI		AERu	DANAMIC	(IND THINNEL (AT)
	IES1_		<u> </u>		-	L WELL		DEL3 DEL	TRANSIT			
INT	ALPHA	HETA	CAF3	Cr3	C+3	*CPF3	YCPF3	CMF4	CHA	C94	XCPF4	YCPF4
1	-1.63	0.0		حفيالمكع		E - 3443	2-2444	-0-0487	-0.0077		0-1581	0-4095
2	9-41	0.0	-0-1254	-0.0107	-6.0054	0.4014	0.2276	-0.0000	-0.0001	-0.0130	0.0044	2-1703
4	1.45	6.0		-0.161 -0.0095			0.2273	u_c38a	0.6125	053 Enso.o	0-2078	0.3393
5	2.45	0.0		-0.0110		0.3613	0.1550	0.1304		0.0502	0-1420	0.3693
6	3.46	0.0		-0.6163		6.3448	0.1977	0.1906	0.0252	0.0771	0.1323	0.4046
<u>7</u>	5-52 4-56	0.0		=010F		0.3554	0.2023	0.5891	0.04+6	0.2650	0.1156	0.4259
•	13.73	6.0			-0.0050 -0.0049		0-1462		_0_0499_	_0.2550	0.0842	0.4499
0	17.92	0.0			-0.0031	0.3334	0.7664	1.0578	0.0079	0.4454	0.0453	0.4248
1	20.09	0.1		=4.121		0.3367	.0.0941	1-1427	0.0402_	0.4764	_0.0352_	0.4169
3	25.5t	0.0		-05165 -05100		C.3505	0.0239	1-2765	0.0257	0.5131 0.5121	0.0224	0.4013
<u></u>	<u></u>		<u> </u>				···			<del></del>		<u> </u>
				<del></del> -								

QLU .	ENGINE	FRING LIE	<u>₩₽1.₽₩₽! 1</u>	CEN)ER(e	FüC1 Pr	204015104	-ainO_Tun	NEL FACILI	IY(Pal)	AER	DDYNAMIC HIND TUNNELLA
	1 OF _					-ARILO -	135166 14	IC EFFECIS			
		•									
			<del></del>								
_	165	I FAFT P	ALE BALLS	6Enl	CURF	L GEL	DELZ	DEL3DELA	_TRANSITI	DN	
	2	61 1.	14 5.5	Ů• <b>©</b> ⊓	3-0f15 0	• 0	0	0 0	FREE		
InT	ALPHA	6514	· ·	CL 4	CY	CLN	CLL	CA	CAP	CAF	XCP
	محملت		-0-10-5		-4-3155	0.4376	-0.0077	2,5939	0.2074		-1-6957
5	-0.51		-0-0143		-0.0156		-4-0077	0.5902	0.2143		-1.4440
<u> </u>	-0.46			<u>=0.1570</u>			-4-0069	0-5645			-1-8726
	1.45			-0.3594	-0.0109		-0.0071 -0.0068	0.5872	0.2176 0.2185		-1.7688 -1.8116
	3.49		7.4416		-0.0113		-0.6054	0.5851	n.5593		-1.8727
<u> </u>	-5.54	6-0	2-1920	-labach	-0-3CAG	4-3354	-0-3325		1055-0	0.3020	-1-9879
•	9,63			-3.11+3			-0.0015	0.~006	9-2501		-2.0507
<u> </u>	13.75 19.01			-5.5244 -5.5365				- 0.5935 · 0.5924	2562- C-2731		-1-9539
	20.21			-5.560e			-9-06/15	0.5527			-1-7367 1-5566
?	25.96	0.0	5.3-27	-6.2241	0.0313	0.064h	-0.0020	0.5176	0.2908	0.2268	-1.1573
	24.35	المنا ا		-6-0155	0.0635			2.6431	0.3020	0-1911	-0.9836
		<del></del>									
							***************************************				
							· · · · · · · · · · · · · · · · · · ·				<del></del>
		-				-					
										<del></del>	
								<u></u>			
		<del></del>		<del></del> -	<del> </del>						
							<del></del>				
_											

			<del> </del>	<del></del>							<del></del>		
E a	ENGISEER 2 OF 3 1 OF 1	ING UE	BELOPME AL	CENTERIAL			HINO TUN			AERO	DYNAMIC.	INO TUNNEL (AT)	
				ьР.н					a_IHAMSII				
	S	01 1.	16 2.5	u ₀	#0F15 G	. 0	0 0	<u> </u>	9 FHE	Ε			
TAIC	AL DHA	HF TA	C.F1	Cml	C41	#CPF1	YCPF1	C4+ S	CuS	C87	ACPF 2	YCPF2	
2	-0.51	l'eu	-0.12-0	-0000001	U-6676	0.165E	-0.3760	-0.060H	-0.0119	-0-0454	0.2713	2.1263	
4 .	0.01	UAU	<u>-0.025°</u>		0.0173		-0.3194		0.0025_		_0.0869 .	-0-3312	
•	1.45	0.0	-1.075+		0.0075		-0.3145	0.6764	0.0097	0.0078	0-1275	0.1025	
_5	2.45	0.0		-0au347	1-0:0:41		P.1697	0.1249	نے دائے		_C-130e_	0.2235	
6	3.44	0.0	-0.326,	-004-	6.0.61		-0.2337	0-1-27	0.0737	0.0499	0-1295	0.2730	
7	5.5u	<u>_0_u</u> _	-0.4235		0.0:17		-0.06ul	3.5750	<u>0.367</u> _	<u>0.1016</u>	0.1121	0.3783	
4	9.63 _13.74_	0.0	-0.0735 -0.070-0-	-1.0(639	C.0120 <u>+6.0107</u>	0.1557 0.1568		0.5759 		0.2146	0.0772	0.3726 	
10	19.67	6.0	-0-03-0		0.0000		-0.2776	1.440	0.0359	0.3906	0.0344	0.3741	
ii	25.27	0.4			_ Calle		-0-2063	1-1274	0.6250_		0.0258 _	0.3691	
12	25.92	0.0	-0.0405	-0-24-05	0.0640	0.1451	-C.0977	1-3005	0.0196	9.4747	P.0152	0.3650	-
13	26.35	0.4	-0514	-0-0-0-	مكيشمتم	0.1529	0.1637	1.3519	4.3175	0.4901	0.0129	0.3625	
										· · · · · · · · · · · · · · · · · · ·		,	
		•											
			<del></del>					• • • • • • • • • • • • • • • • • • • •					

1 -1.49	1	Ł	2 OF 1 OF	3	<u>*************************************</u>	<u> </u>	VENC!			NNEL FACILI		AER(	OZNAMIC .	LIND_TUNNEL_(AT)
2 -(.5) 0.0 -0.0357 -(.727 0.0017 0.05.7 -0.044 -0.053 -0.0065 -0.0257 0.9575 5.1012 3 . 0.47 0.0 -0.0323 -0.023 0.0055 0.0066 -0.1624 0.0376 0.0005 -0.0116 0.0133 -0.3138 4 1.40 0.0 -0.0325 -0.0022 0.0027 0.0456 -0.1763 0.0653 0.0070 0.0059 0.0824 0.0698 5 245 0.0 -0.0325 -0.0022 0.0021 0.0572 -0.0641 0.1327 0.0124 0.0253 0.0936 0.1937 6 3.46 0.0 -0.0357 -0.033 0.0070 0.0036 0.3254 7 5.56 0.0 -0.0357 -0.033 0.0070 0.0038 0.3056 0.0280 0.0938 0.0970 0.0989 0.2534 8 5.67 0.0 -0.0324 0.0029 0.11/3 -0.0831 0.3056 0.0280 0.0988 0.0015 0.3234 8 5.67 0.0 -0.034 0.0029 0.11/3 -0.0831 0.5559 0.031 0.2033 0.0650 0.3656 9 13.66 0.0 -0.034 0.0029 0.11/3 -0.0831 0.5559 0.031 0.2033 0.0650 0.3656 10 10.19 0.0 -0.0440 -0.0058 0.0050 0.0570 0.0057 0.0065 0.3658 11 20.47 0.0 -0.0440 -0.0058 -0.0044 0.0557 0.0057 0.0066 0.4352 0.0072 0.3671 12 20.47 0.0 -0.0633 -0.0044 0.0045 0.0028 1.1657 0.0066 0.4352 0.0072 0.3671	2 -(-a)	THIC		HETA	CHF1-	Cnl	Cn1	ACPF 1		C4F2	CH?	CRP		
3 . G-6c  O.D	3	1												
1.44 0.0 -0.0325 -0.0022 0.0057 0.0056 -0.1763 0.0653 0.0070 0.0059 0.0824 0.0698 0.255 0.0070 0.0059 0.0824 0.0698 0.255 0.0070 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059 0.0059	1.44													
5	5	4												
6 3.46 0.0 -0.0357 -0.033 0.0035 0.0056 -0.1077 0.1453 0.0183 0.0070 0.0989 0.2534 7 5.54 0.0 -0.0356 -0.037 -0.0031 0.1035 0.0038 0.3056 0.0280 0.0280 0.0988 0.0915 0.3234 8 9.07 0.0 -0.037 -0.037 0.0029 0.11/3 -0.0831 0.5559 0.0351 0.2033 0.0650 0.3656 9 13.66 0.0 -0.037 0.0029 0.11/3 -0.0831 0.5559 0.0356 0.2033 0.0650 0.3656 9 13.66 0.0 -0.037 0.0035 0.2033 0.0650 0.3745 0.0837 0.00356 0.2033 0.0650 0.3745 0.0035 0.2033 0.0650 0.3745 0.0035 0.2033 0.0650 0.3745 0.0035 0.2033 0.0650 0.3715 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0	8 3.46 0.0 -0357 -0.0-35 0.0035 0.0-356 0.0-1077 0.1453 0.0183 0.0-070 0.0989 0.7534 7 5.56 0.0 -0.0-10.0 -0.0-10.0 0.0038 0.0038 0.0038 0.0038 0.0038 8 9.67 0.0 -0.0-7.7 -0.0-34 0.0027 0.11/3 -0.7831 0.5559 0.0351 0.2033 0.7650 0.3656 9 13.66 0.0 -0.0-10.0 0.0 -0.0-30 0.0027 0.11/3 -0.7873 0.0356 0.2988 0.0552 0.3163 10 16.19 0.0 -0.0-7.0 -0.0036 0.1077 0.0057 0.779 0.0308 0.3655 0.0316 0.3718 11 20.47 0.0 -0.0-7.0 -0.0036 0.0036 0.1070 0.0057 0.779 0.0308 0.3655 0.0316 0.3718 12 20.47 0.0 -0.0-10.3 -0.0036 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00	-												
7 5-5e c-u =0.032e =0.032 =0.0001 (-10.45 0.0038 0.3056 0.0280 0.0015 0.3234 8 9.67 0.0 = -0.0247 0.0279 0.11/3 =0.0831 0.5559 0.0351 0.2033 0.0650 0.3656 9 13.66 0.0 = -0.0249 0.015 0.1244 0.015 0.1244 0.035 0.7873 0.0356 0.2948 0.0452 0.3745 16 16.19 0.0 =0.0440 -0.0058 0.0058 0.1147 0.0657 0.9749 0.0308 0.3625 0.0316 0.3718 11 20.47 0.0 =0.0057 0.9749 0.0308 0.3625 0.0316 0.3718 120.47 0.0 =0.0057 0.9749 0.0251 0.3858 0.0239 0.3671 12 26.22 0.0 =0.0053 =0.0044 0.0044 0.0044 0.0128 1.1657 0.0066 0.4352 0.0072 0.3671	7 5.5a t.u et.27a = 6.602 - 0.60ul (.10.5 0.0028 0.005 0.0280 0.0280 0.005 0.3656 8 9.07 t.u = -0.707 - t.u.034 0.0027 0.11.3 -0.7831 0.2033 0.7873 0.0233 0.7850 0.3856 9.11.66 0.6 -0.6134 -0.015 0.1284 -0.015 0.7873 0.0356 0.2988 0.0452 0.3785 10.11.60 0.0 -0.7870 -0.0057 0.0057 0.7873 0.0356 0.3055 0.318 10.11.60 0.0 -0.7870 -0.0057 0.0570 0.3787 0.0356 0.3055 0.318 10.2035 0.2036 0.3788 10.2036 0.3785 0.0316 0.3718 11.2047 0.0047 0.0057 0.478 0.0308 0.3055 0.0316 0.3718 11.2047 0.0057 0.0057 0.3251 0.3858 0.0239 0.3671 12.2047 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.005	<del>_</del>												
9 13.66 0.0 -1.0344 -0.0015 0.1244 -0.035 0.7873 0.0356 0.2948 0.0452 0.3745 10 10.19 0.0 -0.0440 -0.0054 -0.0036 0.1157 0.0657 0.4749 0.0308 0.3025 0.0316 0.3718 11 20.47 0.0 -0.0513 -0.0053 -0.0047 2.0478 0.0336 1.0539 0.251 0.3858 0.0239 0.3671 12 26.22 0.0 -0.0633 -0.063 -0.0044 0.0944 0.0128 1.1657 0.0066 0.4352 0.0072 0.3671	9 13.66 0.C -1.034y -0.104 0.015 0.1244 -0.035 0.7873 0.0356 0.2948 0.0452 0.3745 10 14.19 0.0 -0.444 -0.0054 -0.0036 0.1157 0.0057 0.0749 0.0308 0.3025 0.0316 0.3718 11 20.47 0.0 -0.4513 -0.1053 -0.0047 0.0478 0.0936 0.3025 0.0316 0.3718 12 26.72 0.0 -0.0033 -0.0044 0.0047 0.0478 0.0128 1.1457 0.0066 0.4352 0.0072 0.3671 13 26.67 0.2 -0.043 -0.0037 -0.0127 0.0065 0.2937 1.2163 0.0033 0.4444 0.0027 0.3689	ī.												
16 1P.19 0.0 -0.^4^6 -0.0054 -0.0036 0.1157 0.0657 0.9749 0.0308 0.3625 0.0316 0.3718 11 20.47 0.0 -0.0513 -0.0047 0.0047 0.0306 1.0509 0.0251 0.3858 0.0239 0.3671 12 26.22 0.0 -0.0633 -0.0063 -0.0004 0.0959 0.0128 1.1657 0.0066 0.4352 0.0072 0.3671	10 10-19 0.0 -0.000 -0.000 -0.0036 0.1157 0.0057 0.9769 0.0308 0.3025 0.0316 0.3718 11 20.67 0.0 -0.0513 -0.0553 -0.0049 2.0578 0.9751 1.6559 0.2251 0.3858 0.0239 0.3671 12 20.20 0.0 -0.0503 -0.03053 -0.0049 2.0579 0.0128 1.1657 0.0056 0.4352 0.0072 0.3671 13 20.60 0.2 -0.0633 -0.002 -0.0127 0.0652 0.2932 1.2163 0.0033 0.444 0.0027 0.3693	8	9.07	7 0.0	4367	-653	0.0029	0.11.3	-0.7831	7.5559	0.0351	0.2033	0.9650	0.3656
11 20.47 C.W =7.0513 =0.0013 0.0017 2.C478 0.0236 1.C529 0.2251 0.3858 0.0239 0.3671 12 26.22 0.0 =0.0633 =0.0063 =0.0004 0.C454 0.C128 1.1657 0.0066 0.4352 0.0072 0.3671	11 20.47 C.W -7.0513 -0.025 -0.0047 2.6.78 0.0326 1.6529 0.251 0.3858 0.0239 0.3671 12 26.22 0.0 -0.0633 -0.0045 -0.004 0.6954 0.0128 1.1657 0.0066 0.4352 0.0072 0.3671 13 26.67 6.2 -0.0643 -0.0627 -0.0127 6.0062 0.2932 1.2163 0.0033 0.4444 0.0027 0.3669								-0-0435	0.7873	0.0356	8462-0	_0.0452_	0.3745
12 26.22 0.0 -0.0633 -0.063 -0.0644 0.6944 0.0128 1.1657 0.0086 0.4352 0.0072 0.3671	12 26.22 0.0 -0.3633 -0.363 -0.004" 3.69" 0.0128 1.1657 0.0086 0.4352 0.0072 0.3671 13 28.68 0.2 -0.0043 -0.002, -0.0127 6.0852 0.2932 1.2163 0.0033 0.4444 0.0027 0.3683	-												
	13 28.6F 0-2 =													
						<del></del>								
												·		

0f 3 0f 1			CENTENLA				NEL FACIL		AERI	DUYNAHIC	IND TUNNEL (AT)
JES1_											
	#FTA	C*+F3	Cn3	Cp3	ACPF3	YCPF3	CNF4	CH4	C84	XCPF4	YCPF4
	0.0										-1.1460
0.02	<u></u>	-0-0311					-0526				-0-1274
1.44	0.0	-C.0307	-9-019-	-0.065-	0.3000	0.1775	0.0731	0.0090	0.6277	0.0970	0.2977
											-0-3315
											0.3683
4.47	0.0										0.+392
	للوبا	-0.03-4	-C.(13u	-5-0024	0.3767	0.06×5			0.3374	0.0373	0.4340
	U.U					0.0301	0.9635	0.4511	0.4079	0.0510	0.4233
											0.4183 0.4175
25.6b	6.3				0.3934	-0-0246	1.2053				0.4202
	ALPMA -1.00 -0.01 0.02 1.00 2.45 3.40 5.54 4.07 13.80 18.14 20.07 20.07	OF 1  TEST PART #  P 67 1.  ALPMA #FYA  11.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  1.00 ()  2.00 ()  2.00 ()  2.00 ()  2.00 ()  2.00 ()  2.00 ()  2.00 ()	OF 1  TEST PART FACT FRI 1-  P 67 1.20 2.5  ALPMA HFTA CNF3  11.00 6.0 -0.317  0.02 6.0 -0.327  2.45 0.0 -0.327  3.40 6.0 -0.077  5.54 6.0 -0.077  13.60 6.0 -0.031  14.07 6.0 -0.031  14.10 6.0 -0.032  20.27 6.0 -0.034  20.27 6.0 -0.034	OF 1  TEST PART FACE FALSE PRI  P	OF 1  TEST PART FROM FRI 100 PRI CUNE  P 67 1.20 2.5 U.0 03-0715 0  ALPMA FFYA CNF3 CM3 Cb3  1-00 f. 0 0 0.0317 -0.1101 -0.0007  0.02 U.0 -0.311 -0.1101 -0.0007  0.02 U.0 -0.311 -0.0104 -0.0050  1.00 0.0 -0.0327 -0.0104 -0.0050  2.45 0.0 -0.0277 -0.0104 -0.0050  5.54 0.0 -0.0277 -0.0105 -0.0050  7.57 0.0 -0.0317 -0.0115 -0.0041  13.65 U.0 -0.035 -0.0129 -0.0024  18.19 U.0 -0.035 -0.0129 -0.0024  20.27 6.0 -0.045 -0.0131 -0.011	OF 1  TEST PART TAKE FRIDE PRI CURF   UFI    P 67 1-20 2-5	OF 1  TEST PART TALE RAILED PRI CUNF   UFIT DEL2  P 67 1-20 2-5	OF 1  TEST PART FROM FRILES PRI CUNE 1 UFIT OFTS OFTS DEL  P 67 1.20 2.5 0.0 03-0715 0.0 0 0 0  ALPHA FTA CNF3 CM3 CM3 ACPF3 YCPF3 CNF4  1.00 6.0 -0.0317 -0.0101 -0.0034 6.3311 0.1231 -0.0356  0.01 0.0 -0.0317 -0.0101 -0.0047 0.3171 0.1041 6.0095  0.02 0.0 -0.0317 -0.0104 -0.0056 0.3361 0.1775 0.0931  2.45 0.0 -0.0327 -0.0104 -0.0056 0.3385 0.1856 0.1420  3.60 0.0 -0.0277 -0.0294 -0.0056 0.3317 0.1894 0.1965  5.54 0.0 -0.0277 -0.0294 -0.0057 0.3317 0.1894 0.1965  5.55 0.0 -0.037 -0.0115 -0.0041 0.3114 0.1246 0.5547  13.60 0.0 -0.037 -0.0115 -0.0041 0.3516 0.1246  2.55 0.0 -0.0317 -0.0115 -0.0041 0.3516 0.0625 0.7774  13.60 0.0 -0.0324 -0.0124 -0.0036 0.3767 0.0645 0.7774  14.10 0.0 -0.0325 -0.0124 -0.0037 0.3551 0.0632 1.0351  20.07 6.0 -0.0455 -0.0137 0.0013 0.3555 0.0632 1.0351  20.07 6.0 -0.0455 -0.0137 0.0013 0.3567 -0.0363 1.1717	OF 1  TEST PART THEM FRILED PRI CUMF 1 UFL1 DEL2 DEL3 DELA TRANSIT  P 87 1-20 2-5 0-0 03-0715 0-0 0 0 0 0 FME  ALPMA HETA CMF3 CM3 Cb3 ACPF3 YCPF3 CMF4 CM6  1-00 60 -0-0317 -0-1101 -0-0034 C-3311 0-1231 -0-0355 -0-0018  0-001 0-0 -0-0317 -0-1101 -0-0047 0-3171 0-1441 0-0095 -0-0018  0-00 0-0-0311 -0-0100 -0-0054 C-3301 0-1533 0-0526 0-0048  1-00 0-0 -0-0317 -0-0100 -0-0054 0-3008 0-1775 0-0931 0-0090  2-00 0-0-0327 -0-0100 -0-0054 0-3305 0-1856 0-1420 0-0152  3-04 0-0 -0-0247 -0-0094 -0-0054 0-3317 0-1894 0-1965 0-0207  5-50 0-0 -0-0317 -0-0115 -0-0041 0-316 0-1573 0-3137 0-6261  4-57 0-0 -0-0317 -0-0115 -0-0041 0-316 0-1573 0-3137 0-6261  1-10 0-0 -0-0317 -0-0115 -0-0041 0-316 0-1573 0-3137 0-6261  1-10 0-0 -0-0317 -0-0115 -0-0041 0-3555 0-0535 0-7774 0-0290  18-14 0-0 -0-0343 -0-0131 -0-0018 0-3555 0-0082 1-0351 0-0156  20-07 0-0 -0-0343 -0-0137 0-0013 0-3967 -0-0363 1-1717 0-0019	TEST MART FARM FRICE PRI CUME   WFIT DELS DELS TRANSITION    ALDMA META CMF3 CM3 CM3 ACPF3 YCPF3 CMF4 CM6 CM6	TEST PART MALE FRI 1-6 PRI CUNF L LIFT DEL2 DEL3 DELA TRANSITION  APRIL 2.5 U.0 03-0715 0.0 0 0 0 FREE  ALPMA HETA CNF3 CM3 CB3 ACPF3 YCPF3 CNF4 CM4 CB4 XCPF4

Æ	ENGINEES 1 OF 3 1 OF 1	ING DE	AET /JB-AFWT	Cf MTt+ (At	-nc) _F		SISSILE TA			AER	ODYNAMIC MIND 1	UNAEL (AT)
- <u>i</u> z.			ach Palle	0.0 v.		L DEL	1. DEL2_i		A TRANSITI			. 4
1147	ALPHA	BETA	CN	CL*	CY CY	CLN	CLL.	CA	CAP	CAF	XCP	· a
<u>::</u>	-1-63	-0-4	-0-1717	-0-3662		-0-10-0		0.5315	0-1764		-2-1356	
2	-0.59	4.0	-0-0-5	0.1507	1.0514	-0.1105	-0.0201	0.5297	0.1752	0.3545	-3.2452	
3	0.44	0.4						0_5295_			-0-0590	
•	1.45 Z.at	0.0	0.1641	-6-1431 -6-1451		-0.0999 -0.1027		0.5786 	0.1812		-1.0489 -1.2707	
6	3.04	U.U		-0+5+1-		-G.1017		0.5223	0.1440		-1.4316	
ž_	5.56	0.4		-1.100		-4-1133		0-5326	0.1857		-1-5619	
<u>C</u>	9.12	0.0		-2.3171		-6.1239		v.5507	0.2031		-1.6468	
9	13.47	0.4		-3alvai		-0-0960		-0.5005			-1-4742	
0	14.34	0.4		-3.7933		-3.61.7		0.5308	15555		-1-1071	
5	<u>20.62                                   </u>	0.0		-3.c/bn	0.0325	0.0530	-0.0345	0.5225	0.2420	0. 2605.	-0.7450	· <del></del>
3	24.83	0.0			6-0325		-0-0-19	-5361	C-2810		-D-7015	

TEST PART MACH MAIL = 6 PRI CINF L DELI DELZ DELS DELS TRANSITION C 63 122 2.5 0.0 03.0F15 0.0 0 U 0 0 FMEE  AT ALPMA META CAF3 CM3 CM3 XCPF3 YCPF3 CMF4 CM4 XCPF4 YCPF4 -1.53 0.0 -1.72 -0.155 U.5051 U.5051 U.5121 -0.2077 -0.1555 -0.2014 -0.0422 0.0354 0.0256 U.5050 0.0 0 U 0 0 0 0.002 0.030 -0.0744 12.5150-101.4563 0.04 -0.2755 -0.1514 U.5051 U.5053 0.5544 -0.2049 0.0002 0.0030 -0.0744 12.5150-101.4563 0.040 0.0002 0.0002 0.0002 0.0002 0.00000 0.0002 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000		ENGINEES 3 OF 3	TVC DE	VEL DPPE -1	CENTERIAL	nc) bi		ISSILE TA			ΔER		IND TURNEL CA	
2 63 1.27 2.5	ĒĪ_	1_0F_1												
2 63 1.27 2.5							•				•			
2 63 1.27 2.5					<del></del>									
AT ALP-A HETA CAF7 Cm3 Cm3 XCPF3 YCPF3 CmF4 Cm4 Cm4 XCPF4 YCPF4 Cm5 Cm5 Cm5 Cm6 Cm4 XCPF4 YCPF4 Cm5														
-1.63		5	63 1.	24 2.5	9.0 93	1. OF 15 O.	.0	0 0	0	O FHE	E			
0.00 0.0 -5550.015	TAIC	ALPHA	HETA						CNF 4	CHA	CR4	XCPF4	YCPF4	
0.40	1													
1.45 0.0 -0.0017 -0.0130 0.0002 0.4217 -0.2250 0.1009 0.0109 0.1130 0.1702 2.288 0.0 -0.0214 -0.0132 0.0002 0.4217 -0.2250 0.1364 0.0107 0.0302 0.1070 0.2656 3.369 0.0 -0.0214 -0.0132 0.0004 0.0047 0.0047 0.0107 0.0059 0.0098 0.3179 5.550 0.0 -0.0132 -0.0171 0.0004 0.0047 0.7250 -0.3433 0.2086 0.1222 0.0009 0.3175 5.570 0.0 -0.0132 -0.0171 0.0004 0.7250 -0.3433 0.2086 0.1222 0.0050 0.0098 3.155 0.0 -0.0132 -0.0171 0.0004 0.7250 0.0227 0.0504 0.0277 3.1357 0.0 -0.0172 -0.0171 0.0000 -0.4152 0.7317 0.0230 0.3074 0.0315 0.0201 5.150 0.0 -0.0133 0.0000 -0.0152 0.0905 0.0131 0.3773 0.00100 0.0106 5.150 0.0 -0.0132 -0.0000 0.0000 0.0000 0.3054 0.0000 5.150 0.0 -0.0132 -0.0000 0.0000 0.3054 0.0000 0.3054 0.0000 0.0106 5.250 0.0 -0.0132 -0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.0000 0.00000 0.00000 0.00000 0.0000 0.0000 0.00000 0.0000	Š													
2.88 (a.6	<u> </u>													
3.69 0.0 -n.02te -0.0132 ).0069 0.6875 -0.7413 0.1670 0.0167 0.0594 0.0998 0.3179 5.55 0.0 -1.0132 -0.0145 0.1046 0.2544 -0.3433 0.2248 0.1122 0.0829 0.3755 3 7.12 0.0 -0.0132 -0.0114 0.0000 -1.1237 -0.5651 0.5293 0.0267 0.2227 0.5504 0.227 4 13.67 0.0 -0.1122 -0.0143 0.0003 1.0000 -0.4152 0.7317 0.0230 0.3074 0.0315 0.4201 5 11.36 0.0 -1.123 -0.0142 0.0142 0.0003 0.1905 0.131 0.3763 0.0166 0.0166 5 11.36 0.0 -1.123 -0.0142 0.0142 0.0003 0.1905 0.131 0.3763 0.0166 0.0166 5 20.42 0.0 -1.123 -0.0142 0.0142 0.0142 0.0142 0.0142 0.0142 0.0142 0.00070 0.3954 0.0072 0.4167 2 25.41 0.0 -1.135 -0.0142 0.0003 0.5232 -0.1099 1.0759 -0.0076 0.4416 -0.0070 0.4165 3 28.63 0.0 -0.0377 -0.0149 0.0003 0.5232 -0.1099 1.0759 -0.0076 0.4416 -0.0070 0.4165 3 28.63 0.0 -0.0377 -0.0149 0.0003 0.5003 0.5003 -0.0000 0.4611 -0.0070 0.4165	5													
7 5.5h (au -(.2))/ -(.2) into 1.0 (c) 7544 -0.3433 (6.2)48	6													
13.57 0.0 -6.(1yy -0.2)3 0.003 1.0000 -0.4152 0.7317 0.0230 0.3074 0.0315 0.4281 0 15.34 0.0 -1. 2yy -0.0152 0.0142 0.4653 -0.1425 0.4985 0.0131 0.3743 0.0146 0.166 1 20.52 0.0 -1.132 -0.2264 0.4020 0.4571 +0.0750 0.4985 0.0169 0.3954 0.4072 0.4087 2 26.41 0.0 -0.037, -0.0150 0.5932 -0.1099 1.0759 -0.0076 0.4416 -0.0070 0.415 3 28.83 0.0 -7.0337 -0.0150 0.4033 0.5053 -0.0840 1.1311 -0.0122 0.4673 -0.0108 0.4129	1	5.5t	U . U	-6.2396	-1-11-3-	2.0455	3.75mb	-0.3433	S-ZYRA	2-32-4	0.1122	6240°0	0.3755	
1 1 1 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8													
20.57 0.0 -0.135 -0.205 0.007 (.577) -0.0750 0.9626 0.0069 0.3956 0.0072 0.007 2 26.61 0.0 -0.0377 -0.0190 0.0041 0.5232 -0.1099 1.0759 -0.0076 0.4416 -0.0070 0.4105 3 28.63 0.0 -0.0337 -0.0190 0.0033 0.5053 -0.0840 1.1311 -0.0122 0.4671 -0.0108 0.4129	<u> </u>													
2 25.el (.0 -0.037, -0.0190 (.000) f.5732 -0.1099 1.0759 -0.0076 0.4416 -0.0070 0.4105 3 28.el (.0 -0.037, -0.0190 (.0033 6.5053 -0.0840 1.1311 -0.0122 0.4671 -0.0108 0.4129	0													
28.63 0.0 -C.03.7 -LC(147 0.0033 1.555) *0.0860 1.331 *0.6122 0.6671 *8.6108 0.4129	2													
	3													
														· · · · · · · · · · · · · · · · · · ·
								<del></del>						
			•	-										
														<u> </u>
			<del></del>						· <del></del>					
													····	
												_		
												•		
						<del>, </del>								
											-			
								<del>-</del>						
									<del></del>	<del></del>				
														-
				<del></del>	<del></del>									
													<del></del>	
								•						

Ε ,	ENGI4EL 2 Of 3 1 Of 1		ILLOPPENT.	CENTERIA	EuC1 E	HUPULSION H WITHAM		MEL FACIL		AER	ODYMAMIC .	IND TUNNEL (AT)
	1651		LE HALUSA		CONF.	L DEL	1 CELS		A IRANSII D FRE			
147		ë€ 1 ≜	CAF1	Cn1	Col	ACP+ 1	YCPF1	C+.F2	CHS	Ces	xCPF2	YCPF2
	-1.50	0-4	C-2057	10113			Do D		£320 0e	-(-()42	0.0061	0.3553
2	-0.50	( • u	6-60-7	Soutin	い。ひひかち	U-1579	0.5670	-0.0167	-1.0000	-0.0049	2550.0	0,2922
<u>.                                    </u>		-0-0	2-2305	_CairOUA_	- u-6013	4-1274	0-0447	0-0176			-0.0124	_0.2445
<b>•</b>	1.4t	0.0	0.0005 0.0057	0.0013	-0.0065 -0.6063	0-1576	-0.0542 -0.057A	0.0528		0.6205 	-0.0116 -0.0007	0.3890 0.3525
•	3.50	0.0	9.0677	0.0010	-0.0002	0.1375	-0.0208	J.13e7	J. 0001	0.0510	0.0006	0.3677
7	5.5è	See A		Labile	Detrole.	6-17-2	Calain	5-2356		A-una?	_0.006A_	0.3603
5 6	9.60	Ç.U	0.0431	4-0655	6.u13i	6.2412	1.4254	0.4369	0.0064	0.1413	0-0145	0.3220
ŭ	13.73 17.56	0.0	0-0130	<u> </u>	0 <u>115</u> v.0135	C.2452 C.274d	1.2056	0.6516 0.6447	<u>0-0176</u> 0-0302	B-1796. 4.2164		
ì	19.95	Gau	0.0115	2000	C-ú122	0.2751		0.5203	CC_359_		0 <u>_0</u> _0390	0.2529
2	25.24	4.0	0.6159	0.030	0.0002	0.1947	0.2564	1.0566	3.0500	0.2542	0.0473	0.2406
3	27.45	0.6	-c.clo7	C. JOD.	0.0027	-0.6254	-0.1590	1-1978	U-055A	A.25#R	0-0505	0.2358
							<del></del>	<del></del>	<del> </del>			
							· · · · · · · · · · · · · · · · · · ·					
•												

<b>Y</b> (4, 0)	FNG1UFFR	ING OF	ski (ipar st	CENTERIA	FuC) P	Joen Stok	a IND Time	IFI FACTI II		AFDI	OMIN DIMANYOO	TUNNEL (AT)
bŁ	1 OF 3 1 OF 1					MARTI. PI	SSILE TAI	L EFFECTS	DATA			
	IESI_ ?		ALP FAICH		COUF 3=0FI4 (	-L		DEL3 CELA 0 0	JRANSIII FREE			
21-1	ALPHA -1-61	of 1A	( v	CLM	CY =6.00e.1	CL4	CLL	CA 0-2940	CAR	CAF	XCP .	
•	-0.58	0.0	-0.64-	: . ; 744	-U. 0005	E 3	0.0031	0.745.	0.1755	0.1669	-1.8812	
<u>.</u>	1.40	0.0		<u>-6.1531</u>				<del>- 0-2921</del> - 0-2917	0.1049		-0.6930 -1.0568	
<u>. 5</u>	2.45		0.26.00	-4.300	_=0.0434		0.0031	4.2919	-0-1107	0-1812	-1-2692	· <del>····</del>
7	7.51	0.0		=1.+>265 =1:+727			1-00-0 <000-0	0.5455	0.1101		-1.3867	
6	4.41	6.0	1.23-7	-2-150-	-0.6601	-9.0175	0.40-3	6.3121	0.1380	0.1741	-1.7387	
10	17.47	<del>U. V</del>				-f-0113- -f-0+51	_ 0-0047_ 0-0067	1616.0 0.3044	_3.1613 0.1759		-1.7530 -1.6759	
11	19.99	-0.4			0-42m3	_ec.17=\$_		0.2913			-1.6/3V 1.6/41	
12	25.29	C.0		-4.2374		-0.04c5	0.8879	0.2704	0-2177		-1-4254	
					-							
								<del></del>				•
	<del></del>											
									<del></del>			
		<del></del>	·	··		<u>-</u> -				· -		
			<del></del>					<del> </del>	<del></del>	<del></del>		
			<del></del>					· ···				
						······			<del></del>			
											· · · · · · · · · · · · · · · · · · ·	

. •

7 FST PAST TACK RELICES PRIL COME   DELL DEL2 DEL3 DELA TRANSITION   2 TO U.85 2.5. U.0 030010 0.0 0 0 0 0 FREE   ALDMA 55TA CNF3 C-3 C-3 REPS VCPF3 CNF4 C-46 C8A REPF4 VCPF4   -1.51 0.0 -5.0 0.0 -3.0111 -0.0127 -0.032 C.1557 U.3132 -0.0121 0.0012 -0.0111 -0.0971 0.5593   -0.55 0.0 -3.0111 -0.0127 -0.032 C.1557 J.3132 -0.0121 0.0012 -0.0111 -0.0971 0.5593   -0.55 0.0 -3.0111 -0.0127 -0.032 C.1557 J.3132 -0.0121 0.0012 -0.0111 -0.0971 0.5593   -0.55 0.0 -3.0112 -0.0512 -0.0033 J.1552 0.2682 D.6215 D.0010 0.0004 D.0005 0.2225   -1.60 0.0 -0.6113 -0.0623 -0.0033 C.1551 0.3200 U.0550 0.0006 0.0002 0.0006 0.202 0.0139 0.5556   -1.60 0.0 -0.6113 -0.0623 -0.0033 C.1571 0.3254 0.0555 0.0005 D.0331 D.0006 0.202 0.0139 0.5556   -1.60 0.0 -0.0113 -0.0025 -0.0034 D.0325 D.0325 D.0331 D.0006 0.3718   -1.55 0.0 -0.0114 -0.0025 -0.0034 D.0325 D.0325 D.0331 D.0006 0.3718   -1.55 0.0 -0.0114 -0.0025 -0.0034 D.0325 D.0325 D.0331 D.0006 0.3514   -1.55 0.0 -0.0114 -0.0025 -0.0034 D.0325	2 76 U-05 2-5. U-0 03s0f1e 0.0 0 0 FREE  ALPMA SFTs CNF3 CN3 CN3 L0257 UCFF3 CVF4 CM6 C8a RCPF4 VCPF4 CN1	2 76 U.85 2.5. U.0 0380f1e 0.0 0 0 0 FREE  ALPMA SFTA CNF3 CM3 CM3 XCPF3 VCPF3 CM64 CM6 C86 XCPF4 VCPF4  -1.31 0.4 -0.1101 -6.01073 -6.0132 1.2257 U.1169 -0.6610 0.012 -0.61011 -0.0971 0.5103  -0.56 0.0 -0.9111 -6.01073 -6.0122 -0.0121 0.0121 0.0122 -0.0111 -0.0971 0.9176  0.05 C.6 -0.6115 -6.0621 -0.0037 0.1312 0.2206 0.0215 0.8010 0.0008 0.0005 0.222  -1.00 0.0 -0.0113 -6.0621 -0.0037 0.1971 0.2256 0.0056 0.0006 0.0202 0.0139 0.3556  -2.09 U.0 -0.0123 -0.0025 -0.0032 0.1971 0.2256 0.0973 0.0005 0.0351 0.8009 0.3718  3.51 0.0 -0.0113 -6.0025 -0.0032 0.1971 0.2558 0.0973 0.0005 0.0351 0.8009 0.3718  3.51 0.0 -0.0113 -6.0025 -0.0032 0.1971 0.2256 0.1001 -0.0000 0.0558 -0.0002 0.3956  5.50 0.4 -0.1135 -6.0027 -0.0027 0.1709 0.1765 0.2300 0.0026 0.1517 0.0059 0.3559  9.51 0.0 -0.0113 -0.0027 -0.0027 0.1709 0.1765 0.2300 0.0026 0.1517 0.0059 0.3559  13.74 0.6 -0.0174 -0.0034 -0.0032 0.1717 0.1605 0.2266 0.0006 0.2567 0.0038 0.3336 0.3756  13.75 0.0 -0.0027 -0.0028 -0.0028 0.1717 0.1605 0.226 0.0009 0.2367 0.0029 0.2367  10.95 0.0 -0.00223 0.00033 -0.0033 0.1370 0.1370 0.9956 0.0039 0.2762 0.0039 0.2762  27.54 0.0 -0.0221 -0.0033 -0.0033 -0.0033 0.1370 0.9956 0.0039 0.2762 0.0393 0.2755  27.55 0.0 -0.0221 -0.0034 -0.0033 -0.0033 0.1370 0.9956 0.0039 0.2762 0.0393 0.2755  27.55 0.0 -0.00221 -0.0034 -0.0033 -0.0033 0.1370 0.9956 0.0039 0.2764 0.0039 0.2765	3 Or 3 1 OF 1		bel of me vi	LENIEPLA	EUC)P	MARTIN MIS			AER	DDYMAHIC	IND TUNNELIATE
### ### ### #### #####################	ALPMA 5FTE CNF3 C-3 C-3 XCPF3 YCPF3 CNF4 CM6 C86 XCPF4 YCPF4  -1-1 0-W -5-1101 -5-1102 -1-1102 -1-1102 -1-257 Walley -0-6479 D-0610 -0-6244 -1-6217 D-5893  -0-56 0-U -1-0111 -1-1-117 -1-0102 C-1157 -1-1132 -U-0121 D-0012 -0-0111 -1-00071 D-9176  -0-56 C-W -0-61113 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-1102 -1-11	ALPMA SFT= CNF3 C=3 C=3 XCPF3 YCPF3 CNF4 CM6 C86 XCPF4 YCPF4											
-1.51	-0.51 0.0 -0.0111 -0.0123 -0.0132 (.2257 0.1149 -0.6619 0.0610 -0.0244 0.0217 0.5003 -0.50 0.0 -0.0111 -0.0124 -0.0132 0.1502 0.2355 0.0021 0.0012 -0.0111 -0.0071 0.0170 0.2265 0.05 0.0020 0.0130 0.2265 0.0020 0.0020 0.0130 0.3556 0.0020 0.0202 0.0130 0.3556 0.0020 0.0202 0.0130 0.3556 0.0020 0.0020 0.0130 0.3556 0.0020 0.0020 0.0030 0.3718 0.0020 0.0020 0.0030 0.0020 0.0030 0.3718 0.0020 0.0020 0.0030 0.0020 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.00300 0.0030 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00300 0.00	-0.5h 0.u -3.0101 -6.2073 -0.0132 (.2257 u.1164 -0.6614 0.0616 -0.0244 -0.0217 0.5083 -0.5h 0.u -3.0101 -0.0712 -0.032 (.1557 3.3132 -0.0121 0.0012 -0.0011 -0.0071 0.0178 (.255 0.u -0.0114 -0.0212 -0.0222 3.1552 3.2262 0.6215 0.0012 0.0012 0.0016 0.0045 0.2245 1.00 0.u -0.0113 -0.0621 -0.0023 0.1555 0.0020 0.0000 0.0202 0.0139 0.3556 0.u -0.0113 -0.0621 -0.0023 0.1511 0.3200 0.0568 0.0000 0.0202 0.0139 0.3556 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000		. 11						 			~~·
-0.5H 0.U -0.0111 -0.01V -0.032 C.15e7 0.3132 -0.0121 0.0012 -0.0111 -0.0071 0.9178 C.5 C.U -0.011V -0.0122 -0.0022 0.3150 0.3262 0.0262 0.0203 0.0008 0.0202 0.0139 0.3556 0.0 0.0 0.0 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008	-0.56 0.0 -0.0131 -0.0127 -0.027 0.1507 0.3132 -0.0121 0.0012 -0.0111 -0.0071 0.9178 0.55 0.25 0.25 0.25 0.25 0.0010 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.00	-0.58 0.0 -J.0111 -0.071 -0.032 C.15-7 0.3332 -0.0121 0.0012 -0.0111 -0.0971 0.9178   C.55 C.4 -0.0113 -0.0021 -0.0023 0.15-2 0.2820 0.0568 0.0008 0.0008 0.0005 0.2255   L.00 0.J -0.0113 -0.0021 -0.0037 0.1851 0.3220 0.0568 0.0008 0.0002 0.0139 0.3556   L.00 0.J -0.0113 -0.0021 -0.0037 0.1851 0.3220 0.0568 0.0008 0.0002 0.0139 0.3556   L.00 0.J -0.0113 -0.0022 -0.0037 0.1971 0.2556 0.0073 0.0055 0.0081 0.0092 0.3718   L.00 0.J -0.0113 -0.0025 -0.0032 0.1971 0.2556 0.0073 0.0055 0.0081 0.0092 0.3718   L.00 0.J -0.0113 -0.0025 -0.0025 0.1971 0.2000 0.1001 -0.0000 0.0554 -0.0002 0.3756   L.00 0.J -0.113 -0.0025 -0.0025 0.1759 0.1765 0.2000 0.0056 0.1517 0.0059 0.3509   L.00 0.J -0.0025 -0.0025 -0.0025 0.1759 0.1765 0.0328 0.0026 0.1517 0.0059 0.3509   L.00 0.J -0.0025 -0.0025 -0.0025 0.1759 0.0052 0.0026 0.1517 0.0059 0.3509   L.00 0.J -0.0025 -0.0025 -0.0025 0.1759 0.0052 0.0026 0.2367 0.0059 0.3509   L.00 0.J -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2365   L.00 0.J -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2365   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0029 0.2367 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0026 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0026 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0026 0.0026 0.2265   L.00 0.0025 -0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0026 0.0026 0.0026   L.00 0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0026 0.0026 0.0026   L.00 0.0025 -0.0025 -0.0025 0.0025 0.0025 0.0025 0.0026 0.0026   L.00 0.0025 -0.0025 0.0025 0.0025 0.0025 0.0025 0.0026 0.0026 0  L.00 0.0025 -0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.0025 0.								 			
0.95	0.05 (ab -0.01by -0.022 -0.002) 0.1552 0.2042 0.0216 0.0010 0.0048 0.0045 0.2245  1.06 0.0 -0.0113 -0.0021 -0.0032 0.1551 0.3206 0.0556 0.0008 0.0702 0.0139 0.3556  2.09 0.0 -0.0125 -0.0025 0.0032 0.1571 0.2554 0.0073 0.005 0.0361 0.0008 0.3718  3.51 0.0 -0.211 -0.0025 -0.0034 0.2150 0.2906 0.1001 -0.0000 0.0554 0.0002 0.3956  5.55 Gau -0.1145 -0.0025 -0.0027 0.1759 0.1765 0.2000 -0.0002 0.0954 0.0007 0.3229  9.51 0.0 -0.0179 -0.0025 0.1759 0.1765 0.4323 0.0026 0.1517 0.0059 0.3509  13.74 6.0 -0.2147 -0.0034 -0.0041 0.1732 0.2239 0.8052 0.0026 0.1517 0.0059 0.3536  17.77 0.0 -0.0122 -0.0024 -0.0041 0.1732 0.2239 0.8052 0.0029 0.2367 0.0260 0.2964  19.55 0.0 -0.0221 -0.0023 -0.0043 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755  25.29 0.0 -0.0221 -0.0033 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755  77.55 0.0 -0.0221 -0.0034 -0.0034 0.1342 0.1345 0.0044 0.2744 0.0223 0.2863	0.95											
1e 0.0 -0.6113 -0.0621 -0.0632 C.1821 0.3206 0.0568 0.0008 0.0202 0.0139 0.3556  2.49 u.p -0.6122 -0.6002 0.1922 C.1971 0.2555 0.0973 0.0035 0.0351 0.8869 0.3718  3.51 0.6 -0.2110.0025 -0.0038 0.2155 0.2906 0.1401 -0.000 0.0554 -0.0002 0.3956  5.56 0.0 -0.1145 -0.026 -0.022 0.1722 0.1722 0.2755 0.2906 0.1401 -0.0000 0.0554 -0.0007 0.3956  9.51 0.0 -0.512 -0.0025 -0.0025 0.1759 0.1765 0.2300 -0.0002 0.1517 0.0059 0.3509  13.75 0.0 -0.2177 -0.0034 -0.0022 0.1777 0.1606 0.5328 0.0026 0.1517 0.0059 0.3509  17.47 0.0 -0.0024 -0.0022 -0.0048 0.1232 0.2039 0.8052 0.0209 0.2367 0.0260 0.2966  19.95 0.0 -0.0223 -5.1037 -0.0043 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755  27.56 0.0 -0.0221 -0.0034 -0.0013 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755  27.56 0.0 -0.0221 -0.0034 -0.0013 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755	1.00 0.0 -0.6113 -0.0621 -0.0637 0.1871 0.3200 0.0508 0.0008 0.0020 0.0139 0.3550 2.09 0.00 0.00 0.0055 0.0381 0.8899 0.3718 0.3550 0.00 0.0055 0.0081 0.0081 0.0082 0.3718 0.500 0.0055 0.0081 0.0081 0.0082 0.3718 0.500 0.0055 0.0081 0.0081 0.0082 0.0082 0.3718 0.500 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0.0082 0	1.=6											
2-49 u.BC.212u.6023 -u.6032 C.1971 D.2558 D.6973 D.6035 D.6361 D.2049 D.3718  3.51 U.O -C.211U.C.025 -u.0.034 D.215M D.2906 D.1001 -U.0000 D.0554 -0.0002 D.3956  5.5- G.J -D.113C.2124 -U.0.25 D.172- U.1922 D.2306 U.1002 D.6938 -D.8047 D.3929  9.51 D.V -C.512V -U.0.25 D.172 D.1755 D.2363 D.0026 D.1517 D.0059 D.3509  13.74 D.V -C.512V -U.0.25 D.1717 U.1006 D.5328 D.0026 D.1517 D.0059 D.3509  13.75 D.V -C.0122 -U.0.034 D.1717 U.1006 D.5328 D.0026 D.2966 D.0133 D.3138  17.97 D.V -C.0122 -U.0.032 -U.0.031 D.1722 D.2339 D.0026 D.2736 D.0209 D.2737 D.0200 D.2966  19.95 D.D -C.223 -C.1033 D.1370 D.1370 D.9556 D.0391 D.2722 D.0393 D.2755  27.54 D.V -D.0277 -D.0034 -U.0.014 D.1342 U.0069 D.2744 D.0274 D.0023 D.2755  27.55 D.V -D.0277 -D.0034 -U.0.014 D.1342 U.0069 D.2744 D.0023 D.2745 D.0023 D.2755	2.99	2-49 u.B0.312u.6025 -u.0032 0.1971 3-2558 0.0973 0.6035 0.0361 0.0049 0.3718 3.51 0.6 -0.7110.0025 -u.0036 0.215h 0.220h 0.1001 -0.0000 0.0554 -0.002 0.3956 5.5- 0.4 -0.31140.0025 -u.0024 0.1722 0.275h 0.2300 -u.0022 0.0936 -0.0047 0.3929 9.51 0.0 -0.512u.0024 -u.0027 0.1739 0.1765 7.6323 0.0026 0.1517 0.0059 0.3509 13.74 0.0 -0.7170.0034 -u.0032 0.1717 0.1606 0.6328 0.0036 0.1517 0.0059 0.3509 13.75 0.0 -0.5120.5026 -u.0064 0.1732 0.2239 0.8052 0.0209 0.2367 0.0200 0.2964 19.75 0.0 -0.5223 -0.5033 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2875 25.29 0.0 -0.0241 -0.0533 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755 27.56 0.0 -0.0271 -0.0034 -u.0014 0.1342 0.0069 1.6315 0.0036 0.2766 0.0023 0.2766											
3.51	3.51	3.51											
9-51 0-0 -0.1149 -0.024 -0.027 -0.0020 0.1799 0.1765 0.2300 -0.0020 0.1517 0.0059 0.3509 13.78 0.0 -0.0179 -0.0020 0.1717 0.1060 0.5328 0.0026 0.1517 0.0059 0.3509 13.78 0.0 -0.0179 -0.0020 0.1717 0.1606 0.6328 0.0020 0.2367 0.0260 0.2964 19.99 0.0 -0.0223 -0.0020 -0.0024 0.0023 0.2239 0.8052 0.0020 0.2367 0.0260 0.2964 19.99 0.0 -0.0223 -0.0023 -0.0023 0.1370 0.1370 0.0364 0.0257 0.2514 0.0296 0.2875 0.00 -0.0241 -0.0261 -0.0263 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755 0.0027 -0.0221 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0034 -0.0	9-51 0-0 -0.51-7 -0.025 -0.025 0.175 0.1755 7323 0.0026 0.1517 0.0059 9.3509 13-76 0.0 -0.517 0.0 -0.025 0.1517 0.0 -0.059 0.3509 13-76 0.0 -0.025 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0	5.5e 6.u -0.1145 -C.u166 -u-1.22											
13.79	13.7e	13.7e											
17.97 0.0 = 0.0024 = 0.0024 = 0.0043	17.97 0.0 -0.01-2 -0.0020 -0.0003 0.1232 0.2239 0.8052 0.0209 0.2367 0.0260 0.2964 19.95 0.0 -0.0223 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2762 0.0393 0.2755 27.56 0.0 -0.0221 -0.0033 -0.0033 0.1370 0.1370 0.9956 0.0391 0.2762 0.0393 0.2755 27.56 0.0 -0.0221 -0.0034 -0.0014 0.1392 0.0069 1.0315 0.0036 0.2766 0.0233 0.2653	17.97											
19.95 0.0 -0.:2/3 -5.01037 -0.0131 0.1441 0.1355 0.8744 0.0257 0.2514 0.0294 0.2875 25.29 0.0 -0.0241 -0.0633 -6.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755 27.54	19.95 0.0 -0.223 -0.032 -0.033 0.1370 0.1370 0.9350 0.0391 0.2762 0.0393 0.2755 25.29 0.0 -0.0241 -0.0633 -0.0633 0.1370 0.9350 0.0391 0.2762 0.0393 0.2755 27.54	19.95											
25.29	25.29 0.0 -0.324 -6.3633 -6.0033 0.1370 0.1370 0.9956 0.0391 0.2742 0.0393 0.2755 27.54	25.29 0.0 -0.0241 -0.033 -6.0033 0.1370 0.1370 0.9756 G.0391 0.2742 0.0393 0.2755 27.56 f.0 -0.0327 -0.0034 -0.0014 0.1342 0.0069 1.6315 0.0436 0.2744 0.0423 0.2663											
77.56 C-0 =0.027 =0.0074 =0.0014 0.1342 0.064 1.0315 0.0636 0.2766 0.0623 0.2663	27.56 (-6 =0.0271 =0.0034 =0.0612 6.13×2 0.064 1.6315 6.0436 0.2744 0.0423 0.2463	27.54											
					98							3.50	
						<del></del>				 ·	<del></del>	- <del></del>	
										 <del></del>			
						· <del></del>				 			- t
									<del>-</del>	 		•	
									<u>.</u>			•	
									-				
									-			•	
	· · · · · · · · · · · · · · · · · · ·												
	•												
		·			J. 1								

									<del></del>				
				<del></del>									
M-OLD.	ENGINEE!	PING DE	VELOPME AL	.CENIEH (A	ŁUC)	LUPIL STON	-INO TUN	NEL_FACILI	1x(691)""	AER	ODYNAMIC #1	NU JUNNELLAT	<u> </u>
	1 OF 3					MARTIN M	ISSILE TA	IL EFFECTS	DATA				
								_				_	-
	7561	DADT :	ALH PALOS		CUNE	A NEI	1 OF 12	DEL3 DEL4	TOAMETET	Δ			
	5		₹ 5.5		3×0f14 0		0 0	0 0				•	
POINT	ALPHA	FET-	Cn =6-1304	CL >	CY	CLN	CLL	C4	CAR	CAF	XCPXCP		
2	-7.54	0.0	-4.4374	0.0747	-0.0067	+0.u201	0.0021	1.3201	0.1951	0.2150	-1.9713		
	1.47	0.0			<del>-0.065</del> b.		0.0015 0.0018	0.3191			<del>-0.7043</del> -		
	2.50	_0.4	مخدعمه	-0-3580	-0-0633	-0-0229	-0.0018		0-1075	0-5113	-1-2754		
6	3.51	0 <b>.</b> ∪		-1-1563	-0.0030 -0.000		0.0017	0.3179	0.1946		-1.4300 -1.4274		
8	9.64	U.U	1.3000	-2.3747	6.0017	-0.0191	0.0023	0.3439	0.1379	0.2061	-1.8302		•
l u	17.75	U.U.		<u>-3.7293</u> -4.9764		_ <del>0_6107</del> _ 0_377	0.0038	6.3309	0.1749		<del>-1.8245</del> -1.7147		<del></del>
11	20.03			-5,0423		-0-2664	0.0059_				-1-6363		
\$1 EL.	25.41	c.0		-6-2422		-0.0537	0.0045	0.2949	0.2313		-1.3552		
	-21-13	_ المنا	. 5e1/31		C-0444	4510-1	0.0050	4.7643	G-25AB	-0-0145	-1-5345		
												<del></del>	
					· · · · · · · · · · · · · · · · · · ·						·		
									-				
-,,,,,,													•
		-		<del> </del>		· · · · · · · · · · · · · · · · · · ·	<del></del>						
													<del></del>
	<del></del>				··								
											<del> </del>		<del>.,,,,</del>
					<del> =</del>							J	
											•		

	1 UF 3	ING DE	NET OBMENT	CENTENIA	EOC) P			L EFFECTS		AER	DOYMANIC_#IND_IUNHEL14
£1	1OF1.										
	TEST	PART M	ALE HXI J-	e Pal	CUSE	4	DELZ	DEL 3 DEL A	TRANSITI	Get	
	5	72 v.	40 5.5	0.6 H	3 . UF14 0	.0	0 0	0 0	FAE	•	
111	ALPHA	HETM	C∾	CL-	CY	CLN	CLL	Ç.	CAR	CAF	ACP
	-1.56	(- U	-0-15-1	<u> </u>	-0-6-27		0.0010	0.474	0.1324		-1.6602 -2.0577
	0.46	0.0	<u> </u>			-0.0731		.0-4029			-2.03// -c.7985
•	1.49	0.0	0.1734	-0-2540	-0.0011	-0.0246	0.0010	0.4043	0.1352	0.2641	-1.3211
<u>-</u>	_2.49	<u></u>						0-4005	0-1397	0.26CA	-1-4419
6 7	3.45	0.0		-1-132	-3-0(30	-0.0137	0.0614	0.3963	85+1.0		-1.5496 -1.6917
8	4.43	0.0		-2.3524		-0.0125	0.0025	0.4156	0.1795		-1.8914
<u> </u>	13.78	0.0	_ 2-27 ic	-3-2580	u_063c	-150-2-	0.003#	-0-4389	C-1761	0.2629	-1-7597
0	17.47	0.0		-6.4277		-0.0194	0.0051	0.4317	0.2117		-1.6567
2	25.59	<del>11 - 11</del>		-5.3773 -6.0224		-0.0252	0.0076	0.3978	C.2990		-1.2230
	28.01	0.0		-5-6-112		=0-01-6	0-0065	0.3740	0.3107		=1.0463
					<del></del>			<del> </del>	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
								•			
									<del></del>		<del></del>
				•							
						<del></del>				******	
								_			
							4				
				<del></del>			<del></del>			<del></del>	
									·		
				•	•					3-4-	
			· · · · · · · · · · · · · · · · · · ·								
			<del></del> -								<del>'</del>

. .

£	FRGINEE 3 OF 3 1 OF 1		VEL DE 1EUT		EUC) P			SEL FACIL		AE4	ODYNAMIC 1	IND TUNNEL (AT)
•			. 635		_ 12		. 44-14	T 12 22	EW WAY	-	· · · · · · · · · · · · · · · · · · ·	
<b>-</b> -	<u>TEST</u>		-LIER HJA- 50 8.5		3+6f 14 0		DELZ.	DEL3 DEL	O FRE		· <del></del>	
INT	ALPHA	efTe	Co.F 3	CH3	C#3	ACPF3	YCPF3	C+F4	Cri4	C84	XCPF4	YCPF4
<u>.                                    </u>	=1.6v	<u> </u>		-0-10-3 -0-037		0.27/5	6-1107				-0.0640	0.6075
<b>.</b>	0.56	_ U . U		-1013; 		0.2043	3-1130	1-0-0312	0.0019	-0.0124	-0.2042 <b>0.0337</b>	1.3698
•	1	Ű . U		-11139		0.1502	0.1539	0.0695	-3-0Cu7		-0.0095	0.3133
5	2.44	0.4	-0-01×c	. مدنسه ت د	-0-0423	5021.3	-i-1215	0-1136	-0-0316		-0.0144	4.3394
6	3.44	0.0		-C042		0.5019	J. 0873	0.1585	-0.0633		-0.0210	0.3677
<u>.                                    </u>	5.53	<del></del>				<u> </u>	7-1247	0.2551	-0-0054		-0-0213	0-1739
8	9.63	C-0	-	-0.437 -4-3661.		1.1599 0.1525	0-1407	0.4526	0-00-0-0-6-	0.1566	-0.0133 -0.0071	0.3465
LG	17.97	6.0		-0-003-		0.1394	3.1234	0.5250	-0-00¢7	0.2490	-0.0008	0.3014
i	24.13	6.4		-0		0.1563	0.0797	0_5010.			-0.0007	0.2994
2	25.59	0.0	-0.02-1	-[.640	-6.0630	0.14-6	0.1065	1.5337	0.0006	0.2987	0.0064	0.2890
3	25.61	ـ لاحدا	- 10 June	- Bananaa	-0-6613	<u> </u>	0.0408	1.6595	0.0163	0.2933		0.2769
<del></del>												
		· · · · · ·	<u>.</u>		<del></del>			<del></del>	<del></del>		<u></u>	· · · · · · · · · · · · · · · · · · ·
						<del></del>			<del></del>	—— <u>-</u>	<del>-</del> ·	<u> </u>
				•				<del> </del>				

ARLOLD ENGINEERING DEVELOPMENT CENTER(ALUC) PROPULSION NIND TUNNEL EACLLITY (P. C.) AFRODYNAMIC SIND TUNNEL (AT)

MANTIN MISSILE TAIL EFFECTS DATA

PAGE 1 OF 3

ARROLL	ENGINELS	LING JE	ei Oppeni	LENTER LAN	uc) Pi	ROPUL STON	IND TUN	NEL FACIA	17749473	AFH	DDYNASIC	HIMO TUMEL (41)
PAGE	2 OF 3 1 OF 1					MANTIN MI	SSILE TA	IL EFFECT	S DATA			
	TEST	PART =	Lin Billyno	₽π1	CUNF	L DEL1	DELZ	DEL3 DEL	a_transit	IOh		
	5	73 1.	1. 2.5	0.06	3#0F14 0	.0 0	۰.	0	O FRE	E		
POINT	ALPHA	EFTA	CraF 1	CHI	CH1	ICPF 1	YCPF1	CNF2	CHS	C5?	xCPF2	ACOLS
2	-1.53 -0.58	<u> </u>	0.0035	9.0012	U-0115	u.3153	3.2437	-0.0151	0.0003		-0.0206	0.4532
3	<u> </u>	المراب	0.0035	9-0012	_0.0115		5-5431				+0-0305	
4	1.40	5. U	7500.0	3.3015	1500.0	i-+07e	0.8078	0.0526	-0.0026	0.0175	-0.0411	0.2793
5	2-51	0-0	4-3444	3-030-	<u> </u>	G-6813		_ 0-10HO_			-0-0294	0.2074
6 7	3.51	0.0	0.0016	0 = 0004 V = 104	0.0024	0-5677	1.5742		-0.2043		-0.0276	0.3180
	9.67	C. 0	0.0(53	C-2007	V-0153	9-1276	2.8659		-0-0064		-0.0192	0.3084
<u>.</u>	13.82	0.0	2-3-47	7-0715		0-12-0	1-6057		0.0069		-0.0105	
10	10.10	0.0	0.0105	0.0065	0.0157	0.0513	1.4895	0.6204	-0.0059	0.2216	-0.0072	0.2700
<del>-11</del>	20.20	0.4	0_3125		0_0179_	U-06H1	1.4343		-0.0095		-0-0109	
12	25.95	0.u	0.0694	7.J503	0-0261	0.0263	7.8452 1.3307		-0.0101 -0.0152		-0-0102	0.2685 
										<del></del>		
					•							
				•						···		
		<del>.</del>		<del></del> -			·		<del></del>			
			····						······	* * * * * * * * * * * * * * * * * * * *	- <del></del>	
				·				<del></del>	****			
<del></del>					<u> </u>				· · · · · · · · · · · · · · · · · · ·			

2 - 3 6 7	20.5t 0.5t 0.61 1.46 2.51		-0.01+0	Em3	3m0F1 0	•0	L UELZ	DEL3 DEL				
3	20.5t 0.5t 0.61 1.46 2.51	73 1. BETA 0.0	Caf 3 -0-01+5	Em3	3m0F1 0	•0						
3	0.5t 0.5t 0.45 1.46 2.51	0.U 0.U	-0.01+0	ef.035				-	O FAE	E		
2 - 3 6 7	0.58 0.46 2.51	0.0	-0.01+0			ACPF3	YCPF3	CNF4	Cn4	CAA	XCPF4	YCPF4
6 7 6 9	1.46 2.51 . 3.51	2011@100010	-0 013-	-0.0031		C.1011	9.2237	-0.0061	0.0025	-0.0128		1.5744
6 7 6 9	2.51 . 3.51	0.0		.=0.132		9-1606			0-0011			0-1134
6 7 6 9	3.51	- U-V		-9.0032		0.1527 	0-1715		-0.0002 -0.0015		-0.0029 -0.0167	0.2844 0.3516
9 )		0.6	-3-071m	-"O35	-0.0737	6-1902	0.1795	0.1546	-0.4026	0.0565	-0.0161	0.3651
9 )	سددمك	-4-4				4-15/5	-1-1641		-0-0060		-0-02A1	0-3766
	9.47	0.0		-0.0044		0.1335 <del>0.1582</del>	0.1616		-0.0090		-0.0204 -0.0133	0.3490
10 1	19.16	U. U		-9.0041		6.1416	0.1157		-0.0065		-0.0110	0.3072
	20-2H.	-0-4-			-0-4432		0.0997		0-0131-			0.3063
	25.45	0 <b>.</b> u		-0.0350 -0.0352	-0.0024 -0.6643	0.1578	0.0761		-U-0156		-0.0163 -0.0215	0.2971 0.2963
(C)				<u>-</u>	<del></del>	<del></del>						
•												
				<del></del>		<del></del>	<del> </del>					
					i						<del></del>	
											<u> </u>	
				<del></del>					<del></del>	· · · · · · · · · · · · · · · · · · ·		<u> </u>
			· .									
	-											
							<del></del> -	·				
				<del></del>		-,,						

	-4										
GE	ENGINEE 1 OF 3	)	re Copașiei.	CENTENTA	€UC1P			L EFFECTS		AER	GDYNAMIC 4IND TUNNEL (41)
	1451		<u> </u>		CONF.		1 GEL 2	DEL3 DELA		Эн	
POINT	ALPHA	HETA	Cv =::-131a	CL	CY	CLN	CLL	CA	CAR	CAF	XCP =0-7093
2	-1-A2 -0-54	<u> </u>	-2-03-5	9-0145	-0.6193	6.06-57	-0-004	0.53 <del>05</del>	0-1790 0-1758	0.3614	-0.3045
-3-	1.45	0.0		-P. 2534			-0.0004	0.5366	U.1822		-1.8675 -1.4698
_ 5	2.50	4.0			-0.0111 				-C-1614 -		~lo4313
6	3.52	0.0		-6-2404			-0.0011	0.533H	6-1H-0		-1.+281
6	9.72	0.0		- <u>1.261</u>			-0-0013	0.5640	0.2126		-1.4949 -1.5083
	13.PS	4.0	2.07.15	-2,4554	Kenaa		-0.0009.	_4.506b	_u.2230	0.3439	-1-4264
10	19.24	0.0		-3.5752 -3.67x6	0.0163	7.00-0=	0.0007	0.5662 	0.2332 		-1.1750 -1.0056
12	24.24	0.0	5.2044	-3.40#1	0.0497	-6.0000	0.0045	P.5227	0.2697		-0.6821
11-	28-67	0-0	A-Coak	-335V	0-0602	-0-0-11	3-00-5	0.5100	6-2753	0-5365	-0.5624
									•		
						······································	<del></del>				· · · · · · · · · · · · · · · · · · ·
									·· ·· · · · · · · · · · · · · · · · ·	·····	
					<del></del>		· · · · · · · · · · · · · · · · · · ·				
											<del></del>
	<u> </u>										· · · · · · · · · · · · · · · · · · ·
			·					···	***		
									<del></del>		
									<del></del>		
					·	<del></del>					

GŁ .	ENGINEER 2 OF J 1 OF 1	ING LE	VELOPME .T	LENTERIA	(2)			HEL FACIL		AER	DINAMIC	IND TUNNEL (AT)
			ACH FRIGA									
	۷	74 1.	24 2.5	0.0 p.	3muF14 0	•0	0 0	0	O FAE	E		
01×T		SFTA	ChFI	C-1	CHI	ACPF1	YCPF 1	CNF2	CHP	CaS	xCPF2	YCPF2
<del></del>	-1.62 -0.59	<u> </u>	-0-035 -0-035	0. 110	0.002-		-0.7437 -1.6960	-0.0111	-0.0011	-0.027A -0.0126	0.1008	1.1359
3 .	-0.45	C.U		Saulie		-6-27ch		0.6259			_=0.1291	
4	1.45	6.0	-0.1934		0.001-	-4.26.1		0.0635	-0.0047	0.0149	-0.0739	0.2347
_5	2.50	4.2	-C-0:25	3.501.		-0.27=7			2-0-2055_		2.0514_	0.2805
6	1.52	6.0	-0-00-7	v.uu12		-0.27-4			-0.5060	0.0459	-0.0432	0.3077
		_يم	<u>=6-656)</u>	<u> Tariyy</u>	-0-0-42			0.2064		0-0791	-0-0325	0.3209
8	9.72	6.G	-0.002s	0-1915		-0.3	-2.7316 -3.1617		-0.0101	0.1365		0.3005
10	16.24	U.0	-0.04.15			-6.2779			-0-0108	0.2039	-0.0176 -0.0125	0.5665
ii	23.68	C-G	-0-3-14	5-001-		-0.7173			-0-0111		0-0137 _	4.2643
12	26.24	0.0	0.0051	J. CU11	0-0ua2	0.2175	1.6277		-G. Ulde		-0.0203	0.2689
	28.07	0.4	4-32-5	Jen 172	0.0715	0-09-7	0.9128	0.5274	-0.5227	SHAS	-0-0245	0.2675
•												
		<u> </u>	<del></del>	<del></del>						<u> </u>	<del></del>	
									···			

					<u> </u>						·,		= 200
	<u>, , , , , , , , , , , , , , , , , , , </u>												
								·					
S-OFD	ENGINEED	Alag ut	relo?ne al	CENTERIA	ELC) P	ROPULSION		IL EFFECT		AER	ODYNAMIC 1	IND TUNNEL (AT)	<del>-</del>
	1 06 1					787 77 77		IL CITCUI					
	7551	AAST #	ALP PELLS	4 047	COLE		051.7	0613 DEL	4 7044577	·			
	7		₹6 2.5		3×4614 0				O FRE				
POINT	ALPHA	4ET-	Ciof 3	En3	C+3	ACHF3	YCPF3	CNF4	CH4	C84	XCPF4	YCPF4	
<u> </u>	<u>alašė</u>	for the		-ti-127		1239	0-231A				-0-3193	0.5901	
3	-0.54	( _ U	-0-02HI	-6-6327	-L.0048	0.1314 	0.2227	-0.6242	0.0105 -0.0010_		-0.1074 -0.0312.	2.1933 	
4	1.45	0.0	-0.3711	-0.0000	-6.9058	0.1733	0.2751	0.694	-0.0025	0.0219	-0.0354	0-3158	
	3.52	_ <u>u_i_</u> _		<u>=007</u>		0-1431	3.2054_		-0-0038		-0.0346	0.3587	
6	5-55	6.0		-0.1035 -0.1131		0.1325	0.2244		-0.0046		-0.0300	0.3730	
ę	4.76	(				0.1340	0.2030		-0.0103		-0.0243	0.3461	
<u> </u>	13.89	Cak		<u> </u>		201565	0.2014				0.0206_	0.3193	
10	14.24	0.0		-6.00342		0.15:5	9-14m2		-0.0138		-0.0168	0.3112	
12	20.24	n. v		-9.605e		0.14.5 0.14.5	0.1452 0.0338		<u>-0.0108</u>		0 <u>-0180</u> -0-0180	0-3064 0-3035	
13_	24.47	0		-0.0051			-0-0070		-0-0202		=0-0223	0-3009	
							55						
			<del></del>				<del></del>						
			· · · · · · · · · · · · · · · · · · ·										
								•					
						<del></del>				<del></del>			
•													
			<del></del>									<del></del>	
								-					
<u> </u>												····	
							•						
					<del></del>						<del></del>		
							_				= -		
												<del></del>	

	ENGINEER	ILEG DE	AFT OBACTA	CENTERLA	Enc) P		LISTLE TA			REN	ODYMANIC MIND TUNNEL (AT)
1	1_0F1	· · · · · · · · · · · · · · · · · · ·									
	7667	PART N	M = PYID=		COLE		3 451.2		4 TRANSIII	OL	
	5	75 1.	3u 2.5		3=0+14 0		0 0		0 FHEE		
INT	ALPHA	BETA	C4	CL-	CY	CLM	CLL	C4	C48	CAF	ACP =1-7492
ż	⊕r.55	t.u	-C.UA71	0-175-	6.0 132	-0.1746	-9-9027	0.5059	U.1416	0.3273	-7.7649
<u> </u>	1.50	<u> </u>		<u>728_</u> (		-C-1347		0-5077			-0.2738
	2.52	<u></u>					-0-0030				=0.2738 ==0.6154
6	3.55	0.6		-0.3074	0.0414	-0-12-2	-0.0033	0.5000	0.1400	0.3207	-0.8475
7 8	9.76			-1.4567			-0-0016	0.5139 0.5357	G-2078		-1-0928 -1-1917
9	13.96			-20201-			2.0032				-101361
0	16.30	0.0	3.00/3	-2.7713	3-0176	0.24.3	-0.001+	0.5353	0.2294	0.3059	-0.9251
<u> </u>	24.36	0.0		-2-h3lo -3-6153			_ <del>=0.005</del> *. -0.0123	0.5284			0.7853 -0.5616
3	2A.1A	ن مان							0.2000		
									-		
											•
				<del></del>							
											<del></del>
							<del></del>				
				<del></del>					<del></del>		

		oleg ut	er Oper at	CEn1=+(a)	EuC)	PROFULSION	wind lum Issile ta			AER	ODYNAMIC	aind tunnel (ai	1
neel_	2 OF 3					444114 1	1221CE 14	IL EFFECT			•		
		<del></del>					·		<del> </del>			<del> </del>	
	<u>TEST</u> _		<u>acm 8110-</u> 30 2.5	L.O b	COME .		DEL2		A_THANSIT O FWE				
POINT	ALPHA	HETA	CNF1	C+1	Cel	1CPF1	YCPF1	C! F2	CH2	CAS	XCPF2	YCPFZ	
2	-0.55	0.0	0.0145	0.010.	U-C141	1.0226	3.9716	-0. ulal	0.0004	-0.0166	-0.0443		
	1.50	<u> </u>	0.011	<u>-0-00-0-</u> :660-3		0.0136	0.5443	D-C161- J-0514	-0.0015	0-0172	-0.0283	0.1403	
	2-52	0.0	4.0115	-4-404-	عطستا مش	-0-6347	<u> </u>	v_0693_	_=0.0021_	_0.6191	-0-0229	0.2130	
6	3.55	n.u	7.01vl	-1.0000	0.3675	-1-0775	0.7455	0.1305	-0.0732		-0.0247	0.2742	
- 7	9.76	0.0	C-011c	-0.000a	<u> </u>		1.2565	0.3917	-0.0070	0.1131	-0.0254	0.2687	
_ق_	13.40	_0.0_	0-9071	-60.00-		-6.0523	2-1068	4.5420	-0.60-7		-0.0086	0.2663	
10	18.36	0.0	-0.0177	-0.vel3	0.0052	0.0720	-9.7947	0.6742	-0.0001	0.1745	-0.0120	0.2647	
15	20.59 24.38	0.U	-0-11-4	0.6901 2-C31-	-0.009=		_ <del>0.1018</del> . 0.2433	0.8369	-0.0177	0.2167	-0.0219	0.2612 0.2660	
<u> </u>		المنا.	-0-3245	5-0314	-6.0075		0-0617	- C-8689	=0.0227	0.2359		0.2723	
		····	<del>,</del>								<del></del>	<del></del>	
		~											
		-											
_					<del></del>		<del></del>	<del></del>	<del></del>	<del></del>			
												<del></del>	
		<del></del>							<del></del>				
												·	
													<del></del>

									<del></del>			· · · · · · · · · · · · · · · · · · ·
									· · · · · · · · · · · · · · · · · · ·			
É	ENGINELS 1 OF 3	ING LE	AFF DBHE?*I	CFDIFKT	ENC) PE		ISSILE TAI			AER	ODYMANIC - INO TUNNEL	.443)
			ACM HILLE tu 2.5		CJAF Bouf21 0		. <u>1 -3612 - 1</u> 0 0		IRANSII FRE			
I~T	ALFHA	UFTA	CN =0-1144	CL=	CY	CL~	CLL	CA	CAR	CAF	ACP	
<u>.                                    </u>	=1.70 =7.45	0.0 0.0	-0.0171	1007751 -004201	-).ur44 -).ur44	0.0:15	-0-0011 -0-7003 -0-0021	0.2441 0.7445 0.2840	- 3-13 <u>41</u> 0-1331 - 0-1330-	0.1514	-1.0369 -1.5003 -0.5257	
	1.36	(r.0	0.1402	-0-1197	-0.0267 -0.0267	0.060	-0.0010 -0.0027	0.2825	0.1303	0.1521	-0.0538 -1.0095	
` !	3,44 	[ . C		-1-6163			<del>0.0010</del>	0.2968	0-1361	0-1506	-1-1309 1-1726	·
8 <u>u</u> ú	7.66 -13.74 17.96	( . () ( . ()	1.3715	-1.00+1 -1.158- -1.18+1		0-0973 6-0971	0.0024	0.3315 0.3526 0.3574	0.1763 <u>- C.2163</u> - C.2767	-0-1343	-1.0789 -0.8458 -0.5362	· · · ·
<u>1</u>	20-61		2.1635	-1-1175 -0-5669	-0.0052					-0.0508	-0-5213 -0-2268	<del></del>
<u>.                                    </u>	27.76	··· C		-6-757		0-0-22	0.0098	<u>3871</u>	.0.EA.0.		=0-2262	<del></del>
	,	· · · · · ·	·		•						10	
		· · · · ·					· · · · · · · · · · · · · · · · · · ·				•	
						<del> </del>	·					
									,- <u>.</u>		· · · · · · · · · · · · · · · · · · ·	
											··	
		<del></del>			-				<u> </u>		<del></del>	
									-			
				<del></del>						<del></del>	<del></del>	
											····	

E .	3 OF 3		VEL GEME. I	CEMILMIA	EuC) et	ROPULSIGN	•150 film	WEL FACIL	ITY(PWT)	AFRIC	DYNAHIC 4	IND TUNNEL (AT)
	1 OF 1						ISSILE TA					13. 10. WALL   12.2
								,		-		
	IEST	PART =	Aŭn Phi	- 2al -	CUME	1 1151	1 DEL 2	DEL 3 DEL	4 IRANSIT	ION		
•	3		ev 2.5		3-6+21 0.		0 0	0	0 FRE			
INT	ALPHA	FETA	CNF3	Cn3	Сез	ACPF 3	YCPF3	CNF4	CH4	C64	XCPF4	YCPF4
	-0.65	0.U	-c.56.2-	-r.0124	ecounts.	1.6043	0.4248 0.4857	-0.0314	-0.0033	-0.0403 -0.0061	0.1039	0-4974 0-1926
	0.34			-C-407-		L_425b_				0.0061 0.069	0.6861	0.4433
,	1.35	0.0	-0.0256	-6.0110	-0.0105	C.5350	0.5073	0-0741	0.0312	0.0316	0.4215	0.4272
	2.38	_ <u>0_u</u> _							0.0514			-0.4263
,	3.44 5.47	ن من سندان	-0.(216	-0.011.4		0.5157 0.5572	0.5834	2015-0	0-0479	0.0931 0.1472	0.3232	0.4431
	7.50	Ú . U		-0504		C.53( 9	0.2751	0.5387	2000.0	0.2431	0.1784	0.4511
<u></u>	13.75	لامَال	<u>-6-3-4-</u>		0.0145_	u_3834	c_25a		0.0735.	0.2647	_0-1155 _	0.4161
•	17.96	0.0			-0.0095	0.5734	9152.0	0.7364	0-0A37	0.3011	0.1137	0.4089
 s	25.44	<u> </u>		-0-0237			0.0964	<u> </u>	0_187 _			_ 0.4 <u>212</u>
2	21.74	0.4		-0-0237 -0-0212		0.5071	0.0954	0.7637	0.0775	0.3199 0.3396	0-1015	0.4189
						•						
			·		<del></del>		<del></del>	<del></del>	<del></del>			<del></del>
										<del></del> -	· <u> </u>	
					<del></del>		<del></del>					
			<del></del>				<del></del>	<del></del>	<del></del>			<del></del>
	<del></del>		~~				<del></del>		<del></del>			

r E	ENGINEF! 2 OF 3 1 OF 1		vel upre "T	CENTENT	NEUC) P		ATHU TUN ISSILE TA			AERO	DYMARIC .	LND TUNNEL (47)
									A THANSIT			
POINT	2 ALPHA	EFTA.	(\F1	Cnl	+3=uf21 0	xCPF 1	YCPF1	0 C .F2	O FRE	Ces.	XCPF2	YCPF Z
<u> </u>	-1.71	C.L.				0.5248			-C-u225		0-4442	0.4016
2	-0.57	6.0	-0.0074		-3-4235	F.44.4	2.9455	-0.0033	-0.0024	-0.0123	0.8300	3.4446
<u> </u>	0-36	_c_o_			خلليا مناحب						-0.3824	-0-0426
-	1.30	G.U	-0.00.55			6.3505	-1.3363	0-1113	0.0376	\$360.0 	0.3375	0.2712
6	3,44	6.0		-1 3366		U-50c3	-1.0017	0.2647	0.0799	0.0544	0.3018	0.3160
7_	5.46	4.4					-0.3706	0.3543	4-1073	-0-1433	C-2791	0.3729
•	4.54	0.0	-0-2001			0.4456	-1.5239	0.5417	0.1974	0.2196	0-1947	0.3775
9	13.76	0	-0-0154		-0-06-6		<u> </u>	0.6953	2-0773		0.1112 ·	0-3697
10	17.97 20.14	0.0			-6.9167 -6.222	0.4573	0.6454 .0.8920	0.7994	0.0777	0.2936 0.3108_	0.0972 0.0530_	0.3673 0.3864
15	25.57	0.7	-0.0017			-1-1167	0.6670	0.7475	3.0651	1.3100	0.0816	0.3960
13	27.84	6.1			جهينه .		-0-20bs	0-6633	0-6623	0.3423	0.0722	7.3967
											•	

GE	ENGINEFI 3 OF 3 1 DF 1	PING DE	SEL OPHEST	CENTERIA	EDC) PI	MARTIN PI	SSILE TA	MEL FACIL	LTY.(PMT) S DATA	AERO		IND TUNNEL (AT)	
	TES1		ALE EALO-		CONF 0				A IRANSIT				
DINT	ALPHA	HETA	CNF3	CH3	C43	7CPF3	YCPF3	CnF4	CH4	C84	XCPF4	YCPF4	
1	-1-70	E-9	=0.0231	-6-1171		0.7391	C-5436	FORG-0-	-0-0323	_	. 0.4020	0.5190	
2	-0.67	0.0	-0.07->	-6.6160	-6.011=	P-6697	0.4757	-0.6312	-0.0065	-0.0045	9.2080	0.2938	
4	0.30	<u>U. li</u>	-2-2214	<u>-6.66122</u>	<u></u>		_C-7176_	0-0187	-6-0045		0.5080	0.2734	
•	1.38	6.0	-0.0271	-0.0180	-0.0126	0.6643	0.4673	\$040.0	£.0353	0.0268	0.4399	0.3591	
<u> </u>	<del></del>	0.0	-0-02	-0-0-00 -0-0103	<u>-6.0120</u> -0.0137	0.7125 0.6701	_0.4147_ 0.5565	<u>0-1366</u> J.2145	<u> </u>	0.059Z	0.3843 0.3457	0.4269	
7	5.46	5.5		-0-0103 -0-019/		0.6552	1.4458	0.3406	2-1052	0.000	0-3096	0.4299	
ь	9.59	0.0	-0.0414		-0.01-1	0.5360	0.3414	0.5344	(.1035	0.23.9	0.1937	0.4395	
9	13.75	O.v		-0-5211		<u> </u>	0.3366	0.6569.	. <u>. Cau</u> Z31	0.2740	9-1113	D-4171	
0	17.97	0.0		-0.6254		0.5756	0.3035	0.7627	0.0429	0.3116	0.1087	0.4986	
13	25.57	<u>0.</u> u		-0-Je45		0.543R 0.6075	0.0880	0_7642_ 0.7905	0.0825	<u>0.3305</u> 0.3210	0.097 <u>5</u> 0.1044	0.4066	
12 13	27.84	0.0			-0.0/43 -0.0.53	6.5057_	0.0000	0.7905 0.6505		0.3510	0.0916	0.4127	
_													
-						<u>-</u> ,		<del></del>					
						<u> </u>			·		•		
	- <u>,</u>		<del>,</del>		<u>.                                    </u>			<del></del>					
								-				<u> </u>	
												<del></del>	

						<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>	<del></del>		······································	······································			
	<del>,</del>	-	·										
PAGE	1 OF 3		DEL OPPENT	CEDTERIA	EDC) P			MEL FACILI		AER	ODYNAMIC «IN	D TUNNEL (AT)	
SHEET	1 OF . 1						Au 14 au 17 au			···			
		<del></del>		<u> </u>			·	<u> </u>		<del></del>	<del></del>		
			94 2.5		3m0F21 0		DEL2	DEL3 DELA			<del></del>		
POINT	ALPHA	BETA	CN	CL+	CY	CL4	CLL	CA	CAR	CAF	xce		
	-1.74	Call	-C-10at	Sev [3)	enenée7	0.0576	-2-00-7	0.3274	6-1362	0-1863	-0-6991		
2	-0.59 6.36	6.U		0.0417 G.U605			-0.0u31 -2.0021	0.3255 0.3240	0-1366		-1.2745 -0.0120		
4	1.37	0.0	0-12-7	-6.6725	-0.02.7		-0.0005	0.3737	C-1355		-0.5638		
<del> }</del>	3.43	U. 0		-0.3554			-0-0052 -0-0054	0.3249			-0.9541		
"	5.44	_		-0.2724			-0-0051		0.1391		-1-1455		
e	9.62			-1.1632			0.0011	4466.0	0.2071		-1-0717		
10	15.03	<u> </u>		-1-5061			-0.0003	460400 26240	0.3345		-0-7447		
_11_	20.17	0.0	2,3145	-laisyr	0.0012	0.0723	-0-0029	U. 4249		0.0358	-0-6050		<del></del>
13	25.67 23.06	-		-0.0475	0.0040 eú.6141		-0.0017	0.4644	0.4118		-0.2154		
											<del></del> -		
				<del></del>				<u> </u>		<del></del> .			
									•	٠.			
								-	_			<del></del>	
		<del></del>	<del></del>										
											-		
											<del></del>	· <del></del>	<del> </del>
						·							
							<del></del>					<del></del>	<del></del>
		<del></del>		<del></del>					<del></del>		<del></del>	<del></del>	
	· · · · · ·										···		
								-					
<del></del>			<del></del>									<del> </del>	
_													
			· · · · · · · · · · · · · · · · · · ·								······································		
	<u>-</u> -												

252

	•		• •	<del>-</del> ·							_		
		,							, .				
			···										
				==		4-1							
AGE AGE	J OF 3	PING YE	VELOPELLI	<u>realtara</u>		<del>lupulsium</del> Partin mi	SSILE TA	<u>NEL FACIL</u> IL EFFECT	TTY (PaT)	AFRO	MYNAMIC.	IND TUNNEL (ATT	
	1 OF 1				<u> </u>		×						
						· · · · · · · · · · · · · · · · · · ·			<del></del>		·		
	TEST	-10T	4C- 611-	6 enl	CUNE	. TOFA 1	0F1 2	0F1 3 0F1	A TRANSTT	IOM			
	. 2	.62 0.	52 2.5	О.О н	3.0F21 0.	0	0		O FRE				
TATO	ALPHA		CNF 3	Cri3	C#3	xC+F3	YCPF3	CNF4	CH4	CR4	*CPF4	YCPF4	
<del></del>	-1.7L	-		-n-u211	-C-01-7		0.4795		-0.039A -0.0040	-0.00A0	0.5479	0.5449	
3	0.30			-inulia			0.7144		-0.0109	0.0038	0.3297 _0.673e_	0.2335	
4	1.37	.0.0	-0.0215	-0.0160	-9.0153	0.7410	0.7100	0.0667	0.0389	0.0253	0.5666	0.3677	
5		<u>u_u</u>			<u>-0.0147</u>		0.6302		0.0651_		_0.4915		
6	3,43 5,49	0.u		-6.0163	-0.0147 -0.0136	0.6214	0.7704 	0.2047	0.9894 -0.1200	0.0844		0.4026	
8		- Ú - V		-1-1277		v.51/5	0.4257		6-1317	0.2365		0.4500	_
<u> </u>	13.41	n_u			-u-ulv:		0.6392			0.2943.			
10	14.03			-0-055+		0.5707	0.3231	0.6392	0.0933	0.3424	0.0992	0.4080	
15	20.17 25.67					0.6095	0.1617	0.8650	0-0726 0-0756	0.3519	0.0874		
13	26.40			-6.0305		0.80V5	6-11GA	0.6650		0.3579			
													-
											<u>.                                    </u>	<u></u>	
			<del></del>					,					
										····			
								<del> </del>					
		-	·									•	
	. <del></del>								<del></del>			<del></del>	
				<del></del>							<del>-,</del>	<del></del>	
											·		
			<del></del>		<del></del>			<del></del>			·		
				<del></del>						· <del></del>	· · · · · · · · · · · · · · · · · · ·	E 20	

				<u> </u>		<u> </u>						· · · · · · · · · · · · · · · · · · ·
				"		<u> </u>						
							·		***************************************			· · · · · · · · · · · · · · · · · · ·
NOL LI	ENGTHER 9	ING HE	VEL OPHENI	CENTERIA	FOCI P	HOPULSION	NUT UNI	NEL FACIL	IIY(P#T)	AFRO	DOYMANIC	INO TUNNEL (AT)
GE	2 OF 3						ISSILE TA			3.53400		
	<del></del>				·····				·····			
	1551	JAC 7 H	ACH PILL-	4 . Aut	CLINE		. 061.9	0513 051	6_IRANSII	T.04.	<del></del> -	
	5		A0 5.2		3-01-21 0		0 0	0	0 FRE		<del>*************************************</del>	<u> </u>
DINT	ALPHA	af Ta	CAF1	Cnl	C+1	ACPF1	YCPF1	CHF2	CHS	CB?	xCPF2	YCPFE
2	-0.01	0.0		-0.3674 -0.3674	-0.017n	0.36.5 0.1637	1.0103	-0-6121	-0.021h	-0.0218	0.0659	1.7996
<u> </u>	0.37	6-3	-CaGllu	0.0012	0.0002	_20.10.9.	0.3781		6.0235		_0.30A2	0.0768
•	1.30	0.0		-6.6054	0.0630	0.3269	-3-1941	0.1358	J.0376	0.0391	0.2690	0.2797
5	2.42	0.0		-0-1140		0.2556		<u> </u>	0_U589		0.2520_	
7	3.46	0.0		-0.0042	0.0123	0.2143	-1-5258	0.32H0	0.0790	0.1029	0.2408	0.3138
8	9.65	0.0			0.0107	6.9136	-0.5416	0.6932	0.1308	0-2009	C.1944	0.3850
5	13.62	0.0	-2.0350	-0-0057	116041= .	0.1639	0.2233		0.4951	0.3133	0.1161	0.3824
16	18.09	6.0		-0.0057		0.2053	0.2623	0.9692	0.0721	1.3743	9.0729	0.3784
ц	20.26	<u> </u>		<u></u>		u-1842_		1.0652	0.3669_		_0.062#_	0.3864
12	25.09 26.17	0.0		-0-0034	E010-0-	0.1270	-0.3783 2.2198	1-0767	0.0532	0.4728	0.0494	0.3927
			- 11 - 11 - 11 - 11		MANUARY							
				<u> </u>								<u></u>
							··			<del></del>		
								-				
												·····
	<del>.</del>											
					<u>.</u>							
				<del></del>								
							<del></del>			<del> </del>	<del> </del>	
												•
							·					
						•						<del></del>
							· - · - · · · · · · · ·	<del></del>	····			
<u>`</u>											······	· · · · · · · · · · · · · · · · · · ·
						-						

MARTI . MISSILE TAIL EFFECTS DATA

PAGE

4 06 3

SHEET 1 OF 1

·E 1	G1Ei F   UF 3   OF 1	PING DE	elők4 si	LESTERIA	EDC) Pi	<u> </u>	ISSILE TA	EL FACIN	LTY(PYI)	AE.6	COVERTIC STAND THREE STANDS
	TEST.		ALH #X10=		CUNE		1. DEL21		TRANSITI D FHEI		
PINT	ALUMA	mETA	(^	CL"	CY	CLM	CLL	C.	ĊĀĐ	CAF	кср
2	-1-71	<u> </u>	-G-1401	# <u>#7647</u>	<del>-1-0355</del> -0-0335	0-10:0	-0.010a-0-	0.5729 0.5716	1975-0	0.3639 0.3651	-1.5786
3	0.37	_Uau			0331			0.5729	0-5101		=1.6185
•	1.36	U. U	nolelu	-0.3067	-0.1337	0.1034	-0.0115	0.5720	0.2157	0.3564	-1.6951
<u> </u>	<del>2.18</del>		<u> </u>		-0-0122		<u>-0.0113</u>	45743			*1.7235
7	3.43 5.51	() . J	7564.0	-1-:171	-9.0293 -4.4367		-0.0107	0.5712 C.5804	0.2236		-1.6985
F	4.25	C. v	1.1275	-1.5072			-4.0109	0-6011	2.2579		-1.4073
<u>.</u>	13.51	C.0_		-1.4541			-0.0040	0.6126	6.2994		-0.9113
10	14.25	0.0		-1.3359			-0.0151	0.6121	0.3597		-0.5698
ц	20.55			_= <u>1.159%</u>			-4-0074	3.5976_	<del></del>		-0.4171
17	27.2t	0.9 —0.4	4-1270	_	0.0053		-0.0030	0.5721 0.5598	0.3621		-0.1132
								. ———			<del></del>
										*****	
									<u> </u>		
										<del></del>	
				,	•						
											<del></del>
				<u></u>				<del></del>			

	FAIGIALLE	TAG	Vel Doerer	Chateura	*((C) Pi	DOW SION	alab fue	MEL FACTIT	TV/DUTL	150	ODYNAMIC	MIND TUNNEL (AT)
	3 OF 3	LASIS . DE	II CIN-15-91	·				IL EFFECTS		<u></u>	OD: MANAGE.	
	· · · · · ·							•				
	TEST	PAPT E	ach sale	e EMI -	CONF	L GFL 1	L_::FI 2	DEL3 DELA	IRANSII:	tow		
	2		10 2.5		3.0f21 0		0	0 0				
T	ALPHA	dETA	Cnf 3	C=3	C+3	ACPF 3	YCPF 3	CNF4	CH4	C64	KCPF4	YCPF4
	-0.00	4.0	-0.04-1	-U - v 2 tt C		0.6363	0-235¢	-0.0404	-3-06/A 0-0152	-0.0728	-0.3724	0.7205
	2.37			-Coue:32		C. 5a.u _	6-2674		\$-0284_	-0-0035	0.6436.	-0-0781
	1.76 2.36	6 - D		0.0240 £11£1-0-		0.6096 	9-1337	J.122× <del>1813-</del> -	0.0426 0.0364	0.0305 0.0621	0.3474	0.2483 
	3.43	0.0		-0.6283		r.63e2	J.1305	V.2664	0.0510	0.1065	0.1780	0.3718
_	5.51	4-4				C-6535	1516	-0.AZ65	0.0690	0.1833	0-1461	0.3644
	13.91	0.0		-0-0234		0.63-0 0.5223	0-1957 	6.7773	0.0410	0.3164	0.1042	0.4096
	14.25	(° . u		-4-2-1		0.5151	101750	1.0253	6.0519	0.4734	0.0796	0.4116
	20.55	0.0	-6-15+7	-# C2H1	-0.0076.		1-1276		0.0567		0.0667	0-4197
	24.24 28.74	0.0		-0.(335		6.6606	0-16-6	1-2357	0.0596	0.5103	2640.0	0.4130
_	78.14		-11-11777	-Finale	e li diii lik	u_biv5	0.0676	1-2755	0.0569	0.5265	0.0444	_0_4127
				· · · · · · · · · · · · · · · · · · ·								
_												
					<del></del>							
-												
						•						
					•							
							<del></del>					
_												
							•					
							<del></del>					<del></del>

. . . .

										•		•	
<del></del>	· <u>·</u>	_ <del></del>			~								
							····	<del></del>				<del></del>	
بالمناه	ENGINEE	PING LE		CENTERIA	Euc)2					AFRO	DYNA-IC.	HIND TUNNEL (AT)	·
	2 OF 3	-				M . ITHAM	ISSILE TA	IL EFFECTS	DATA				
									<del>, , , , , , , , , , , , , , , , , , , </del>				<del></del>
								DEL3 DELA					
			iev 2.5	4.0 6	3+0F21 0		0 0	0 0	FRE	<b>.</b> 			
POINT	ALPHA =1.71	BFTA.	C4F 1 -0-11 72	Crl	Cel	ECPF1	YCPF1	CNF2 -0-6765	CHS	Ces	XCPF2	YCPF2	
2	-0.56	0.0			-0.013>		0.6965	0.4040	0.0014	-U.U061		-1.0130	
	<u>35</u>		-6.:121				-0-2169	2.0972			0.2037_	_0-1931	<del></del>
	1.36 2.36	0.0	-0.0179		-0.0677 6-0531.		0.4303 0.1060	0.1746	0.0281	0.0527 	0.1611	0.3016	
•	3.43	6.0	-0-0148		-0.0030		0.1610	0.3422	0.0460	0.1144	0.1344	0.3343	
6	5.50 9.71	0.0	<u>=:.&lt;0.0=</u> ==================================		-v.0ú35	-6-1643	0.1347	0.4452 0.7966	0.0515	0.2946	0.0048	0.3698	
9	13.45		<u></u>	الإستانات	حلالمنا ملتج		0.6320_	_1.4110	_0_0803_	0+3925	0.0793	_0.3880	
16 11	14.41 23.74	0.0		-0.0024 -0.003c		0.0350 -6.0567	0.4465 0.513G_	1.0551	0-0725 _0-0660_	0.4090 	0.0687	0.3877	
15	26.60	C-U	-0.cn-y			-0.0242	0.3461	1.2430	0.0557	0.5070	0.0434	0.3952	
13_		(-3	<u>-c/-5</u>	-haudec	-0.6361	<u> </u>	0.4034	1-3345	4-4524		_0.0393	0.3040	
					<u> </u>						<u> </u>		
									·			· · · · · ·	
					<del></del>							······································	
			_										
					•								
	<u>.</u>					- <del></del>							
										<del></del>			
					<del></del>	<del></del>							
						<del></del>						<del> </del>	

क्रमान्यकार व्यवस्थात । स्वर्धान विकास स्वर्धान । स्वर्धान विकास स्वर्धान । स्वर्धान । स्वर्धान । स्वर्धान । स

. Als en la la surrigio contro como en como esta en la como en la c

-1.71 0.2 -0.132x 7.165x C.6164 -0.65x7 -0.0120 U.5069 0.16x7 0.3382 -1.3380 -0.68 0.0 -0.643x 7.2947 C.0171 -0.070 -0.0117 0.5045 U.1679 0.3365 -2.1589 0.35 0.0 0.365x 4.0549 0.6160 -0.0524 -0.0108 0.5043 0.1676 0.3365 0.1020 1.40 0.0 0.1649 -0.1000 0.0146 -0.0552 -0.0105 0.5051 0.1724 0.3327 -0.6806 2.43 0.0 0.2513 -0.295  0.0167 -0.0674 -0.0113 0.5051 0.1766 0.3265 -0.7550 3.47 0.0 (.3471 -0.2847 0.0167 -0.0544 -0.0113 0.5051 0.1766 0.3265 -0.6259 5.55 0.0 0.55x1 -0.2847 0.0114 -0.0599 -0.0115 0.5043 0.1782 0.3260 -0.6259 5.55 0.0 0.55x1 -0.435x 0.010x -0.036x -0.0104 0.5231 0.1863 0.3264 -0.7994 9.75 0.0 1.67x1 -0.7279 0.6014 0.0009 -0.0073 0.5492 0.2068 0.3424 -0.7095 14.07 0.0 1.65xx -0.0517 -0.0014 0.0004 -0.0073 0.5492 0.2068 0.3424 -0.7095 14.07 0.0 1.55xx -0.0517 -0.0026 0.0046 -0.0115 0.5666 0.2345 0.3121 -0.2824 20.80 0.0 2.5327 -0.7152 -0.0026 0.0669 -0.0115 0.5666 0.2355 0.3121 -0.2824		. 05		Tr. 4= 40 1 2.	CENTERLA	EUC)	PROPULSIA	M MINO TUN	WEL FACILI	TATA TIT	AER	ODYNAMIC MIND TUNNEL (AT)
TEST PART MICH RIDGE PRI CONF L UELL DELZ DELS DELS TRANSITION  2 8h 1-30 2-5							MAINAM	W1221FE 11	IL EFFECIS	UAI4		
2							<del>-</del>					
1 -1.71 0.2 -0.112							0 • 0					
2 -0.68	THIO			- ·						•		
1 1.4	2	-0.6P	0.0	-0.1434	100447	0-0171	-0.05/0	-0.0117	0.5045	0.1679	0.3365	-2.1589
5 2.43 6.0 0.2513												
9 3.47 0.0 (.347) -0.2ee7 (.015) -0.0599 -0.0115 0.5043 0.1782 0.3260 -0.8259 7 5.55 0.0 0.5mm; -0.4100 0.4100 -0.4346 -0.5231 0.1663 0.3368 -0.7994 8 9.15 (.0 1.02n) -0.7779 0.004 0.0099 -0.0073 0.5492 0.2060 0.3244 -0.7095 9 14.07 (.0 1.45mm -0.4617 -0.4036 0.0368 -0.0092 0.5513 0.2218 0.3295 -0.5284 10 18.55 0.0 2.5327 -0.7152 -0.0026 0.0409 -0.0115 0.5066 0.2365 0.3121 -0.2226 11 20.40 0.0 3.6muz -0.252 -0.0020 0.0997 0.0006 0.5525 0.2464 0.3061 -8.1388 12 26.80 0.0 4324 -0.277 0.2150 -0.0159 0.5596 0.2797 0.2799 -0.0016 13 29.31 0.0 5.6316 -0.0159 -0.0155 0.5757 0.2963 0.2794 -0.0737	<u>.</u>											
8 9.75 (.0 1.07-1 -C.777 0.0014 0.0029 -0.0073 0.5492 0.2068 0.3424 -0.7095 9 14.07 (.0 1.650h -C.5517 -0.0036 0.0344 -0.0092 0.5513 0.2218 0.3295 -0.5284 10 18.55 0.0 2.5327 -0.7152 -0.0026 0.0040 -0.0115 0.5466 0.2345 0.3121 -0.2826 11 24.60 0.0 3.6402 -0.6252 -0.0030 0.0977 0.0006 0.5525 0.2464 0.3061 -8.1380 12 25.80 0.0 4324 -0.6276 -0.0297 0.2150 -0.0159 0.5596 0.2797 0.2799 -0.0016 13 29.31 0.0 5.6316 -0.0150 -0.0395 0.2797 0.2794 -0.0737	6	3.47		1.3671	-0.2Fe7	0.0151	-0.0579	-0.0115	0.5043	0.1782	0.3260	-0.8259
9 18-07 CaV 1-53m -Cab17 -0.0036 0-03n6 -0.0092 0-5513 0-2218 0-3295 -0.5284 10 18-55 0-0 2-5327 -0.7152 -0.0026 0-069 -0.0115 0-566 0-2365 0-3121 -0.2824 11 20-60 0-0 3-6502 -0.0252 -0.0060 0-0927 0-0006 0-5525 0-2666 0-3063 -8-1380 12 26-80 0-0 4-324 -0.0252 -0.0252 0-2150 -0.0159 0-5596 0-2797 0-2799 -0.0616 13 29-31 0-0 5-6316 -0.0152 -0.0395 0-2364 -0.0155 0-5757 0-2963 0-2794 -0.0737	7											
11 20-00 0.0 3.6402 -0.4252 -0.0020 0.4977 0.0006 0.5525 0.2464 0.3061 -8.1380 12 26.80 0.0 4324 -0.2976 -0.0297 0.2150 -0.0159 0.5596 0.2797 0.2749 -0.0016 13 29.31 0.0 5.6316 -6.0134 -0.0145 0.2344 -0.0155 0.5757 0.2963 0.2794 -0.0737	_											
12 26.80 0.0 4320.2976 -0.0297 0.2150 -0.0159 0.5596 0.2797 0.2749 -0.0616 13 29.31												
13 29-31 D-U 5-6-16 =017/ =0-0395 U-23-A =0-0155 0.5757 U-2963 0-279A =0-0737												
			<del></del>									
									-			
	<del></del>			<del></del>		<del></del>			<u>.</u>			
								_				
								<del></del>				
			•						-			
		<del></del>			· · · · · · · · · · · · · · · · · · ·							
				· · · · · · · · · · · · · · · · · · ·		<del></del>						

	ENGINEES 2 OF 3 1 OF 1	ILG LE	SELOPAENT	CENTERIA	EUC)P			NEL FACILI		AEH	GLYNARIC_I	INO TUNNEL (A	
	TEST.		ALM RAIL-6				DEL2	DEL3 DELA					
INT		META	C/F1	CHI	Cul	*CPF)	YCPF1	CHES	CHS	. C95	KCPF2	YCPF2	<del></del>
5	-1.71 -0.68	1 . U	<u> </u>	0-005+	1500 au	0.6252	J.9173	-0.0054	0.0017	-0.0500	-0.3221	<del>- 0.6248</del> 3.9167	
3	2.35	Uall	0.619c	_1_11	ڪويئےيا.	0-2113	- 0-3155	-0-3645	_0-C125_	C. DOZA	0.1943	0-0378	<del></del>
4	1.40	(, _e t _e	0.0047	0.1043	J. 0395	0.8400	1.9160	0.1364	0.0209	0.0329	0.1533	0.2409	
<del></del>	3.47	( , U	2.0000	0.0035 0.0073	<del></del>	1.6215 3.30e7	3.4568	0.2949	_0.0353 0.0353	0.067A 0.0907	0.1065 0.1198	0.3074	
<u>i</u> _	5.55	6.0	.+0-0055	Course	40.01	-1-11-9	-4-3782		0.3372	0.1513	0.0856	0.3473	
6	4.75	6.4	-0.000	0.0907		-1.7753		0.7043	0.0509	0.2556	0.0723	0.3629	
<u>9</u>	18.55	<u>UU</u> G_0_U	-0.0170 -0.0100			26.5671	0.7163	0 <u>.9241</u> 1.1035	0.0741	0.4366	0.0613. 0.0672	0.3958	
<u> </u>		0.6				-0-1215				-0-4345	0.0567	0.3956	
15	24.70	C. U	-4.0130		-6.0275		0.3773		0.0463	0.5216	0.0357	0.4028	Siz Wi
13	54-31	Let		-0-1350	43-5	C-6543	0.3763	1.3635	0-0444	0.55CA	-0.0326	0.4040	
											<u> </u>		
	<del></del>		· · · · · · · · · · · · · · · · · · ·					,					
							illi						
									<del></del> -				
												<del></del>	
						· · · · · · · · · · · · · · · · · · ·							
						_							
				<u> </u>	<del></del>								
						··							

		· <del>-</del>				-						
									· · · · · · · · · · · · · · · · · · ·			
				<del></del>	<del></del>	•						
بما	ENGIALL OF 3	PING LE	<u> </u>	LENIERLA	EuC) PR	COPULSION	ISSILE TA	NEL FACIL	ITY (PAT)	AER	ODYNAMIC	IND TUNNEL (AT)
I	1_0F_1										<del></del>	
												·
—			<u> AL- BIll-</u> Ju 2.5	9-0 F			) OFL2		A IRANSIT			
NY.	ALPHA	PF TA	CNF 3	CH3	Cv3	*CPF3	YCPF3	Č~F ◆	CHA	C84	XCPF4	YCPF4
	-1.71		-5-5177	-44/201		1.31/6	e0.2245	_ev-1167_		-0-0074		0.5770
	-0-50	4.0		-9-9305	0.0166	1.4537	-0.3108	-0.0467	0.0106	-0.0279	-0.2179	0.5739
	1.46	0.U		-0.(26)	0.0055	<del>1.5200</del> . 1.4601	-0.3021 -0.3024	<u>6.3301</u> 0.1123	6.0153_ 0.0290	0.005k_ 0.0263	<del>0.5081</del> _ 0.2584	
	2.43	- C-G			0.0055		-0-2449			0.0574		0.2301
	1.47	6.0	-0.01-0	-0-4257	0.0061	1.7020	-0.7823	0.7657	U-0374	0.0636	0.1425	0-3155
	5-55			-0-120-			-u-1754	0-3476	<u> </u>	4-1438		0-3617
,	9.75 -14.07	0-0		-0.033a	-0.01.64 -0.0647	1.0129	0.0114	0.4657	0.0522 0.0624	0.7641 0.3666_	0-0762	0.3962
,	19.55	0.0				0.8127	0.1023	1.0490	0.0797	9.4563	0.0760	0.4293
	20.46	0.0	-G-0374	-2-2335	0-0001	<u> </u>	-0.0029	101059	o-nela-	0. 4676		0.4402
?	26.60	0.0			-3.0302	0.5457	0.0050	1.2404	0.0522	0.5412	0.0421	0.4363
	29.31		<u>=0.0000</u>	-0-030-	2.0415	3-6217	-0-0339		0.0496	0.5600	0.0381	
										,	4	•
								,				
									<del></del>			
			•									
						<del></del>			<del></del>	<del></del>		
												•
								· · · · · · · · · · · · · · · · · · ·				<del></del>
											····	
										-		
			<del></del>					<del></del>	<del></del>			
								<del></del>				
									•			
				<del></del> -	<del></del>		<del></del>					
						<del></del>		<del></del> -		<del></del>		
	-							···				

bŁ	ENGINEER 2 OF 3 1 OF 1	LING DE	ELGPSE: T									
					EuC) PI		LAIND TUN ISSILE TA			AER	ODYNAHIC.	IND TURNEL (AT)
·	TESI				CUNF			DEL3 DEL				
	2	91 6-6	u 2.5	0.0 b	3-0f36 0.	• 0	a o	0	0 FRE	€ .		
OINT		bF.Ta	CHF1	C+1	CRI	*CFF1	YCPFI	CNF2	CHS	CBS	XCPF2	YCPF2
2	-1.41 -0.36	<u> </u>	0.0034		-0.63ve	0.62-2	-1.2615 -0.1436	-0-02-5			0.0767	0.3436
3	£642	0.4	מבונים.	Carthia	-6-0036	0-4631	-0-6109	0-G166.	-0.0006.	0.0055_	0_0367	. 0.3283
<b>4</b>	2.66	0.0	0.0059		-0.0050	0.0630	-0.8447	0.03el	-0.0010	0.0146	-0.0263	0.3632
-3	3.60	0.0	0.0020		-0.0605		-0-661A	0.0925	-0.0013.	0.0327	-0.0209	0.3529 0.3649
<u>i</u> _	-5-50_	4.4	0.0020	9-1441	-6-0:03	C-2542	-ii.1527	1-1577	-L-0015	0.0515	-0-6095	0.3262
6	9.71	0 <b>. u</b>	0.Julr 0.4452		-0.00cul		-0.0938 -0.5563	0.3025	0.0016	0.0837	0.0053	0.2762
10	17.57	U. J	0.1076		-0.0134		-0.3763	0.5666		0.1330	0.0219	0.2347
<b>1</b>	19.90	0.0	0.6153	0.0025	20.0150_	0.1550	_+u-3779	0-5178	-0.0164	0-1406	0.4265	0.2275
12	25.43 27.21	0.0	0.007=		-0-0046 -0-0055		-0-6260	U-7376	0.0252	0.1570	0.0341	0.2129
ш		<u> IIaii                                 </u>	- HOUL	<u> </u>		CCALLIAN.		_ 4-5032	0.0237	0.1706	<u> </u>	0-2124
			···	<del></del>				<del></del>		·····		
	,									B 200		
							<u>.</u>					
												<del></del>
		<del></del>										
					<del></del>							
										_		
						•				•		
			<del></del>									
								· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			
						•						
						····	•					
										•		

	OF 1			- LUIER (A	EUC1P		ISSILE TAI			AER	COYNAMIC. AIND TURNEL LA
	TEST .	PART "	AL: 9116-				I DELZ	DEL3_DEL4	L TRANSILL	ON	
	5	97 U.	to 2.5	3.0 4	3+0+35 0	•0	0 0	0 (	FHEE	•	
NT	ALDHA	EFTA	Cv	CLM	CY	CL*	CLL	CA	CAR	CAF	ACP
	-1.41 -0.34	6.0	-0.1246	-0.0396	-0-0204 3-06u7	-0.0477	-0.0020 -0.0026	0.3277	0.1093	0-2173	2.1876
	-0.01	_0.0_		-ia1521			0-0020	0_3251	_4.1110		-1-7592
	1.00	U.U		-0.2790		-0.0551		0.3272	0.1123	0.2149	-1.4282
<u> </u>	2.69	<u> </u>		_=0.457×		<u></u>		0.3252_	_LallaZ_		m1.A303
	3.40	6.0		-9.6554M -9.2.42		-0.0617	-0-00-0-	0.3743	0.1174 1.1158		-1.4866
	5.71	( • u		-1.ce7+		-1.05-0		0.3274	0.1250		-1.6130
	9.71	0.0		-2.1500			=0-0090	4105-1	0_1553		-1.7668
1	13.75	0.0		-4.46m3			-0.0093	0.3660	0-1-5t		-1.7939
	17.80			-7.3507		-r.1954	-0.0173.	0.3766	2625°0		-1.7745 -1.7588
	25.115	- نئون		-11.1764		-5.2.23		ù-3366	1.3520		-1-7166
•	ch.+7	u . ū		-10.0203		-0.2155		U-2978	0.2962		-1.6943
<u> </u>	21.27	Lau	4.5007	-Hailes	<u>Ual 3a9</u> .	-4-3-41	-0-003H	_0.2446_	c.2913 <u></u>	2500-0-	<u> </u>
				•							
	<del></del>										· <del></del>
								<del></del>			
							<del>., </del>				
						<del></del>					
				0 ==							
			<del></del> ,								
											<del></del>

Cold	FT	1 05 1		# 1 P. O.	CENTERIA	EOC)	MOLE JUNEAN	ISSILE TA	CHEL_FACIL	ITY(P=T)	AER	OUYNAMIC .	LIND TUNNEL (AT
2 92 0.65 2.5							··						<del> </del>
2 92 0.65 2.5		<del>.</del>											
PMG bfTA CM1 Cm1 Cm1 Cm1 rCmf1 VCPf1 CM2 CM2 CM2 CM2 VCPf2 LA1 Cm1 Rdd													····
1.41 C-U 0.4022 - 0-5011		٠	72 0.0	J 243		390736 (	/···			U PRE	L		
0.39	INT	ALPHA											
1.60	-	-1-41											
1.00 0.0 0.0070 0.0070 0.0030 0.0070 1.1527 0.0039 -0.0011 0.0100 -0.0315 0.2050 2.60 0.0 0.0010 0.00315 0.2050 0.0010 0.00315 0.2050 0.0010 0.0031 0.0027 -0.0263 0.3183 0.40 0.0 0.0026 0.0020 -0.0031 0.0077 -0.5676 0.0060 -0.0021 0.0267 -0.0267 0.3391 0.60 0.0027 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0031 0.0													
2.66		1.64											
3.40 0.0 0.00 0.002 0.0000 -0.0014 0.0077 -0.5870 0.0021 0.0021 0.0227 -0.0227 0.3391 3.60 0.00 0.0027 -0.0001 -0.0027 0.0305 -0.9129 0.1576 -0.0021 0.0306 -0.0228 0.3381 5.71 0.0 0.0027 0.0001 -0.0027 0.0305 -0.9129 0.1576 -0.0020 0.0496 -0.0127 0.3156 3.73 0.0 0.0010 -0.0007 0.0000 0.0005 -0.0116 0.5051 0.3028 0.0008 0.0021 0.0021 0.2712 3.75 0.0 0.0050 -0.0004 0.0004 0.0005 -0.01165 0.3273 0.0302 0.0040 0.0125 0.0100 0.2486 7.86 0.0 0.0050 -0.0007 0.0011 0.0022 -0.0111 0.8511 0.5615 0.0066 0.1021 0.2014 0.2486 7.86 0.0 0.0010 -0.0007 0.0011 0.0022 -0.0111 0.8511 0.5615 0.0066 0.1323 0.0174 0.2387 9.90 0.0 0.0100 0.0007 0.0015 0.0025 0.0027 0.0127 0.0121 0.1375 0.0229 0.2237 5.05 0.0 0.0017 0.0017 0.0021 0.0055 -10.3018 0.1289 0.77327 0.0121 0.1585 0.0229 0.2237 5.05 0.0 0.0017 0.0017 0.0055 -10.3018 0.0287 0.0000 0.7737 0.0702 0.1058 0.0287 0.2136 5.07 0.0 0.0017 0.0026 0.0055 0.0055 -10.3018 0.0287 0.0059 0.1059 0.1058 0.0261 0.2142 7.27 0.0 0.0017 0.0026 0.0055 0.0055 0.0055 0.00878 0.0159 0.1732 0.0267 0.2148		2.64											
5.71 0.0 0.0027 0.0001 -0.0027 0.03.5 -0.9729 0.1576 -0.0120 0.0496 -0.0127 0.3156 2.73 0.9 0.0010 -0.0005 -0.0005 -0.0015 -0.105 -0.3010 0.020 0.0001 0.0021 0.0021 2.75 0.0 0.0550 -0.0004 0.0010 -0.1165 0.3273 0.0309 0.0500 0.0000 0.1005 0.0100 0.2406 7.66 0.0 0.0050 -0.0010 0.0062 -0.0101 0.0525 0.0037 0.0010 0.0006 0.1223 0.0170 0.2367 9.90 0.0 0.0170 0.0004 0.0004 0.0525 0.0937 0.0107 0.0101 0.1375 0.0229 0.2237 5.65 0.0 0.0077 -0.0072 0.0015 0.0525 0.0937 0.0107 0.0101 0.1375 0.0229 0.2237 5.67 0.0 -0.0062 0.0017 -0.0055 -16.3010 20.2000 0.7737 0.0702 0.1058 0.0261 0.2142 7.27 0.0 0.0072 0.0062 0.0050 0.3580 -0.7452 0.0070 0.1732 0.0247 0.2144		3.40	0.0	0.0626		-0.0014							
9.73	Z	3-60	D-U	0-0020	-0.0000	4.444	-6-0150	0.060	U-0915	-0-0021	0.0306	-0.0228	0.3341
3.75 U.U 3.005U -C.:000 0.Culm -f.1165 9.3273 (.e369 0.0064 0.1085 0.0100 0.2486 7.86 0.0 0.005U -0.005U 0.0062 -0.0111 0.0652 -0.005E 0.005E 0.1323 9.0174 9.2347 9.94 0.0 0.015t 0.005t 0.005t 0.005t 0.005t 0.005t 0.0229 0.2237 9.94 0.0 0.015t 0.005t 0.0		5.71	0.6	0.6027	4 u 3 u e ù	-0.0624	6.03.5		0.1574	-0.0020	0.6496	-0.0127	0.3154
7.86 0.0 0.0056 =0.0051 0.0062 -0.0151 0.0525 0.0097 0.0167 0.0161 0.1375 0.0229 0.237 0.00 0.0156 0.0025 0.0037 0.0167 0.0161 0.1375 0.0229 0.237 0.05 0.00 0.0055 0.00 0.0055 0.0037 0.0167 0.0161 0.1375 0.0229 0.237 0.05 0.00 0.0055 0.00 0.0055 0.00 0.00	)	9.73											
9.44 0.0 0.017t 0.000t 0.0015 0.0525 0.0937 0.6147 0.0141 0.1375 0.0229 0.2237 5.65 0.0 6.0007 =6.1721 0.0012 0.0145 0.0145 0.7327 0.7211 0.1565 0.0287 0.2145 0.407 0.0 0.0017 =6.1721 0.0016 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017 0.0017		13.75											
5-65 0-m 6-0mh7 = (-1.27) 2-0mi2 = mi-3la6 6-la587327 6-211 0-1565 0-0287 0-2136 0-687 0-6	—	17.66											
7.67	1	19.94											
7-27 C-U 0-BB72 U-UG2b -C-005b U-35ab -0.7452 0-0878 V-0159 0.1732 0-0247 0-2144	3_												
	<b>6</b>												
			LAN	_uaun.e_	. Ualinza			-0.1632		N-01-33			
										-			
			•										
							<del> </del>						
						<del></del>			<del></del>	<del></del>			<del></del>
													•
	_												
								_					
			····										
						•							
	_												
					-								•
	_												
•			•										
•	_												
· ·													_ <del>-</del>
	_												
	_							<del></del>					

.

												<u> </u>
		PAPILE	LCH RX 10-	6 Pn1			1 DEL2					
	5	92 0.	42 5.2	0.0 8.	3-0F36 0	.0	0 0	0	O FRE	£ 		
INT	ALPHA	6FTA	CMF 3	C∺3 =001:	C+3	XCPF3	YCPF3	CNF4	CH4	C84	XCPF4	YCPF4 
	-0.39	0.0	C-01.24	-7-11045	J. FUZ6	-( -2176	1-1046	-0-6001	-0.0001	-0.0030	0.6668	20.0667
3	1.64	0.0		-( .u311		-1.65:33-2 -35.33-2	B-01-9	\$810-0-C	-0.0007		-0.0292	0_189
. <b>.</b>	2.24	U.U	0-62-1	-0.0000		-1-04-5		-0-0363 	-0.0011 -0.0011	0.02+3	0-0321.	
6	3.40	0.0		-0.630× -0.630×		-66-6 -6-1426	2.6270	10m0-0 54kg-0	-0.0023	0.0332 0.035A	-0.0266	0.3851 0.3798
8	5.71	G. U	9.0017	-5-5007	9.0054	-0.3557	2.4043	6.1588	-0.0023	0.0562	-0.0144	0.3539
9	9.73	C-A		<u>-5-106)</u>		-0-0258 -0-0776		0-2950	0-00e5	0.1734	0.0101	0.2951
	12005	_G_V_		-0-50u5		-(-6451		0.5302	0.0105		-0.0101	
	19.94	0 <b>.</b> U		-0.0000 -0.000-		-0.0419		0-5747	0.0145	0.1527	0.0250	0.2639
	25.05	6.0		-0.7014		-0.0735		0-77A3 0-77A7		0.1844	0.0216	0-2614
15	27.27	Cal		-PU-0013			0.5640	0.7874	0-0106	0.2054	1150-0	0-2608
	•				·							
									_			
	100					<del></del>				<del></del>	-	·
							<del></del>					
				–								
												<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>

	-	•											
		ING LE	MEL OPMENT	CENTERLA	EUC) P	<u> HOFULSIUN</u>	MIND TUN	NEL FACIL	ITY (PAT)	AER	ODYNAMIC	LIND TUNNELL	ATI
	2 0  3 1 0  1					M VITHAP	ISSILE TA	IL EFFECT	S DATA				
	TEST		ACH RAID-				1 DELZ	DEL3 DEL	A TRANSIT	104			
ç	S	43 ".	5c 2.5	0.0 +	3*9F36 )		0 D	. 0	0 FHE	E			-i
INT	ALPHA	BFTA	Carl	C=1 =C=USDS	C#1	>CPF1 #0.0158	YCPF1	CNF2	CHS	CBS	*CPF2	VCPF2	
2	-0.3e	<u> </u>	0.063e	0.0001	3.6.32	0.0212	3.4434		-10004	-0.0138	9.0903	1.2454	
3	_0.63_	li ii	0-0423	G_0			1-0008		0.0004		0.0560_	0.0573	<del></del>
<u>.                                    </u>	1.64 2.68	0.0	0.0117		-0.0015 -0.0015	0.0 _=0.1500_	-1.1170 -6.6167	0.0355	-0.0013	0.0101 	-0.0366 -0.0302	0.2861 -0.3657	
6	3.65	5.0	0.0013	-0-0001	\$100.0	-0.0514	0.8593	0.0920	-0.0025	0.0295	-9.0269	0.3202	
<del>/</del>	5.69 4.74	<u> </u>	<u> </u>	0.7002	-0-0042	0.0541 0.0746	-1.8874	#-1599 #-30n7	-0.0013	0.0477	-0-0171 -0-00+1	0.2984	
9	13.78	0.0	OV.	-0.0004	0.0615	-u-0922	0.3053		6000-0	0.1105	9-0007	0.2496	<del></del>
0	17.87 _19.93	U.U 	0-0132	7.000J -0.0005	0.0037 0.3657	0.0055 -0.05e7	0.4055	0.5657 	0.00+6 4.0067	0.1338 	0.0081	0.2366	
2	25.13	0.0	-C.00ny	-0.0007	0.6:15	C.1039	-0.2583	0.747R	0.0118	0.1653	0.0158	0.2211	
13	_21 <u>.3</u> 4		-0-6127	n=nyga	-11-0415	-c-0731	0-1155	0.n073	0.0137	0.1774	-0-0169	0-2197	
											¥		
													•
								•	•		<del></del>		······································
	· • · · · · · · · · · · · · · · · · · ·		·····										
<u>e</u> :													
										•	<del></del>		
							<del> </del>						
					<u> </u>								
									<del></del>				
								<del></del>					
								•				·	
						-							
	<del></del>					······································		<u>~~</u>		95.25			<del></del>
					<del>.</del>								
							•						

	1 OF 1	THE DE	SELVECEN	CESTERIA		MAHTIN N	ISSILE TAI	L EFFECTS	DATA .	ZER	ODYNAMIC WIND TUNNEL (A)
	TEST.		ALM RX10=	0.0 p	COAF		1 DEL2 1		TRANSITI D FALE		
POINT	ALPHA	HFT.	C+	CLM	CY	CLN	CLL	CA	ÇAB	CAF	ACP
1	-1001 -0030	<u> </u>		-0.1364		-0-06u3		0.4251	0-1325	0.2959	1.7742
_ā	0.05	0.4		-u-lo32	_U_GIES		-4-0051	_0.e23F_	_0.1340_	-N-2847	-1.6431
2	2.64	0.0		-0.7495		-0.0504	-0.9097	0.4134	0-1303		-1.4534
6	3.60	0.0		-9-710-			-0-0105		0.1293 0.1333		-1.4742
	5.05	Lau.	Sept 27c	-1.3555	4155	-0.0524	-)-00-4	0.4250	0-1435	0.2415	-1-685B
<b>8</b>	4.1u	(int		-7.7556 -4.7552		-0.0044	-0.0120 -0.0157	0.=421 0.567	0.1735 0.221A		-1.4086 -1.8197
10	17.67	0.0		-0.7341			-0-0550	0.4790	C-2528		-1.7620
11	19.95	0.4	4.4437	-1.75.2	0.6701	-0-1760	-0.0200	J.4778	0.2975	0-1BU3	-1.7441
12	25.24 27.49	ψ.υ 0.π		-10.0M57			-0.0124 -0.0251	0.4191.	0.3099		-1.5953 -1.4980
				<del></del>				· · · · · · · · · · · · · · · · · · ·	***		
<del></del> -				· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·	<del></del>		
							· · · · · · · · · · · · · · · · · · ·			<del></del>	······································
			<del></del>						<del></del>		
	•										
						··					<del></del>
							-				
		-			100						

					<del></del> .		<del></del>				<del></del>	
2.01.5		The		## N. P = . A * * * *		Som. 4 1 1 ==		C. 5400			A0W44	
	1 04 3	TWO DE	NET SPORT	CEMIERIAL	<u> </u>		LAIND TUNE ISSILE TAI			AEH	ODYNAMIC_	AIND TUNNEL (AT)
HELT	1 01 1		<del></del>									
		<del></del>										· · · · · · · · · · · · · · · · · · ·
	TEST	PACT W	A £ 11	6 <u>-24</u> I	LONE		1 DEL2 !	)61 3 DE1	_ TDANETT	*O# :		
	S		40 2.5		-0F36 0		0 D		0 FRE			
PG 1 ~ T	_	HETA	(11)	Cm3	Co3	XCPF3	YCPF3	CAFA	Cn4	CR4	XCPF4	YCPF4
	-l.+l	1.0	-013.	-0.0014 .	0-2325 0-0031	-3.1004	7.6500	0.0017	0.0000	-0.0174	0.0316	-1.8421
_i	6.65	0.0	-0-1016			1.2522	3006	0.0225	_=3=003#		_=0.0372_	0.2006
•	1.00	0.4		-0.6010	0.0627	-0.753A	2.0448	0.0422	-0.0017		-0.0402	0.3422
.5	<u> </u>	<u> </u>		<u></u>			1.2271		-0-0030		-0-0441	0.3722
7	3.66	0.0		-4.000		-0.53es	1.9379	0-0990	-0-0039		-0.0342	0.3773
	9.76	U.U		-0-0267		-0.2035	1.5817	£00F.c	-0.0053		-0.0175	0.3113
<u>.</u>	13.70	0.0		-0-0535			1.3379_		0.0031		-0.0073	0.2979
10	17.47	(· . V		-0.0000-		-1712	0.6347	0.5414	-0.0023		-0.0037	0.2608
11	_19.95_	_0		-0.005-		هندن منع			-0-0021		0.0035_	0.2772
12	25.24	0.0	(-ul-2	-0-00us		-0.6522	0.5692 J.5226	0.7471	-0-0017		-0.0023	0.2746
							443245			U46540.		
											٧	
								<del></del>				
								· .				
•				.,						<del>,</del>		<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>
					<del></del>				<del></del>		<del></del>	
											-	
-												
							<del></del>					
								·				
			<del></del> _	<del> </del>				<del></del>	<del></del>	<del></del>	<del></del>	
											<del>-</del>	
					-	•						

1 -1.61 0.4	AE.	S OL 3	THE DE	VEL OPHENT	CENTERLA	<u> </u>	MOIZJURDA M FITRAM	SIND TUN	SEL FACIL	IIYIPHII_ S DATA	AER	ODAWWIC"	NIND TUNNEL (AT)
1 -1-61													
2 -0.41	POINT												
\$ 1.63	<del></del> _												
5	_3												
6 3.66 0.8 0.005 0.001 0.0032 0.0702 0.5985 0.0786 -0.0044 0.0792 -0.0488 0.2984 7 5.71 0.0 0.6614 -0.004 0.0782 -0.004 0.2087 0.0061 0.6630 -0.0368 0.2987 0.0061 0.6630 -0.0368 0.2987 0.0061 0.6630 -0.0368 0.2987 0.0061 0.6630 -0.0061 0.6630 -0.0368 0.2987 0.0061 0.6630 -0.0061 0.6630 -0.0368 0.2987 0.0061 0.6630 -0.0078 0.0631 -0.0782 -0.2880 0.5388 0.6380 -0.0078 0.1105 -0.0178 0.2523 0.0067 0.0067 0.0067 -0.0067 0.0067 0.0078 0.1105 -0.0178 0.2523 0.0067 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0.0078 0	\$												
9 13.86 0.0 0.0013 -0.002 0.014 -0.1029 1.1270 0.3095 -0.0067 0.0925 -0.0216 0.2666 9 13.86 0.0 0.0021 -0.1713 0.0022 -0.2500 0.5388 0.4380 -0.0076 0.1105 -0.0174 0.2523 10 17.95 0.0 0.0022 -0.0011 0.0053 -0.3474 1.6027 0.5504 -0.0076 0.1348 -0.0139 0.2449 11 20.05 0.0 0.0023 -0.0014 -0.0009 -0.0667 -0.2069 0.6055 -0.0087 0.1466 -0.0144 0.223 12 24.42 0.0 0.014 -0.0003 0.0044 -0.0223 0.3848 0.7453 -0.0122 0.1793 -0.0164 0.243 13 27.75 0.0 -0.003 0.0054 -0.0056 1.4095 0.7980 -0.0134 0.1931 -0.0168 0.2419	6												
9 13.86 0.0 Caucal =0.1013 0.6u22 =0.25u0 0.5388 0.4380 =0.0076 0.1105 =0.0174 0.2523  10 17.95 0.0 0.3027 =0.0011 0.6u53 =9.3474 1.6027 0.5504 =0.0076 0.1348 =0.0139 0.2449  11 20.05 0.0 0.0023 =0.3004 =0.0009 =0.0667 =0.2069 0.6u55 =0.0087 0.1466 =0.0144 0.2421  12 24.42 0.0 0.0114 =0.0003 0.0044 =9.0283 0.3848 0.7453 =0.0122 0.1793 =0.0164 0.2421  12 24.42 0.0 0.0114 =0.0003 0.0044 =9.0283 0.3848 0.7453 =0.0122 0.1793 =0.0164 0.2421  13 27.79 0.0 =:.00=4 0.0144 =0.0119 =0.4476 1.4095 0.7980 =0.0134 0.1931 =0.0168 0.2419	<u></u>												
17.95 0.0 0.0027 -0.0011 0.6053 -9.3474 1.6527 0.5504 -0.0076 6.1348 -0.0139 0.2449  11 20.05 0.0 0.0063 -0.3064 -0.0009 -0.0667 -0.2069 0.6055 -0.087 0.1466 -0.0164 0.2421  12 25.42 0.0 0.0114 -0.0003 6.0044 -0.0263 0.3848 0.7453 -0.0122 0.1793 -0.0164 0.2405  13 27.75 0.0 -1.00-4 0.6541 -0.0119 -0.4676 1.4095 0.7980 -0.0134 0.1931 -0.0168 0.2419	5			_									
11 20.05 6.0 0.0643 -0.0609 -0.0667 -0.2069 6.6055 -0.6087 0.1466 -0.0164 6.2421 12 24.42 0.0 0.0114 -0.6003 6.0044 -0.0263 0.3648 0.7453 -0.0122 0.1793 -0.0164 6.2405 13 27.79 0.0 -1.00-4 6.6541 -6.6119 -6.4476 1.4095 0.7980 -0.6134 0.1931 -0.0168 0.2419	10												
27.75 R.U =: -U0== (-f:4) =f.(  \Q  =0.4h76   .40\S   .79\RU =0.0  34    C. \Q  =0.0 68   0.24  Q    .	11_							0.2069.	0.6055_		0_1466	-0.0144	
	15		-										
				•									
					<del> </del>								
		<del></del>	<del></del>			-							<del></del>
			·				· · · · · · · · · · · · · · · · · · ·						
					-								

. .

E 3 UF ET 1 OF	3			-	#4117#1	ISSILE TA	IL EFFECT	5 DATA	5		AIMO TUNNEL (A	
		ACS RAIL-	<u>6 -41</u>	<u>com</u> F B3nOF3b (	· L	DELZ	DEL3 DEL	A THANSIT				
INT ALPH		CNF3	6-3	Cm3	ACPF 3	YCPF 3	CHF4	CH4	CR4	ECPF4	YCPF4	
			(.) 14		-3-333m	7.3704 9.5000		-0.0010		<u>-0-0506</u> -0-0577	<u>0.6780</u>	
0.0	يسف خ	-0.6617		لتحديدها	1.37.8_	-3-5114	_0.0229	-0-1012	0.0052	-0-0533	0.2272	
1.5			-(-0115		-1-1937	2.5677		-0.0021		-6.0464	0.3164	
3.0			-0-101= -0-101=		1-511E -1-1019	2.0148		-0.0347		0.04 <b>36</b> .	0 <del>.3579</del> 0.3705	
5-7	L Davi				التة يوسو	2.9640		-6-0062		-0-0374	0.3419	
9.7			-1.0.015		-9-4175	1.8120		-0.0061		-0.0273	0.3168	
17.9			-0.001e		-0-22 <u>09</u>	1 <u>.22</u> 55.				-0.0123 -0.0123	0.29 <del>98</del>	
20.0		9,0115	-0.3007	241112	-C-1736	0.8535	0.5760	-0.0057				<del></del>
25.4		6.710-	-5.9007		-0-0440	0.6429		-0.0117		-0.0163	0.2018	
27.7	<u> </u>	7-1144	<del> Carrier</del>	<u> </u>	-5-04-2-	0.5354	3.7749	-0.0153	0-2210	-0-0197	. 0.2452	
										<u> </u>	·	
		•										
							<del></del>					
	<u>.</u>											
								<del></del>				
										·		<del> </del>
			<del> </del>			· ·			· · · · · · · · · · · · · · · · · · ·			<del></del>
							•		-			

						-	-					
					4							
	ENGINEED		PET OB AE	CERTERIA	<u> </u>		ISSILE TAI			AE.K	DYMANIC -IN	D TUNNEL (AT)
SHEET	I DE_I											
					***							
	5		. 2.5		3> UF 36 0		O O		FREE			
Dr. I L. T	ALPHA	r#1=	Ch	CLH	CY	CL.	CLL	CA	CA4	CAF	ACP	
1	-1	G and			-C-5544		-0-0058	3-5686	G-1846		0.0052	
2	-01	(· . v	-(-0025	-0.123-	-0.0:24	C+5c+1	-3-00m9	0.5672	U.1905	0.3747	43.1859	
3	4.64	_44}_			الفراه ماد		-0-0096	<u>0.5661</u>		374B_		
•	1.60	0.0		-0.3011			-0.0107	0.5672	0.1924		-1.6347	
<u>5</u>	7.60	<u>نميا .</u> . 0 • 0		-6.255 <u>1</u>	<u>-0-000-</u> 0-0057		-0.0112 -0.0117	_0.565 <i>L</i> _	0.1962		-1-5149 -1-5406	
7	_ 5.7u	ن مانا		-1.3ezz			-uallag	6-5754	6-2373		-1-5920	
ė	4.77	6.0		-2./610	6.0194	0.0150		0.6154	0.2427		-1.6713	
9	13.86	بدمقب		-44/445		-0.0135	C.01#5		2655		-1-6328	
10	14.07	C - 7		-5.7.41		-0-0-51		0.5131	0.5800		-1.5078	
	20-21			-5-3-72			-0-0176		<del>2633</del>		-1-4044	
12	25.64	( . u		-7,442/ -8,5813			-0.014Z	0.5724 	0.3086	D-2639	-1.2004	
			1.3353		14.178		Y IAMANA				=1+1300	
											<u> </u>	
												<del></del>
								•				•
												<del></del>
			•									
										-		
					<del></del>			<del></del>	<del></del> -			
							-					
									······			
				<del></del>				<del></del>	<del></del>			<del></del>
												<del></del>

0				00.01.04						,		
	OF 3	ING LE	<u>vel døge vi</u>	CEMPERIA	EUC) P	* * ITAA*	ISSILE TA	IL EFFECT	S-UATA	AER	DOYNAMIC	ING TUNNEL (AT)
	IEST	PAkl -	ALM RULU-	- Pnl	CONF	L ČEI	1. DEL2	DEL 3 DEL	A TRANSIT	104		
	2		cu 2.5			-0	0 0	•	O FRE	E	-	
INT	ALPHA	AT \$4	CHF1	CH1	Col	*CPF1	YCPF1	C>F2	CH?	-0-01 <b>4</b> 4	KCPF2	YCPF2
5	-0.41	0.0	-0.00.1	0.3512	<u> ع تريات منا -</u> -ناس نا ه ما	-1 -37e7	-0.1424	-0.0052	-6.0014	-0.0064	0.2715	1.2256
3	0.60	-0.0	-0-8-39				-0-4726				-0-1620	-0.0782
5	2.00	6.0	-0.0076 - <u>4666-0-</u>	C-,100-	0.0007 6.0005	-0.15/h -0.179#	-0.1206 -0.1043	0-0346	-0.0036	0.00H9 0.61H6	-0.0973 -0.0745	0.2305 0.2857
6	1.69	0.0	-0.0005	0.6011	0.0003	-0.2330	-0.0571	0.0546	5000.0-	0.0ZA6	-0.0652	0.3020
<u>,                                     </u>	5.74	0-0	-0-6112		<u></u>	-1-13-3	- Made 2	0-1584	-0-037H		-0-0490	0.2963
9	4.77 13.50	Ú.U G.N	=0.0.75 =0.00e7	0.0014 <u>- 1167au</u>	-1.655 -0.0623	-0.20+7 -0.33#4	0.0859	0.2934 0.4113	-0.0089 -0.0094		-0.0302	0.2688 9.2571
i u	14.07	6.0	-0.00>0	0.6304	-0.0015	-0.0644	9.2714		-0.0114		-0.0221	0.2499
ц	20.21	4.0	-0-0016	0.3009	<u></u>	-Cap Zil	-0.0100	-0-5684	-0.0126		1258-0-	9-2482
12	25.65 28.00	0. J	-0.00v1 -0.02v2	0.701	-v.0013		G-1397		-0.0155		-0.0216	0.2463
		Heil.	- Heile FC			- III		<u> </u>		U.1591		0.2477
				Set (1)								
								•				
			<del></del>									
												· · · · · · · · · · · · · · · · · · ·
	<del></del>		······································									
				<u> </u>								
							-		_			
								<del></del>	·····			
									· · · · · · · · · · · · · · · · · · ·			

01.6	£ NG 1 F	FDIAG US	Fuel 3046 vt	CHAIFUIA	Fuch a	MODEL STAN	alao Tua	-FI FACTI	17749473	AFD	Onverte	aIND TUNNEL	
E	3 OF 1 OF	3					ISSILE TA					10.000	
		0.00	ALM RX10=		CONF -	L ČEL			. IRANSII				
	5	96 1	· 2 · 2 · 5	0.0 d	13ruf 36 0		C O	0	0 FRE	E			
13 ∾T	ALPHA		CNF.4	CH3	Cd7	ACPF3	YCPF 3	C\F4 =0_0166	C44 -0.0004	CB4 -0-0125	#CPF4 0-0368	VCPF4	
2	-0.4		-8-9114		0.0011	n.5511	-0.5737	U.0031		-0.0017		-1.2013	<del></del>
3	1.64			<u>-Canour</u>	u.Dića	0 <u>~2125</u> 0~2475	_0.807A_ -0.8780	0-02451	u.ucza.			_0-1897	<del></del>
5	2.6		-0-0013	70000	0-0029 0-0025	6-3016	-1-5-50		-0.0037 -6.0030		-0.0813 -0.0728	0.3101	
0	3-6		-0-0410	-0.0006	6.0637	ŭ.63×3	-3.7835	0.4995	-0.0050	0.0354	-0.0603	0.3555	
<u></u>	9.7				0.0003	-1.01e2 v.23.v	-1.71.3	0-1624	-0.0072	0.0552	-0.0327	0.3115	
Ş	_13.0			-0-6607	0-0053				-0.0100		-0-0250	0.3009	
U	18.0			-5-0205	v-01(1	-0-0474	J.#376	0-4997			-0.0535	0-2912	
2	25.6			-7-1014 -11-0007	0.0119	-0.06-1 -0.0325	<u>0.7909.</u> 0.5520	5- <u>5521</u> G-6877	-0-0126 8-210-0-		-0.0231	0.2495 0.2901	
<u> </u>	28.0			-6-0207		-2-02-0			-0.0195		-0-0264	0.2923	
				-									
							<del></del>				· · · · · · · · · · · · · · · · · · ·		
				<del></del>									
			<del></del>									·	
									<u></u>				
										······	<del></del>		
					<del></del>								
				<u> </u>	·	<del></del>							
													-
				<del></del>			······································	···		<del></del> -			
										•			

TINT ALPI 2 -0. 3 -0. 4 1. 5 2. 6 3. 7 5. 8 9. 9 13. U 14. 2 25.	71 0.00	-1605 -0.0405 -0.0736 -0.1913 -0.1913 -0.4731 -0.7977	0.0 H	CY 6-04H3 0-0513 6-04H4 0-0534		-5.0124	CA 		CAF	XCP =105490		
2 -0.3 -0.3 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	71 0.00	1.3v 2.5 A CN -1.1605 -0.0vn5 0.1713 0.1713 0.1717 0.7777	0.0 H	CY 6-04H3 0-0513 6-04H4 0-0534	CLN -3-1-47 -0-1+70 -G-1de6	CLL =) G132 =0.012H	CA 	C48 0.2013	CAF			
1 =10 2 =0. 3 iii 4 10 5 2 6 3. 7 5 8 9 13 0 14.	37 0.00 36 0.00 66 0.00 71 0.00 71 0.00 71 0.00	-1.1605 -0.0005 -0.1736 -0.1713 -0.1713 -0.1717	1.2662 1.1677 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676 1.1676	0.0513 0.0513 -0.0534	-3-17 -0-1-70 -6-1dr6	-0.013Z	U.>374	0.2013	0.3344		<del></del>	•
2 =0. 3	37 (0.00 pp. 10.00 pp. 10.	-0.0en5 -0.736 -0.1913 -0.1913 -0.4731 -0.7977	0-1-7/ 1111-0- 2-25-0-	0.0513 6-0444 0.0534	-0.1+70 -6.1dr6	-5.0124	0.5374			_=1.5490		
6 1.6 5 2.6 6 3.7 7 5.8 8 9.13.1 U 14.1	66 0.0 71 0.0 71 0.0 71 6.0	0.1913 0.4242 0.4751 6.7977	-0-1131 -0-29-2	0.0534		-4.0145			0.3415	-3.1767	•	
5 2. 6 3. 7 5. 8 9. 9 13. U 14. 1 22.	71 0.0 71 0.0 71 0.0	0-4242 0-4751 6-7977	-0.525e		-C.1908			_0.1934	0.3442	-0+2199		
5 3. 7 5. 8 9. 9 13. U 14. 1 22.	71 0.0 71 5.5 41 5.6	7.475l 6.7977	-F525#		4 - 1 - 1 - 1 - 1		0.539J 	0.1966	0.3427 _0.3380	-0.5911		=
n 9. 9 13. U 14. 1 20.	4) 0.0				-0.1A72	-6.0155	0.5358	6.1499		-1.1068		
9 13. U 14. 1 20.			<u>-1</u> ~~4//		-6-1413		-0-5485	u-2016		-1-3134		
v 14.			-2.4422 -2.4424 -2.4424		-0.1671 0.1655		2065-0	0.2360 		-1.4919 -1.4794		
			-5.215.		-0.1755		6.5661	0.645.0		-1.3535	<del>* * * * * * * * * * * * * * * * * * * </del>	-
.2 25.	34 0.6	4-50-5	-5.0597	2255		-0-6277	0.5773	_C-2709	0.3064.	-1-2715		
3 2			-7.2541		-0.2603		0.5762	0.3784		-1.0922		
3 75.	16 6.1		-7-n2n+	101191	-6-1car	-6.5333	0.5G14	u-3299	0.5018	-1-0485		
		<del></del>	<del></del>							<	<del></del>	
	. 1			······································			<del></del>		100			
					•	-						
									,		•	
											_ <del></del>	
				<del>,</del>					- · · · <u>·                               </u>			
		<del></del>	· · · · · · · · · · · · · · · · · · ·									

<del></del>				<del></del>		<u></u>		<del></del>			<del></del>	
∍ <b>E</b>	ENGINEES 2 UF 3 1 OF 1		ref isement	CENIERIA	:LC)			MEL FACILI		AFR	ODYNAMIC	INO TUNNEL (AT)
	IESI 2		ALD LAIUS		Cint		1 .GEL2	AEL3 DELA				
UINT	ALPHA	#ET4	CNFI	Cnj	Cel	#CFF1	YCPF1	CNFZ	Cus	CeS	*CPF2	YCPF2
<del></del>	-0.37	0.0	C-Cut/	-1.0013		-F 2119	1.4741	-0-0096	0.0014 0.0011		-0-1100	2882.1
_3	0.66			الألايامتح	Laugar		1.3793_	G-61ZA_	_0.0002.	. +4.4051_	D.D170_	-0-4087
5	2-71	6-9		-0-(uld		-6.2-jü -40202-	1.6117	0.0337	-0-3016.		-0.0249 0.025#-	0-0676
*	3.71	C-0	0.0031	-6-1304	0-0-50	-6.2731	1.5413	0.0900	-4.0026	0.0770	-0.0316	0.2448
-}-	<del>- 5-71</del>	0.0		-0-0064		-0-3111 -0-313	2-0441		-0.00-7		-0.0309	0.2625
ξ.	13.34	0.0		-0.3011		-6-17-2			-0-0077.		-0-0196	0.2470
10	14.16	0.0		-0-0206	3.0041		-7.1579	0.4922	-0.6111	0.1202	-0-0226	0.2442
12	25.4s	0.0	-0.00yu			-G-0440 -G-0177				0-1327	-0.0233 -0.0272	
<u> </u>	24.14	0.0	-							1639		0.2530
							-					· · · · · · · · · · · · · · · · · · ·
			<del> </del>	<del> </del>				<del> </del>			***	
						·		<del> </del>				
												<del></del>
							<del></del>					····
											<del></del>	

; -		<b>~.</b> ·	••••••					. •		·	· · · · · · · · · · · · · · · · · · ·	
<del></del>						<del> </del>			<del></del>			
Ł	ENGINELI 1 OF 3 1 OF 1		vet OPutal	CENTERIA	FDC) P	MARTIN M	EIND THE	IEL FACIL	ITY (PAT)	AFR	ODYNAMIC HIMD	CUBINEL (AT)
	IFSI						1 DEL2 1	DELS DEL	THANSIT	LOM	, ,	
	Ś	104 0.	e 5.2	•	3+uf 32 0		0 0	0	D FHE	E		
INT	ALPMA	SF Ta		CLH	CÝ 4			ÇA	CAR	CAF	XCP	a * ##
<u> </u>	-0.49	Cou.		-0.0170			-C.OU11	0.3093	0-1133 0-1131	0.1954	0.6704	•
3	0.57	Q_V	يونونمو	-0-1007	-:•3212		-0-0007	_وويدهم	_0.1136_	0-1962	-1.6548	
	1.57 2.56	0 - W		-0-2423		0.0710		0.3076	0.1136		-1.4004	
-	3.63	0.,		-060c -0574		0.0315	0.700a	0.3077	G-1152 G-117d		-1.3884 -1.4269	<del>:</del>
<u> </u>	5.43		عجنةمك	-1-316	-undia 7	C-0470		0.3051	3-1250		-1-6223	
h	9.76	0.0		-3.0461			0.0016	0.3151			-1.6917	
9 0	17.82	0.0		-5.4263 -4.5277		0.027		0.3264	0.1783_ 0.2057		-2-0492 -2-0695	
<u>.                                    </u>	19.86	-6.0		-4-1457				0.3265			-2.0764	
2	25.03	0.0	6.0650	-17-1560	L.07u9	-9-1776	0.0305	0.3279	6065.0	0.6310	-2.0090	
3	27.25	- 0-6	5-5415	el3.alta	0.0545	-0.2152	3-0420	0.3095	0.3279	-0.0184	-1-9699	<del> </del>
_												
				· · ·								
					<del></del>							
		-									<del></del>	
					<del></del>		<del></del>					<del></del>
											· · · · · · · · · · · · · · · · · · ·	
				· · · · · · · · · · · · · · · · · · ·					<del></del>			
							<u> </u>					
												•
							<del></del>		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	
					•							
												<del></del>
									<del></del>			
					•							

13 C.

288

E .	9 OF 3		•				ISSILE TA					IND TUNNEL (	
	IESI		ALP FAIGH		Cint 3=0F32		DELZ.		a TRANSIT		<del></del>		
INT	ALPHA	eF74	CVF1	CH1	Cel	XCPF1	YCPF1	C-#Z	CHS	CBZ	XCPF2	YCPFZ	
1	-1.02	<u> </u>	0.0435	_Calent			-7-9016		-0.0045	-0.010-	التتمو	0.3882	
2	-0.44 - 0.57	L.u	4c 60 an	100%-0	-0.0053	1.2901	-6.6557 7.7459	-5.0047 	-0.0012 	-0.0025 	0.2468 0.3577	0.5253	
<del>-</del>	<u>F.57</u>	0.0		-0.003+ -0.003+		(i.e.746		0.0372	0.0120	0.0165	0.3275	0.4442	
٠	2.59	CAU	C-0000	-5-2663	-6-0614	-5.6666	-24-0000	0-4644	B-U19A	0.0252	0.3055	0.3934	- 44
•	3.73	C.v		-0000				6.6437	0.0266	0.0346	0.5865	0.3926	
<u>7</u>	5-63 4-70	<u> </u>		-Lalin				<u>0-1679</u> J-3307	<u>i_u_u_03</u>	0.0692	0.2473		
Ç	13.73	6.0				-0.6367 -0.8367	=11.71.3		U.U627 0.0735.	0.1471	0.1896	0.4448	
10	17.Ac	0.0					-6.4102	0.7531	0.0907	0.3361	0.1205	0.4384	
<u> </u>	19.56	6.)	0.7614	- uall 13		-4.7423	1.3421	0.2436.	0-0987	0.3748	0-1170_	0.4395	
13	25.03	6.0		-1-1000		-0.0004 -0.0335		1-1268	6.1105 8-1150	0.44/3	0.1057	0.4277	
				·· <u>·</u>			· · · · · · · · · · · · · · · · · · ·		<del> </del>		<del></del>		

		····	: 								•	
<u>.</u>	ENGINEER 3 OF 3 1 OF 1	ING DE	rel opment	CFNISH (A	EuC1 P		LAIND JUS			AERI	OYNAMIC .	IND TUNNEL (4T)
	7561	649 <b>7</b> #	ALM RAlus	4 4-1	C . F		1 DELZ	DEL 3 DEL	4 2014		<del></del>	
	5		£6 5.5	7.0 0	3.cf 32 0	0.0	0 0		0 FHE			
G Į '+T	ALPHA	dFT#	Crif 3	C#3 -5.0001	CH3	ACHF3	YCPF 3	C4F4	CH4 =0_40H7	CH4 -G_0143	TCPF4	7CPF4
5	-0.44 0.57	0.0	-0.J627 -0.J624	5.6007 3.0125	6.00005	-0.2771	-0.1454	-0.0036	-0.0010	-0.6050	0.2798	1.3906
•	1.57	0.0	-0.3J2v	C-0010	0.9003 -0.6365	-0.5172	-0.1527 C.2039	0.0386	0.6133	0.0154	0.3441	0.3984
6	3.53	0.0	-0.0026 -0.4430	0.0009	0.0 0.0	-0.3659	3.0 -0-6735	0.0913	0.0276	0.0399	0.3051	0.4374
8	9.70	0.0	-0-0J*N	-0.0002	2-0613	0650.0		0.3148	1500.0	0.1597	0.1974 	0.5075
] v ] ]	17.82	0.0	-0.0195	-5-6055	0.000	0.0153	-0.1042	0.7101	0.004	0.3591	0.1194	0.5058
12	25.03	0.0		-0.0002 -0.000	0-0025	0.0292		0.5992	0.1079	0.4594	0.1080	0.465R
			-112.111									
		<del></del>									•	<del> </del>
								<del></del> -	<del></del>	<del></del>		
								···		•		
						-						•
			<del></del>	<del></del>			–		·	·		
			<del></del>			<del></del>	·					- · · · · · · · · · · · · · · · · · · ·
		<del></del>		<del></del>			<del></del>	<del></del>				
		<del></del>	<del></del>	<del></del>	·	· · · · · · · · · · · · · · · · · · ·		·· <del></del>				
									<del></del>		_	
	,										•	
		<del></del>	······································	<u> </u>					<del></del>			
				<del></del>								
	101	-										
					<del></del>					<del></del>		

	I OF 1				54	784117 7	1221FE IN	IL EFFECTS	SOATA			
				. <del></del> .		- <del></del> -						
	TEST	PART P	41- 8110-	6 Pri	CONF.	L DEL	1 DELZ		TRANSIT		<del></del>	•
INT	ALDHA	BETA	CAFT	Cnl	C41	ACPF1	YCPF1	CAFZ	CHS	C85	X CPF Z	YCPF2
1	-1-64	0.0	. 0.0025		et 0054	-5-1216	E3-HATI		-0-0066		4-3511	0.5786
3	-0.47 0.57	0.0	0.3 	0.0	-0.0009 -0.0013	e.6 =0.4736	-4-0009 	9500.0	0.0005 	-0.0024	0.2759	-0.9428
4	1.57	0.0	0.001	() = i)	-0.0100	0.0	~>.5369	6.6472	0-0146	0.0154	0.3093	0.3256
5	7.59 7.60	0.0	-0 <u>-000                                </u>	<u>-0-003</u>	-6.0054	-1.26 <u>92</u> 0.5667	<del>-24.230a.</del> 5.9667	0.1046	U-0246	_ 0.0263 0.0395	0.2770	0.3534
7	<u>. 5.67</u>			-00000J			2.5602	3,1767	0.0437	0.0732	0.2432	0-4076
6	9.64	( • U	5.00.13		-0.0047		-21-7047	0.3500	0.0650	0.1524	0.1359	0.4356
10	13.75 17.83	0.0	-5.003/			0.4350	0.3406	0.7738	0.076B_ 0.090#	0.3366	0.1173	0.4350
11	13.49	. 0.4	-0-0-27	-5.6025	-u-00al	G. HSGH	2.7621	0.0697	-0.0994	0.3749	_0-1143_	-0-4311
12	25.0e	0.0		-0-1051		-0.20-4	~0.0232 _0.5035	1.0589	0.1084	0.4454	0.1024	0.4207 
		,	9600	,				111342	444401	- 34 m - 14 m	V64738	400101
			·									
								•				
								.4	<del></del>	******		
		· · · ·						•				
	<del></del>											
										<del></del>	······	<del> </del>
					<del> </del>		<u> </u>					
			•	•		•	•					
							<del></del>					
									·			· · · · · · · · · · · · · · · · · · ·
							<del></del>			····	<del></del>	

									· 		• .	
				_ <del>.</del>			<del></del>	<u>.</u>		<del></del> -	·	
						<del> </del>						
		RING UE	MEL UPPE .T	CENTERIA	Euc1 P					AER	DOYNAMIC #IND	ILLYNEL (AT)
	1 OF 1					MARIIN M	ISSILE TA	L EFFECTS	DATA			
	<del>•</del>							-				
					65.4		55.0			•		
	5		AC 5.5	6.6 6	3= 0 32 0		DELZ		FREE		·	<del></del>
) I % T	ALPHA	HETA	C٨	CL4 .	CY	CLN	CLL	CA	CAR	CAF	KCP	
2	-2-47	0.0	-0-1341	-0547	=0.016F	*******	-0.0029	0.3437	0.1151 0.1141	0.2251	2.0770	
3	_1_1_	-0-0	تعفيمت	-4-1461			-0-0022	_0.3465.				. ,
•	1.57	0.0		-0. 1-07			-0-0055	u.3435	0.1143	0.2292	-1.5488	
<del>-</del> -	3.43	0.0		-1.70ur			-0.0031	0.3421	0-1133::	-0-2316-	-1-4743 -1-5310	
ï	5.68	Cak		Tlanate		C-0306	~3~003I	4-3376	6-1204	0.2091	=1-7122	9200000
t	4.70	0.0		-3.41/5		0.6155	0.0053	0.3590	6.1471		-1.9805	
4	13.73	_ <del>c.o</del> _		-5. 4352		G_432 <b>4</b> .	4-0067	3.3773 .			-2-1230	
10	17.83 19.8n	0.0		-11.1335		0-0201	0.0117	0.3701	0.2132		-2.1509 -2.1297	
15	25.13	G. U		-17.7:07	J.0435		0.0369	0.3332	0.2810		-1.9864	
i3	27.44	H-H	7-17-5	-13-5115	G#37	1527	0-0614	0.3112	0-3075		-1-89A7	
											- Table	
	700		<del></del>								<del></del>	
											<del> </del>	
								,				
							····					
						· · · ·		<del></del>				
						•						
				-								
							<del></del>					<del></del>
											-11.	
			<u> </u>									·
,												
										_		
				<del></del>							<del></del>	<del></del>
										<del></del>		

	ENGINEE 3 OF 3		WEL OPMENT	CENTERIA	EUC) F		ISSILE TA			AERO	DINAMIC	IND TUNNEL	1911
SMEET	105							IL EFFECT	3. DATA	<del>,</del>			
	JEST	+AGI .	ACH PAlus		CONE	I DEI	1_0EL2	DEL3 DEL	TOANSIT	10%			
. 7.	5	107 0.	46 2.5	4.0	3-0F32	0.0	0 0		O FRE				v - 3
POINT	ALPHA	BFTA	C'IF 3	CH3	Cn3	xCPF3	YCPF3	CNF4	CHA	C84	XCPF4	YCPF4	
2	-0.47	E . U	-0-1144 -0-0-0-		1200-3 5100-0-	-0.13+1	U.3557	0.0035	0.0076	-0.0113	0.1723		
	0.57	0.4	كفيك مده	0_000 a		بنخوه مند.	0.32+6_	4.0258	-0-0094	0.0068_	0.3474	D.2642	
<b>•</b>	1.57	6.0	-0.1.113-	0.0965		-9.1677	9-2-26	0.6470	0-0162	0.0179	0.3452	0.3800	
6	3.53	0.0	-0.00ec	<u></u>	-0.00]+	-0.26-7	0.4724	G-1027	U.0322	8P\$0+0 7E+U.0	0.33AZ 0.3131	0.4252	
<u> </u>	5.68	0.4	-C-3052	-4-005				3-1741	1.0462		0.2655		
8	9.74	U . U	-6.6407	0.0001		-0.0173		0.3525	0.0747		0.2120	0.4937	
10	13.73 173	6.0		-0-000-c		0.0260		9.7699	0.0845		0.1097	0.4935	····
<u> </u>	196	0.0		-5.uC35			-D-D466				0-1036		
12	25.13	0.4		-0.9004	6.0024	0.0554	-0.322.	1.0720	0.0994	0.5098	0.0927	0.4755	
13	27.40	0_11	-0-Jun7	25000-4-	3-000-3	C-0075	-0.1206	1-1374		0.5419	0.0865	0.4765	·
								•					
											<del></del> :		
		: ·											<del></del>
											·		
			-	-									
					<del></del>					<del></del>			
												······································	
											<u>.                                    </u>	<del></del>	
								•					
													•
												<del></del>	

	1.6134.66 0F 3 0F 1		her upae's t	CENTES (A	<u> </u>	ROPULSION MARTIN M	IND THE	EL FACIL	TY(P=T)	AERO	DYNAMIC_	WIND TUNNEL (A)
	1 <u>F</u> \$1		ALM RALL-				1 - DEL2		A IHAMSII O FRE			
NT	AL CHA	eF TA	CNF1	CHI	Cel	*CPF1	YCPF1	CNFS	CHS	CRS	XCPF2	ACDES
_	-1.00	0. u	0.0011	-0.6661	-0.0:14	-6.0727		0.0037	-3-4064 0-000H	-0.0016	0.2213	-0-6458
	6.56	0.4							0+00#0_			. 0.1938
	1.56	6.6	-0-0017	-0.000-	-0.00hp	0.5244	6.8793	0.0521	0.0157	0.0156	0.3006	0.3000
	_2-61_	0-4			ــــــــــــــــــــــــــــــــــــــ			-0+C7¥7	_ELS0.0_		0.2926	
	54.6	0.0	-0.0015	-C-60u7	-0-0000 -0-00-0-	3.4933	2-3873	0-1147	0.0310	0.0414	0.2699	0.3613
_	4.04	6.0		-0.0000		-2.5000		0.3920	0.0462 0.0659	0.1665	r.178+	0.4239
	13.7E	0.4			_	-	2_2413_	0-6014	0. U 7.67		0-1274.	
	17.67	6.6		-0-1055		^.7751	0.1799	0.6135	0.0405	0.3458	0.0989	0.4250
_	15.93	C-V			<u></u>			0-5195	0.0837			2254.0
	25.26	G. U		-0-6324		-0.1634		1.1724	0.0527	0.4958	0.0706	0.4229
-	<u> </u>	<u>fa_li</u>	C. Llub	-11-1-124	1.0049	-5-2616	0.6550	1.2458	60000	0.5242	0.0724	0.4208
										<u> </u>	•	
							<del> </del>					
								•				
-				<del></del>							<del></del>	
	_			_								
_								<del></del>				
,												· · · · · · · · · · · · · · · · · · ·
						-						-
_												
_					<del></del>				<del></del>			
-												
										-		
								_				

	<del></del>					<del></del>	_ <del>:</del>						
						w		<del></del>				<del></del>	<del></del>
AHNOLD PAGE SHEET	ENGINEE LOF I		ber opment	CENILALA	FUCI P		L.MIND TUNY			AER	ODYNAHIC_WING	TUMELIATI	
	77.6	2 0407 ~		4 Dul	EUNE		1. KEL2	VE 3 DE L	7014617				
	<u>123</u> 1	109 1.			3-0F32 C		0 4		FREE			3	
PUINT	ALPHA	PETA	C4 -0-1554	CLM	C₹ -0_01=5	CLN 0-00+3	CLL SU-DON7	CA 	* CA8	CAF D. 3845	KCP =0.5028		
<i>\$</i>	-Ce	0.6	-0-6747	-10462	-11-0163	-0.0070	-0.0054 -6.0050	0.6010	0.2126	0.3842	4.1547		
	1.57	0.0	0.2435	-C-4347	-3.01/0	Course		0.5974	0.2199	0.3779	-1.8671		
6 7	3.62	U. U	2.5554	-6.7520 -1.7315	-toute7	0.0756	-0-0051	0.5920	0.270¢	0.3712	-1.7328 -1.8683		
Á	\$.72 13.77	U.J	1.0000	-3.0001	0142	0.6510	6.0011	U-6255	0.2553	0.3694	-2.0638		
16	27.44	r. 6	* . 1 vv 1	-0-0021	-4.0222	0.0545	6-012m	G-6367	0.3039	0.3328	-2.0529 -1.9415	-	
55	25.46	0.0	6.44 35	-11-4662	6.0292	-6.002A	Q.0239 Q.0152	0.5078	0.3449	0-2429	-1.7147		
					. 1								
									•				
		•				-						•	
						_							
											•		
•													
								•					

t i	OF 1		<u>selopmen</u> I	CENTERIA	EDC) P	PARTIN :	MISSILE TA	NEL FACIL	ITY(P=T). S DATA	AER(	DUYNAMIC	HIND TUNNEL (ATS
	1551	PART =	ALW 9111	6 Pn1	LONE	l of		DEL3 DEL	4 TRANSTE	TON	·	
	5		10 2.5		3.0F32 0		0. 0		0 FRE			
INT		WFTA	CAF1	CHI	Ce)	#CPF1	YCPF1	CNF2	CHZ	C82	XCPFZ	YCPFZ
2	-1-51 -0.40	- <u>Lav</u>	-0-1:13 -0-1:13	=1-11u1	-0.0027	C.83.5	3.4407	-0.5169 5.6u32	-0-0000			-0.4479
3	0.50	0.0	0.0031	-6-06-5	-0-0257	-5.7544	-71-0000	0.0037 		0.0071	0.0728	
•	1.57	6.6	0.006	-6.0003	-0.6097	-0.2564	-10.8444	0.0536	0.0140	0.0179	0.2608	0.3340
5	2.60	0.0				0.0021	5.7619	0-0807.	0-0215	0-0287	0.2700	4.3560
6	3.62 5.55	0.0	-0.001u		-6.0194	-0.0673	9.0769	0-1158	0-058+	0.0439	0.2450	0.3769
<del></del>	4.7€	0.0	-0-1115			0.7366		0.3860	0.0576	0.1663	0.1544	0.4309
•	13.77	0.3					-1-4951	-0.5913		-0.2549	0.1194	
G	17.54	6.6		-0-001-		0.9126		9.7802	0.0674	0.3325	0.0464	0.4262
11 <u></u>	25.46			-0-1015 -0-1035	<u>-6-6</u> 10 <b>03</b> .		2.7358 0.0128	1.0935	0_959 <b>6</b> 0_0666	0.4596	0.0603	<del>8.426</del>
13	27.E7	0.0		-0-1059		-0-71(5		1-1-1597		0.4851_		
					<del></del>				<del> </del>	· · · · · · · · · · · · · · · · · · ·		
									`			•
			<del></del>								<del></del>	
				-								
											<del></del>	
								-				
					<del> </del>							
					-							
				<del></del>				· · · · · · · · · · · · · · · · · · ·			<del></del>	·····
							•	····				
				<del></del>	<del></del>			<del></del>	<del> </del>		<del></del>	
							<del></del>	<del></del> -			·	
						·						· · · · · · · · · · · · · · · · · · ·
												<del></del>

)£	ENGINES 3 OF 3 1 GF 1		MELOPMENI	CENTERLA	EUC) PI		<u>mind Tum</u> Issile ta			AEM(	DIMANYO	IND TUNNEL	(AT)
			ein dille 10 2.5		CONF		1_LEL2		TRANSITO FRE				
1 mil	ALF#4	FFTA	( F3	Chs	Eu3	YCot 3	YCPF 3	C+F4	· CHA	CR4	XCPF4	YCPF4	. 🔟
2	-0.48	0.0	-( . UII 37	-1.5131 -7.55005	<u> </u>	<u> </u>	-0-1-01 -0-0595	0.0024	0.4003	-0.0131 -0.0039	0.1464	-1.631A	
<u>.                                    </u>	6.50	0.0	-0-00-6	-363-	3 ئايدىلىم ئا	. Lalbre .	-0.2044	0-6241	_0.0041_	0.0005_	0-2874	_0.2318	
4	1.57	0.0		-1.006	1.000	0-1364	-0.0636	0-(527	0.0151	0.0177	0.2866	0.3365	
<del>-</del> -	7.06 7.72	0.0		-1.0007	C_0CC1 C_0C11	0.1-63	-0.1276 -0.1254	0.1112		0.0305	0.2598	0.3 <u>869</u>	
<u>"                                    </u>	5.05	0.0	ei die		in the day	C-1813	-0-1336	3-1897	3-7404	0.0256	0.2159	0.4577	
•	4.72	0.0		1215	ROUVES	6.1016	-9.2A53	0.3730	0.0551	0.1797	0.1609	0-480R	-
<u> </u>	_13.77	0.4		سخيده مناهب				<u> </u>		0.2762	-0-1261	. 0-4871	
1 5	17.54	ύ υ		-0-0305	17.0016 *1016	4-0658	-0.2755 9001-0-	0.7541 0.0374	0.0560 0.0677_	0.3626 8008	0.0876	0.4808	
12	25.00	U a ti		-:-:01:	0.0028	0.09-5	-0.2679	1.0509	C.v657	0.4971	0.0625	0.4730	
13	27.87		-:-:111	ويبنيه: -	0-0631	4072	-0-2765	1-1267	6-0651	0.5271	0.0581	0-4743	
							·						
										· · · · · · · · · · · · · · · · · · ·			
						<del></del>					- 12.		
													<del></del>
					·	<del></del>	~	<del></del>					·····
	_										<del></del>	<del></del>	<del> </del>

. . . . .

_ ____

								<u> </u>					
						<u> </u>							
ijE į	LHSINEE 2 OF 3 1 OF 1		<u>Vel Opvē</u> at.	Chalthia	EUC)P			NEL FACIL		AER	DIMANIC	LIND TUNNEL C	<b>^u</b>
						L DELI	DEL2.	DEL3 DEL					
		110 1.	ê. 2.5	(,) P	3=0F32 0	0.0	0		0 F#E	E			
I T	ALPHA	GFTA ( . G	CNF3	Cn1	cħ1 "	ACPF1 =0.3280	YCPF1	CHF2		C95	XCPF2	YCPF2	4
>	-0.47	0.0	-0-0145		-0.0042		0.9422		-0-0050	-0.0016		-0.3529	
<b>.</b>	9-51	يامي	<u> </u>			_=C.2E30_				_ 0.0477.			
<b>.</b>	1.55 2.62	0.0	-0-0044	_ <del>r=30nz</del> 	-0.0104 -0.0006		+551+5 +54 <b>E</b> + <b>L</b>	0.0554 0.651_	0.0107 6-6177	0.01AZ 0296	0-1934 	0.3290 <u>0.3474</u>	
	3.04	(I . V	-0.0.45		0073		1.5156	6.11**	0.0739	0.0448	0.2019	0.3780	
	5.00	لتمنا	-0-4653	6.3505	-0-6:75	-5-16-1	1514121	0-1855	4-2356	0-0766	0-1877	SA0A_0	
4 0	9.7t	() . () () . ()	-v.o.71	0.0067		-6-1013	1.1646	0.3597	0.0542	0-1568	0.1-67	0.4240	
	19.05	0.0	-00000		-0-000	# <u>#1455</u> 0.3695	1.5576	3.7515	6-0714	0.3195	0.0950	0.4250	
1	20.27	u_e		-4.4.031				0.5220			0.0797	0.4207	
2	25.82	0.0	-0-0-1-		-0.0uñ1	0.2532	5.1519	1-017-	6-0532	0.4271	0.0621.		
3	28.16	C-E	<u> </u>		(-0113		0-4721	1.4853	3.0667	0.4547	0.0559	0.4189	
		_							•				
		<del></del>											
	_												_
					•	-							
							· · · · · · · · · · · · · · · · · · ·			-			
										•			
			<del></del>										
													•
											· · · · · · · · · · · · · · · · · · ·		

SE .	3 OF 3		WEL OPHE T	CENTERIA	EDC) P		ISSILE TA			AER	DOYNAMIC	=1ND TUNNEL (AT)
EET_J	1 OF 1									•		
-			rica Bilba				L UELZ					
	5		2.5		3.0532 0		0 D		O FRE			
01-1	ALPMA	ee T A	CAF3	CH3	CH3	#CPF3	YCPF3	CVF4	CH4	C#4	XCPF4	YCPF4
<u>-</u>	-C.44	( • U	=0.00 <i>n</i> 2	6.0135	u.cae3	-u.0725	-v.0423	0.0055 -0-1344	-0.0097	-0.0035	-0.5302 -0.3886	-0.7102
ــــــــــــــــــــــــــــــــــــــ	0.57		-Labore	حنافشما	_C.uucl		-520-02		2.0055_	0.4070_		0.2416
•	1.55	6.0	-0.0002	0.3005	0.0005			0-0541	0.0115	0.0196	0.2119	0.3624
<u> </u>	3.64	6. Ú	-0-0043 -0-0045		0.0005 0.0009	-0.6569 -0.2762		0-0822_	C.US+8 	0.0318	0.2239	0.4161
<u> </u>	5.66	Lau	=0.0072	Ochid	0.030F		-3-23-9	0-1470	C-1361	. 0.0836	0.1432	0.4472
P	4.70	ů.ů	-0.0017	-4003	0.JUZ7	P. G. 36	-0.3804	0.3545	0.6535	0.1711	0.1487	0.4760
¥	13.56	<u> </u>	-0-00-u	6-000=		-0-1456		0.5e6x_	_ £500.0	.0.2623		
10	20.27	0.0	-0.0051 -0.0051	0.0001		-0.010/ -5.0586		0.7294 0.8027	0.0706 	0.3489 .0.4798	0.0968	0.4784
15	25.52	0.0	-0.00-1	0.6004		-0-0-75		0.9884	U.0605	0.4666	0.0612	0.4721
13	24.14	_لنون	-0.6265	24,205		-0-10-5		1-4636	0.663		-0.0578	0.4684
					· <del>-</del>							<del></del>
			<del></del>									
<del></del>												
												<u> </u>
												· · · · · · · · · · · · · · · · · · ·
				·····				<del> </del>	<u></u>		<del></del> -	
-												

	EMGLMELE 1 OF 3		<del>YELOPHEN</del> 1	CENTERIAL	nc) b		AIND THE			AFR	OUYNAMIC -IMO TUNNE	LIATI
	G I	<del></del>			<del></del>						<del></del>	
								<del></del>		<del></del>		
			3. 5.5		CUSE 0		1. DEL2 . 1	EL3 DEL4				
PaT	ALPRA	êF TA	C٧	CLH	CY.	CL V	CLL	CA	CL9	CAF	ACP	<del></del>
	-1.44	4-4	-2-1736	1.22	<u> Cacilai</u>	-tauatta		0.5659	0.2061	0.357A	-1-2915	
	-0.46 2.56	liels Felt	-6.0737	0 = (.044		-6.0457	-0.0053 -3-0054	0.5624 	0.7C73 _0.2071		-1.3750	
	1.56	0.0	(-21c2			-0.04ul		0.5625	0.2059 		-1-1435 -1-2583	<del></del>
	_ قمعی_	C.O	5.3055	-C. 901		-0555	-0-0029	0.5017	0_2064	. 0-4550	-1-3572	
•	3,44 5,64	l e il	0.5749 - C-554	-0.7/45		-0.0479 -0.0474	-0.0016	0.5507 	0-2135		-1.4615 -1.6259	
	ÿ.76	6.0		-3.2521		-0.0332	0.0021	0.6057	0.2363		-1.82+3	
	14.42	O.v	3.6412	-0.5100	0-4136	-0-2313	0.0654	_ G.0045_	0.2642	0.3603	-1.4091	
)	14.15	0 . u		-7.:1326 -1.:5043		-7-1100	2.0110	0.5971	0.2575		-1.6660	
2	25.35	U . G		-4-5561	. 1016.00		0.0134	<del></del>	_ <del></del>		-1.5821 -1.3586	
	28.30			حداثثثناء		C 0279	1450-0	_0.6055	0.3294		-1-2931	
						_						
			·····									
											· · · · · · · · · · · · · · · · · · ·	
			<del></del>		<del></del>							
			<del></del>			<del></del>	<del></del>					
		<del></del>										
										<del></del>		
											•	
			<b>.</b>									
											·····	<del></del> -
											· <del></del>	
												-

	ENGINEE		VELOPPE .1	CENTENCE	éuCì P		R_WIND.TUN			AEnc	DYNAMIC	MIND TUNNEL (AT)	
	1 OF 1	· .	···										
	7E \$1		ACH 2110-		C)NF		1 DEL2		A JRANSIT				
GINT'	ALPHA	PETA	CNF3	Cr3	C#3	XCPF3	YCPF3	CNF4	CH4 =0.0061	CR4 -0-0161	XCPF4	YCPF4 9-6945	
ž	-0.46 0.56	(.0	-0.0010	-6.0016	0.0075 5210.0	1.7171		7000-0	0.0010	-0.0062	1.3562	-8.5205 .0.1573	40
•	1.5e	0.U		-4-0245		4-6173	-7.6421 -2.5556		0.01+0 0.01+0	0.0156 0.02 <del>06</del>	0.2458 0.2587	0.3189 0.3774	
<u> </u>	3.64 5.64	0-1	-0.0715	-1.006.1	2.0020	0.2967 0.2560	-0.8799	0.1045	0.0255	0.0438	0.2347	0.4039	
4 9 17	9.76 16.02 18.18	6.0 - 5.0 1.00	-0.0945 -0.095 -0.096	\$200-0- \$200-0- \$2000-0-	7.0031 		-0.6416 -0.5663 -0.5154	0.3393 0.5132 0.6794	0.7509 0590_ 0.0607	0.1593 0.2430 0.3200	0.1500 - 0.1149 0.0893	0.4695 	
11	25.45	C.0	-0.00-6	-0-000v	0.0451	0.6240	-1.0159	0.7590 0.4140	0.0561 0.0561	0.4315	0.0012	0.4710	
13	2H.36	G. H	<u> </u>	कुर्गाएक		<u>=11 . 11 4 3 7</u>	-1.15-9	4,4906	11-2544	0-A55A	0-0555	0.4645	
										·····	·		
				· · · ·		<del></del>		<del> </del>					
							•					<del></del>	
				······································								<u> </u>	
				<del></del>		<del></del>							
				<u></u>									
						-							
	<del> </del>						<del></del>						
												·	

						· · · · · · · · · · · · · · · · · · ·						
							-	· · · · · · · · · · · · · · · · · · ·				
			-		<del></del>	<del></del>						
OLD	ENGINEL	RING DEVE	OPMENT C	ENTERCAED	C) PROP	ULSION WIND TUN	HEL FACILITY	(PHI)	AERODYNAMIC_FINO_TUNNEL(AT			
	1 OF 1				74	RT14 MISSILE TA SPLITTER PL	ATE DATA					
									•			
				· <del></del>	<del></del>				<del></del>			
		_PAPİ_PAC				<del></del>			· · · · · · · · · · · · · · · · · · ·			
	2	153 0-80	2.5	F14 F	REE				•			
DINT		CNF	CH	Co		YCPF						
그		<u>-0.466</u>			-0.0293							
2	-1.00	-0-0242	0.0011		-0.0451 0.1463	0.5373 1.5491						
	1.00		-0.4005		-0.0312	0.4043	<del></del>					
5	2.03	0.0445	0-0465	0-0194	0.0173	0.8573						
6	2.98		-0.0005		-0.0094	0.4964						
	6.06	0.0713	-0.9014		-0.0095 -0.0100	0.4959						
8 9	5-06		-0-0019			0.4603 						
10	10.05		-0.0027	0.1152	-0.0100	0.4290			<u>, , , , , , , , , , , , , , , , , , , </u>			
11	12.04		-0-0046	0.1391	-0.6139	0.3965			· · · · · · · · · · · · · · · · · · ·			
12	14.78		-0.0052		-0.0122	0.3814						
<del>_13</del> _	16.09 18.11		-0.0u44 -0.0u37		-0.0063	0.3630	<del></del>					
14 15	20-17		-0.0037			0.3933						
16	22.15		-0.6015		-0.0019	0.3317						
17	24.16		0.4420	0.2/65	0-0024	0.3231						
18	26.20	0.43#4				0.3167						
19	27.21	0.4004	0-6050	0-3102	0.0351	0.3105						
								_				
							11-2					
		<del></del> -						·				
	_	•										
		<del></del>						<del></del>				
		•										
							****					
				·								
							<del></del>					
									<del></del>			

Ł	ENGINE 1 OF 1 OF	1	NG LEVE	LOPMENT C	ENTERLAED		PTIN MISSILE	UNIEL FACILITY! TAIL EFFECTS DA PLATE DATA	
								•	
	TE:		ART MAC		CONF. IRAN	SITION			
INT			CNF	Cn	Ch		YCPF	· · · · · · · · · · · · · · · · · · ·	
<u> </u>	28.1	3	1.0076	0.0064	0.3300	0-0061	0.3149		
5	29.1		1.0425	0.0059	0.3421	0.0063	0.3132		
3	30-1/		1.1246	0.0102	0.3603	0.0072	0.3106		
\$	31.10		1.1000	0-0126	0.3670	0.0106	0.3119		
6	33.1	9	1.leoz	0.0260	0.3596	0.0168	0.3031		
7_	34.1	۸	1-1980	0.0357	0.3.150	0.0311	0-2918		
A	36.1		1.0651	0.0317	0.2072	0.0315	0.2857		
9 10	35.13 40.1		1.0656 0.7546	-0.0006	<u>0.257a</u> 0.2911	-0.0306 -0.0007	0.2861 0.3049 .		
11	42.1		6.9632	-0.000B	0.2951		0.3064		
15	***1	b	6. 4044	-0.0045	0.30-3	-0.0046	0.3089		
13	40-1		1-6311	-0.4466 <u>-</u>	<u> </u>	-D-005B	0-3086		
14 15	48.1 50.1		1.0167	-0.0046	0.3136	-0.6069	0.3103		_
16	1.58		1.0341	-0.u141	0.3544	-0.0117 -0.0136	0.3109		
il .	54.1			-0-6104	0.3305		0-3150		
18	56.1			-0.0194	0.3357	-0.0182	0.3158	•	
19	57.1	6	1-0051	-0-0202		-0.0190	0.3172		
						. <del></del>	<del></del>		
-	900					<del></del>			
		_				<del> </del>		<del></del>	
					-				
						·		<del></del>	
				· · · · · · · · · · · · · · · · · · ·				<del></del>	
									•

Æ	ENGINEER 1 OF 1 1 OF 1		LOPMENT C	ENTERCAED		TIN MISS	ID JUNNEL FACILITY ILE TAIL EFFECTS ( IER PLATE DATA	DATA	AERODYNAMIC WING TUMMEL (AT)
	TEST	125 0-80	<u> </u>		51110M				
DINT	ALPHA	CNF	Ch	Ch		YCPF		<del></del>	
2	58-11 54-12	1.0375	-0.0214		-0.0184	0.3186			
3_	60.05	1.0456	-0.0217 -0.0217		-0.0223	0.3192			•
•	41.12	1.0467	-0.0252	6.3376	-0.0241	0.3219			
_5	67.14	1.0567	-0.0249		-0-0268 -0-0282	0.3216			
7	69-15	1.0505	3650-0-		-0.0249	0.3220			
8	66.14	1.0007			-0.030B	0.3270			
9	_69.1i		-0-1354		0 - 0 3 3 1	0-3293			
10	70-11	1.0693			-0.0358	0.3308			
11	72 <u>-14</u> 74-14	1.0727 1.0F3u	-0-U-10.		-0-0382 -0-0413	0.3338			
13	75-17		-0-0-6-		-0-0446	0.3382			
14	78.15	1.0735	-0.0527	0.3724	-0.0482	0.3404			
15		lalu3&_			-0-0522	0.3426			
16	47.14 54.16		-0.0627 -0.4659		-0.0595	0.3437			
16	66.17		-0.0709		-0.0545	0.3496		· <del>-</del>	
19	87.20		-0-0718		-0.0659	0.3514			
	7.7.1			_					
			<del></del>				<del> </del>		
	_								
							<del></del>		
							<del></del>		
								<del></del>	
					<del></del>		<del></del>	<u></u>	
		<del></del>							
									•
		·					<u> </u>		
	·								

E	ENGINEE 1 OF 1 1 OF 1		OPHENT C	enieh Laed	MA	JLSION WIND TUNNEL FACILITY (PWT) RTIN #ISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYMAHIC UNIN JUNNELSATA
		<u> </u>					
<del></del>	TEST	PART MACE	2.5		SITION		
	ALPHA	CNF	CH	Ce		YCPF	·
1	90.08		-0-0768		-0-0741		
2	41.05	1.0325	-0.4740	0.3674	-0.0766	0.3559	
3	92.09		-0-0-21	0.3056_	-0-0802	0.3573	<del></del>
5	44-08		-0.0856 -0.0856		-0.036 -0.0556	0.3574	
6	96.00	1.0139	-1.0959		-0.0945	0.3619	
1	49-12		-0-1423		-0-1024	0.3657	
6	100-11		-0.1090		-0-1340	0.3688	
9	102.12		-0-1164 -0-1204		-0-1165 -0-1211	0.3675	
ŭ_	106.11		-0-1256		-0.1263	0.3683	
12	108.16	6.9911	-0-1243	0.3669	-0.1705	0.3702	
13_	110-11	0.4016	-0-1314		-0-1339	0.3717	
14 15	112.16	0.4059	-0.1357 -0.1369	0.3049	-0.1372 -0.1400	0.3701 8.3691	1
6	116.11		-0.1379	0.3636	-0.14]1	0.3722	
17	117-13			0.3581	-0-1-24		
		<u> </u>					
					- — <del>-</del> -	<del>-</del>	•
			<del></del>				
		<del></del>	~ <del></del>				
					-		
			<del></del>		<del></del>		
		-	-				
					<del></del>		•
=							<del></del>
						<del></del>	

	Enginee 1 of 1 1 of 1					UISIGN AIND TUNNEL FACILITY (PWT)  RTIN MISSILE TAIL EFFECTS DATA  SPLITTER PLATE DATA	AERODYNAMIC.WIMO.TUNNEL(AT)
	······································	<del></del> _					·
	1ESI	PART PAC		CUNE TRA	REE		•
NT.	ALPHA	CHF	CH	C4		YCPF	
	118-02				-0-1440		
	119.05		-0-1366		-0.1452 0.1456		
	121.06	0.9434	-0.1377	0.3455	-0.1459	0.3660	
	122.05				0.1064		
	123.04		-0-1376 -0-1368		-0.1467 -0.1468	0.3620	
	126.05	1134.0	-0.137U	0.3352	-0-1-76	0.3612	
	128-05			0.3309	-0-1482		
	130.03		-0.1346		-0.1463	0.3608	
	134.10		-r.1342		-0.1499	0.3610	
_	136.09	0.8466	-0.1350	0.3212	-0-1503_	0.3577	- M- C - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
	136.07	0-0720	-0.1343	0.3201	-0,1505 -0,1512	0.3588	_
	142.12	0.000	-0.1354	0-3169	-0.1531	0.3582	
	144.09	0.0765	-0.1364	3.3146	-0-1579	0.3589	
	146.11	0.0009	-0-1-14	. 0.3102	-0.1643	0.3602	•
	19/119	0.839.1	-11-19-13		-0.1683	9. 1he i	
							· · · · · · · · · · · · · · · · · · ·
_							
		:					
						•	
_							

GE	Enginee 1 of 1 1 of 1		LOPHE HI_CE	NTER (AFU	C1PROPI	ILSION MIND TUNNEL FACILITY (PMT) RTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYMANIC WIND TUNNEL 1471
			·				•
			H RXIG-6				
	5	128 0.68	2.3	F14 F	REE		
THIO	· ALPHA	CNF	CH	Ce	X CPF	YCPF .	
<u> </u>	148-01		-C-1349		-0-1640	0.3626	<del></del>
2	149.01 150.01		-0.13Y2 -0.1379		-0.1703 -0.1726	0.3649	
_J	151.03	0./e71	-0.1329		-0.1733	0.3636	
<u>.</u>	152.04		-0-1282		-0-1740	0.3626	
6	153.01	0.7053	-0.1242	0.2554	-0.1761	0.3622	
	154-01	0-6701	-0-1199		-0-1789	0.3661	
A	156.01	0.0215	-0.1164		-0.1476	0.3656	
_ <del>_9</del>	159.03	0.5159	-0-1129 -0-112e	0.1749	-0-1997 -0-2187	0.3760	··
11	165-05		-0-11-9	0.1826		0.3898	•
12	164.02	0.4026			-0.2669	0.4079	
13	166-02		-0-1403		-0.2901	0.4278	
1.	160,03		-llevehé		-0.3074	0.4226	•
.15	170-05		-0-1736		-0.3231	0.4254	
16	177.05		-0.0584 -0.0421		~0.3379 -0.3494	0.4255 8.4179	
18	176.00		-0.0261		-0.3601	0.4065	
19	177-05		-0-0190		-0.3541	9-4063	
		7,17-					
							•
							***************************************
				-	· · · · · · · · · · · · · · · · · · ·		
						<del></del>	
			<del></del>				
			·			<del></del>	

				•			<del></del>	· · · · · · · · · · · · · · · · · · ·		,	·	
			<del></del>	·	<del></del>			·		·		<u>.</u>
			<u> </u>	<del></del>								_
KOLO	ENGINEE 1 OF 1	ring Weve	LOPMENT C	ENILUI ALD	C) PRUP	ULSION MINO.	IUNNEL FACI	LITY(PHT)	AERODYMAMI	C -IND TUNNE	LIATI	
	1 0f 1					SPLITTER	PLATE DATA			·-···	<u></u>	
	TESI	PART PAL 130 1-10	# RX10=6	CONF TRAM	SITION			<del></del>	-			
	ALPHA	CNF					• • • • • • • • • • • • • • • • • • • •				•	
701741			CH 0-0437		-0-070a	YCPF 0-4091				·	<u></u>	
2	-0-37	-0.0265	0.0020		-0-0734	0.3473					•	•
3	1.03	0-0151	-0.0010		-0.1412	0.5928		<del></del>	······································			
. 5	2.04	<u> </u>	-0-0415	0.0101	-0.0393	0-4617						
6	3.02		-0.0030		-0.0470 -0.0365	0.4673				•		
	6.06		-0.0072		-0.0480	0.4356		<del></del>		•		
9	A. 05	0.215a	-0-0099	_0_0+28_	0-0458	0.4300						
10 _11	10.09		-0.01-7 -0.0176		-0.0486 -0.0481	0.4096						
12	14.09		-0.0216		-0.0484	0.3846						-
13	15ale		-0-0245	6-1773	-0.0469	0.3770				<del></del>		
14 15	1ª.12 20.20		-0.0263 -0.0318		-0.0467 -0.0460	0.3650 0.3696						
16	22.17		-0.0326		-0.0419	0.3393		-				
17	29.29				0-0373	0.3313						
18	26.23	0.4325	-0.0327		-0.0349 -0.0342	0.3264						
					4117							
					<del> </del>	<del></del>						
			·	•			<del></del>		<del> </del>			
		<u> </u>	· · · · · ·		<u> </u>							
										•		
						<del></del>						
				•	•							
					·						•	_
						·			<del> </del>			
										<del></del>		

ET	1 OF- 1				MAI	TIN MISSIL	E TAIL EFFE	CTS DATA			
. <del></del>	1 OF 1					SPLITTE	R PLATE DAT	[ <b>A</b>			
					•			<del></del>			
	IESI S	PART -AC 131 1-10	M_RX10-6	CONF. THAN	HEE			-		-	
INT .	ALPHA	CNF	CH	Cs		YCPF					
1	29.16		-0.0342		-0.0338	0.3246					
5			0	6.3503	-0.0328						
4	31.20		-0.0355 -0.0375		-0.0325 0.0325	0.3235					
5	32.19		-0.037#		-0.0319				<del></del>		
7	34.20	1.2203	-0-4386	0.3910	-0.030A					·	
8	36.22		-0.V3Mn Ud£v.0-		-0.0302	0.3164 2.3147					
0	40.24	1.3137	-0.0190	0.4606	-0.0144	0.3049			_	-	
12	44.22		-0.0080		-0.0061	0-3003					<del></del>
3	46.24	1.4527	-0.003b	0.4084	-0.002B	0.3019					
l • l 5	48.26 50.25		-0.0200		-0.0197 -0.0220	0.3114 0.3152					
16	52.3C	1.3774	-0.0342	0.4372	-0.0248	0.3174			,	· ·	
17	56.3U		-0.0371		-0-0267	0.3212	<del></del>				
ف ا					-0-0277		<u> </u>				
								·			
						<del></del>					
											•
	•			•							
					-			············			
		<u>.                                    </u>								<del> </del>	<del> </del>
									· · · · · · · · · · · · · · · · · · ·		

Ε	ENGINEED 1 OF 1 1 OF 1		LOPALNI C	<u>ENTER (ALD</u>	M &	ULSION WIND TUNNEL FACILITY (PWT). HTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	TA)CHIW_CINANYCORRAL
	TESI	PAPT MAC	M_RA10-6_	COVE TRAN	SIT104		
	5	137 1.10			REE		
INT	ALPHA	CNF	CH	Сн		YCPF	
<u></u>	59.17	1.3585	-0.03 <u>00</u> -0.0344		-0.0284	0.3206	<del></del>
š	60.10		0.4411.		0.0299_		•
•	61-17		-0.0420		-0.0304	0.3229	
5 5	63.10		9a4+31_ -0.0+53		-0.0310 -0.0325	0.3246	
	64.17	1.3754			-0.0323	0-3744	
	66.21		-0.0501		-0.0354	0.3264	
	50.20		<u>-0.0525</u>		-0.0369	0.3300	
0	70.20		-0.0561		-0.0391	0.3315	
<u>5</u>	74.21		<u>-0.0594</u> -0.0634		-0.0414_ -0.0441	0.3340	
3		1.9394			-0.0469	0.3368	
4	75.23		-0.0705		-0.0491	0.3378	<u> </u>
<b>5</b>	80.26		-0-07.15		-0.0516	0.3347	
6 7	82.25		-5.0765 -0.0500		-0.053B	0.3411	
6	86.25		-0.0033		-0.0591	0.3448	
9	B7.27		-0.0859		-0-0612	0.3647	<u></u>
	-						
		<del></del> -	<del> </del>				
		· <del>- · ·</del> -	<del></del>				
	<del></del> -						
			<u> </u>				
			-				
							•

				<del> · ·</del>						<del></del>	
	ENGINEE		LOPHENT	ENTERLAEL	C) PROP	ULSION HIN	LE TAIL EFF	CILITY(PMI)	L	erodynamic wi	O TUNNEL (AT)
	OF I					SPLITI	R. PLATE DA	TA			
		1									
	TEST	133 1-14 133 1-14	N PA10-5.	CU:4F TRAM	REE		· · · · · · · · · · · · · · · · · · ·		<del></del>		
-	ALPHA	CNF	CH	Cr		YCPF		<del> </del>			
) T	90-13		-0.4939		-0-0582	0.3464					
	91.12	1.3770	-0.0477	0.4784	-0.0710	0.3473				· · · · · · · · · · · · · · · · · · ·	
	92.13	1.3700	-0-1000		-0.0726	0.3499					
	93.14 - 94.14		-0.1045 -0.1043		-0.0757 -0.0784	0.3504					•
	96.13		-0-1177	0.4921	-0.0×42	0.3520				<del></del>	······································
	98.14	1.4486	-1-1264	0.4960	-0-0898	0-3523			·		
	100.14		-0.1330		-0.0942	0.3542					
	102-15 104-16		-1 <u>-1395</u> -0 <u>-1443</u>		-0-0986 -0-1021	0.3560					
	106.24		-0-1461			0.3553				•	
	108.20		-0.1512		-0.1074	0.3576					
	110-19		-0-1554	0.5033	-0.1103	0.1571		<b></b>			
	112.17		-0.1583	U.5648	-0-1125	0.3586					
	114.22	1 2152	-0.1625 -0.1656	0.5(31	-0.1156_ -0.1176	0.3565				<del></del>	
	117.24	1-4052	-0-1663	0.5026	-0-1163	0.3576					
	88.10	1.3e39	-0.0062	0.4769	-0.0637	0.3446					
	89.14	1.3502	-0-0-09	0-4772	-0-0659	0.3458	····	<del></del>			· · · · · · · · · · · · · · · · · · ·
		<del></del>						<del></del>			
_											<del> </del>
							· <del></del>				
						<del></del>					
						•					
_										·	
		-							- <del></del>		
								<del></del>			

GE	1 OF 1 OF	a l	TWO NEAF	LOPHEMT CI	THIEK (ARD)		ULSION WIND T PTIN MISSILE SPLITTER			AERODYNAMIC AINO TUNNE	
			-								
			134 1.10	<u>  0-510-6</u>		SITIUN					
											30
OINT	ALPH 118-0		CNF	CH -0.1671	C4	-0-1180	YCPF 0-3566	- 6	* *		AP.
<del></del>	115.3		1.4146			+0-1187	0.3545				
3	120.0	7	1.4069	-0.1076	0.4996	-0-1190	0.3546				
4	121.1	0	1.4052	-0.1075	0.4467	-0.1192	0.3549				
. 5	122-0		_latut2	-0-1640	0.4975	0-1200	0.3534	<del></del>			
•	123.4			-2-1667		-0-1202	0.3531				
-	126.1			-0-1045 -0-1646		-0.120B -0.1225	0.3521				<del></del>
9	128.1			-0-1704		-0.1244	0.3524				
10	130.1			-0.1007		-0.1236	0.3516				
11	132.1	6 _	1.3944	-0-16/1		£e12e3	0.4517				
12	134.			-0.1657		-0.1259	0.3510				
13	135-1			-0-1663		-0-1295	0.3527				
14 15	138.1			-0.1676 -0.1655		-0.1339 	0-3551				
16	142.			-0.1574		-0.1430	0.3536				
17	1444			-0.1666		-0-1499	0-3572				
18	146.	16	1.0573	-0.1657	0.3413	-0.1567	0.3607				
19	197.	16_	1.4421	-0.1640	<u> </u>	-0.1604	0.3626				
									-		
	-										
								.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
				<del></del>							
		•								·····	
							•				
						<del></del>	·		<del></del>		
	*										
				-							
10											

135 1.  2 1.016 1 0.900 2 0.904 0 0.909 2 0.815 4 0.837 1 0.804 1 0.703 1 9.501 3 0.615 1 0.538	CM RX10-6 10 2.5 CM 7 -0.1549 e -0.1530 0 -0.1563 4 -0.1563 4 -0.1536 3 -0.1515 5 -0.1655 6 -0.1577 0 -0.1477 0 -0.1358	Cd 0.3671 0.3549 0.3520 0.3320 0.3379 0.2775 0.2775 0.2754	#EE #CPF -0.1522 -0.1062 -0.1702 -0.1701	0.3677 0.3699 0.3843				,	
2 1.016 1 0.900 2 0.904 0 0.909 2 0.815 4 0.837 1 0.804 1 0.703 1 0.015 3 0.015 1 0.538	7 -0.1049 e -0.1030 0 -0.1006 2 -0.1563 9 -0.1563 4 -0.1536 3 -0.1555 5 -0.1055 6 -0.1577 3 -0.1477	0.3671 0.3509 0.3020 0.3320 0.3079 0.3079 0.2575 0.2566	-0.1522 -0.1062 -0.1702 -0.1701 -0.1701 -0.1835 -0.1846 -0.2163	0.3610 0.3610 0.3620 0.3652 0.3658 0.3677 0.3699					
1 0.900 2 0.904 0 0.909 2 0.815 1 0.804 1 0.703 1 0.015 3 0.015 1 0.538 1 0.466	e -0.1530 0 -0.1563 2 -0.1563 9 -0.1563 4 -0.1536 3 -0.1515 5 -0.1655 6 -0.1577 3 -0.1477	0.35-9 0.3-26 0.3320 0.3079 0.3079 0.2575 0.2534	-0.1062 -0.1702 -0.1701 -0.1707 -0.1835 -0.1886 -0.2169	0.3610 0.3629 0.3652 0.3658 0.3677 0.3699				,	
2 0.994 0 0.909 2 0.815 4 0.837 1 0.814 1 0.703 1 0.891 1 0.615 1 0.518 2 0.466	0 =0.1508 2 =0.1563 9 =0.1563 4 =0.1536 3 =0.1515 5 =0.1655 6 =0.1577 3 =0.1477	0.3:26 0.3:20 0.3:20 0.3:79 0.3:79 0.2:75 0.2:34	-0.1702 -0.1701 -0.1707 -0.1835 -0.1846 -0.2163	0.3629 0.3652 0.3658 0.3677 0.3699 0.3843					
0 0.909 2 0.815 4 0.837 1 0.804 1 0.703 1 0.615 3 0.615 4 0.538 2 0.466	2 -0.15k3 9 -0.1563 4 -0.1536 3 -0.1515 5 -0.1655 6 -0.1577 3 -0.1477	0.3320 0.3079 0.3079 0.2575 0.2534	-0.1741 -0.1747 -0.1835 -0.1846 -0.2163	0.3652 0.3658 0.3677 0.3699 0.3843					
2 0.8/5 4 0.837 1 0.844 1 0.703 1 0.951 3 0.015 4 0.538 2 0.466	9 -0.1563 4 -0.1536 3 -0.1515 5 -0.1655 6 -0.1677 3 -0.1477	0.3251 0.3279 0.2575 0.2534 0.2666	-G.1747 -0.1835 -0.1984 -0.2163	0.3658 0.3677 0.3699 0.3843			··		
4 0.837 1 0.844 1 0.753 1 0.653 3 0.615 4 0.538 2 0.466	4 -0.1536 3 -0.1515 5 -0.1655 6 -0.1577 3 -0.1477	0.3079 0.2575 0.2534 0.2565	-0.1835 -0.1886 -0.2169	0.3677 0.3699 0.3843	-				
0.7n3 0.651 0.615 0.615 0.616	5 -0.1655 6 -0.1577 3 -0.1477	0.2434 0.2666	-0.2169	0.3843 -					
0.651 0.615 4 0.538 2 0.466	8 -0.1577 3 -0.1477	0-2065							
3 0.615 4 0.538 2 0.466	3 -0.1477		-0.2279						
2 0.466		0-2360							
2 0.466	0 -0-1358		-0.2400	0.3836		•			
			0.2523_	0-3864	<del></del>	<del></del>			
	5 -0.123m	0.1790	-0.2651	0.3833					
24540 0	1 -0-1105	1509	<u>-0.2197</u>	0.3819	<del></del> -				
5 0.322	-0.0947	0-1227	-0.2937	0.3805					
					•				
0 0.469	1 -0-0307	0.0253	-0.3450		·			<del></del> -	
						·			
								<u> </u>	
				· · · · · · · · · · · · · · · · · · ·	•••				
							:		
	0.176 0.136 0.089	0.1964 -0.0640 0.1382 -0.0468 0.0691 -0.0307	0.1764 -0.0640 0.0730 0.1382 -0.0468 0.0470 0.0691 -0.0307 0.0253	0.01387 -0.0468 0.0470 -0.3387	0.1764 -0.0640 0.0730 -0.3758 0.3716 0.1387 -0.4468 0.0470 -0.3387 0.3397	0.1764 -0.0640 0.0730 -0.3758 0.3716 0.01387 -0.0468 0.0470 -0.3387 0.3397 0.0891 -0.0307 0.0253 -0.3450 0.2840	0.1764 -0.0640 0.0730 -0.3758 0.3716 0.0.1387 -0.0468 0.0470 -0.3387 0.3397 0.0891 -0.0307 0.0253 -0.3450 0.2840	0 0.1964 -0.0640 0.0730 -0.3758 0.3716 0 0.1382 -0.0468 0.0470 -0.3387 0.3397 0 0.0591 -0.0307 0.0253 -0.3450 0.2848	0 0.1964 -0.0640 0.0730 -0.3758 0.3716 0 0.1387 -0.0468 0.0470 -0.3387 0.3397 0 0.0591 -0.0307 0.0253 -0.3450 0.2840

Æ	1 OF 1		ar mill		MA	HTIN MISSIL	E TAIL EFFECTS DATA	AERODYNAMIC - IND TUNNEL (AT)
	IEST	PART MAC 137 1.30			SITION			
OĨŃT	ALPHA	CNF	Сн	Сы	, 'XCPF			
7	-2.01 -1.01	-0.4324 -0.102	-0.0000	-0.0260	0.0601	1-2522	<del></del>	
3	-0-01	0-0153	-0.0000			-0-3171		
•	1.01	0.0351	-0.0027		-0.6778	0.1694		
<u> </u>		0.0001	-0.0050		-0.0915 .		<del></del>	
6	3.03	0.4646	-0.0ubl	0.0264	-0.0685	0.3201		
		0.1173	-0-00-		-0-0683	0-3671	<del></del>	
*	6.04		-0.0099		-0.0574	0.3844		
9			-0.0133		-0.0557	0.385A	<del></del>	
10 11	10.98		-0.0167 -0.0200		-0.0538 -0.0523	0.3723 2045.0		
12	14.13		-0.0217		-0.0480	0.3561		
13	16-15		-0-0256		-D-GAR5	_0-3431		
14	18.17		-0-4540		-0.0465	0.3337		···
15.	20.19		-0.u309	U-2224	-0.0453	0.3260		
16	22.22		-0.0310		-0.0409	0.3207		•
17	24.23		<u>-0.1317</u>		-0.0380	0.3167		
18	26.28	0-9695			-0.0375	0.3130		
19	27.30	O-Assh	-0-0347	0.2457	-0,036B			
					·			
						<del></del>		
			<del></del>					
			<del> </del>					
						·	•	
						<u></u>		
								-

GE	ENGINEE! 1 OF 1 1 OF 1	ING DEVE	LOPMENT CI	NIEH LAED	MA	RTIN MISSILE	TUNNEL FACILITY (PWT) TAIL EFFECTS DATA PLATE DATA	AEHODYMAHIC. HIND. TUNNEL (AT)
			•				. <u> </u>	
			H PA10-6			<del></del>		
	5	130 1.30		F14 F	HEE			
POINT	ALPHA	CNF	C+-	Co		YCPF		
2	20.19	1.0046	-0.0375		-0-0379	0.3123		
3	29.15 30.17	1-0470	-0.0375 -0.0376		-0.0373 	0.3124		
4	31.16	1.0716	-0.0309		-0.0363	0.3106		
. 5	32.17	1.1013	-0.3391	3.3425	-0-1355	0-3110		
•	33.10		-0.0343		-0.0340	0.3134	•	
7	34.29		-0 <u>-0397</u> -0.0393		-0.0342	0-3111		
9	35.20		-0.0393		-0-0302			
10	40.24		-0.0315		-0.0246	0.3083		
11	42.24	1.6784	-0.0000		-0.0204	0.3082		
15	44.76		-0.0261		-0.0515	0.3100		
13	48.30		<u>-0_6245</u> -0_0308		-0.0229	0.3124		
15	50-29			9-4-44	8450-0-			
16	52.30	1.3007	-0.0436	0.4365	-0.0321	0.3208		
_17	59.39	1.3/47.	-0.0474		-0.0344	0.3220		
18	56.35		-0.0560		-0.0358	0.3233		
19	3/4.13	1.4044	-0.0500	2.4560	-0.0356	D.3246		
			<u> </u>					
			•		_			
		<del></del>					<del> </del>	
		•						
	•							
							•	
						<del></del>		
	· · · · · · · · · · · · · · · · · · ·						<del></del>	
			-					
								<del></del>

	1 OF 1			<u></u>	MA(	RTIN MISSILE SPLIITER	TAIL EFFECTS DATA PLATE DATA	
				•				
	tesi_	PART HAC	н RX19-6_3	CUNF IRAN	SITION			
	2	139 1.30	2.5		REE		1	•
POTNT	ALPHA	CNF	CH	C:	the ACOF	TCPF	न्हें। केंद्रे	4,1 46
<u> </u>	SA-IB	1-3/55	-0-0045		-0-0469	0.3302		
2	59.16	1.3073	-0.0623		-0.0451 -0.0436	0.3314 0.3316		
-	61.19	1.3413	-0.0610		-0-0438	0.3310		
	62.21	1.3766	-0-0621	_0.40+1_	0.0445	0.3324		
6	63.20		-0.0659		-0.0468	0.3314		
	64.22		<u>-0-uo75</u>		-0-0474	0-3316	<del> </del>	<del></del>
	66.23 68.21		-0.0051 -0.0051		-0.0450 -0.0437	0.3315		
10	70.26		-0.0674		-0.0-58	0.3316		
-ii	_72.25		-0-0691		0.0466	0-3325		·
12	74.26		-0.0699		-0.0470	0.3333		
13	76.27		-0.u723		-0-0484	.0.3354		
10	78.25 80.28		-0.0/33		-0.0443	0.3361 .		
15	<u> </u>				-0.0526 -0.0546	0-3367 0-3393	<del></del>	
17	84.28		-U-U-5H		-0-0575	0.3388		
18	86.30		-0.0297		-0.0599	0.3401		
_19	A7.32	1.4414	-0-0403	u-5399	-0.0505	0.3413		
	•						•	
	<del></del>		<del></del>					
	•							
			•					
		_				· · · · · · · · · · · · · · · · · · ·		
					<del></del>	<del></del>		
			•					
	- <del>-</del>		<del></del>			<del></del>	<del></del>	
							•	

				<del></del>							
										•	
OLD_I	OF 1	RING DEVE	LDP4ERI_C	ENTLYCAE	MA	TIN MISSILE	TAIL EFFECT	IS DATA		C MIND TUNNELL	<u> </u>
Eİ	1_0F_1					SPLITTER	PLATE DATA				
			·					<u> </u>			
	7557	PART MAC	w Deln-4	COUF TRA	LETTION				•		
	5	140 1.30			FHEE		-				
INT	ALPHA	CNF	Сн	C=	xCPF	YCPF	<del></del>				· · · · · · · · · · · · · · · · · ·
1	90.16	1.4085	-0-0434	0.5055	-0-0636	0.3442					
2 3	91.15 92.15		-0.0951 -0.0991		-0.0651	0.3457					
٨	93.14	1.4627	-0.1035	6.5162	-0.0707	0.3474					
5	96.16		-0.1116		-0.0726 -0.0761	0.3499					<del></del>
7	48-10	1.4464	-0-1165		-0.0506	0.3527					
	100-16		-n-125A		-0.0578	0.3544	•				
	192.17		-0-1357 -0-1410		-0.0946 -0.0980	0.3577					<del></del>
1	106.20	1.4333	-0.1465	0.5157	-0-1022	0-3598					
	100-21		-0.1529 -0.1576		-0.1066	0.3610					
	112.24		-6.1606		-0.1125	0.3612		·			•
	114-22			172 د ن	-0.1148	0.3625		<del> </del>			
	116:24	1.4216	-0.1565		-0.1171 -0.1189	0.3625					
					341		•				
			•					<del></del>	<del></del>		
<u> </u>						······································	·	<del> </del>			
				·		· · · · · · · · · · · · · · · · · · ·				<del></del>	
											<u> </u>
		_				·					
						•					
					<del></del>					<del></del>	
			<del></del>	·	•	***************************************		<del></del>		<del></del>	
				<del></del>			<del></del>				
									•		
	· · · · · · · · · · · · · · · · · · ·	<del></del>									
							<del></del>				

šĒ.	ENGINEE 1 OF 1 1 OF 1		<u>LOPMENT : CI</u>	entep (aed)	**A	ULSION WIND 1U RTIN PISSILE T SPLITIER P	AIL EFFECTS DATA	AERODYNAMIC WIND TU	NNEL (AT)
		· · · · · · · · · · · · · · · · · · ·	· · · · · ·						
		FART MAL	H_RX10-6.		SITION				
•	2	141 1.30	2.5	F14 P	HEE				
INY	ALPHA	CNF	Сн	CH	. XCPF	YCPF	<b>≱.</b> ≥		نهة ب
1	115.08		-0-1064		-C.1163	D-3616			
S	119.09	1-4006	-0-1673	0.5072	-0.1195	0.3621			
<u>.                                    </u>	120-14	1.3087	-0-1 <u>006</u> -0-1689		-0.1216	0.3610			
5	121.10		-0.1684 -0.1684	0.5009		0.3619			•
6	123.00	1.3730	-0.1696	0.4467	-0.1236	0.3617			· · · · · · · · · · · · · · · · · · ·
7	124.10	1.4650	-0-1791	0.4935	-0.1246	0.3615			
ь	126-15	1.3-46	-0-1646		-0.1257	0.3610			
<u> </u>	125-13		<u>-0.1693</u>		0.1270	B ₄ 3599	- <del> </del>	<del></del>	
0	130.10		-0.1677		-6.1278	0.3593	•		
5	134.14	1.297		0.4539	-0.1296 -0.1266	0.3582 0.3581			<del></del>
3	136-19	1.2336		0.4407	-0.1320	0.3573			
•	136.15	1,2017			-0.1344	0.3588		· · · · · · · · · · · · · · · · · · ·	
15	140-17		-0-1005		-9-1373	0.3560			
16	147.16		-0.1576		-0.1+0+	0.3606		_	
17	144-15		-0.1567	0.3473 0.3678	-0-1-55	0.3598			···-
18 19	146.18		-0.1545 -0.1538		-0.1512	0.3599 0.3597	,		
	-171445	647733	-01122					· · · · · · · · · · · · · · · · · · ·	····
								<del></del>	
					<del></del>				
						<del></del>			
			<del></del> -					<del></del>	
								•	
								·	

	ENGINEE 1 OF 1 1 OF 1	PING DEVE	LOPMENT CI	ENIER (AED	C) PRUPI	ATIN MIS	IND TUNNEL FACILITY (PHT) AERODYNAMIC WIND TUNNEL (AT) SILE TAIL EFFECTS DATA TIEM PLATE DATA	
	TEST	PAPT MAG 142 1.30	H_R110-6		SITION			
NT	ALPHA	CNF	CH	Co		YCPF	•	
	148-01				-0-1675			
?	149.03	0.7004	-0.1070	0.3560	-0.1698	0.3622	•	
		0.9>6E_	-0-1059	0-3-56	D-1733			
	151.01		-0-167A			0.3607		
					0 <u>1895</u>			
					-0-1582			
	156.02	0.7440	-0.1469	0.2/22	-0.1974	0.3658		
	154-02	0.6690	-0.1389	0.2952	-0-2068	0.3665		
)	160.04	6.5492	-0.130M	0-21+0	-0.2183	0.3571		
<u></u>	162-04	0.5247	<u>-0.1205</u>	7-1998	-0.2296.	_0-3601_		
2	164.08	0.4544	-0.1102	0-1014	-0.2425	0.3553		
	168.10	0.3-43	=0 044H	<u></u>	-0.2552	0.3489	······································	
					-0.2808			
	172.68	0.2036	-0.0549	0.0656	-0.2940	0.3219		
7	174.10	0.1463	-0.4440	4-0-25	-0.3007	0.2883		
В	176.1	0.0975	-0.0291	9.0209	-0.2990	0.2133		
9	177.15	0. u737	-0-0212	4-0143	-0-2473	0-1948	<del> </del>	
							•	
			<del></del>					
				•		•		
-								
							•	
			<del></del>	<del></del>				

I_	ALPHA	<u> </u>					LE TAIL EFFECTS DAT ER PLATE DATA		
	TES 2	PART MAC	n 0410-4				LO. PLAIR WAIR.		
	ALPHA	143 1.3u	- D-1A-4						
	ALPHA	143 1434	Z KYTRSE		SITION			<del></del>	
	ALPHA					<u> </u>			
		CNF	CH	Ca		FYCPF			
	179-02		-0.0175		-0.2788				
	179.00	0.0471	-0.ulln		-0.2514 -0.1486	0.066B			
	180.94	0.0060		-0.0150	0.3278	-2.4818	·····		<del></del>
<b>)</b>	182.01			-0-0519		1.0066			
	183.02			-0.0296		0.8986			
		-0-0551	Oaye35	-0.0.394	-0.4329	0.7153			
		-0.1v52		-0.6549		0.5689			
		-0.15he	0.0233		-0-3365	0.5080			<del></del>
		-0.2152		-0.1026		0.4778			
-		<u>-0.275a</u> -0.3+21		<del>-U_1279</del> -U-1520		0.4637			
		-0.3421 -0.4817		-0.1520		0-6367			
		-0.5544		-6-2357		0.4251			
	202.11	-0.0204	U.1328	-0.2532	-0-2121	0.4204			
	204.09	-0.7005		-4.2094		6-4153			
<u>'                                     </u>	205.14	-6-7734	0-1489	-C-3185	-0.1927	0.4120			
	207.12	-0. ouf 1	0.1519	-0.329#	-0.1850	0.4081			
			<del></del>					<del></del> -	<del></del>
									•
								***************************************	
_									
				<u> </u>					
							•		
		<del></del>		·	····	<del></del>	<del></del>	<del></del>	
							-		
					<del></del>				· · · · · · · · · · · · · · · · · · ·
								-	
									•
_									

Ε [	1 OF 1	iii_Ui, EZ	LUPALNY C	ENIEHLAED	C) PROPI	411V MISS	ND TUNNEL FAC ILE TAIL EFFE IER PLATE DAT	CTS DATA			IND TUNNEL (AT
· <u>·</u>	IESI	PAPT PAC	H 9X10-6	CONF TRAN	SITION					•	
	e	144 1.26	2.5	F14 F	REE						
INT'	ALPHA	CNF	CH	Ce		YCPF					
2	-2.92	-n.0019	-0.0016	-0.0117	0.0399	6.1737					
	-0.00		-0.0052		-0.1504 ·	0.1426	<del> </del>			<del></del>	
<u> </u>	1.03		-0-4460		-0-1105 -0-0459	0.1028			· - · · · - · -		
•	3.01		-0.0073		-0.0765	0.3096					
,	6.03		-0.utet		-0.0700	0.3673					·
	8.00			4-0908		0.3615	<del></del>		<del></del>		- <del></del>
) L	10.08		-0.0170 -0.0213		-0.0533 -0.0536	0.3681					
2	14.14		-0.0234		-0.0497	0.3477					
•	16.13		-0.0262		-0-0451	0.3368					
5	20.20			0.2327		0.3278				<del></del>	
6 7	27.23 24.22		-0.0346 -0.0348		-0.0435	0.3199					
8	26.26		-0.0355 -0.0373		-0.0377 -0.0379	0.3123	•				
¥	21.25		*U = U 3 / 3	Healiso	-0.01/9.	O-TIDA			<del></del>		
		<del> </del>									
					·						
		· · · · · · · · · · · · · · · · · · ·				<del></del>	<del></del>	<del></del>			<del></del>
							•				
								·			
										<del></del>	

Ł	1 OF	1	LOPMENT CE	MILRIAED		RTIY MISSILE T	ALL EFFECTS DATA	AERODYNAMIC HIND TUNNEL (AT)
EI_	1 OF	1				SPLITTER P	LATE DATA	
	TES	I PART MAC	H RE10-6 (	CONF TRAM	SITION			
	ž	145 1024	2.5		REE			
DÎNT'	ALPHA	CNF	Cn	Co	* KCPF	YCPF	٠, ن	·
1	26.14	1.0003	-0-0375		-0-0375	0.3123		
5	29.10		-0.0390		-0.0376	0.3098		
3	_30.15		-0-0399		-0.0369	0.3094		· · · · · · · · · · · · · · · · · · ·
•	31.16		-0.0399		-0.0363	0.3113		
5	32-17		-0-0-03			0.3105		····
6	33.16		-0.3410		-0.0353	0.3106		
<del>/</del>	36.2		-0-3415 -0.0423		-0.0346 -0.0339	0.3106	<del></del>	
0	30.2		-0-0-20		-0.0334	0.3098		
10	40.20		-0.03-3		-0.0261	0.3063	····	
1 1	42.24		-0-0350		-0.0211	0-3031		
2	44.2		-0.0233		-0.0174	0.3012		
13	46.29		-0-022h		-0.0166	0-3031		
1+	48.2		-0.0259		-0.0167	0.3054		
is	50.3		-0.0329		-0.0236	0.3132		
16	57.70	1,3001	-0.u461	0.4370	-0.0334	0.3166		
17	54.3		-0.6463		-0.0345_	0.3706		
16	56.3		-0.0511		-0.0361	0.3210	•	
19	57.3	3 1.425E	-0.4522	Cassia	-0-0366	0.3222	<del></del>	
						<del></del>		
					•			
								······································
								•
					<del>~</del>			
					<del> </del>			
		<del></del>						

1 58.19 1.4173 -0.0539 0.4585 -0.0380 0.3235 2 59.20 1.4263 -0.0541 0.4001 -0.0379 0.3226 3 60.19 1.4252 -0.0533 0.4018 -0.0376 0.3259 4 61.21 1.4162 -0.0533 0.4018 -0.0376 0.3256 5 62.21 1.4150 -0.056 6.4627 -0.0393 0.3278 6 63.22 1.4150 -0.0599 0.4666 -0.0417 0.3290 7 64.21 1.4150 -0.0629 0.4665 0.3300 9 68.23 1.4553 -0.060 0.4755 -0.061 0.3310 9 68.23 1.4653 -0.060 0.4755 -0.061 0.3330 10 70.22 1.4504 -0.099 0.4664 -0.0479 0.3354 1 72.25 1.4568 -0.0735 0.4664 -0.0597 0.3355 2 74.24 1.4631 -0.0771 0.4921 -0.0527 0.3363 3 76.26 1.4720 -6.0805 6.4827 -0.0551 0.3371 4 78.25 1.4768 -0.0714 0.4921 -0.0557 0.3371 5 80.25 1.4768 -0.0714 0.4964 -0.0557 0.3371 6 82.25 1.4768 -0.0714 0.4967 -0.0551 0.3377 7 84.30 1.4708 -0.0675 6.5025 -0.0579 0.3391 7 84.30 1.4708 -0.0675 6.5025 -0.0579 0.3391 7 84.30 1.4708 -0.0675 6.5025 -0.0579 0.3391 7 84.30 1.4708 -0.0675 6.5025 -0.0579 0.3391 7 84.30 1.4708 -0.0675 6.5025 -0.0579 0.3391	E	1 OF 1	PIRG DESE	COPALI			ULSION AIND TUNNEL FACILITY (PHT). 471N MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	- AEROVINARIL - TINO TORRECTELL
01NT ALPMA CMF CM CH CH CH XCPF VCCF  1 58-19 1-173 -0.0549								
1 58.19 1.4173 -0.6539 0.4585 -0.0380 0.3226 2 59.20 1.4263 -0.0541 0.4601 -0.0379 0.3226 3 60.19 1.4252 -0.4025 0.4665 -0.0368 0.3259 4 61.21 1.4162 -0.0533 0.4018 -0.0376 0.3256 5 62.21 1.4154 -0.0536 0.4627 -0.0393 0.3278 6 63.22 1.4154 -0.0596 0.4665 -0.0417 0.3296 7 64.21 1.4154 -0.059 0.4666 -0.0417 0.3296 8 66.22 1.4330 -0.0462 0.4755 -0.0461 0.3316 9 68.23 1.4553 -0.01629 0.4659 -0.0461 0.3316 9 68.23 1.4553 -0.0462 0.4755 -0.0461 0.3316 10 70.22 1.4560 -0.0595 0.4664 -0.0479 0.3355 11 72.25 1.4560 -0.0735 3.4847 -0.0550 0.3355 12 74.24 1.4531 -0.0771 0.4921 -0.0527 0.3363 13 76.26 1.4120 -0.0805 0.4762 -0.0547 0.3377 14 78.25 1.468 -0.013 0.4072 -0.0547 0.3377 15 80.25 1.4754 -0.0830 0.5084 -0.0565 0.3377 16 82.25 1.4754 -0.0830 0.5084 -0.0565 0.3377 17 84.30 1.4108 -0.0755 0.5055 -0.0579 0.3391 17 84.30 1.4108 -0.0755 0.5055 -0.0595 0.3317 18 86.26 1.4576 -0.0761 0.4950 -0.0618 0.3420								
2 59.20 1.4263 -0.0561 0.4061 -0.0379 0.3226 3 60.19 1.4262 -0.41225 1.4985 -0.0368 0.3259 4 61.21 1.4162 -0.0533 3.4018 -0.0376 0.3256 5 62.21 1.4159 -0.0556 0.4627 -0.0393 0.3278 6 63.22 1.4159 -0.0560 0.4666 -0.0417 0.3296 7 64.21 1.4159 -0.1629 0.4666 -0.0417 0.3296 8 66.22 1.4330 -0.0600 0.4755 -0.0661 0.3310 9 68.23 1.4551 -0.0760 0.4755 -0.0661 0.3310 9 68.23 1.4551 -0.0765 0.4864 -0.0498 0.3356 10 70.22 1.4504 -0.0955 0.4864 -0.0479 0.3356 11 72.25 1.4504 -0.0713 3.4887 -0.0504 0.3355 12 74.24 1.4031 -0.0771 0.4921 -0.0527 0.3363 13 76.26 1.420 -0.0805 0.4862 -0.0547 0.3371 14 78.25 1.408 -0.0714 0.4971 0.4371 0.3377 15 60.25 1.4164 -0.0746 0.5057 0.3391 16 82.25 1.4164 -0.075 0.5025 -0.0579 0.3391 17 84.30 1.4088 -0.075 0.5025 -0.0579 0.3391 18 86.26 1.4576 -0.0761 0.4464 -0.0618 0.3420 19 87.31 1.4958 -0.0914 0.4496 -0.0618 0.3420	THIO							
3 60.19 1.4252 + C.4025	<del>-</del> -							
5 62.21 1.4154 -0.4356	_ā	60.19	1.4252	-04025		-0.0368	0.3259	····
6 63.22 1.4124 -0.0709 0.4046 -0.0417 0.3290 7 64.21 1.4156 -0.01529 0.4059 -0.6465 0.3300 8 66.22 1.4330 -0.0460 0.4755 -0.0461 0.3318 9 68.23 1.4453 -0.0076 0.4075 0.4085 0.3330 10 70.22 1.4504 -0.0095 0.4804 -0.079 0.3354 11 72.25 1.4504 -0.0735 0.4087 -0.0527 0.3355 12 74.24 1.4031 -0.0771 0.4921 -0.0527 0.3363 13 76.26 1.4120 -0.0005 0.402 -0.0547 0.3371 14 78.25 1.4768 -0.0714 0.492 -0.0547 0.3377 15 80.25 1.4758 -0.0716 0.4908 -0.0563 0.3394 16 82.25 1.4718 -0.0075 0.5025 -0.0579 0.3391 17 84.30 1.4708 -0.0075 0.5025 -0.0579 0.3391 18 86.26 1.4576 -0.0716 0.496 -0.0618 0.320	•							
7 66.21 1.4156 -0.0529 0.4645 0.3300 8 66.22 1.4330 -0.060 0.4755 -0.0661 0.3318 9 68.23 1.453 -0.0050 0.4843 -0.0688 0.3330 10 70.22 1.4504 -0.095 0.4864 -0.0504 0.3354 11 72.25 1.4560 -0.0735 0.4867 -0.0504 0.3355 12 74.24 1.4631 -0.0771 0.4921 -0.0527 0.3363 13 76.26 1.420 -0.005 0.442 -0.6547 0.3371 14 76.25 1.4768 -0.014 0.4907 -0.0551 0.3377 15 80.25 1.4754 +0.0830 0.5088 -0.6563 0.3394 16 82.25 1.4516 -0.0750 0.5025 -0.0579 0.3391 17 84.30 1.4708 -0.0875 0.5025 -0.0579 0.3391 18 86.26 1.4576 -0.0961 0.4964 -0.0618 0.3428 19 87.31 1.4459 -0.0910 0.4964 -0.0618 0.3428	6							<del></del>
6 66.22 1.4330 -0.0460 0.4755 -0.0461 0.3318 9 68.23 1.4451 -0.046 0.4813 -0.0468 0.3338 10 70.22 1.4504 -0.0475 0.4847 -0.0504 0.3354 11 72.25 1.4508 -0.0715 0.4847 -0.0504 0.3355 12 74.24 1.4031 -0.071 0.4921 -0.0527 0.3363 13 76.26 1.4120 -0.0805 0.4462 -0.0547 0.3371 14 78.25 1.4768 -0.014 0.4947 -0.0551 0.3377 15 60.25 1.4754 -0.0839 0.5008 -0.0563 0.3394 16 82.25 1.416 -0.0839 0.5008 -0.0563 0.3391 17 84.30 1.4708 -0.0275 0.5025 -0.0595 0.3417 18 86.26 1.4574 -0.946 0.4464 -0.0618 0.3420 19 67.31 1.4550 -0.0414 0.4954 -0.0618 0.3420	ĭ				-			
10 70.22 1.0504 -0.0095 0.0804 -0.0079 0.3356 11 72.25 1.0508 -0.0735 0.0807 -0.0508 0.3355 12 74.24 1.0031 -0.0771 0.0921 -0.0527 0.3363 13 76.26 1.0120 -0.0805 0.00402 -0.0547 0.3371 14 78.25 1.0708 -0.0014 0.0007 0.0551 0.3377 15 80.25 1.0150 -0.0030 0.5008 -0.0563 0.3394 16 82.25 1.0016 -0.0007 0.5025 -0.0579 0.3391 17 84.30 1.0708 -0.0075 0.5025 -0.0595 0.3417 18 86.26 1.0074 -0.0010 0.0006 0.3020 19 87.31 1.0050 -0.0010 0.0070 -0.0633 0.3040		66.22			0.4755	-0.0-61	0.3318	
11 72.25								
12 74.24 1.4631 -0.4711 0.4921 -0.0527 0.3363 13 76.26 1.4/20 -0.0805 0.4462 -0.6547 0.3371 14 78.25 1.4768 -0.0814 0.4967 -0.0551 0.3377 15 80.25 1.4/55 -0.0830 0.5028 -0.0579 0.3394 16 82.25 1.4616 -0.0856 0.5025 -0.0579 0.3391 17 84.30 1.4708 -0.0875 0.5025 -0.0595 0.3417 18 86.26 1.4576 -0.7461 0.4964 -0.0618 0.3420 19 87.31 1.4950 -0.0914 0.4970 -0.0633 0.3440								
14 76.25 1.4768 -0.0514 0.4767 -0.0551 0.3377 15 80.25 1.4754 -0.0530 0.5008 -0.0563 0.3394 16 82.25 1.4616 -0.0555 0.0575 -0.0579 0.3391 17 84.30 1.4708 -0.0675 0.5025 -0.0595 0.3417 18 86.26 1.4574 -0.7401 0.4764 -0.0618 0.3420 19 87.31 1.4450 -0.0716 0.4770 -0.0633 0.3440								
15 80.25 1.415 -0.0030 0.5008 -0.0563 0.3394 16 82.25 1.416 -0.000 0.5025 -0.0579 0.3391 17 84.30 1.4708 -0.0075 0.5025 -0.0595 0.3417 18 86.26 1.4576 -0.0401 0.4464 -0.0618 0.3420 19 87.31 1.4450 -0.0416 0.4470 -0.0633 0.3440								
16 82.25 1.4616 -0.0000 0.5025 -0.0579 0.3391 17 84.30 1.4708 -0.0075 0.5025 -0.0595 0.3417 18 86.26 1.4576 -0.0401 0.4464 -0.0618 0.3420 19 87.31 1.4450 -0.0416 0.4470 -0.0633 0.3440								
17 84.30 1.4708 -0.0275 0.5025 -0.0595 0.3417 18 86.26 1.4576 -0.7401 0.4464 -0.0618 0.3420 19 87.31 1.4450 -0.0416 0.4470 -0.0633 0.3440								
19 67-31 1-4-50 -0.0914 0-4970 -0.0633 0-3440								<u> </u>
								•
	19	87.31	1.4950	-0.0914	0.4970	-0.0633	0.3440	
							·	
						<u> </u>		
				<del></del>				
								<del></del>

GE	1 OF 1	PING DEVEL	<u>OPHENJ</u> (	ENTERIAE		ULSION WIND TUNNEL FACILITY(PHT) HTI - MISSILE TAIL EFFECTS DATA	AERODYNAMIC HIND TUNNEL (AT)
EET	10E1					SPLITTER PLATE DATA	
					<del></del>		
		PART PACE					
3 m. 4	5	147 1.26	2.5	F14	FREE		
THIO	ALPHA	CNF	CH	CH	ACP+	YCPF	
<u> </u>	89.13	1.4467	-0.099A	0.4958		0.3470	· · · · · · · · · · · · · · · · · · ·
3	90.10	1.9407	-0-1 000		-D-0743	0.3484	
•	41.20	1.4215		0.4477		0.3501	
<u>-</u> -	93.14	1.4146	-0.1156	0.4961		0.350A	<del></del>
7	94.15		-0.1221	0-5000		0.1533	
8	46.18	1.4217	-0-1295	0.5021	-0.0912	0.3532	
	_95.1à	1.4252			-0.0763	0.3540	
10 11	106.19		-0.1509		-0.1010 -0.1050	0.3560 0.3576	
15	104.20	1.4-06	-0.1347		-0.1073	0.3591	
13	106.10	1.4426	-0.1500	<u> </u>	-0.1399	0.3589	
14	104.18		-0.1021		-0.1128 -0.1151	0.3589 0.3581	
16	112.22		-0.1063 -0.1695		-0.1173	0.3587	<del></del>
_i7	114.24		-0-1707		-0.1146	0.3602	
18	116.27	1.4316	-0-1726		-0.1205	0.3590	
19	117,29		0_1/39	0-5129	-0-1217_	0.3590	<del></del>
							•
			·				<del></del>
				•			
		-					
<del></del>							
			<del>* • • • • • • • • • • • • • • • • • • •</del>			17,	
				<u>-                                    </u>			
						· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
						•	

				<del> </del>					
		ING HEVE	LOPMENT C	ENTER LAED	C) PROP	LSION NIND TUN	VEL FACILITY (PET)	AERODYNAMIC MIN	D TUNNEL CATE
	1 OF 1						IL EFFECTS DATA		
						· ·			
	TEST	PAPT MAG	- PX10-6.	CONF TRAN	SITION				-
	5	108 1.20			REE			•	
	ALPHA	CNF	CH	Cr		YCPF			
	118.09 119.05		-u_1726 -0_1718	0.5173	-0.1194	0.3567		<del></del>	
	120.09		-0-1713		-0.1192	0.3542			
	121-13		-0.1699		-0-1184	0.3548		•	
	122-14	1.4140		C-5027		0.3516 0.3526			
	124-06	1.9116		6-9487		0.3534			
	126.12		-0.1002	6.4725	-0-1207	0.3534			
	120.12		-0.1071		-0.1212	0.3521			
	130.13		-0.1647 -0.1625		-0.1209	0.3508			
2	134.14		-0.1028		-0.1248	0.3513	·, · · · · · · · · · · · · · · · · · ·	<del></del>	
3_	136.12		-0.1660		-0-1296	0.3528			
14	136.16		-0.1n75		-0.13-1	0.3549			_
15	142.14		-0.1661 -0.1638		<u>-0.1377</u> -0.1431	0.3542			
17	196-13		_0021 <u>_0</u>		-0-1483	0.3549			
8	146.20	1.0197	-0.1568		-0.1538	0.3563			•
9	197.16	0.9761	-0.1573	0.3555	-0-1579	0.3569			
								•	
							•		
							<del></del>	···	
	<del></del>		<u> </u>					•	<del></del>
		<del></del>		<del> </del>		•	<del></del>		<del></del>
			······································			<del></del>			
			<del></del> -						

	ENGINE 1 OF 1 OF	1	YÉI	LUPSENT CI	LMIRH (AEU	PROP	ATIN MISSI	LE TAIL EFFECTS DATA  LE PLATE DATA	AEHODYNAMIC HIND TUNNEL (AT)
									··
	TES	T PART M	44	H_RX10-6	CUMP IRAN	SITION			
	2	1-9 1-	20	2.5		REE			
<u>.</u>	ALPHA	CNF	_	CH	CH	) <del>-</del>	YCPF		
~1	148.02			+0-1573	-	-0-1604	0.3589		
-	144.00			-0-1365	0.3431		0.3600		······································
	150.04			-0-1557		0.1555	0.3634		
	151.03			-0.15eA		-0.1732	0.3626		
	152.05			-0.1241		-0.1784	0.3506		
	153.03			-0.1673		-0-1932	0.3729		
_	154.03	0.531		-6-1050		-0.1953	0-3702		
_	150.00	0.756	H	-6-1574		-0.2074	0.3726		
				-0.1965		-0.2177	0.3734		
	160.0			-0-1384		-0.2277	0.3758	• •	
_	162.0			-0.1261		-0.2404	0.3703		
5	164.06			-0-1172	0-1/32	-0-2530	0.3739		<del></del>
_	166.05	0.393	16	-0-1647	0.1461	-0.2665	0.3718		
•	168.00	6.326	1	-0-0-19	0.1163	-0.2801	0.3607		
5	170.0			-0-0773	0-0420	-6.2534	0.3495		
ь	172.00			-0-0529		-0.3076	0.3378		
<u> </u>	174.10			-0-0463		0.3165	0-2947		
8	176-17			-0.0305		-0.3184	0.2530		
	<u> </u>	2 0.073	11	-0-0221	0.0167	-0-3019	0.2287		<del></del>
								<del></del>	
								<del></del>	
								<del></del>	
									<del></del>
									•
_			_		···			<del></del>	
							•		•
			_						
		<del></del>		<del></del>					
_		<del></del>					······································		

				· .							min says and	*. <del>.</del>
									<del></del>			
<del></del>		<del></del>	<del> </del>									
								•			·	
ADMOUNT	EAGTLE	DILE HEVE		ELTEDIALA	C) BOOK	111 STON N	TAN THRUEL E	ACILITYPHIL	AFPO	OYNAMIC MIND	TIMMEL (AT)	
PAGE	1 OF	l	<u>LVFAL:II_C</u>	-HILL LALL	4/	ATIN MIS	SILE TAIL EF	FECTS · DATA	ERV	DIMPLIA MINT.	IVANEL INII	
SHEET	1 OF	<del>1</del> -			<del></del>	SPLI	HER PLATE D	ATA			·	
				· · · · · · · · · · · · · · · · · · ·								
	756	T PART MAC	W DY10_4	COME TRAM	STTION							
	5	150 1.20	2.5		REE			· · · · · · · · · · · · · · · · · · ·				
POINT	ALPHA	-CNF	CH	Cr	I CO	YCPF						
1	178.01	0.0034	-0.0185	0.0114	-0.2936	0.1792						
. 2	179.01	0.452	-0.0117	0.0036 -0.0036	-0.2594	0.0830					•	•
•	161.01	0.0090	0.0024	-0.0132	0.2653	-1.4693					•	
<u> </u>		-0-0067 -0-0270	0.0092	-0.0185	-1-0564	2-1305 1-0511	···-	<del></del>		<del></del>		<del></del>
<u>;</u>	104.02	-0-0514	0.0242	-4-0370	-0.4713	0.7207						
a	186.01	-0-1006	0.0396	-0.0575	-0.3934	0.5721						
						***********	· · · · · · · · · · · · · · · · · · ·			<del></del>	· · · · · · · · · · · · · · · · · · ·	
							<del></del>		<del></del>			<del></del>
						•						
	-						<del></del>		<del></del>			
	<u> </u>	<del></del>						<del></del>	<del></del>			· <del></del>
									<del></del>			
							<del> </del>			<del></del>		
								•				
											· · · · · · · · · · · · · · · · · · ·	
		•										
						<del></del>		<del></del>				
					<del></del>							
										<del></del>		<del></del>
							•					•

11 12-11 6-3565 -0-0052 0-1473 -0-0146 6-4133 12 14-13 0-4352 -0-0000 0-1700 -0-0138 0-3905 13 16-16 0-5631 -0-3041 0-1416 -0-6081 0-3609 14 14-16 0-5667 -0-0024 0-2166 -0-0050 0-3626 15 20-16 0-6104 -0-0040 0-2375 -0-0060 0-3541 16 22-20 0-7637 -0-3017 0-2606 -0-0023 7-3412	GŁ	ENGINEE 1 OF 1 1 OF 1		LOPMENT C	ENTERCAED		HTIN MISS	NO TUNNEL FACILITY (PMT) ILE TAIL EFFECTS DATA IER PLATE DATA	AERODYNAMIC WIND TUNNEL (AT)
1 -2.08 -0.4877 C.0021 -0.0163 -0.0130 D.3409 2 -0.07 -0.02c 0.0008 -0.073 -0.0352 D.3265 3 -0.08 -0.02c 0.0077 0.0186 0.2004 3.013 5 -0.08 -0.02c 0.0017 0.0186 0.2004 3.013 5 -0.08 0.0007 0.0008 0.0357 0.0265 0.2041 0.2025 6 -0.05 0.0007 0.0008 0.0357 0.0161 0.7187 7 -0.07 0.0008 0.0357 0.0008 0.0355 0.0161 0.7187 9 -0.01 0.0160 0.0001 0.0716 -0.0056 0.5215 9 -0.08 0.1373 -0.0007 0.0716 -0.0056 0.5215 9 -0.08 0.1373 -0.0007 0.0716 -0.0056 0.5215 1 -0.11 0.215 -0.0002 0.1213 -0.0150 0.3302 1 -0.11 0.0 0.2015 -0.0002 0.1213 -0.0150 0.302 1 -0.11 0.0 0.2015 -0.0002 0.1700 -0.0136 0.302 1 -0.13 0.0352 -0.0000 0.1700 -0.0136 0.3005 1 -0.14 0.0513 -0.0000 0.1700 -0.0136 0.3005 1 -0.16 0.0513 -0.0000 0.1700 -0.0136 0.3005 1 -0.16 0.0503 -0.0000 0.1700 -0.0136 0.3006 1 -0.0007 -0.0007 -0.0007 0.2006 0.3026 1 -0.0007 -0.0007 -0.0007 0.0000 0.3006 1 -0.0007 -0.0007 -0.0007 0.0000 0.3006 1 -0.0007 -0.0007 -0.0007 0.0000 0.3006 1 -0.0007 -0.0007 -0.0007 0.3006 0.3006 1 -0.0007 -0.0007 0.0007 0.0007 0.3288 1 -0.0007 -0.0008 0.2007 0.3006 0.3008									
2 -0.97 -0.0cc 0.0008 -0.0073 -0.0352 0.3265 3 0.00 -0.0025 0.000	POINT		•						
3									· · · · · · · · · · · · · · · · · · ·
\$ 1.04 0.0162 0.0017 0.0260 0.0261 0.9265  \$ 2.05 0.027 0.0008 0.0359 0.0161 0.7187  7 4.07 0.0160 0.0001 0.0511 0.016 0.6325  \$ 6.00 0.1373 -0.007 0.716 -0.055 0.5215  9 8.08 0.2087 -0.002 0.1213 -0.0150 0.022  10 10.10 0.2214 -0.002 0.1213 -0.0150 0.002  11 12.11 0.3564 -0.0025 0.1213 -0.0150 0.302  12 14.13 0.3352 -0.0020 0.1700 -0.0136 0.3905  13 16.16 0.531 -0.3061 0.011 0.0010 0.3005  14 14.16 0.507 -0.0027 0.2126 -0.050 0.3266  15 22.20 0.7037 -0.0017 0.2086 -0.0023 3.3012  17 24.22 0.0526 0.005 0.3252 0.0005 0.3228  19 27.25 0.9997 0.3066 0.3178 0.0005 0.3228									
9 3.05 0.497 0.008 0.0354 0.0161 0.7167 7 4.07 0.0760 0.0001 0.0001 0.0016 0.6325 8 6.08 0.1373 -0.0007 0.0716 -0.0054 6.5215 9 8.08 0.2006 -0.0022 0.0006 -0.0123 -0.0150 0.4325 10 10.10 0.2019 -0.0022 0.1213 -0.0150 0.4302 11 12.11 0.3365 -0.0052 0.1473 -0.0146 0.4133 12 14.13 0.4352 -0.0000 0.1700 -0.0130 0.3905 13 16.16 0.5031 -0.0051 0.1716 -0.0050 0.3905 14 14.16 0.5031 -0.0027 0.2106 -0.0050 0.3626 15 20.16 0.0104 -0.0040 0.2275 -0.0060 0.3566 16 22.20 0.7637 -0.0017 0.2006 0.2033 3.3412 17 24.22 0.8526 0.0066 0.2202 0.0005 0.3228 18 76.25 0.7456 0.0005 0.3052 0.0005 0.3228 19 27.25 0.9077 0.3066 0.3178 0.0006 0.3211	•	1.04	0.0062		U-0186	0-2804	3.0113		
7									
8 6.00 0.1373 -0.007 0.0716 -0.0054 0.5215 9 E.06 0.4066 -0.0025 0.0046 -0.0123 0.4576 10 10.10 0.2014 -6.0042 0.1213 -0.0150 0.4302 11 12.11 0.3065 -0.0052 0.1713 -0.0146 0.4131 12 14.13 0.352 -0.0000 0.1700 -0.0138 0.3905 13 16.16 0.5031 -0.0040 0.116 0.4060 0.3905 14 14.16 0.5067 -0.0020 0.2106 -0.0050 0.3626 15 20.16 0.0070 -0.0040 0.2375 -0.0050 0.3526 16 22.20 0.7637 -0.0017 0.2606 -0.0023 3.3412 17 24.22 0.7657 0.0006 0.2402 0.0007 0.3288 18 76.25 0.9450 0.0006 0.2402 0.0006 0.3288 19 27.25 0.9697 0.3006 0.3178 0.0006 0.3211	_								
9									
10 10.10	_							•	
11 12.11	10								
12 14.13 0.4352 -0.0000 0.1700 -0.0130 0.3905 13 16.16 0.5031 -0.0012 0.1116 -0.0081 0.3609 14 14.16 0.5007 -0.0027 0.2106 -0.0050 0.3626 15 20.16 0.6704 -0.0040 0.22375 -0.0060 0.3561 16 22.20 0.7037 -0.0017 0.2606 -0.0023 3.3412 17 24.22 0.4526 0.0006 0.2242 0.0007 0.3286 18 76.25 0.9450 0.0005 0.3052 0.0005 0.3226 19 27.25 6.9097 0.3006 0.3178 0.0006 0.3211	11								
13 16.16 0.5031 =0.00e1 0.1v16 =0.0081 6.3608  14 14.16 0.5067 =0.0027 0.2106 =0.0050 0.3626  15 20.16 0.6104 =0.0040 0.2375 =0.0060 0.3541  16 22.20 0.7637 =0.0017 0.2606 =0.0023 0.3412  17 24.22 0.6526 0.006 0.2602 0.2007 0.3288  18 76.25 0.9456 0.0065 0.3052 0.0005 0.3228  19 27.25 0.9097 0.3066 0.3178 0.0006 0.3211	12								
15 20.16 C.0/04 -0.0040 0.2375 -0.0060 0.3561 16 22.20 0.7637 -0.0017 0.2606 -0.0023 3.3612 17 24.22 C.0026 0.2402 0.0007 0.3286 18 26.25 0.9454 0.0065 0.3052 0.0005 0.3228 19 27.25 G.9097 0.3066 C.3178 0.0006 C.3211	13								
16 22.24 0.7637 -6.3017 6.2606 -0.0023 3.3412 17 24.22 0.8526 0.006 0.2802 0.0007 0.3288 18 76.25 0.9454 0.0005 0.3052 0.0005 0.3228 19 27.25 6.9897 0.3066 0.3178 0.0006 0.3211	14	14.16	C->0G7	-0.0024			0.3626		
17 24.22 C.8526 O.Qu06 O.2F02 O.QU07 0.3288 18 76.25 C.9450 U.QU05 U.3U52 C.0U05 O.3228 19 27.25 G.9897 O.JU06 C.3178 O.QU06 G.3211	15								#
18 76.25 0.9454 0.0065 0.3052 0.0005 0.3228 19 27.25 6.9497 0.3066 0.3178 0.0066 0.3211	16								
19 27-25 G-9697 0-3006 C-3178 0-0006 G-3211	_17							······································	
				. VaJuud	1,93110	U a U I U II	Wa Well	<del></del>	Late Control
			***		<del></del>			<del></del>	
								· · · · · · · · · · · · · · · · · · ·	
					<del></del>				

	OF 1		LOPMENT C		MA	ULSION MIND TUNNEL FACIL PTIM MISSILE TAIL EFFECT SPLITTER PLATE DATA	E DATA	AERODYMANIC HIND TUNNEL (AT)
			<u> </u>	- ner			· .	
	7 <u>ES1</u>	156 0.83	2.5	Flo F	<u>ree</u>			
NT :	ALPHA	CNF	CH	Co		YC#F		
2	24.20	1.0773	0.0013		0.0013	0.3222	<del></del>	
3		1.1090						•
•	31.21	1.1.49	0.0035	0.3628	0.0031	0.3169		
5	32.21	1-1681	0.0057		0.0049			<u>-</u>
5	33.72	1.1791	0.0126	0.3044		0.3090		
<u>/</u>	30.22	0.9986	0.0326		0.0327	0.2693		
•	38.20	1.0167			0.0327	0-2944		
0 .	40.15		-0.0023	0.2454		0.3092		
i	42.19	0.9563	-0.4444	0.2785	-0-0046	0-3115		
5	44.20		-0.005A		-0.0060	0.3126		
3	45.21	0.9562	-0-00A3	1015	-0.0035			
5	48.21		-0.0100		-0.0101 -0.0125	0.3182		
5	52.24		-0.0155		-0.0150	0.3100		
7	54.25	1.0475	-0-217#	u. 3356	-0.0170	0-3204		
6	56.25	1.0677	-0-0208	0.3026	-0.0178 -0.0194	0.3209		
9	57.25	1.0710	-0.0212	0.3062	-0-0198	0.3233		
						· · · · · · · · · · · · · · · · · · ·		
					·	·		
			<u></u>					
		<del></del>		<del></del>			· · · · · · · · · · · · · · · · · · ·	
								·
					<del></del>			
								·
			_					
							<del></del>	
	•	•						
		··	<del></del>		<del></del>		<del> </del>	

JEST PART   PACH   PART   PACH   PARTITION	1 OF	1	)EAFT	OPMENT CI	ENTERCAED		ATIN MISS	ND TUNNEL FACILITY (PWT) ILE TAIL EFFECTS DATA IER PLATE DATA	AERDOYNAMIC FIND TUNNEL (41)
2 157 0.65 2.5 F14 FREE  INT ALPHA CNF CH CR XCPF YCPF  1 56.0B 1.0424 -0.0218 0.3039 -0.0208 0.3248  2 59.16 1.0433 -0.0218 0.3099 -0.0208 0.3249  3 59.17 1.0457 -0.0258 0.3249 -0.0224 0.3295  4 61.18 1.0457 -0.0258 0.3249 -0.0227 0.3289  5 62.18 1.0513 -0.0246 0.3247 -0.0272 0.3298  6 63.16 1.0592 -0.0311 0.3296 -0.0297 0.3301  7 64.17 1.0393 -0.0315 0.3296 -0.0297 0.3305  8 66.18 1.0602 -0.0328 0.3557 -0.0399 0.3355  9 68.18 1.0616 -0.0350 0.3564 -0.0399 0.3355  9 68.18 1.0616 -0.0373 (0.3593 -0.0351 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.3366 0.33									
INT ALPMA   CNF   CM   CR   XCPF   YCPF     58.08   1.0428   -0.0218   0.3897   -0.0195   0.3248     59.16   1.0493   -0.0218   0.3809   -0.0208   0.3249     3   90.17   1.0457   -4.0423   0.4396   -0.0224   0.3255     4   61.16   1.0457   -0.0258   0.3444   0.3457   -0.0247   0.3289     5   02.18   1.0513   -0.0284   0.3457   -0.0277   0.3298     6   03.16   1.0597   -0.0311   0.3496   -0.0297   0.3398     7   64.17   1.0493   -0.0311   0.3496   -0.0297   0.3306     8   64.18   1.0602   -0.0328   0.3557   -0.0309   0.3355     9   68.18   1.0602   -0.0350   0.3557   -0.0309   0.3356     0   70.20   1.0012   -0.0373   0.3555   -0.0310   0.3366     1   72.19   1.0719   -0.0411   0.3655   -0.0310   0.3366     2   74.19   1.0637   -0.0469   0.3717   -0.0414   0.3430     3   76.26   1.0451   -0.0467   0.3750   -0.0469   0.3461     4   77.32   1.0477   -0.0408   0.3780   -0.0461   0.3468     5   60.20   1.1096   -0.0575   0.3282   -0.0557   0.3555     6   82.22   1.1076   -0.0608   0.3421   -0.0557   0.3556     6   86.23   1.0795   -0.0669   0.3421   -0.0657   0.3557     6   86.23   1.0795   -0.0669   0.3421   -0.0657   0.3578									
The state   China		157	0.53	2.3	, 10 A	MEE.		·	. 1
2 59.16 1.0493 -0.0218 0.3409 -0.0208 0.3249 3 59.17 1.0457 -0.0250 0.3484 -0.0220 0.3285 4 61.18 1.0457 -0.0250 0.3484 -0.0220 0.3289 5 62.18 1.0513 -0.0286 0.3467 -0.0272 0.3298 6 63.16 1.0592 -0.0311 0.3496 -0.0294 0.3301 7 64.17 1.0293 -0.0315 0.3507 -0.0297 0.3398 8 65.18 1.0602 -0.0325 0.3557 -0.0309 0.3355 9 66.18 1.0602 -0.0325 0.3554 -0.0309 0.3355 9 66.18 1.0612 -0.0373 0.3557 -0.0309 0.3356 0 70.20 1.0012 -0.0373 0.3553 -0.0351 0.3306 1 72.19 1.0714 -0.0411 0.3655 -0.0351 0.3306 2 74.19 1.0537 -0.049 0.3717 -0.0414 0.3430 3 76.20 1.057 -0.049 0.3717 -0.0414 0.3430 4 77.32 1.077 -0.0500 0.3600 -0.0401 0.3461 4 77.32 1.077 -0.0500 0.3600 -0.0401 0.3469 5 80.20 1.1076 -0.0515 0.3600 -0.0401 0.3469 15 80.20 1.1076 -0.0515 0.3600 -0.0401 0.3469 16 82.22 1.1070 -0.0510 0.3921 -0.0557 0.3535 17 54.22 1.1052 -0.0009 0.3921 -0.0557 0.3536	NT ALPH						YCPF		
3	56.0	B 1.0	424	-0.0203					
4 61.18 1.0457 -0.0258									
5 02.18 1.4513 -0.0285 0.3657 -0.0272 0.3298 6 63.16 1.4552 -0.0311 0.3-96 -0.0294 0.3361 7 64.17 1.4353 -0.4315 0.3502 -0.0297 2.3306 8 65.18 1.4566 -0.4350 0.3557 -0.4309 0.3355 9 65.18 1.4566 -0.4350 0.3554 -0.0351 0.3366 0 70.20 1.4012 -0.4373 0.3554 -0.0351 0.3366 1 72.19 1.6714 -0.0411 0.3655 -0.4354 0.3418 12 74.19 1.0037 -0.049 0.3717 -0.444 0.3430 3 76.20 1.0577 -0.0500 0.3704 -0.0414 0.3450 1 77.32 1.0577 -0.0500 0.3704 -0.0416 0.3461 1 6 82.22 1.1476 -0.0515 0.3512 -0.0557 0.3535 1 54.22 1.1052 -0.0616 0.3491 -0.0557 0.3555 1 54.22 1.1052 -0.0616 0.3491 -0.0557 0.3568									
6 63.16 1.057 -0.0311 0.3-96 -0.0294 0.3301 7 64.17 1.053 -0.0315 0.3507 -0.0309 0.3355 8 66.18 1.0602 -0.0329 0.3557 -0.0309 0.3355 9 68.18 1.0406 -0.0350 0.3557 -0.0309 0.3356 0 70.20 1.0012 -0.0373 0.3553 -0.0351 0.3366 1 72.19 1.0719 -0.0411 0.3655 -0.0354 0.3410 2 74.19 1.0637 -0.049 0.3717 -0.0414 0.3430 3 76.20 1.0551 -0.049 0.3717 -0.0414 0.3430 1 77.32 1.077 -0.0500 0.3000 -0.0461 0.3461 6 82.22 1.1070 -0.0500 0.3000 -0.0461 0.3498 7 64.22 1.1052 -0.0557 0.3502 -0.0557 0.3535 7 64.23 1.0795 -0.0509 0.3921 -0.0655 0.3548									
7 64-17 1-0393 -0.0315 0.3307 -0.0297 2.3306 8 64-18 1.0602 -0.0329 0.3557 -0.0309 0.3355 9 64-18 1.0616 -0.0350 0.3564 -0.0330 8.3356 0 70.20 1.0612 -0.0373 0.3593 -0.0351 0.3366 1 72-19 1.0719 -0.0611 0.3655 -0.0350 0.3366 2 74-19 1.0637 -0.0449 0.3717 -0.0414 0.3430 3 76-20 1.0951 -0.0462 0.3717 -0.0414 0.3430 4 77.32 1.0977 -0.0506 0.3603 -0.0461 0.3469 5 80.20 1.1094 -0.0555 0.3503 -0.0518 0.3469 6 82.22 1.1070 -0.0616 0.3921 -0.0557 0.3535 7 54-22 1.1055 -0.0603 0.3921 -0.0655 0.3548									
8									
0 70.20 1.0012 -0.0373 (-3593 -0.0351 0.3306									
1 72.19 1.0717 -0.041 0.3655 -0.0314 0.3410 2 74.19 1.0637 -0.0449 0.3717 -0.0414 0.3430 3 76.20 1.0951 -0.0462 0.3717 -0.0461 0.3460 4 77.32 1.0977 -0.0500 0.3603 -0.0461 0.3469 5 80.20 1.1096 -0.0575 0.3502 -0.0518 0.3469 6 82.22 1.1070 -0.0016 0.3913 -0.0557 0.3535 7 64.22 1.1055 -0.0603 0.3921 -0.0605 0.3568	69.1	B Jav	616	-0.0350	V. 3564	-0.0330	0.3356	-	
2 74.19 1.0e37 -0.0e49 0.3717 -0.0e14 0.3430 3 76.20 1.0951 -0.0e82 0.3750 -0.0e60 0.3e61  • 77.32 1.0977 -0.0506 0.3008 -0.0e61 0.3e69  5 80.20 1.1096 -0.0575 0.3m82 -0.0518 0.3e98  6 82.22 1.1070 -0.0016 0.3913 -0.0557 0.3535  7 54.22 1.1055 -0.0e89 0.3921 -0.0e55 0.3548									••
3 76-20 1-0751 -0.0687 M-3770 -0.0600 0-3661  • 77-32 1-0777 -0.0500 0.3000 -0.0401 0.3469  5 80-20 1-1076 -0.0575 0.3502 -0.0518 0.3498  • 82-22 1-1070 -0.0016 0.3713 -0.0557 0.3535  7 64-22 1-1055 -0.0609 0.3721 -0.0605 0.3548									<del></del>
- 77.32 1.0777 -0.0505 0.3606 -0.0461 0.3469 5. 80.20 1.109c -0.0575 0.3582 -0.0518 0.3498									
5 80.70 1.1046 -0.0575 0.3582 -0.0518 0.3498									<del></del>
6 82.22 1.1070 -0.0016 0.3413 -0.0557 0.3535 7 54.22 1.1052 -0.0699 0.3921 -0.0695 0.3568 8 86.23 1.0795 -0.0722 0.3~25 -0.0657 0.3570									₹
7									
9 87.23 1.0954 -0.0761 5.3936 -0.0676 0.3593									•
	87.2	23 1.0	<u> 450 </u>	-0.0/41	0.3934	-0-0676	0.3593		<del></del>
				<del></del>		<del></del> -	<del></del>	<del></del>	<del> </del>
		<del></del>			<del></del>				
					,			<del></del>	<del> </del>
							<del></del>		

				·····	<del> </del>		<u> </u>	and the second of the second of the second
					· .			·
								<del></del>
		PING HEVE	LOPMENT C	ENTERIALD	C) PROPI	ILSION MIND TUNNEL	FACILITY (PHT)	AERODYNAMIC WIND TURNEL (47)
	1 OF 1				MAI	TIN MISSILE TAIL E	FFECTS DATA	
P.I.	1_0F1			·		SPLITTER PLATE	· ·	•
	7E51	PART MAC		CUNE TRAN	SITION	·· <del>···································</del>	<u> </u>	
)1MT	ALPHA BB.CE	CHF	-0.0731	CH () 3502	4CPF -0.6692	YCPF		
2	89.95		-0.0756		-0.0716	0.3597		
3	90.14		-0-0769	U.3772	-0.0736	0-3606		
•	91.14		-0.0791	0.3760	-0.0759	0.3611		
<u> </u>	93.14	1-4-5-	<u>-0.0513</u> -0.0057		-0.0390 -0.036	0.3632	·	
7	94.14		-C_ub80		-0.0559	0-3665		
8	96.15		-0.6453		-0.0943	0.3664		
9	98.15	1. WUAD	-0.1045	0.3750	-0.1026	0.3717		· · · · · · · · · · · · · · · · · · ·
0	100.14		-0.1102		-0.1095	0.3734		
<u>ų –</u>	102-15		-0-1164	0.3771	0-1154	0.3739	<del></del>	
12	104.16	_1.0072	-0.1555		-0-1713 -0-1750	0.3737 9.3759		
14	166.10		+0-12-7	9-37-8	-0.1303	0.3764		<del></del>
15	110.15	0.9773			-0.1361	0.3771		
16	112.1/	1.0006	-0.1305	6.377A	-0.1365	0.3776		
	114.10	0.7730	-0.1376		-0-1-06	0.3767		
18	116.18		-0.1401		-0.1420	0.3766		
14	11/.1/	0.9570	-0.1015	0.3680	-0.1439	0.3728		
						<del> </del>		
						<del> </del>	· <del></del>	
							<del></del>	
		· · · · · · · · · · · · · · · · · · ·	<del></del>					
				- <del></del> <del>-</del> , —	<del></del>			
								<del></del>
						<del></del>	<del></del>	<del></del>

TEST PART MALE ARIBER COMF   IGANSIIION										ILE TAIL TER PLATE							
2 159 0.65 2-5 F10 FREE  **POINT ALPMA CNF CN Cn Cn ACPF VCPF 1 118.01 0.9471 -0.1394 0.3151 -0.1401 0.3738 2 113.10 0.9462 -0.1394 0.4573 -0.1400 0.3706 3 120.10 0.9469 -0.1389 0.3555 -0.1450 0.3706 4 121.10 0.9462 -0.1389 0.3555 -0.1461 0.3738 5 122.10 0.9462 -0.1389 0.3552 -0.1461 0.3698 6 123.11 0.946 -0.1389 0.3512 -0.1461 0.3698 6 123.11 0.946 -0.1377 0.3537 -0.1470 0.3669 7 124.15 0.4475 -0.1377 0.3537 -0.1470 0.3669 9 128.11 0.9465 -0.1377 0.3537 -0.1470 0.3669 9 128.11 0.9465 -0.1352 0.3363 -0.1471 0.3662 11 132.11 0.9465 -0.1352 0.3363 -0.1471 0.3662 11 132.11 0.9465 -0.1352 0.3363 -0.1471 0.3662 11 132.11 0.9466 -0.1352 0.327 -0.1470 0.3661 13 130.12 0.6466 -0.1272 0.3277 -0.1470 0.3661 13 130.13 0.6466 -0.1352 0.3363 -0.1471 0.3661 13 130.12 0.6669 -0.1114 0.3193 -0.1465 0.3661 13 130.13 0.6866 -0.1279 0.3165 -0.1465 0.3662 15 140.13 0.8691 -0.1466 0.3193 -0.1465 0.3662 15 140.13 0.8691 -0.1366 0.3165 -0.1460 0.3632 15 140.13 0.8691 -0.1366 0.3165 -0.1503 0.3619 17 144.15 0.8656 -0.1330 0.3199 -0.1550 0.3629 19 147.16 0.8655 -0.1184 0.2492 -0.3629 0.3629 19 147.16 0.8655 -0.1184 0.2492 -0.1629 0.3629											_						
2 159 0.65 2.5 F14 FNEE  OINT ALPMA CNF Cn Cn Cn XCPF YCPF  1 18.01 0.961 -0.1394 0.3515 -0.161 0.1738  2 119.10 0.962 -0.1394 0.3573 -0.160 0.3706  3 120.10 0.966 -0.1394 0.3555 -0.1651 9.1706  4 121.10 0.966 -0.1384 0.3555 -0.1651 9.1706  5 122.11 0.951 -0.1384 0.352 -0.161 9.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368 0.368																	
118.01									<del></del>	<del></del>					<del></del>		
118.01	OLNE	_	N DHA	CNE			<u> </u>		w/ DE								
3 120,10 0,900 -0,137	1				_												
121-10   0.906   -0.1349   0.352   -0.1652   0.3716	2																
5 122a10 0.4926 -0.1384 0.3912 -0.1460 0.3692 7 124a16 0.497a -0.1390 0.4683 -0.1467 0.3677 8 126a16 0.497a -0.1377 0.3537 -0.1470 0.3669 9 128a11 0.497a -0.1354 0.3187 -0.1465 0.3663 16 130.11 0.4916 -0.1352 0.3349 -0.1471 0.3642 11 132a11 0.4957 -0.1329 0.3297 -0.1470 0.3663 12 13a.12 0.4964 -0.1322 0.3297 -0.1467 0.3641 13 13a.12 0.4964 -0.1322 0.3675 -0.1478 0.3641 13 13a.13 0.4963 -0.1244 0.3162 -0.1465 0.3661 14 139.13 0.4963 -0.1249 0.3162 -0.1465 0.3661 15 143.13 0.4964 -0.1326 0.3165 -0.1508 0.3652 15 143.13 0.4964 -0.1399 -0.1506 0.3165 -0.1508 0.3161 16 142.13 0.4810 -0.1249 0.3165 -0.1508 0.3189 17 144.15 0.4856 -0.1330 0.3199 -0.1659 0.3588 18 140.16 0.4837 -0.1337 0.329 -0.1602 0.3629 19 147.16 0.4855 -0.1346 0.2992 -0.1629 0.3625										<del></del>		<del></del>	<del></del>	<del></del>		<del></del> -	
6 123-11 0.491e -0.1389 0.3512 -0.1460 0.3667 7 124-16 6.4917 -0.1377 0.3937 -0.1470 0.3667 8 126-16 6.4917 -0.1377 0.3937 -0.1470 0.3669 9 128-11 0.9929 -0.1354	•																
7 124.16	6																
9 120-11 0-9247 -0.1354	1_	_12	24.16	6.4474	-0.139	0_0	1483	-C-1467	0.3677								
10 130.11 0.9196 +0.1352 U.3349 +0.1471 0.3642 11 132.11 0.9157 -0.1329 0.3297 -0.1467 0.3641 12 134.12 0.6944 -0.1322 0.3297 -0.1479 0.3641 13 130.12 0.6849 -0.1314 0.3199 -0.1485 0.3615 14 139.13 0.6763 -0.1299 0.3162 -0.1682 0.3632 15 143.13 0.8691 -0.1306 0.3165 -0.1503 0.3619 16 142.13 0.8610 -0.1299 0.3089 -0.1509 0.3588 17 144.15 0.8556 -0.1330 0.3090 -0.1509 0.3629 18 140.16 0.8347 -0.1337 0.3329 -0.1602 0.3629 19 147.16 0.8255 -0.1346 0.2992 -0.1602 0.3625																	
11. 132_11				D-9447													
12 13-12 0.644 -0.1322 0.3257 -0.1478 0.3461 13 130-12 0.6469 -0.1314 0.3199 -0.1485 0.3615 14 134-13 0.6463 -0.1299 0.3162 -0.1482 0.3632 15 147-13 0.6610 -0.1299 0.3069 -0.1503 0.3619 16 142-13 0.6610 -0.1299 0.3069 -0.1509 0.3588 17 144-15 0.6556 -0.1330 0.3090 -0.1554 0.3612 18 140-10 0.6347 -0.1337 0.3329 -0.1602 0.3629 19 147-16 0.6255 -0.1346 0.2792 -0.1629 0.3625						9 0-	3297	-4-1467									
14 135-13						7 C.	3/57	-9-1478									
15																	
16 142.13 0.861c -0.1299 0.3089 -0.1509 0.3580 17 144.15 0.8556 -0.1430 0.3090 -0.1554 0.3612 18 140.16 0.8347 -0.1337 0.3029 -0.1602 0.3629 19 147.16 0.8255 -0.1344 0.2992 -0.1629 0.3625																	
17. 1-4-15 0.6556 -0.1330 0.3:190 -0.1554 0.3612 18 14-16 0.6347 -0.1337 0.3:29 -0.1602 0.3629 19 147-16 0.6255 -0.1366 0.2792 -0.1629 0.3625					-0-129	9 0-	3089	-0-1509									· · · ·
19 1e7.1e 0.8255 =0.1366 G.2792 =0.1629 0.3625	-																
	19	_4	alale	0.8255	-6.13	-11-	2492	-0-1629	0.3625								
														·			
								•									
		_															
				_					•								
				<del></del>				<del></del>	<del></del>			<del> </del>					
															····		
														<del></del>			

	ENGINEE 1 OF 1 1 OF 1		LOPMENT C	ENTERLAED	C) PROPI	HIL MISSILE	TUNNEL FACILITY (PHT)  TAIL EFFECTS DATA PLATE DATA	AERODYNAMIC WIND TUNNEL (AT)
			H 9×10-6					
	2	160 0.65			REE			
	ALPHA 147.9t	CMP U. N.1.75	-0-1333	C9	-0.1639	VCPF		
	149.0h	0.8031			-0.1669	0.3560		
	150.08		-0-1367		-0-1592	0.3592		
	151.05 152.08		-0.1260 -0.1239		-0.1692 -0.1723	0.360D 0.359A		
	153.07		-0.1203		-0.1746	0.3607	<del></del>	
	150.08	0.5050	-6-1184		-0-1763	8196.0		
	156.09		-6-1137		-0.1866	0.3662	•	
	158.08 160.08		-0_3104 -0.1669		-0.2107	0.3805	· · · · · · · · · · · · · · · · · · ·	
	162-05		-0-1061		-0-2316	0.3905	·	
?	164.09		-0.1049		-0.2583	0.4849		
	166.00		-0-10u3		-0-2857	Des 226	- <u>-</u>	
	168.09 170.09		-0.0793		-0.3103 -0.3335	0.4243		
	172.10		-0.0606		-0.3422	0.4884		
Z	174.10		-6-0992		-0.3530	0.0079		
	176.12		-0-0514		-0.3622	0.3686	•	
9	177.11	0_6535	-0.0192	0-0189	-0.35A3	0.3529		
								•
								·
							· · · · · · · · · · · · · · · · · · ·	<u> </u>
							<del></del>	
					<del></del>			
								· -

ìΕ	EMGINEE 1 OF 1 1 OF 1	PING DEVE	LOPMENT C	ENTERIAED	C) PROPI	TIN MISSILE	TUNHEL FACILITY TAIL EFFECTS OF	ATA	AEROOYNAMIC_HI	ND TUNNEL (AT)
				<del></del>		<del></del>	·	· · · · · · · · · · · · · · · · · · ·	<u>.</u>	
	TEST	PART MAC	2.5	CONF_TRAM	NEE		<del></del>	•		· · · · · · · · · · · · · · · · · · ·
THE	ALPHA	CNF	Cri	Cs		YCPF				<del></del>
	178.00		-0.0138		-0.3395	0.3559				
2	176.99	0.0256	-0.0082	G.0077	-0-3193	0.3010				
		0.0126		0.0010.	-0-2145	0-0791				
	180.99	-0.019£	0.0038	-0.0039 -0.0121	-1.1528	0-6099				
6	163-03	-0.0347	0.0171	-D-0143	-0.4585 -n1113	0.4608				
7	184.05	-0.4510	0.0250	-0.0271	-0-4789	0.4434			•	
8	186.04	-0.1104	9.0415	-4.0490	-0.3742	0.4418				
									-	
				·						

						SPLITTE	E TAIL EFFECTS DATA R PLATE DATA	· · · · · · · · · · · · · · · · · · ·		
	TEST	PART MAC 162 0.92		COMF TRAN	SITION					
NT	ALPHA	CNF	Сн	DZ		F YCPF .	<del></del>			
		-0.0175		-0.0239 -0.0130	0.000	0.7404	·			
	0.04	0.4459	-0.0000	-0-0024	-0.2639	-0.9549				
	2.05		-0.0015 -0.0010		-0.05d2 -0.0230	0.2639				
	3.05		-0.0011	0.0299	-0.0164	0.4661				
_	4.07		-0.0020	0-0407	-0.0222	0.4461				
	6.07		-0.0031 -0.0061		-0.0278	0.4485				
	10.16	0.2452	-0.00Bl	0.1205	-0.0274	0.4083	<del></del>		-	
_	12-12		-0.0109	0.1676	-0.0299	0.3924				
	14.13		-0.0127 -0.412d		-0.0278 -0.0238	0.3751				
	16.17	0.6146	-0.0134	0.2150	-0.0218	0.3498				
	20.19			0.2405			<del></del>			<del></del>
	25.25	0.4602	-0.0144 -0.0135	0.2040 0.2557	-0.0161					
	26.25	0.4734	-0.0153	0.3106	-0.6158	0.3191				
	27.26	1.015	-0.6155	0.3724	-0.0155	0.3175				
		<del></del>					<del> </del>			<del>~~~</del>
							•		<del></del>	
									· · · · · · · · · · · · · · · · · · ·	
										•
									***************************************	
					<del> </del>					
	•									

€	ENGINE 1 OF 1 OF		EL OPPENT C	ENTERGALD	C) PHOP	RTIN MISS	NO TUNNEL FACILITY IP ILL TAIL EFFECTS DATA IER PLATE DATA	4 <u>1)</u>	<u>AERODYNAMIC</u>	HIND TUNNELIAT)
. —	1ES	1 <u>Pari Pa</u> 163 0.4	CH_RX10-6_		SITION					
INT	ALPHA	CNF	CH		<b>ACPF</b>	YCPF		<del> </del>		· · · · · · · · · · · · · · · · · · ·
1	13.02	0.4296	<b>-0</b> -2117		-0.0271	0.3743				
5	14.11			6-1771	-0.0261	0.3727				
3	15.11 16.13		-0.0125 -0.0123		-0.0244 -0.0224	0.3596	· · · · · · · · · · · · · · · · · · ·	<del></del>	<del></del>	
5	17-13		-0-0134		-0-0226	0.3509				
6	16.1		-0,01+0		-0.0220	0.3429				
1	19.15	0.6/34	-0.ulel	1.2297	-0.0210	0.3411				
8	21.17		-0.0139		-0.0162	0.3325			-	
9	23.16		-0-0132		-0.0155	0.3216			•	<del></del>
0	25.26		-0.0138 -0.0159		-0.6146 -0.6154	0.3171				
2	29.23			<u>u.3607.</u> 0.3514		-463146	<del></del>			
3	31.76			0.3646		0-3123				
4	33,27	1.1740	-0.0015	0.3047		0.3042				
15	35.27	1.1392	0.0379		0.0286	0.2877	· · · · · · · · · · · · · · · · · · ·			
6	37.28			0.3757	0.0240	0.2857				=
<u>7</u>	_39.20		-0.0922		-0.0021	0.3003			·	
9	42.20				-0.0102	0.3041				
-1.	42.42			WAJING						
									-	
							<del></del>			
										•
		<del></del>					<del></del>		<del></del>	·
								· · · · · · · · · · · · · · · · · · ·		
									•	
			· <del></del>				<del></del>		<del></del>	<del> </del>
							•			
										•
			•					-		

E	ENGINE 1 OF 1 1 OF 1		LOPSENT C	ENTER CAEU	C)PROP MA	KTIN MISSIL	LIUNNEL FACI E TAIL EFFEC R PLAIE DATA	TS DATA	AERODYNA	MIC_HIND_TUN	NEL (AT)
	TEST	PAPT MAL.			SIIION					•	
TAT '	ALPHA	CNF	Сн	CH		YCPF		·			
1	58.64	1.0759	-0-1447	11.3372	-0-0230	0.3136			<del></del>		
2	54.17	1.0006	-0.0263		-0.0244	0.3143					
	61.10	1.0075	-0-0214 -0-028		0.0252 -0.0250	0.3153			<del></del>		
	62.18	1.0560	-0.0263		=0 <u>+0261</u>	0-3166					
	63.17	1.0419	-0.0303		-0.0277	0.3204					
	64.15		-0-417	<u> 10-3-01</u>	-0-0291	0-321A					<del></del>
}	66.14	1.0414	-0.03-4		-0.0322	0.3236		-			
	70 31		-0.0372		-0 <u>-0362</u> -0.0372	0-3271					<del> </del>
	70.21	1.0891	-0.0405 -0.0450		_0.0312 0.0409	0.3301					
	74.21	1.1002	-0.0468		-0.0441	0-3304				<del></del>	
_	76.22	1-1155	-0-0533		-0.0477	0.3376					
	75.22		-0.Up79		-0.6512	0-3403					
	80.23				-0-05-0	0-3427					
;	82.22		-0.uchl		-0.0583 -0.0522	0-3432					
	84.24		-0.0743		-0.0559	0.3473					
i	87.25				=0.0585	0-3-83					
			225		100	0.5466					
				<del></del>			···				
											•
					···				<del></del>	<del></del>	
		·			····						
									····		
										<del></del> -	· · · · · · · · · · · · · · · · · · ·

. .

				<del></del>		SPLITTER	PLATE DATA	
						<u> </u>		
	<u>1E</u> \$1	167 0-4c	M <u>Ex14-6.</u> 0		<u>517104                                   </u>		<u> </u>	
INT	ALPHA bB-08	CNF	Cn	C-		YCPF .		
<del>}</del>	59.08		-0.0760		-0-0711	0.3510		
<u>.                                    </u>	90.13	1.4524	-0-1610	6.3/30	-0.07.76	0.3544	•	
4	91.13		-0.4643		-0.0804	0.3560		
<u>5                                    </u>	93.14		-0.0:30 -7.0:31		0 <u>-0853</u>	0.3572 0.3581		·····
7		1.4302	-1-0461		=0.0952	0.3599		
8	95.15		-0-10-0		-0.1031	259F.0		
<del>9</del>	98.19. 100.15		-0-1127_ -0-1200		-0.1101 -0.1157	0.3651		
			-0-12-0		0-1194	0.3670		
	104.15		-0-1240		-0.1239	0.3666		
	108.17				-3-1277	0-3675		<del></del>
			-0-1360 -0-1391		-0.1307 -0.1338	0.3664 -0.364A		
6	112.16	1.0020	-0.140M	4.3005	-0.1351	0.3651		
			-2-1-16		-0-1361	0.3659		
			-0.1-29		-0.1369 -0.1379	0.3638		
					-441114			
					59			
			<del></del>					•
			, <del>, </del>				· · · · · · · · · · · · · · · · · · ·	
						<del> </del>		

E	EAGINER 1 OF 1 1 OF 1		LOPMENT C	ENTERIAED		STATEMENT STATE PLATE DATA  SPLITTER PLATE DATA	AERODYNAMIC HIND TURNEL (41)
			~_ ~ ^ ~				
		PART MAG			S <u>ITION</u> HEE		
	2	100 0.72	2.5				
INT	ALPHA	CNF	CH	Co		YCPF	
1	118.02		-0-1403		-0.1363	0.3612	
2	119.06	1.0146	-0.1412		-0.1367	0.3596	•
<del>_</del>	120.09	1.0005			-0.1386 -0.1389	0.3576	
5	122.11		-0-1397		-0.1396	0.3569	
6	123.10		-0.1397		-0.1399	0.3565	
1	124.11	0.9792	-0-1-147	FEEE	-0-1345	0.3560	
8	126.11		-0.1572		-0.1431	0.3556	
9	128-11		-6-1374		-0.1410	0-3552	·
0	130.11		-6-1371		-0.1422	0.3516	
	132.11		-0.130A	_ <del>33335 ئ</del> 10د 3 ئ	-0-1439	0.3509	•
2	136.12		-0-1366		-0.1405	0-3505	
14	136.13		=0.1373	- 153E-U	-0.1985	0.3485	
5	140.12		-0-1362	0.3191		0.3516	
6	147.14		-0.1356		-0.1523	0.3527	
17	144.14		<u>-2.1379</u>		-0.1559	0.3506	
8	146.15		-0.1366		-0.1592	0.3536	
19	1-7,15	0.5447	-0-1364		3-1615	0.3507	
			<del></del>	<del></del>			
					· · · · · · · · · · · · · · · · · · ·		
							<u> </u>
		-					
		T					

•	
,	
,	
,	
,	
,	
,	
,	
,	
,	
	•
· <del></del>	
	·
	•

Þ	
m	
0	
Ü	
ä	
D	
÷	
ĢΙ	
_	
w	
•	

							·		· · · · · · · · · · · · · · · · · · ·	
									•	
					?					
APHOLD	ENGINE	DING UEUR	I OPPEST C	FATEN (AFI)	C) PP(13	III SION DI	MD TUNNEL FACTOR	JY (PWT)	AERODYNAMIC_4IND_TUNNEL(AT)_	
PARE	1 OF 1		TASSER! T	Train I had trained	144	HTIN MISS	ILE TAIL EFFECTS	- DATA		
SMEET	i OF I						IER_PLAIE_DAIA			
		2-14	10							
	JESI 2	PAPT MAC	<u>+ RX10-6</u> 2-5	CONE IRAN	<u>sition                                   </u>		······································			
POINT	ALPHA	CNF	СН	C ₂	ACPF	YCPF				
1	175.00	0.0531	-0.0177	6.0134	-0.3332	0.2531				<del></del>
	179.01	0.0144	-0-0110	0.0056	-0.3342 -0.2154	0-1545				
4	161.01	0.0067	0.0613	-0.0066	0-1860	-0.9851	<del></del>			
5		-0.0101	0.0000	U_U127	-0.7921	1.2654 0.6463				<del></del>
7	104.01	-0.0520	0-2242	-0.0207	ES++.0-	0.5408				5.0.
	185.06	-0.1041	0.0429	-0.6517	-0.4423	0.4740				
	,	···								
					<del></del>					
			<del></del>							
-										
								···		
		<del>•</del>			·····					
	·					<del></del>			·	
				<del></del>				<del></del>		
				<del></del>					· · · · · · · · · · · · · · · · · · ·	
						_		_	_	
	·	<del></del>				<del></del>				

TEST PART PALH PX10-6 CONF IRANSITION 2 171 0-50 2-5 F14 FMEE  POINT ALPMA CMF CM CM CM ACPF VCPF 1 -2-03 -0.000 0.0007 -0.0271 -0.0160 0.6698 2 -0.57 -6.0161 -0.0010 -0.0122 0.0738 0.6680 3 0.03 0.0987 -0.0014 -0.0020 -0.1609 -0.4448 4 1.05 0.0331 -0.0028 0.0070 -0.0047 0.2108 5 2.05 0.0058 -0.0042 0.0070 -0.0047 0.2108 6 3.05 0.0015 -0.0049 0.0325 -0.0598 0.3866 7 4.06 0.1091 -0.0049 0.0325 -0.0598 0.3866 7 4.06 0.1091 -0.0043 0.0033 -0.0573 0.4011 8 6.06 0.1726 -0.0099 0.0718 -0.0575 0.4155 9 8.09 0.2643 -0.0176 0.1268 -0.0554 0.3910 10 10.10 0.323 -0.0176 0.1268 -0.0544 0.3910 11 12.12 0.4062 -0.0222 0.1565 -0.0554 0.3910 11 12.12 0.4062 -0.0229 0.1007 -0.0528 0.3665 12 14-13 0.4903 -0.0259 0.1007 -0.0528 0.3665 13 16.16 0.575a -0.0254 0.2267 -0.0519 0.3536 15 20.20 0.7511 -0.0340 0.2272 -0.0559 0.3369 16 17-17 0.0556 -0.0314 0.2316 -0.0479 0.3536 17 2-2-25 0.4315 -0.0345 0.3272 -0.0359 0.3369 17 2-2-25 0.4315 -0.0346 0.3273 0.0345 0.3224 18 26-27 1.026 -0.0346 0.3233 -0.0345 0.3224		DATA.	TIM MISS!					1 OF 1	AGE
2 171 0.56 2.5 F14 FMEE  POINT ALPHA CMF CM CM CM CM MCPF VCPF  1 -2.03 -0.000				<del></del>			·		
1 -2.03 -0.040a									
2 -0.47 -6.0141 -0.0010 -0.0122 0.0738 0.8680 3 0.03 0.0067 -0.0014 -0.0034 -0.1609 -0.4448 4 1.05 0.031 -0.0028 0.0070 -0.0047 0.2108 5 2.05 0.0258 -0.0042 0.0193 -0.0731 0.3401 6 3.05 0.0019 -0.0049 0.0325 -0.0598 0.3964 7 4.06 0.1091 -0.0049 0.0718 -0.0575 0.4011 8 5.06 0.1726 -0.0099 0.0718 -0.0575 0.4155 9 6.09 0.2243 -0.0130 0.0041 -0.0532 0.4016 10 10.10 0.3243 -0.0174 0.1268 -0.0544 0.3918 11 12.12 0.4052 -0.0222 0.1555 -0.0547 0.3853 12 14.13 0.4903 -0.0259 0.1007 -0.0528 0.3685 13 16.16 0.5756 -0.0259 0.1007 -0.0528 0.3685 14 18.17 0.0556 -0.0314 0.2267 -0.0519 0.3536 15 20.20 0.7411 -0.0340 0.2572 -0.0479 0.3536 16 27.21 0.4324 -0.0344 0.2722 -0.0459 0.3479 17 20.25 0.4155 -0.0345 0.3233 -0.0345 0.3224 18 26.27 1.0029 -0.0345 0.3233 -0.0345 0.3224		· · · · · · · · · · · · · · · · · · ·					•		POINT
3									
5		•							<u> </u>
6 3.05 0.0619 -0.0649 0.0325 -0.0598 0.3964 7 4.06 0.1991 -0.0063 0.0433 -0.0574 0.4011 8 5.06 0.1726 -0.0099 0.0718 -0.0575 0.4155 9 8.09 0.2243 -0.0130 0.9481 -0.0532 0.4016 10 10.10 0.3243 -0.0176 0.1268 -0.0544 0.3918 11 12.12 0.4062 -0.0222 0.1565 -0.0547 0.3853 12 14.13 0.4903 -0.0259 0.1607 -0.0528 0.3685 13 16.16 0.5754 -0.0259 0.1607 -0.0528 0.3685 14 18.17 0.0556 -0.0314 0.2267 -0.0519 0.3552 14 18.17 0.0556 -0.0314 0.2216 -0.0479 0.3536 15 20.20 0.7611 -0.0340 0.2272 -0.0459 0.3470 16 27.21 0.0325 -0.0346 0.3733 -0.0371 0.3269 17 20.25 0.4165 -0.0346 0.3733 -0.0345 0.3224 19 27.27 1.0436 -0.0342 0.3376 -0.0328 0.3236	•								•
7	·								<del></del>
8									<u>, , , , , , , , , , , , , , , , , , , </u>
10			0.4155	-0.0575	0.0718	-0.0099	r.1726	5.06	8
11 12-12 0-4062 -0-0222 0-1565 -0-0547 0-3653 12 14-13 0-4903 -0-0259 0-1607 -0-0528 0-3685 13 16-16 0-5/5a -0-0259 0-2657 -0-0519 0-35592 14 18-17 0-656 -0-0314 0-2316 -0-0479 0-3536 15 20-20 0-7411 -0-0340 0-2572 -0-0459 0-3470 16 27-21 0-0345 -0-0346 0-3733 -0-0371 0-3269 17 20-25 0-9465 -0-0345 0-3733 -0-0345 0-3224 19 27-27 1-0436 0-0342 0-3376 -0-0328 0-3236		·							<u>. y</u>
12									
14 18-17 0-055C -0-0314 0-2316 -0-0479 0-3536 15 20-24 0-7411 -0-0340 0-2572 -0-0459 0-3470 16 27-21 0-032F -0-0340 0-2798 -0-0416 0-3359 17 29-25 0-9105 -0-0340 0-3203 -0-0371 0-3269 18 26-27 1-026 -0-0345 0-3233 -0-0345 0-3224 19 27-27 1-4436 -0-0342 0-3370 -0-0328 0-3236									
15 20.2u 0.7ell =0.03e0 0.2572 =0.0e59 0.3e70 16 27.2l 0.8324 =0.03en 0.2798 =0.0e16 0.3359 17 29.25 0.9185 =0.03e0 0.3013 =0.0371 0.3269 18 26.27 1.0026 =0.03e5 0.3233 =0.0345 0.3224 19 27.27 1.0e36 =0.03e2 0.3376 =0.0328 0.3236									
16 27.21	•								
17									
19 27.27 1.ue36 -0.0342 u.3376 -0.6328 0.3236			0.3269	-0.0371		-0-0360	6.YIP5	20.25	_12
	<u>-</u>								-
	· · · · · · · · · · · · · · · · · · ·		0.3236	-0-0328	. 0. 3376	-0-0-4-2	1-44-16	21.21	19
								•	
						<u>-</u>	<del></del>		
					_				
•			<del></del>		<del>-,</del>				
					•				
			<del></del>					-	
				•					
		<del></del>				<del></del>			

IEST PAPT MALM 9A10-6 CONF TRANSITION   2   177 U-50 Z-5   F12 FMEE   2   177 U-50 Z-5   177 U	SE	ENGINE 1 OF 1 OF	1	ig nfati	LOPMENT C	ENTER LAEU	46	HTIN MISSILE	TAIL EFFECTS DATE	A AFRODYMAMIC WIND	IUNNEL(4)
TEST PANT MALM PRIDES CONF TRANSITION   2   177 U.568 Z.5   FIA   FMEE				<u> </u>			·e		·····		
OINT ALPMA CNF CM Cy XCPF YCPF  1 29-13 1-1053 -0.4363 0.3536 -0.0329 0.3197  2 29-14 1.1636 -0.0367 (.3562 -0.0321 0.3203  3 30.14 1.1756 -5.2373 4.3755 -0.0318 0.3196  4 31.2C 1.244 -0.0371 0.3670 -0.0307 0.3200  5 32-19 1.2614 -0.4366 0.3430 -0.0265 0.3165  6 33.22 1.2704 -0.4366 0.419 -0.0271 0.3164  7 3-22 1.2704 -0.4366 0.419 -0.0271 0.3166  8 36.25 1.2183 0.4069 0.3476 -0.0208 0.3106  8 36.25 1.2183 0.4069 0.3476 -0.0208 0.3106  10 40.23 1.1663 -0.0069 0.3453 -0.0062 0.2966  11 42.23 1.1664 -0.0197 0.3536 -0.0170 0.3051  12 44.22 1.1569 -0.0197 0.3536 -0.0170 0.3051  13 45.33 1.1065 -0.0197 0.3569 -0.0170 0.3051  14 46.24 1.155 -0.0222 4.3561 -0.0178 0.3069  15 50.25 1.1752 -0.2232 4.3661 -0.0198 0.3098  16 51.36 1.1736 -0.0246 C.3641 -0.0208 0.3104  17 54.20 1.2406 -0.0233 4.3746 -0.0178 0.3098  18 56.29 1.2206 -0.0301 0.3756 -0.0235 0.3122			1.2	NEI_MAL	M .PALO=6_						
1 29.13 1.1053 -0.0364 0.353e -0.0329 0.3197 2 29.19 1.163e -0.0367 1.3662 -0.0321 0.3203 3 .30.19 1.175e -0.0371 0.3670 -0.0331 0.3194 4 31.20 1.2049 -0.0371 0.3670 -0.0307 0.3200 5 .32.19 1.2049 -0.0366 0.3730 -0.0295 0.3165 6 .33.22 1.2704 -0.0344 0.419 -0.0271 0.3164 7 .34.22 1.2764 -0.0344 0.419 -0.0271 0.3164 8 .36.23 1.2163 0.0049 0.357 0.0057 0.2919 9 .38.22 1.1559 0.0221 0.3109 0.0191 0.2662 10 40.23 1.1643 -0.0049 0.3453 -0.0042 0.2966 11 42.23 1.1600 -0.0154 0.3555 -0.0133 0.3038 12 44.22 1.1569 -0.0197 0.3536 -0.0170 0.3051 13 45.33 1.1665 -0.0197 0.3536 -0.0170 0.3051 14 46.24 1.1559 -0.0208 0.3694 -0.0177 0.3097 15 50.25 1.1752 -0.0232 0.3641 -0.0198 0.3108 16 51.36 1.1730 -0.0244 0.3644 -0.0266 0.3164 17 54.20 1.2004 -0.0201 0.3744 -0.0208 0.3160		5	11	72 0.58	2.5	F14 F	HEE				
2 29.1V 1.143a = 0.0367	DINT					C+	<b>KCPF</b>	YCPF		•	
3 30.19 1.1756 -9.2373 4.3755 -0.9318 0.3194  4 31.20 1.2094 -0.0371 0.3070 -0.0307 0.3200  5 32.19 1.2014 -0.0366 4.3730 -0.0295 0.3165  6 33.22 1.2704 -0.0344 0.419 -0.0271 0.3164  7 34.22 1.2764 -0.0344 0.377 -0.0208 0.3108  8 30.23 1.2183 4.4009 (.3557 0.0057 0.2919  9 38.22 1.1559 0.4221 (.3305 0.0191 0.2662  10 40.23 1.1643 -0.0049 4.3453 -0.0042 0.2966  11 42.23 1.1664 -0.4197 (.3536 -0.0173 0.3038  12 44.22 1.1559 -0.4197 (.3536 -0.0170 0.3051  13 45.33 1.1565 -0.4197 (.3536 -0.0170 0.3051  14 46.24 1.1555 -0.4200 4.3526 -0.0177 0.3097  15 50.25 1.1752 -0.4232 (.3441 -0.0198 0.3049  17 54.20 1.200 -0.0244 (.3641 -0.0198 0.3104  17 55.20 1.2400 -0.0244 (.3640 -0.0235 0.3122  18 50.29 1.2200 -0.0301 (.3650 -0.0236 0.3160	1_										
4 31.20 1.204 -0.0371 0.3e70 -0.0307 0.3200 5 32.19 1.2e14 -0.03e4 0.a132 -0.02e5 0.31e5 6 33.22 1.2f04 -0.03e4 0.a19 -0.02f1 0.3le6 7 39.22 1.2fea -0.02e6 0.3y7e -0.02e8 0.3le8 8 30.25 1.2le3 0.009 0.3b57 0.0057 0.2e19 9 38.22 1.1b59 0.0221 0.3le3 0.0141 0.2e62 10 40.23 1.1e63 -0.009 0.3e53 -0.00e2 0.2e66 11 42.23 1.1e00 -0.0197 0.3e53 -0.00e2 0.2e66 12 44.22 1.1b69 -0.0197 0.3e36 -0.0170 0.3e51 13 45.33 1.1beb -0.0197 0.3e56 -0.0170 0.3e91 14 46.24 1.1b5 -0.02e6 0.3e69 -0.0170 0.3e97 15 50.25 1.1f52 -0.02e6 0.3e69 -0.0177 0.3e97 15 50.25 1.1f52 -0.02e6 0.3e69 -0.0198 0.3e98 17 54.20 1.2e0e -0.03e1 0.3e59 -0.02e6 0.3le6	S										
5 32-19 1-2-15 -0-0-366 0-3530 -0-0-255 0-3165 6 33-22 1-2-704 -0-0-344 0-4-19 -0-0-271 0-3164 7 39-22 1-2-708 -0-0-357 0-0-0-208 0-3108 8 30-25 1-2-708 0-0-0-5 0-2-90 9 38-22 1-1555 0-0-0-5 0-0-0-2 0-2-966 11 42-23 1-16-0-0-0-5 0-3-55 -0-0-0-2 0-2-966 11 42-23 1-16-0-0-0-5 0-3-55 -0-0-0-2 0-3-966 11 42-23 1-16-0-0-0-0-5 0-3-55 0-0-0-17 0-3-0-5 12 44-22 1-15-5 -0-0-0-5 0-3-55 0-0-0-17 0-3-0-5 13 45-33 1-15-0 -0-0-0-0 0-3-55 0-0-0-17 0-3-0-9 14 46-24 1-15-5 -0-0-0-0-0 0-3-0-0-0-0-17 0-3-0-9 15 50-25 1-17-5 -0-0-2-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-											
6 33.22 1.2704 -0.0344 0.4(19 -0.0271 0.3164 7 34.22 1.2704 -1.0266 0.3774 -0.0208 0.3108 8 34.25 1.2163 0.0049 0.3557 0.0057 0.2919 9 38.22 1.1559 0.0221 0.3309 0.0191 0.2662 10 40.23 1.1643 -0.0049 0.3453 -0.0042 0.2966 11 42.23 1.1660 -0.0197 0.3536 -0.0170 0.3051 12 44.22 1.1569 -0.0197 0.3536 -0.0170 0.3051 13 45.33 1.1565 -0.0208 0.3526 -0.0174 0.3049 14 46.24 1.1555 -0.0208 0.3694 -0.0177 0.3097 15 50.25 1.1752 -0.0246 0.3641 -0.0198 0.3094 16 51.36 1.1730 -0.0246 0.3641 -0.0208 0.3104 17 55.20 1.2008 -0.0301 0.3659 -0.0225 0.3122 18 50.29 1.2208 -0.0301 0.3659 -0.0246 0.3160	3										
7 39-27 1-2/88 -9-0-266 0-3-76 -0-0-208 0-3108 8 39-25 1-2163 0-00-9 0-3557 0-0057 0-2919 9 38-22 1-1559 0-0221 0-3109 0-0191 0-2662 10 40-23 1-16-3 -0-00-9 0-3553 -0-00-2 0-2966 11 42-23 1-16-9 -0-0197 0-3536 -0-0170 0-3051 12 44-22 1-15-9 -0-0197 0-3536 -0-0170 0-3051 13 45-33 1-15-5 -0-0207 0-3526 -0-0176 0-3049 14 46-24 1-15-5 -0-0208 0-3609 -0-0177 0-3097 15 50-25 1-1/52 -0-0238 0-3691 -0-0198 0-3098 17 55-20 1-2408 -0-0244 0-36-1 -0-0208 0-3164 17 55-20 1-2408 -0-0244 0-36-1 -0-0208 0-3164 17 55-20 1-2408 -0-0301 0-36-9 -0-0246 0-3160	-										
8 30.25 1.2183 U.UUNY (.3557 U.0057 0.2919 9 38.22 1.1559 0.U221 (.3309 0.0191 0.2862 10 40.23 1.1643 -0.0049 U.3453 -0.0042 0.2966 11 42.23 1.1600 -0.0197 (.3536 -0.0173 0.3038 12 44.22 1.1569 -0.U1Y7 (.3536 -0.0170 0.3051 13 45.33 1.1565 -0.U27 U.3526 -0.0170 0.3069 14 46.24 1.155 -0.U200 U.3607 -0.0177 0.3097 15 50.25 1.1752 -0.U232 U.3641 -0.0198 0.3098 16 51.36 1.1730 -0.0244 (.3641 -0.0198 0.3104 17 54.20 1.2400 -0.0249 U.3743 -0.0235 0.3122 18 50.29 1.2200 -0.0301 U.3750 -0.0240 0.3160	<u> </u>										
10	_		, 7	1.2163	u. u 059			0.2919			
11	_										<del></del>
12	-										
13									n	<del></del>	
14 46.24 ].1655 ~0.0206 0.3067 -0.0177 0.3097 15 50.25 ].1/52 -0.1232 0.3041 -0.0198 0.3098 16 51.36 1.1730 -0.0244 0.3041 -0.0208 0.3104 17 54.20  .200 -0.0231 0.3743 -0.0245 0.3122 18 56.29  .2206 -0.0301 0.3658 -0.0246 0.3160											
15 50.25 1.1/52 -0.1232 0.3041 -0.0198 0.3098 16 51.36 1.1730 -0.0244 0.3041 -0.0208 0.3104 17 54.20 1.200 -0.0233 0.3743 -0.0235 0.3122 18 56.29 1.2206 -0.0301 0.3658 -0.0246 0.3160											
17 55.20 1.200 -0.0293 0.3740 -0.0235 0.3122 18 56.29 1.220c -0.0301 0.3050 -0.0246 0.3160											
18 56.79 1.2200.0301 0.3050 -0.0246 0.3160											
	Control of the Control										
										•	
	17	- 3/ 4/		I AZZON		_114.37111.		HAJI (B.	<del></del>		
											_
						<del></del>		······································			
											•
								· <u>-</u>			<del></del>
						•					
							<del></del>		<del></del>	* ***	
						_					
					<del></del>						<del></del>

GE	ENGINEES 1 OF 1 1 OF 1		OPMENT (	ENTER (AEC	MA	TIN MISSI	TUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA ER PLATE DATA	TENODYNAMIC HIND TUNNEL (4)
				CONF TRAI				
TAIT	2 ALPHA	173 u.98	2+7 CH	F14 /	REE	YCPF		
M i	58-11	1-136a	-		-0.0755			
2	59.16	1.1552			-0.0269	0.3164		
3	_60.14	اعلاملة	-0.6322	0.3096	-0.4277	0.3177		·
•	61.19	1.1705	-0.3337		-0.0288	0.3169		
.5 . <u> </u>				4.3/25	_0.029 <u>6</u>		<del></del>	
6	63.18		-0.635A	0.3/43	-0.0308	0-3216		
8	64.14	1 1506	-0-0375	- 3726	-0.0328 -0.0344	0.3240		
9	_68.19				0-0365			
10	70.20		-0.0445		-0.0389	0.3302	· · · · · · · · · · · · · · · · · · ·	
ii			-0.0-27			0.3323		
15	74.21	1.1546		0.3409	-0.0455	0.3358		
13	76.22	lale73			E940-0-			
14	75.23	1-1426			-0.0527	0.3404		
15_					0.0566	0.3397		<del></del>
16	82.74	1-1-77			-0.0595 -0.0627	0.3416	_	
16		1.1936			-0.0664	0.3464		
19					-0-0684			<u> </u>
							-	
		_						
								•
						<del></del>		
					•			
								<del> </del>

MEET 1 OF 1  ***********************************				OPMENT	CEMILALIAEL	C) 280P	ULSION DIND TU	NYEL FACILITY	Y LPWT)	AEHODYNAMIC MIND THNHEL (AT
TEST PART ACM FX10-4 COM TRANSITION  2 174 0.90 2.5 F14 FACE  POINT ALPMA CMF CM CM CM CM CM CMF YCPF  1 88.08 1.1203 -0.0795 0.3491 -0.0767 0.3565 2 90.00 1.1114 -0.0602 0.3497 -0.0757 0.3565 3 91.13 1.1095 -0.0070 0.3421 -0.020 0.3536 5 93.14 1.115 -0.091 0.3931 -0.0020 0.3536 5 93.14 1.115 -0.091 0.3931 -0.0020 0.3568 6 90.10 1.1114 -0.090 0.3766 -0.0890 0.3568 6 90.10 1.1114 -0.01045 C.3491 -0.0078 0.3578 7 96.10 1.1114 -0.11415 C.3491 -0.078 0.3578 8 98.10 1.112 -0.1161 0.0002 0.0162 0.3592 9 100.15 1.1164 -0.1224 0.4044 -0.1099 0.3561 10 102.15 1.1164 -0.1224 0.4044 -0.1099 0.3621 11 100.15 1.1231 -0.1762 0.0057 -0.1141 0.3612 11 100.16 1.1220 -0.1371 0.0049 -0.1222 0.3609 13 100.17 1.1234 -0.1603 0.0174 0.3178 14 116.17 1.1247 -0.1455 0.0104 -0.1260 0.3608 15 112.16 1.1335 -0.1497 0.0114 0.01285 0.3609 16 114.19 1.1007 -0.1490 0.4127 -0.1306 0.3620 17 116.20 1.1165 -0.1521 0.4194 -0.1265 0.3699 17 116.20 1.1165 -0.1521 0.4194 -0.1305 0.3599 18 117.21 1.1702 -0.1530 0.0222 -0.1306 0.3608									DATA	
2 174 0.90 2.5 F14 F4EE  **OINT ALPHA CNF CN CH CH ACPF VCPF  1 68.08 1.1243 -0.1795 0.3691 -0.0767 0.3661  2 40.00 1.1111 -0.0002 0.3497 -0.0757 0.3505  3 91.13 1.1115 -0.3911 0.3931 -0.0020 0.3536  5 93.14 1.1122 -0.0912 0.3496 -0.0896 0.3548  6 90.10 1.1114 -0.0090 0.3466 -0.0896 0.3548  6 90.10 1.1114 -0.0090 0.3466 -0.0896 0.3548  7 96.10 1.1102 -0.1161 0.4002 -0.1040 0.3549  7 96.10 1.1102 -0.1161 0.4002 -0.1040 0.3578  8 95.10 1.1102 -0.1161 0.4002 -0.1040 0.3578  10 102.15 1.1261 -0.1222 0.4044 -0.1099 0.3621  10 102.15 1.1261 -0.1262 0.4057 -0.1141 0.3612  11 100.16 1.1220 -0.1371 0.4009 -0.1220 0.3609  13 100.17 1.1231 -0.1603 0.4009 -0.1220 0.3609  13 100.17 1.1231 -0.1635 0.4009 -0.1260 0.3609  14 110.17 1.1240 -0.1635 0.4009 -0.1260 0.3609  15 112.16 1.1335 -0.1657 0.4116 -0.1265 0.3609  16 114.19 1.1007 -0.1400 0.4129 -0.1306 0.3620  17 116.20 1.1555 -0.1521 0.4129 -0.1305 0.3509  18 117.21 1.1702 -0.1530 0.4222 -0.1306 0.3609	PEI	1 UF 1				****	SPLITIER	LAIE DAIA		
2 174 0.90 2.5 F14 F4EE  POINT ALPHA CNF CN C1 ACPF VCPF  1 68.08 1.1243 -0.0795 0.3491 -0.0767 0.3461  2 40.00 1.1114 -0.0462 0.3497 -0.0757 0.3461  2 40.00 1.1114 -0.0462 0.3492 -0.0764 0.3533  4 92.13 1.1115 -0.3411 0.3431 -0.0402 0.3534  4 92.13 1.1115 -0.3411 0.3431 -0.0402 0.3536  5 93.14 1.1122 -0.0490 0.3466 -0.0890 0.3548  6 94.14 1.1114 -0.0490 0.3466 -0.0890 0.3548  7 96.14 1.1114 -0.0490 0.3466 -0.0890 0.3548  8 48.14 1.1122 -0.1145 C.3484 -0.0478 0.3578  8 48.14 1.1122 -0.1161 0.4002 -0.1042 0.3592  9 100.15 1.1164 -0.1224 0.4044 -0.1039 0.3621  10 102.15 1.1231 -0.1262 0.4057 -0.1141 0.3612  11 104.16 1.1232 -0.1322 0.4091 -0.1174 0.3623  12 106.16 1.1230 -0.1371 0.4049 -0.122 0.3609  13 109.17 1.1234 -0.1403 0.4049 -0.122 0.3609  14 110.17 1.1247 -0.1457 0.4104 -0.1249 0.3632  16 114.19 1.107 -0.1490 0.4124 -0.1306 0.3620  17 116.70 1.105 -0.1491 0.4124 -0.1305 0.3639  18 117.21 1.1702 -0.1530 0.422 -0.1305 0.3608			· · · · · · · · · · · · · · · · · · ·							
2 174 0.96 2.5 F14 F4EE  POINT ALPHA CMF CM CM CM ACPF VCPF  1 68.08 1.1243 -0.0795 0.3691 -0.0767 0.3661  2 V0.06 1.1114 -0.6642 0.3497 -0.0757 0.3505 3 91.13 1.1497 -0.070 0.3421 -0.0784 0.3533  4 92.13 1.1115 -0.3411 0.3431 -0.0420 0.3536 5 93.14 1.1122 -0.0462 0.3466 -0.0896 0.3548 6 94.14 1.1124 -0.0490 0.3466 -0.0890 0.3548 6 94.14 1.114 -0.0490 0.3466 -0.0890 0.3548 7 96.14 1.1142 -0.1185 0.3494 -0.0478 0.3578 8 V8.14 1.1122 -0.1185 0.3494 -0.0978 0.3578 9 100.15 1.1164 -0.1224 0.4044 -0.1039 0.3621 10 102.15 1.1231 -0.1262 0.4057 -0.1141 0.3612 11 104.16 1.1229 -0.1326 0.4057 -0.1141 0.3612 11 105.16 1.1229 -0.1311 0.4049 -0.1222 0.3609 13 104.17 1.1240 -0.1463 0.4478 -0.1249 0.3623 14 110.17 1.1240 -0.1463 0.4478 -0.1249 0.3632 15 112.16 1.1334 -0.1463 0.4478 -0.1249 0.3632 16 114.19 1.1407 -0.1440 0.4124 -0.1265 0.3648 17 116.20 1.1656 -0.1621 0.4124 -0.1306 0.3620 17 116.20 1.1656 -0.1621 0.4124 -0.1305 0.3608 18 117.21 1.1702 -0.1530 0.4222 -0.1306 0.3608		_922		. === .			•	•		
POINT ALPHA CMF CM CA ACPF VCPF  1										
2	POINT									
3 91.13 1.147 -0.0070	<del></del>									
4 92.13 1.115 -0.341 0.3431 -0.0620 0.3536 5 93.16 1.1122 -0.0402 0.3466 -0.0840 0.3548 6 94.14 1.114 -0.0440 0.3466 -0.0840 0.3549 7 96.14 1.1142 -0.1161 0.4002 -0.1042 0.3578 8 98.14 1.1142 -0.1161 0.4002 -0.1042 0.3592 9 190.15 1.1166 -0.1224 0.4044 -0.1099 0.3621 10 102.15 1.1231 -0.1262 0.4057 -0.1141 0.3612 11 104.16 1.1232 -0.1322 0.4091 -0.1174 0.3623 12 106.16 1.1220 -0.1371 0.4049 -0.1222 0.3609 13 109.17 1.1230 -0.1603 0.4049 -0.1222 0.3609 13 109.17 1.1230 -0.1603 0.4049 -0.1220 0.3632 14 116.17 1.1247 -0.1455 0.4104 -0.1276 0.3646 15 112.16 1.1334 -0.1657 0.4114 -0.1285 0.3630 16 114.19 1.1607 -0.1490 0.4124 -0.1306 0.3620 17 116.20 1.1556 -0.1521 0.4125 -0.1305 0.3699 18 117.21 1.1702 -0.1530 0.4222 -0.1306 0.3608	2						0.3505			
5 93.14 1.1122 -0.0762 0.3766 -0.0855 0.3548 6 94.14 1.114 -0.0790 0.3766 -0.0870 0.3549 7 96.14 1.107 -0.1045 0.3707 0.3578 8 98.14 1.1122 -0.1161 0.4002 -0.1022 0.3592 9 190.15 1.1161 -0.1222 0.4044 -0.1039 0.3621 10 102.15 1.1231 -0.1262 0.4057 -0.1141 0.3612 11 104.16 1.1232 -0.1322 0.4091 -0.1174 0.3623 12 106.16 1.1220 -0.1371 0.4049 -0.1222 0.3609 13 104.17 1.1230 -0.1403 0.4078 -0.1222 0.3609 14 110.17 1.1230 -0.1403 0.4078 -0.1249 0.3632 14 110.17 1.1230 -0.1403 0.4104 -0.1276 0.3640 15 112.16 1.1334 -0.1457 0.4110 -0.1285 0.3630 16 114.19 1.1407 -0.1490 0.4124 -0.1306 0.3620 17 116.20 1.165c -0.1521 0.4145 -0.1305 0.3599 16 117.21 1.1702 -0.1530 0.4222 -0.1306 0.3608										
6 94.14 1.114 -0.0790 0.3766 -0.0870 0.3549 7 96.14 1.127 -0.1285 0.3724 -0.0778 0.3578 8 98.14 1.112 -0.1161 0.4002 -0.102 0.3592 9 190.15 1.1164 -0.1224 0.4044 -0.1099 0.3621 10 102.15 1.1231 -0.1262 0.4057 -0.1141 0.3612 11 124.16 1.1272 -0.1371 0.4047 -0.122 0.3609 12 106.16 1.1220 -0.1371 0.4047 -0.1222 0.3609 13 104.17 1.1234 -0.1403 0.4174 -0.1249 0.3632 14 116.17 1.1247 -0.1435 0.4104 -0.1276 0.3648 15 112.16 1.1334 -0.1407 0.4114 -0.1285 0.3630 16 114.19 1.107 -0.1490 0.4127 -0.1306 0.3620 17 116.20 1.105c -0.1530 0.422 -0.1306 0.3608	_5							·		
8	6	94.14	1.1114	-0.0990	0.3766	-0.0890	0.3569			
9 190-15 1-116t -0.122+ 0.4044 -0.1099 0.3621 10 102-15 1-1231 -0.1262 0.4057 -0.1141 0.3612 11 104-16 1-1292 -0.1326 0.4091 -0.1174 0.3623 12 106-16 1-1220 -0.1371 0.4049 -0.1222 0.3609 13 109-17 1-1230 -0.1403 0.4174 -0.1249 0.3632 14 116-17 1-1247 -0.1435 0.4104 -0.1276 0.3646 15 112-16 1-1334 -0.1457 0.4116 -0.1285 0.3630 16 114-19 1-1407 -0.1490 0.4129 -0.1306 0.3620 17 116-20 1-1656 -0.1521 0.4195 -0.1305 0.3599 18 117-21 1-1702 -0.1530 0.4222 -0.1306 0.3608										
10 102.15 1.1c31 -0.1262 0.4057 -0.1141 0.3612 11 104.16 1.1292 -0.1326 0.4091 -0.1174 0.3623 12 106.16 1.1220 -0.1371 0.4049 -0.1222 0.3609 13 104.17 1.1c30 -0.1403 0.4049 -0.1269 0.3632 14 116.17 1.1c47 -0.1435 0.4104 -0.1276 0.3640 15 112.16 1.1334 -0.1457 0.4114 -0.1285 0.3630 16 114.19 1.1c07 -0.1490 0.4124 -0.1306 0.3620 17 116.20 1.165c -0.1521 0.4145 -0.1305 0.3599 18 117.21 1.170c -0.1530 0.4222 -0.1306 0.3608	- I									
11 109-16 1-1292 -0-1326										
12 106.16 1.1220 -0.1371 0.4049 -0.1222 0.3609 13 109.17 1.1230 -0.1403 0.4.78 -0.1249 0.3632 14 110.17 1.1247 -0.1435 0.4104 -0.1276 0.3640 15 112.16 1.1335 -0.1457 0.4116 -0.1285 0.3630 16 114.19 1.1407 -0.1490 0.4124 -0.1306 0.3620 17 116.20 1.155c -0.1521 0.4145 -0.1305 0.3599 18 117.21 1.1702 -0.1530 0.4222 -0.1306 0.3608	_									
13 109-17 1-1634 -0-1603 G-0-78 -0-1269 G-3632 14 11G-17 1-1647 -0-1435 0-4104 -0-1276 0-3646 15 112-16 1-1335 -0-1657 0-4116 -0-1285 G-3630 16 114-19 1-1607 -0-1690 G-6129 -0-1306 0-3620 17 116-20 1-1655 -0-1521 G-6129 -0-1305 G-3599 18 117-21 1-1702 -0-1530 0-0-222 -0-1306 0-3608										
15 112.16 1.1335 -0.1657 0.416 -0.1265 0.3630 16 114.19 1.1607 -0.1690 0.4127 -0.1306 0.3620 17 116.70 1.1655 -0.1521 0.4125 -0.1305 0.3599 18 117.21 1.1702 -0.1530 0.422 -0.1306 0.3608										
16 114.19 1.1007 -0.1490 0.412v -0.1306 0.3620 17 116.20 1.105c -0.1521 0.41v5 -0.1305 0.3599 18 117.21 1.170c -0.1530 0.422 -0.1306 0.3608	14					-0-1276	0.3640			
17 116.20 1.165c -0.1521 0.4145 -0.1305 0.3599 18 117.21 1.170c -0.1530 0.422 -0.1306 0.3608		112.16							· · · · · · · · · · · · · · · · · · ·	<del> </del>
18 117.21 1.1702 -0.1530 0.422 -0.1306 0.3608										
*									<del> </del>	
	10	111061	101.05	-0.1330	0.4666	-061306	0.3000			€
					<del></del>			·		
								•		
								<del></del>		
				<del></del>					<del></del>	
			_							
							<del> </del>	<del></del>	<del></del>	
										· · · · · · · · · · · · · · · · · · ·
									· · <del> </del>	
	~	·								
									<del></del>	<del></del>

GE	ENGINEES 1 OF 1 1 OF 1	ING. DEVE	LOPMENT CI	ENIER (AED	AM	TIN MISSILE TAIL EFFECTS SPLITTER PLATE DATA	
	1 <b>FP</b> T	175 U.Sa	₽ 9X10-6_0 2.5		BEE STITES		
OINT	ALPHA	CNF	CH	Co	xCDF	YCPF	
1	118-05		-0.1515			0.1573	
2	114.06	1.1020	-0.1525	0163	-0.1312	0.3583	
_3	120.05		=0.1537			0.3559	<del></del>
•	121-10		-0.1542		-0.1301	0.3552	
_5	155-10		-0-155A		0.1320	0.3566	
7	123.11		-0.1559		-0.1302 -0.1305	0.3556	
8	120.12		=0.1505		-0.1317	0.3539	
9	129.11		-0.1246		-0.1331	0.3536	
10	130.12		-0-1732		-0.1340	0.3540	
11	132.12	1.1400	-0.1538		-0.1350	0.3516	
12	134.12		-0.1555		-0.1360	0.3505	
13_	135.12		-0.155t		-0-13-2	0-3502	<del></del>
1 4	138.13		-0.1571		-0.1362	0.3504	
15 16	142.15		-0.1563 -0.1559		-0-1408 -0-1429	0.3496	
17	144.16		-0.1559		-0.1.71	0.3491	
18	106.17		-0.1546		-0.1523	0.3526	
19		6.9425	-0.1592	6.3505	-0-1554	0.3532	· · · · · · · · · · · · · · · · · · ·
		<del>i</del>				·	
			<del></del>		<del></del>	··	
						<u> </u>	
							= = =
					· · · · · · · · · · · · · · · · · · ·	<del></del>	
						····	

GE I	OF 1	ING DEVE	LOPHENI C	ENTERIALD		HTIN MISSI	G TUNNEL FACILITY(PMT) LE TAIL EFFECTS DATA ER PLATE DATA		<u></u>
	TEST	PARI MAL	H_HX19-6_	CUSE_IRAN	SITION				
	5	176 0.50			REE				
OINT	ALPHA	CNF	Сн	C:+	XCPF	YCPF		,	
<u> </u>	45.00	0.9dka	-0-1555	9.3945	-0.1573	0.3686			
-	49.46	4646.0	-0.1552	v.3397		0.3525			
	150 <u>-06</u> 151-06		-0.1562		-0.1550 -0.1697	_0 <u>.352<b>S</b></u>			
	152.07		-0.1562 -0.1627			_9.3590			
	57.06		-0.1576		-0.1927	0.3602			
1	154.46	0.6.21	-0.1577	6-3028	-0-1895	0.3639			
	156.07		-0-1536		-0.2021	0.3704			
	158.06		-0-1714 - -0-1019		<u>-0.2350</u> -0.2477	0.3861 0:3837			
	162.47		-0-1019 0-1-65		-0.2596	-0-3097			
	14.06		-0.1356	0.1915		0.3846			
13	166.07	0-4/43	-0-1204	G-1618	-0-2850	0.3614			
	lok.cu		-0.1040	0.1336		6.3824			
	170-0a_				0-3127	0 <u>_3735</u>			
	172.10 174.11		-0.0703 -6.0536		-0.3251 -0.3368	0.3533			
	174.11		-0.0351		-0.3345	0.2769			
			-0.0202		-0.3325	0.2350		•	
		<del></del>				<del></del>			
•							.•		
····									
				·					
									_
								· · · · · · · · · · · · · · · · · · ·	
· · · · · · ·						<u> </u>			

						-	•	: .
		<u>,,,</u>		<del>-,</del>				
								· · · · · · · · · · · · · · · · · · ·
<del></del>								
HNOLD.	ENGINEE	RING DEVEL	LOPHENT	ENTERCAEU	C1PROF	ULSION -	IND TUNNEL FACILITY (PHT)	AERODYNAMIC HIND TUNNEL (AT)
AGE	1 OF 1				H	ZIM FITAL	SILE TAIL EFFECTS DATA	
		<u>-</u>						
	<del>-</del>				·			
		PART PAC	H RX10-6	CUNF TRAN				
	2	177 0.98	2.5	F14 F	REE			
POINT	ALPHA	CMF	CH	Co	ACPI	YCPF		
_ <u>}_</u>	178.99	0.0407	-n.v112	0.0013	-0.3095	0.0315		
	100.01	0. VE+U_	-0.0042	-3-0636	-0-1746	-0-1501		
2		0.0076	0.0071	-6.0114	0.25d3 -0.7938	-1.4563		
6	183.05	-0.UZE	0.0143	-0.0595	-0.5242	0.7509		
	164.06	4010-0-	0.0407	-6.0424	-0-9384	0.6056		
8	186.05	-6.4467	0.0229	-0.0361	-0.4709	0.7417		
		<del></del>	······································					
		<del></del>				100		
								•
		·····					······································	
					- ·			<u> </u>
								•
							<del></del>	
								· · · · · · · · · · · · · · · · · · ·
	•							·
					<del>.</del>			
				<del></del>	··			
							·	
					<del></del>			<del></del>
		-						
							· · · · · · · · · · · · · · · · · · ·	·

TEST PAPT WALT WAID-A CONF. TRANSILION  2 184 U.BU 2.5 F11 FREE  POINT ALPMA C. C. C. C. KOPF VEPF  1 -2.03 -0.001 -0.0221 -0.022 0.022 0.0255  2 -0.07 -0.001 -0.0221 -0.022 0.022 0.0255  3 -0.07 -0.001 -0.0201 -0.0201 -0.022 0.0255  5 -0.07 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001 -0.00				YCPF 0.0625 0.7886	XCPF	F11 FR	2.5	184 0.60	IESI	TET .
TEST   PAPE   MAID   CONF. TRANSTITION				0.7886	XCPF	F11 FR	2.5	184 0.60	5	
TEST PART   PACE   STANSSITION				0.7886	XCPF	F11 FR	2.5	184 0.60	5	·
2 184 v.bu 2.5				0.7886	XCPF	F11 FR	2.5	184 0.60	5	
1 -2.04 -0.0201 -0.0201 -0.0322 0.4°21 0.6925 2 -0.07 -0.0234 -0.0122 -0.0104 0.5232 0.7866 3				0.7886	0.4021		r-		AL Gua	
-2.04				0.7886	0.4021					POINT
3					A 4			-0-0-01	-2.09	1
\$ 1.00 0.0223 0.0033 0.0000 0.1058 0.2667  \$ 2.06 0.6053 0.0112 0.0103 0.2661 0.3586  \$ 3.05 0.6070 0.0266 0.0324 0.3048 0.0651  \$ 4.00 0.0745 0.0274 0.0234 0.3112 0.6578  \$ 6.08 0.1571 0.0003 0.0766 0.2765 0.6689  \$ 9 0.09 0.2270 0.0013 0.1150 0.2096 0.5070  10 10.11 0.3060 0.0717 0.1552 0.2344 0.5073  11 12.13 0.3702 0.0766 0.1792 0.2210 0.0105  12 10.10 0.0766 0.0775 0.2008 0.1032 0.5073  13 16.16 0.5509 0.0766 0.2767 0.1371 0.5059  14 19.16 0.0012 0.0047 0.3230 0.1007 0.5037  15 20.16 0.7252 0.0091 0.3621 0.0948 0.4966  16 22.19 0.7766 0.0563 0.3763 0.0731 0.0907  17 20.20 0.7895 0.0450 0.3763 0.0568 0.4862										2
5 2.06 0.053 0.0112 0.0103 0.2561 0.3586 0 3.05 0.0576 0.0206 0.0324 0.3748 0.4851 7 4.06 0.0745 0.0245 0.033 0.3112 0.4578 6 6.08 0.1571 0.043 0.0156 0.2745 0.4689 9 6.09 0.276 0.013 0.1156 0.244 0.5074 10 10.11 0.3060 0.0717 0.1552 0.244 0.5073 11 12.13 0.3702 0.0746 0.1792 0.2710 0.5105 12 14.14 0.4746 0.0775 0.2408 0.1032 0.5073 13 16.16 0.5509 0.0700 0.2747 0.1341 0.5059 14 14.16 0.4612 0.0470 0.2230 0.132 0.5059 15 20.16 0.7746 0.0563 0.3763 0.4966 16 22.19 0.7746 0.0563 0.3763 0.4966 17 24.20 0.7855 0.0452 0.3763 0.4862										-3-
7										
6       6.08       0.1541       0.443       0.0746       0.2745       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4689       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669       0.4669 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>•</td></td<>										•
9										
10										
12 10-10 0-0766 0-0775 0-2008 0-1032 0-5073 13 16-16 0-5509 0-4766 0-2767 0-1391 0-5059 14 19-16 0-6012 0-0691 0-3230 0-1007 0-5037 15 20-16 0-7292 0-0691 0-3621 0-8968 16 22-19 0-7766 0-563 0-3763 0-0731 0-6907 17 20-20 0-7695 0-0452 0-43717 0-0507 0-4836 18 26-21 0-7700 0-400 0-3763 0-0568 0-4862		•		0.5073	0.2344	0.1552	0.0717	0.3060	10.11	
13 16-16 0-5509 0-1765 0-2767 0-1391 0-5059 14 19-16 0-6612 0-0697 0-3230 0-1567 0-5037 15 20-16 0-7292 0-0691 0-3621 0-0966 16 22-19 0-7766 0-0563 0-3763 0-0731 0-6907 17 24-20 0-7695 0-0452 0-1717 0-0587 0-4836 18 26-21 0-7760 0-1460 0-3763 0-0568 0-4862										
14 19-16 0-0-12 0-0-47 0-3230 0-1-0-7 0-5037 15 20-16 0-7-92 0-0-91 0-3621 0-0-9-8 0-4966 16 22-19 0-77-04 0-0-6-3 0-37-03 0-0-731 0-0-907 17 20-20 0-7-0-5 0-0-5-2 0-3717 0-0-5-87 0-4836 18 26-21 0-77-0 0-0-0-0 0-37-03 0-0-5-6 0-4862										
16 22-19 0.776# 6.0563 0.3763 0.0731 0.4987 17 24-20 0.7655 0.6452 0.3717 0.0587 0.4836 18 26-21 0.7740 0.0440 0.3763 0.0568 0.4862										
17 24-20 0.7695 0.0452 0.3717 0.0587 0.4836 18 26.21 0.7740 0.0440 0.3763 0.0568 0.4862										
18 26.21 0.7740 0.0440 0.3763 0.0568 0.4862										
	<del></del>									
			· · · · · · · · · · · · · · · · · · ·							
		•								
		<del></del>	<del></del>	<del></del>						
					<del></del>					
· · · · · · · · · · · · · · · · · · ·	<del></del> -	<del></del>		<del></del>				<del></del>		
			•							
				<u> </u>			····			

<u>.</u>	NGINEEF OF 1 OF 1	PING_PEAF	_DPMENT_CE	MTERLAEDO	1PROPI	<u>ulsion bino turnel.</u> Itin missile tail ei splitter_plate.i	FACILITY (PVI) FFECTS DATA DATA	AEHDUTUNEL_GI
<u>.                                    </u>							,	
	- irri	145 0.60		<u>ione irans</u> Fil ++	EE ITIO≈		······································	
ÑT.	ALPHA	CNF	CH	Cr		YCPF		
	29.06	<u>0-107u</u>	0-1415	4.3791		0.4804	·	
	24.15	0.7442	0.4-74	0.3068	0.0-31	0.4639		
_	_30.15_ 31.16	0.5441	0.v+27 0.0+23	3457 . 4.3486	.0.4525 . 0.0513	0.4833		
	35.16			0.3788	0-0-74			
	33.15	0.8374	(ieijum5	U-405A	0.6450	0.4845		
	34-17	0.0516		0.4101		0-4016		
•	30.16	0.0/36	0.4345	0.4210	0.0394	0.4620		
<b>-</b> ·	39.17		6-4317	U-4351	0.4352	0.4826		
	+0.18	0.9266	0.0544	0.0009	0.0315	0.4844		
	92.19		0.0273	0.45.72		0-4826	· · · · · · · · · · · · · · · · · · ·	······································
2	44.20	0.9615	0.7234	0.4/36	0.0238	0.4625		
	44.55	1.0475		0-4-92		0.4855		
	50.21		0.1184	0.5090 <u>0.5176</u>	0.0160	0.4859 0.4872		
5	52.23	1.0579	0.0135	0.5340	0.0125	0.4908		
7	54.24	1.1.01		u.5387		0.4897		
A	56.25	1.1134	0.0060	U.5491	0.0054	0.4932		
4	57.25	1.1235		0.5535				
						· · · · · · · · · · · · · · · · · · ·		
		···		<del></del>			·	· · · · · · · · · · · · · · · · · · ·
		-						
							•	•
			<del> </del>					
				1000				
						<del></del>	· · · · · · · · · · · · · · · · · · ·	

2 3	IEST 2 ALPHA 58-10 59-16	186 U.BU	<u> </u>						
2 3	58-10	-		F11 +	SITION				
2 3 •			Сн	C+		YCPF		·····	
3 5	3-110	1.0595	0.0:20	545.0	0.0046	0.4924			
5	60.16		-0.5003		-0.0003	0.4915			
	61.17		-0.0025		-0.0023	0.4914			
	62.18		-0-6029		-0.0026	0. 9950	<del></del>		
	63.18		-0.0048		-0.0044	0-4940			
	64.17	101-35	-0.00re	6.5467	-0.0047	0.4965			
	68-18		-0.0110	0.5507	-0.0098	0.5020			
	70,19	1.1621	-0.0167	0.5640	-0.0149	0.5027			
	72.19	1.1.84	-0.0235		-0-0205				
	74.20	1.1525	-0.32-9		-0.0216	0.5071			
	75-20		-40 uc 13		-0-0235	-0-7105	<del></del>		
	78.21 79.31		-0.0351 -0.6376		-0.0299 -0.0318	0.5063			
	95.55		-0.0-39		-0.0370	0.5156			
	64.23		-0-6-78		-0.419	0.5151			
	66.23		-0.0-36		-0.0449	0.5218		501	
9	67.23		-0.0579	0-6136	-0.0488	0.5173			
					<del></del>				
	-								
			·		<del></del>				
							•	<del></del>	
							·	** ! *******	
								· · · · · · · · ·	

NT AL HE	2 LPMB 6-1u 9-10 0-16 1-17 2-16 3-17 4-16 6-17 6-16 0-16 2-17	187 0.80 CRF 1.1573 1.1504 1.1557 1.1546 1.1546 1.1646 1.1647 1.171	Cn =0.0567 -0.0591 -0.0687 -0.0787 -0.0769 -0.0756 -0.0566 -0.057	CE Jahl22 U-6007 U-9200 U-6008 U-949 J-5499 U-5499 U-6003 U-6003	#EE #CPF -0.0514 -0.0550 -0.0594 -0.0637	YCPF 0.5203 0.5222 0.5214 0.5140 0.5140 0.5140			-		
91 92 93 94 95 100 100 100	8.1u 9.10 0.16 1.17 2.16 3.17 4.16 6.17 8.16 0.18 2.17 4.16	1-1573 1-1504 1-1557 1-1579 1-1546 1-1646 1-1646 1-1719 1-1719	-0.0567 -0.0591 -0.0533 -0.0687 -0.0737 -0.0769 -0.0759 -0.0556 -0.0557	J.6122 U.8007 U.9200 U.6008 U.6009 U.5799 U.6003	-0.0490 -0.0514 -0.0550 -0.0594 -0.0637 -0.0665	0.5203 0.5222 0.521a 0.5199 0.5191					
90	9.10 0.16 1.17 2.16 3.17 4.16 6.17 8.16 0.18 2.17	1.1504 1.1557 1.1579 1.1549 1.1569 1.1699 1.1719	-0.0591 -0.0633 -0.0687 -0.0737 -0.0759 -0.0759 -0.0556 -0.0557	0.007 0.002 0.000 0.000 0.000 0.000 0.000	-0.0514 -0.0550 -0.0594 -0.0637 -0.0665	0.5222 0.521a 0.5190 0.5181 0.5190					
90 91 92 92 96 100 100 100 100	0.16 1.17 2.16 3.17 4.16 6.17 8.16 0.18 2.17	1.157 1.157 1.159 1.159 1.159 1.169 1.171 1.171	-0.0633 -0.0687 -0.0737 -0.0769 -0.0769 -0.0556 -0.0557	0.000 0.000 0.000 0.000 0.000 0.000	-0.0550 -0.0594 -0.0637 -0.0665	0.5216 0.5199 0.5181 0.5190			 		
91 92 93 94 96 100 100 100 100	1.17 2.16 3.17 4.16 6.17 8.16 0.18 2.17	1.1557 1.1279 1.1500 1.1509 1.1600 1.1719 1.1719	-0.0687 -0.0737 -0.0769 -0.0769 -0.0556 -0.0556	0.6008 5.2999 0.5990 0.6003	-0.0594 -0.0637 -0.065 -0.066	0.5199 0.5181 0.5190			 		
93 96 100 100 100 100	3.17 4.16 6.17 8.16 0.18 2.17	1.154e 1.1564 1.1642 1.1699 1.1714 1.111e	-0.0769 -0.6794 -0.0556 -0.0557	0.6003 0.601H	-0.0665 -0.0666	0.5190		<del></del>			
96 96 100 100 100 100 100	4.16 6.17 8.16 0.18 2.17	1.1569 1.1692 1.1699 1.1719	-0.0794 -0.0556 -6.0916 -0.0957	0.6003 0.601H	-0-0046						
100 100 100 100 100	6.17 8.16 0.18 2.17 4.16	1.1696 1.1699 1.1710 1.171n	-0.0556 -0.0516 -0.057	G.6018					 		
100 102 104 106	0.18 2.17 4.18	1.1719	-0.0957	6-5464		0.5169					
100	2.17 4.16	1.1710			-0-0763	0.5128			 		
100	4.16		-0.1000		-0.0816 -0.0554	0.5111					
100		1.1/35	-0.1036		-0.0663	0.5069			 		
	6.15	1.1727	-0.1u76	6.5.19	-0.6918	0-5067			 		
-11	8.19		-0.1130		-0-0959	0.5064					
117	0.19 2.21		_=0.1145_ =0.1174		-0.09A3 -0.1013	0.5020 0.5050	···		 		
	4.21		-0-1204		-0-1048	0.5021			 		
110	6.22	1.1-09	-0-1237	0.5693	-0.1081	0.4990			 		
11	7.22	1.1392	-0.1269	0.5/12	-0-1096	0.5014			 		
		_							 		
<del>-</del>									 		
									 	•	
									•		
_											
						<del></del>	<del></del>	<del></del>	 		
				•							

2 11 3 12 4 12 5 12 6 12 7 12 6 12 9 12 0 13 13 2 13 3 13 4 13 5 12 6 14	Z	CNF 1-1092 1-1006 1-1417 1-1029 1-1016 1-044 1-045 1-057 1-056 1-057 1-056 1-057 1-056 1-057 1-0465 1-077 1-466 0-965	2.5 Cm -0.1216 -0.1231 -0.1243 -0.1266 -0.1256 -0.1315 -0.1315 -0.1375 -0.1375 -0.1377 -0.1377 -0.1377 -0.1374 -0.1374	Ch 0.5547 0.5547 0.5547 0.5470 0.5470 0.5492 0.5405 0.5302 0.5170 0.5170 0.4469 0.4469 0.4469 0.4436	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	XCPF 1116 1128 1150 1175 1183 1231 1235 1331 1330 1374 1404 1438	VCPF 0.5000 0.4980 0.4980 0.4984 0.4984 0.4934 0.4934 0.4935 0.4935 0.4929 0.4915 0.4698 0.4910 0.4877 0.4857 0.4857			
1 11 2 11 3 12 4 12 5 12 6 12 6 12 9 12 0 13 1 13 2 13 3 13 4 13 5 13 6 14	Z ALPMA 19-12 20-12 21-13 23-13 23-13 23-13 23-13 23-13 24-13 30-14 30-14 30-14 30-15 30-14 30-16 40-17	CNF 1-109 1-100 1-1417 1-1029 1-1016 1-074 1-077 1-066 1-077 1-066 1-077 1-0965 1-077 1-0965 1-077 1-0965 1-077 1-0965 1-077	2.5 Cm -0.1216 -0.1231 -0.1243 -0.1266 -0.1256 -0.1315 -0.1315 -0.1375 -0.1375 -0.1377 -0.1377 -0.1377 -0.1374 -0.1374	Ch 0.5547 0.5547 0.5547 0.5470 0.5470 0.5492 0.5405 0.5302 0.5170 0.5170 0.4469 0.4469 0.4469 0.4436	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	XCPF 1116 1128 1150 1175 1183 1231 1235 1331 1330 1374 1404 1438	YCPF 0.5000 0.4980 0.4984 0.4960 0.4961 0.4936 0.4952 0.4952 0.4955 0.4960 0.4915 0.4870 0.4857 0.4850 0.4860			
1 11 2 11 3 12 4 12 5 12 6 12 6 12 9 12 0 13 1 13 2 13 3 13 4 13 5 13 6 14	19.05 19.12 20.12 21.13 23.13 24.13 26.13 27.26 30.14 32.14 34.14 34.14 34.14 34.14 34.14 34.14 34.16 46.17	CNF 1.109 1.100 1.117 1.1029 1.1010 1.0079 1.0079 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.0056 1.0071 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00571 1.00	Cm -0.1216 -0.1231 -0.1268 -0.1268 -0.1295 -0.1315 -0.1315 -0.1375 -0.1375 -0.1377 -0.1377 -0.1377	0.5547 0.5491 0.5492 0.5405 0.5403 0.5362 0.5362 0.5129 0.4469 0.4576 0.4576 0.4576	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1118 1128 1150 1175 1183 1205 1231 1256 1301 1330 1374 1404	0.5000 0.4980 0.4980 0.4980 0.4980 0.4936 0.4936 0.4952 0.4929 0.4915 0.4898 0.4918 0.4870 0.4857 0.4850 0.4860			
1 11 2 11 3 12 4 12 5 12 6 12 6 12 9 12 0 13 1 13 2 13 3 13 4 13 5 13 6 14	19.05 19.12 20.12 21.13 23.13 24.13 26.13 27.26 30.14 32.14 34.14 34.14 34.14 34.14 34.14 34.14 34.16 46.17	1.109; 1.1000 1.1117 1.1029 1.1016 1.0949 1.0979 1.0071 1.0071 1.4445 1.0184 0.9043 0.9043 0.9043 0.9043 0.9043	-0.1216 -0.1231 -0.1243 -0.1265 -0.1245 -0.1315 -0.1315 -0.1315 -0.1315 -0.1317 -0.1317 -0.1375 -0.1374	0.5547 0.5491 0.5492 0.5405 0.5403 0.5362 0.5362 0.5129 0.4469 0.4576 0.4576 0.4576	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1118 1128 1150 1175 1183 1205 1231 1256 1301 1330 1374 1404	0.5000 0.4980 0.4980 0.4980 0.4980 0.4936 0.4936 0.4952 0.4929 0.4915 0.4898 0.4918 0.4870 0.4857 0.4850 0.4860			
3 12 4 12 5 12 6 12 7 12 8 12 9 12 9 12 13 13 13 13 13 13 13 13 13 13	20.12 21.13 22.13 23.13 20.13 20.13 20.13 20.14 30.14 30.14 30.15 30.14 30.15 30.14 30.15 42.16 42.16 46.17	1.1 y 17 1.1 02 y 1.1 01 b 1.0 07 y 1.0 07 y 1.0 07 b 1.0 07 l 1.0 07	-0.1263 -0.1268 -0.1265 -0.1375 -0.1375 -0.1375 -0.1375 -0.1377 -0.1377 -0.1377 -0.1377	0.5470 0.5470 0.5492 0.5405 0.5403 0.5302 0.5176 0.5179 0.4469 0.4576 0.4436	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1128 1150 1175 1183 1205 1231 1256 1300 1374 1404 1438	0.4984 0.4960 0.4951 0.4936 0.4952 0.4952 0.4915 0.4698 0.4910 0.4879 0.4857 0.4850 0.4860			
4 12 5 12 6 12 7 12 6 12 9 13 1 13 2 13 3 13 4 13 5 13 6 14	21.13 22.13 23.13 24.13 26.13 27.26 30.14 32.14 30.15 30.15 30.15 30.15 30.15 30.16 30.15 40.15	1.1029 1.1016 1.0079 1.0066 1.0071 1.0066 1.0071 1.0066 0.9076 0.9043 0.9043 0.9043 0.9047 0.9043	-0.1268 -0.1295 -0.1395 -0.1315 -0.1375 -0.1375 -0.1375 -0.1377 -0.1377 -0.1377 -0.1377	0.5470 0.5492 0.5493 0.5302 0.5302 0.5176 0.5129 0.4469 0.4469 0.4469	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1150 1175 1183 1205 1231 1256 1301 1330 1374 1404	0.4960 0.4934 0.4935 0.4952 0.4929 0.4915 0.4696 0.4916 0.4679 0.4657 0.4650 0.4680			
5 12 6 12 7 12 6 12 9 13 1 13 2 13 3 13 4 13 5 12 6 14	22.13 23.13 26.13 26.13 27.26 30.14 32.14 34.14 34.14 39.15 39.14 39.16 47.16 46.17	1.101e 1.3949 1.0979 1.0966 1.0971 1.0445 1.0184 0.9076 0.9043 0.9047 0.9047 0.9047	-3.1295 -3.1295 -9.1315 -9.1365 -0.1375 -9.1367 -0.1367 -0.1367 -0.1377 -0.1377	0.5492 0.5405 0.5302 0.5302 0.5176 0.5129 0.4469 0.4576 0.4576	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1175 1183 1205 1231 1256 1301 1339 1374 1404	0.4941 0.4936 0.4952 0.4929 0.4915 0.4898 0.4918 0.4870 0.4857 0.4850			
6 12 7 12 6 12 9 13 1 13 2 13 3 13 5 13 6 14 7 19	23.13 20.13 26.13 27.26 30.14 30.14 34.14 34.14 34.15 37.26 47.16 46.17	1.3444 1.0074 1.0076 1.0076 1.0071 1.4445 1.0144 0.9076 0.9043 0.9467 0.9467 0.8926	-7.1295 -0.1315 -0.1339 -0.1365 -0.1375 -0.1367 -0.1367 -0.1375 -0.1376 -0.1374	0.5405 0.5362 0.5362 0.5176 0.5129 0.4469 0.4576 0.4576 0.4676	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1183 1205 1231 1256 1301 1330 1374 1404 1438	0.4936 0.4952 0.4929 0.4915 0.4898 0.4918 0.4679 0.4857 0.4850			
6 12 9 12 0 13 1 13 2 13 3 13 4 13 5 12 6 14 7 19	26.13 27.26 30.14 32.14 34.14 34.15 38.15 38.14 39.26 42.16 94.16 94.16	1.007v 1.006b 1.0071 1.0045 1.0144 0.707b 0.9043 0.7047 0.9161 0.8712	-9.1339 -2.1365 -0.1375 -0.1367 -0.1367 -0.1377 -0.1377 -0.1378 -0.1374	0.5362 0.5392 0.5176 0.5129 0.4969 0.4976 0.49710 0.4936 0.436	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1	1231 1256 1301 1330 1374 1404 1438 1457 ,	0.4929 0.4915 0.4898 0.4910 0.4879 0.4857 0.4850			
9 12 0 13 1 13 2 13 3 13 4 13 5 13 6 14 7 19	27.26 30.14 32.14 34.14 34.15 38.15 38.14 39.26 42.16 94.16	1.0066 1.0071 1.4445 1.0144 0.9076 0.9043 0.9043 0.9047 0.6926 0.6926	-0.1365 -0.1375 -2.1369 -0.1367 -0.1367 -0.1377 -0.1377 -0.1378 -0.1374	0.5392 0.5176 0.5129 0.4969 0.4979 0.49710 0.4436	-Gal -O-1 -O-1 -O-1 -O-1 -O-1	1256 1301 1330 1374 1404 1435 1457	0.4915 0.4698 0.4910 0.4679 0.4657 0.4650 0.4680			
0 13 1 13 2 13 3 13 6 13 5 13 6 14 7 19	30.14 32.14 34.14 34.15 30.15 38.14 34.26 42.16 94.16 46.17	1.0571 1.4445 1.4144 0.9674 0.9643 0.9643 0.9647 0.6926 0.6926	-0.1375 -2.1359 -0.1400 -0.1367 -0.1367 -0.1377 -0.1375 -0.1376	0.5176 0.5129 0.4469 0.4576 0.4576 0.4518 0.4436	-0.1 -0.1 -0.1 -0.1 -0.1	1301 1330 1374 1404 1438 1457	0.4898 0.4918 0.4879 0.4857 0.4850			
1 13 2 13 3 13 4 13 5 13 6 14 7 19	32.14 34.14 30.15 38.14 37.26 42.16 94.10 46.17	1.4995 1.4144 0.4776 0.4903 0.4907 0.4161 0.6926 0.8712	-9.1369 -0.1403 -0.1367 -0.1377 -0.1375 -6.1464 -0.1374	0.4769 0.4769 0.4769 0.4576 0.4510 0.4324	-0.1 -0.1 -0.1 -0.1	1330 1374 1404 1438 1457	0.4918 0.4679 0.4857 0.4650 0.4680			
2 13 3 13 4 13 5 13 6 14 7 19	34.14 30.15 38.14 39.26 42.16 94.10 46.17	1.01% 0.9076 0.9043 0.9447 0.9161 0.6926 0.6712	-0.1400 -0.1307 -0.1307 -0.1377 -0.1375 -0.1304	0.4969 U.4576 U.4576 - 0.4518 U.4436	-0.1 -0.1 -0.1	1374 1404 1438 1457	0.4879 0.4857 0.4850 0.4880			
• 13 5 13 6 14 7 19 6 14	38.14 37 <u>.26</u> 42.16 94.16 46.17	0.9643 0.9447 0.9161 0.8926 0.8712	-0.1387 -0.1377 -0.1375 -0.1364 -0.1374	0.4576 	-0-1 -0-1	1436 1457	0.4850 0.4880			
5 13 6 14 7 19	39 <u>.26</u> 42.16 94.16 46.17	0.9-47 0.9161 0.6926 0.8712	-0.1377 -0.1375 -6.1364 -0.1374		-0.1	1457	0.4680	•		
6 14 7 19	42.16 94.16 46.17	0.9161 0.6926 0.8712	-0.1375 -6.1364 -0.1374	0.4436	-0.1					
719 0 14	94.16_ 46.17	0.692 <u>6</u> 0.6712	-0-1304 -0-1374	0.4324					<del></del>	<del></del>
e 14	46.17	0.8712	-0.1374				0.4844			
<u> </u>	47.16	0.8633	-u. 13h2		-0.1	1577	0.4825			
					-0.1	1601	0.4802			
							· · · · · · · · · · · · · · · · · · ·		<del></del>	
										•
									<del></del>	<del></del>
							•			
										***************************************
All I						<del></del> -				<del></del>
									······································	
										· · · · · · · · · · · · · · · · · · ·
									•	

GE	ENGINEE 1 OF 1 1 OF 1	PING WEVE	LOPMENT. C	ENIER (AEÙ	MAH	ILSION WIND TIN MISSILE SPLITIER	TAIL EFFECTS DATA	(T)AERODYNAHIC.MIND_TURNEL(A)
		9407 544	u Driv4	COLE TOAK				
	· 5	PART. MAL	5.2 1-471826		REE			
								· · · · · · · · · · · · · · · · · · ·
OINT	ALPHA	CNF	CH	Ce		YCPF		
<del></del> _	149.05		-0-1361 -0-1356		-0-1616 -0-1642	0.4847	<del></del>	
3	150.05		-0.1336		-0.1652	0.4836		
•	151.09		-0.1306		-0.1656	0.4855	<del></del>	
5	152.09	0.7095				0.4812		
6	153.09	0.7553	-0.1272	0.3635	-0-1684	0.4813		
_1_	150.05		-0-1254		-0-1699	0.4809		<del></del>
8	156.09		-0.1225		-0-1693	0.4657		
-9- 10	159.10		-0.1272		-0-1734 -0-1971	0.4875	<del></del>	
11	162-10		-0-1-907		-0.2221	D.4998		
12	164.09		-0.1425		-0.2465	0.5090		
<u> 11                                   </u>	166-10		-0.1369		-0.2732	0.5124		
	168.11		-0.1544		-0.3032	0.5026		
	170.10		-0.1155		0.3322	0.4982		<del> </del>
	172.10		-0.0444		-0.3525	0.4779		
18	<u> 174.12</u> 176.12		-0.0720 -0.0475	£6.65.03	-0.3694	0.4531		<del></del>
	177.11		-0.0368			0.4386		
		WALLST.	- 44 4 44 4					
							•	
		·						
								•
		<del> </del>						
								•
		· · · · · ·		<del> </del>	<del></del>			
						•		
	•		<del> </del>		<del></del>			

PAGE	ENGINE L	. •	LOPMENI_C		MA	RTI- MISS	IND_IUNNEL_FACILITY[P] SILE TAIL EFFECTS DATA TIER_PLATE_DATA	A	AERODYNAMIC WIND TUNNEL (41)	4
			•						•	
	7561	PAPT PAC	L 0210-6	CONF TOAL	614104					
	. — ا احتا	190 0.10	S.2		HEE TOWN					
PUINT	ALPHA	Caf	CH	Cs	<b>LCPF</b>	YCPF		<del></del>		<del></del>
	178.00	0.0739	-0-0-46	0.6274	-0-3422	0-3709				
5	178.97	0.0500	-0.0184	0.0126	-0.3752	0.2506				
3	179,97	0.0235		0.0515_	-0.3451		- <del></del>	·		
		-0.0026			-0.4776 -0.4854	4.1372			•	
6	162.99	-0.055	0.0452	-0-0446	-0.4510	.0.5287				
	184.01	-0.0026	0.0359	-0.0439	-0-4365	0.5357				
•	184.01	-0.1-15	0.0512	-4.0746	-0.4031	0.5254				
									,	
							· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	
										<del>.                                      </del>
						•				
				-						
	<del> </del>	<del></del> -				<del></del>		<del></del>		
							······································			
					····-				·	· · · · · · · · · · · · · · · · · · ·
	<del></del>					<del></del>				
							•			
_	-									

<u> </u>	1 OF 1				M.	UTTA MICC	D. JUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA	
					<del></del> -	SPLIT	ER PLATE DATA	
	7557	BART MAC	w 6210-A	CONF_IRAN	e te tou			<del></del>
	S	194 0.85			REE			
	ALPHA	CNF	Cri	CH		YCPF		
<u> </u>		-0.0433		-0.0267 -0.0176	0.45#3 G.8206	1.2294		
<u>.</u>	0.04	0-0092	-0-0951	-0-0056		-0.6281	· · · · · · · · · · · · · · · · · · ·	· · ·
)	1.05	0.0313	0.0038	0.0062	0.1215	0-1966		
	2.0b_ 3.07	0.000b	0.0199	0.020 <u>5</u> 0.0321	Q.2023 0.2460	0.3679		
	4.07	0.1104	9-4246	0.0437	0.25A1	0.3945		
) }	6.06	0.1753.		0.0/66	0.2568	0.4484		
<u>-</u> -	10.12	Q <u>_&amp;*9</u> c_ u.3292	<u></u>	0.1052	0.2511	0.5018		
	12.15	0.4196		0.2123	0.2188	0.5059		
S	14.15	0.4851	0.0754		0.1554	0.4991		
<u>.                                    </u>	18.15	<u> </u>	0-0592		0.0901	0.4907	<del> </del>	· <del></del> - <del></del>
j	20.20	_0.7c09	0.0512	0.3511	0.0702	0.4817	·	
6	55.51	0.766H	0.0474		0.0618	0.4613		•
7 8	26.22	0.0002	0.0410		0.0512	0.4644		
9	27.24				0.0507	0.4858		
_								
								· · · · · · · · · · · · · · · · · · ·
								,
_								<del></del>

OLO_	ENGINEER	ING JEVEL	OPPENT CE	NTER CAEDO	<u> </u>	USION DING TUNNEL FACILITY!	PUT) AERODYNAMIC WIND TUNNEL (AT)
E E T	1 OF 1				P4(	TIV MISSILE TAIL EFFECTS DATE SPLITTER PLATE DATA	· A
						`	
	<u>IFZI</u> _	195 0.65		UNE_TRANS	ILE ILE	<del></del>	-
INT	ALPHA	CNF	CH	Ce .	ACPF	YCPF	
1	28.19	0.4451	0.0485	6.3581	0-0-76	0.0620	
2	24.16	0.6159	0.0371	0.3437	0.0454	0584.0	•
	_30.15_	<u> </u>	_0.0 5 1.0_	<u> </u>	9.0.45	0.4809	
	31.16	0.5440	0.0367 0.0372	0.4053	0.0435 0.0437	0.4801	
	33.16	0.8565	0.349	t. 4101	0.0407	0.4788	
,	34.17	0.0671	0.0352	U-0199	0.4907	0.4843	
)	36.18	0.8942	2.0301	6.4286	0.0337	0.4793	
!	38.18_ •0.19	0.91 <u>67</u>	0.0292	U.454D	0.0291 0.0291	0.4824	
	45.50	0.4746	0.0230	0.4683	0-0236	0.4805	
	44.21	1.0016	0.0215	6.4848	0.0215	0.4840	
<u> </u>	95.22	1-0322	_n.ulaz_	0.4995	0-0176	0.4839	
	50.23	1.0672	0.0150	0.5180 0.53e3	0-0140	0.4854	
<u>.                                    </u>	52.20	1.1097	0.0063	V-3393.	0-0110	0.4866	
L	54.25	. 1.1313	_ 2-00-5_	_0.55.3_	G-00-0	0.4904	
8	56.26	1.1316	0.0631	0.5557	0.0027	0.4911	
9	57.76	1.1363	0.0019	0.5592	0-0017	0.4930	
						•	
						-	
			<del> </del>				
	-				· · · · · ·	· · · · · · · · · · · · · · · · · · ·	
							•
_							
	_	•					

E	1 OF 1				MA:		ATE DATA	AERODYMAMIC_BIND TUNNEL(AT)
			M RALO-6.	CONE IPAN	S1710N		•	
T	2 ALPHA	196 0.65	CH CH	F11 +	REE	YCPF		
	58.11	1.0963	0-0032		9.0929	0.4932		
5	59.17	1.0437	0-0003	0.5365	0.0003	0.4905		
<u>.                                    </u>	60.17		-0.0016		-0.0014	0.4930		
5	62-16		-0.0025	0.2492	-0.0023	0.4960		
5	63.17	1.1103	-0-9671	0.5477	-0.0064	0.4932		
7	64.18		-0-9685		-6.0074	0-4977		<del> </del>
8 9	65.18		-0.0117 -0.0146		-0.0105 -0.0130	0.4967 0.5013		
0	79.19		-0.0198		-0.0174	0.4997		
1	72.20	Lalabe	-0-2234	0.5510_	-0.0202	0.5027		
5	74.21		-0.1265		-0.0743	0.5067		
<u>.                                    </u>	75.22		-0.0333		-0.0281	0.5056		
5	80.23		-0.0444		-0.0352			
6	62.23	1.2000	-0.0473	0.6174	-0.0393	0.5127		
7	84.24	laZuvo_	-0.0513		-0.0.24	0-5170	<u> </u>	
8 9	87.24		-0.0562		-0.0464 -0.0479	0.5202 0.5211	•	
	- GIACG	145,003	-444311	NAUF BI		WASZII		
								•

E,	ENGINEE 1 OF 1 1 OF 1		LOPMENT (	ENTERIAEU	"HA	RTI~ MISSILE	TUNNEL FACILITY (PHI) TAIL EFFECTS DATA PLAIE DATA	AERODYNAMIC -IND TUNNEL (AT)	
	7561	GART NA		CUNE IHAN	ETTTON		•		
	5	197 0.65			REE	- ·	•		
TME	ALPHA	CNF	CH	C=	ACPF	VCPF			
1	90.15		-0.0000		-0.05b7	0.5160			<u> </u>
5	91.15		-1.0447		-0.0541	0.5212			
3	ولمعتجد	1_1715_	-0.0760		0.0626	0-5180			
-	93.15		-0.0760		-0.065	0.5168			
6	96.16		-0-0760		-0.0731	0.5167			
7	95.16		-9-4077		-0-0761	0.5155			
6	100-16	1.1750	-0.6491	0.6686	-0.0829	0.5093			
	TISSET.		-Unlung		-0.0247	0.5089			
10	104.18		-0-1071		-0.0893	0.5048			
11_	100-10	_lekyal_			-0.0904	0.5094			
12	102.1e		-0.1136		-0.0955	0.5032			
	110-14		-0-1157		-0.0950	0.5057			
14	117.70		-0.1179		-0.1004	0.5059 0.5029			
16	115.31		-3.12+2		-0.1063	0.5028	<del></del>		,
17	117.20		0-1247		-0-1084	0.992			•
**									
									•
							•		
				<del> </del>		<del></del>			
				•					
								•	
_				_				·	
								,	
<del></del>				<del></del>	<del></del>				
				···					
									~

1 OF 1  1 OF 1  TEST PART MALM PRILED COME TRANSITION  2 198 0.65 2.5 F11 FREE  T ALPHA CMF CM CD XCPF VCPF  120.00 1.1106 -0.1250 3.5565 -0.1125 0.6957  121.11 1.1143 -0.1240 0.5491 -0.1149 0.4028  122.11 1.1043 -0.1271 0.5473 -0.1167 0.4947  123.12 1.1060 -0.1307 0.5577 -0.1162 0.4952  124.12 1.1092 -0.1310 0.5507 -0.1161 0.4965  126.12 1.1059 -0.1353 0.5649 -0.1224 0.4952  126.13 1.0936 -0.1369 0.5371 -0.1251 0.4911  130.13 1.056 -0.1384 0.5307 -0.1251 0.4911  130.13 1.056 -0.1384 0.5300 -0.1278 0.4879  132.13 1.0563 -0.1314 0.5300 -0.1278 0.4879  132.13 1.0563 -0.1314 0.5300 -0.1278 0.4879	
1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1 OF 1 1	
TEST PART MALE PRIVE CONF TRANSITION  2 198 0.65 2.5 F11 FREE  T ALPMA CMF CM CD XCPF VCPF 120.00 1.1106 -0.120 0.5505 -0.1125 0.4957 121.11 1.1143 -0.120 0.5441 -0.1149 0.4928 122.11 1.1063 -0.1291 0.5473 -0.1167 0.4947 123.12 1.1060 -0.1307 0.5477 -0.1161 0.4947 123.12 1.1060 -0.1307 0.5477 -0.1161 0.4965 120.12 1.1059 -0.1310 0.5507 -0.1161 0.4965 120.12 1.1059 -0.1353 0.5449 -0.1224 0.4927 128.13 1.0736 -0.1365 0.5307 -0.1261 0.4927 128.13 1.0736 -0.1365 0.5307 -0.1261 0.4927 128.13 1.0736 -0.1365 0.5371 -0.1251 0.4911 130.13 1.0062 -0.1344 0.5300 -0.1278 0.4879 132.13 1.0063 -0.1365 0.5071 -0.1345 0.4865 134.14 1.0425 -0.1402 0.5071 -0.1345 0.4864 134.10 0.9059 -0.1402 0.5071 -0.1345 0.4864 140.10 0.9059 -0.1407 0.4780 -0.1420 0.4850 142.11 0.7360 -0.1367 0.4851 0.4850 142.11 0.7360 -0.1367 0.4851 0.4864 140.10 0.7740 -0.1367 0.4852 -0.1403 0.4864 140.10 0.7740 -0.1371 0.4822 -0.1501 0.4864	<del></del>
TEST PART MALM PRIDED COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.5 F11 FMEE  VALUE COME TRANSITION  2 198 0.b5 2.7 0.116. 0.498.  120.10 1.106 0.116 0.507 0.116 0.498.  120.10 1.106 0.116 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10 1.106 0.498.  120.10	TUNNEL (AT)
TEST PART MALM PAIN D COME IRANSITION  2 198 0.65 2.5 F11 FREE  OT ALPMA CMP CM CD ACPF VCPF 120.00 1.1100 -0.1200 0.5401 -0.1125 0.8957 121.11 1.1143 -0.1400 0.5401 -0.1149 0.4928 1.22.11 1.1053 -0.1401 0.5471 -0.1147 0.4947 123.12 1.1000 -0.1307 0.5477 -0.1161 0.4947 123.12 1.1000 -0.1307 0.5477 -0.1161 0.4952 124.12 1.1059 -0.1310 0.5507 -0.1161 0.4955 126.12 1.1059 -0.1353 0.5449 -0.1224 0.4927 128.13 1.0730 -0.1365 0.5409 -0.1224 0.4927 128.13 1.0730 -0.1365 0.5409 -0.1278 0.4911 130.13 1.076c -0.1374 0.5307 -0.1251 0.4911 130.13 1.076c -0.1374 0.5307 -0.1251 0.4911 131.13 1.0765 -0.1402 0.5071 -0.1375 0.4852 134.14 1.0425 -0.1406 0.4946 0.4948 -0.1321 0.4852 134.15 1.0750 -0.1406 0.4946 0.4948 -0.1381 0.4861 137.10 0.9759 -0.1400 0.4780 -0.1420 0.4864 140.10 0.9759 -0.1401 0.4780 -0.1420 0.4864 140.10 0.9759 -0.1317 0.4822 -0.1433 0.4864 140.10 0.9759 -0.1317 0.4822 -0.1561 0.4864	
2 198 0.65 2.5	·
2 198 0.65 2.5 F11 FREE  NT ALPHA CW CM CM CM ACPF VCPF  120.00 1.1106 -0.1250 3.5565 -0.1125 0.4957  121.11 1.1143 -0.1260 0.5491 -0.1149 0.4928  122.11 1.1043 -0.1291 0.5473 -0.1167 0.4947  123.12 1.1060 -0.1307 0.5477 -0.1162 0.4952  124.12 1.1052 -0.1310 0.5507 -0.1161 0.4965  126.12 1.1055 -0.1353 0.5449 -0.1224 0.4927  128.13 1.0736 -0.1365 0.5371 -0.1251 0.4911  130.13 1.0762 -0.1344 0.5300 -0.1278 0.4879  132.13 1.0763 -0.1344 0.5300 -0.1278 0.4879  133.14 1.0425 -0.1406 0.5071 -0.1345 0.4864  134.16 1.0425 -0.1406 0.5071 -0.1345 0.4864  138.10 0.9757 -0.1400 0.4780 -0.1420 0.4861  138.10 0.9757 -0.1400 0.4780 -0.1420 0.4861  140.10 0.9759 -0.1400 0.4780 -0.1420 0.4850  142.11 0.9366 -0.1387 0.4651 -0.1447 0.4850  144.14 0.97136 -0.1371 0.4422 -0.1501 0.4864	
NT ALPMA	
1 120.0h 1.110h -0.1250 3.5565 -0.1125 0.4957 2 121.11 1.1143 -0.1270 0.5441 -0.1149 0.4928 3 .122.11 1.1143 -0.1271 3.5473 -0.1167 0.4947 4 123.12 1.1000 -0.1307 0.5477 -0.1162 0.4952 5 124.12 1.1059 -0.1310 0.5507 -0.1161 0.4965 6 125.12 1.1059 -0.1353 0.5549 -0.1224 0.4927 7 126.13 1.073h -0.1355 7.5371 -0.1251 0.4911 8 130.13 1.0562 -0.1355 7.5371 -0.1251 0.4911 8 130.13 1.0562 -0.1355 7.5371 -0.1251 0.4911 13 1.0063 -0.1156 7.5371 -0.1251 0.4869 13 1.013 1.0065 -0.1171 0.5103 -0.1261 0.4852 10 134.14 1.0425 -0.102 0.5071 -0.1355 0.4864 11 13b.11 1.0186 -0.1406 0.4948 -0.1381 0.4861 12 138.10 0.9859 -0.1406 0.4988 -0.1381 0.4861 13 140.10 6.7594 -0.1387 0.4851 -0.1447 0.4850 14 142.11 0.7366 -0.1384 0.4553 -0.1443 0.4864 15 144.10 0.7136 -0.1371 0.4522 -0.1561 0.4864 16 146.13 0.4746 -0.1377 6.4293 -0.1561 0.4864	
2 121-11 1-11+3 -0-1c/0 0.54/1 -0-11+9 0.4928 3 122-11 1-1043 -0-1c/1 0.54/3 -0-1167 0.4947 4 123-12 1-1040 -0-1307 0.54/7 -0-1162 0.4952 5 124-12 1-1052 -0-1410 0.5507 -0-1181 0.4965 6 125-12 1-1052 -0-1353 0.54+9 -0-1224 0.4927 7 128-13 1.0736 -0-1365 0.54+9 -0-1224 0.4927 8 130-13 1.0766 -0-1344 0.5300 -0-1278 0.4879 9 132-13 1.0766 -0-1344 0.5300 -0-1278 0.4879 10 134-14 1.0425 -0-1406 0.5071 -0-1355 0.4864 11 136-11 1.0160 -0-1406 0.4968 -0-1381 0.4861 12 134-10 0.9857 -0-1400 0.4780 -0-1420 0.4864 13 140-10 0.9857 -0-1400 0.4780 -0-1420 0.4850 14 142-11 0.4360 -0-1387 0.4851 -0-1447 0.4850 15 144-10 0.4736 -0-1371 0.4822 -0-1561 0.4864 16 146-13 0.4746 -0-1377 0.4223 -0-1561 0.4864	
4 123,12 1.1000 -0.1307 0.5477 -0.1102 0.4952 5 124,12 1.1092 -0.1310 0.5507 -0.1101 0.4965 6 120,12 1.1059 -0.1353 0.5449 -0.1224 0.4927 7 126,13 1.0930 -0.1365 0.5371 -0.1251 0.4911 6 130,13 1.0063 -0.1304 0.5307 -0.1278 0.4679 9 132,13 1.0063 -0.1314 0.5103 -0.1321 0.4652 0 134,14 1.0425 -0.1402 0.5071 -0.1345 0.4661 1 130,11 1.0106 -0.1406 0.4948 -0.1381 0.4661 2 134,10 0.9659 -0.1400 0.4780 -0.1420 0.4869 3 140,10 0.9659 -0.1400 0.4780 -0.1420 0.4869 4 142,11 0.4360 -0.1384 0.4553 -0.1443 0.4864 5 144,14 0.4136 -0.1371 0.4422 -0.1561 0.4664 6 146,13 0.8948 -0.1397 0.4293 -0.1561 0.4799	
5   124.12   1.1092   -0.1110   0.5207   -0.1181   0.4965   6   129.12   1.1059   -0.1153   0.5449   -0.1224   0.4927   7   128.13   1.0936   -0.1365   0.5371   -0.1251   0.4911   8   139.13   1.0962   -0.1389   0.5300   -0.1276   0.4879   9   132.13   1.0963   -6.141   0.5183   -6.1321   0.4852   10   134.14   1.0425   -0.1402   0.5071   -0.1345   0.4864   11   136.11   1.0186   -0.1406   0.4948   -9.1381   0.4861   12   138.10   0.9859   -0.1400   0.4780   -0.1420   0.4849   13   140.10   6.9996   -0.1387   0.4851   0.4850   142.11   0.4936   -0.1387   0.4851   0.4850   15   144.14   0.4136   -0.1371   0.4423   -0.1561   0.4844   16   146.13   0.4946   -0.1397   0.4293   -0.1561   0.4799	
6 125.12 1.1059 -0.1353 0.5669 -0.1224 0.6927 7 128.13 1.0736 -0.1355 0.5371 -0.1251 0.4911 8 130.13 1.056 -0.1344 0.5300 -0.1278 0.4879 9 132.13 1.056 -0.1344 0.5183 -0.1321 0.4852 10 134.14 1.0425 -0.1602 0.5071 -0.1345 0.4864 11 136.11 1.0186 -0.1406 0.4948 -0.1381 0.4861 12 138.10 0.9857 -0.1400 0.4780 -0.1420 0.4849 13 140.10 0.9857 -0.1400 0.4780 -0.1420 0.4859 14 142.11 0.4360 -0.1387 0.4851 -0.1647 0.4850 15 144.14 0.4136 -0.1371 0.4622 -0.1561 0.4864	
7 126.13 1.0936 -0.1365 0.5371 -0.1251 0.4911 8 130.13 1.0962 -0.1389 0.5300 -0.1278 0.4879 9 132.13 1.0963 -0.1011 0.5183 -0.1321 0.4852 0 134.14 1.0925 -0.1402 0.5071 -0.1345 0.4864 1 136.11 1.0186 -0.1406 0.4948 -0.1381 0.4861 12 138.10 0.9859 -0.1400 0.4780 -0.1420 0.4869 13 140.10 0.9959 -0.1400 0.4780 -0.1420 0.4859 14 142.11 0.9360 -0.1387 0.4851 -0.1647 0.4858 14 142.11 0.9360 -0.1387 0.4553 -0.1643 0.4864 15 144.14 0.9136 -0.1371 0.4522 -0.1501 0.4864	
9 132-13 1.0063 -G.1-11 0.5183 -G.1321 0.4852 10 134-14 1.0425 -G.1402 0.5071 -0.1345 0.4864 11 136-11 1.0166 -0.1406 0.4448 -0.1381 0.4861 12 138-10 0.9659 -0.1400 0.4780 -0.1420 0.4849 13 140-10 G.9596 -0.1367 0.4651 -0.1447 0.4850 14 142-11 0.9366 -0.1388 0.4551 -0.1463 0.4864 15 144-14 0.9136 -0.1371 0.4422 -0.1501 0.4864 16 146-13 0.8546 -0.1397 G.4293 -0.1561 0.4799	
10 134.14 1.0425 -0.1402 0.5071 -0.1345 0.4864 11 136.11 1.0180 -0.1406 0.4948 -0.1381 0.4861 12 134.10 0.9859 -0.1400 0.4780 -0.1420 0.4869 13 140.10 0.9596 -0.1387 0.4851 -0.1447 0.4850 14 142.11 0.4360 -0.1388 0.4553 -0.1403 0.4864 15 144.14 0.4130 -0.1371 0.4822 -0.1501 0.4864 16 146.13 0.4546 -0.1397 0.4293 -0.1561 0.4799	
1 13n-11 1.0180 -0.1806 0.6598 -0.1381 0.6861 12 138.10 0.9859 -0.1800 0.4780 -0.1420 0.6869 13 140.10 0.9596 -0.1387 0.6851 -0.1647 0.6850 14 142.11 0.9360 -0.1388 0.6553 -0.1643 0.6864 15 144.14 0.9136 -0.1371 0.6922 -0.1561 0.6864	
2   139.10   0.955   -0.1400   0.4780   -0.1420   0.4849	
14 142.11 0.4360 -0.1388 0.4553 -0.1463 0.4864 15 144.14 0.4130 -0.1371 0.4422 -0.1501 0.4844 16 146.13 0.8546 -0.1397 0.4243 -0.1561 0.4799	
15 104_10 0.713G -0.1371 G.0022 -0.1501 0.6800 16 106.13 0.8700 -0.1397 G.0273 -0.1561 0.0799	
16 146.13 0.8746 -0.1397 0.4293 -0.1561 0.4799	
<u></u>	
•	
•	
	<del></del>

6E	ENGINE		LOPMENT C	ENTERCAED		TIN MISSILE	JUNNEL FACILITY (PY TAIL EFFECTS DATA PLATE DATA	ATT AERODYNAMIC HIND TUNNEL (4)
	<u></u>	· <del>····································</del>				-		
	Z TES	DAM TRAP T	H PA10-6	<u>COMF_IRAN</u> F11 F	SITION			
OINT	ALPHA		CH	C-		YCPF		
<u> </u>	146.02		-0.1391		-0.1614	0-4789	· · · · · · · · · · · · · · · · · · ·	
5	144.04				-0.1628	0.4803	•	
<del>_3</del>	1-9-40				-0.1636	0-4755		
-	150.08		-0-13/1 -0-13+6		-0.1656 -0.1662	0.4742		
6	152.10		-0-1320		-0.1673	0.4778		· · · · · · · · · · · · · · · · · · ·
<u>, , , , , , , , , , , , , , , , , , , </u>	153.06				-0.1681	0.4782		
8	154.09		-0.1299		-0.1697	0.4749		
9	156.10		-0-1279		-0-1722	0.4743		
10	158.04		-0.1240		-0.1751	0.4780		
	160-10		0-1-26_		-0.1933	0.4775		<del></del>
12	162.10		-0-1429		-0.2108	0.4666		
19	165.10		-C-1393 -0-1367		-0.23A7 -0.2586	0.4922	<del></del>	····
15	100-10		-0.1367 -6.1315		-0.3065	0.4922	•	
16	170.10		-0.1277		-0.3547	D.4744		
	172.10		-0.0995		-0.3666	0.4531		
18	174.11		-0.075A		-0.3672	0.+152		
19	175-11		-0522		-0-4004	0.3824		
Zū	177-11	0.6492	-0.4347	6.03.0	-0.4004	0.3431		
							,	·
								-
							<del> </del>	<del> </del>
		-						
					<del></del>			
						, , , <u>, , , , , , , , , , , , , , , , </u>		
			•	•				
			<del></del>					···

| TEST FART WALM PAIG = CONF IMANSITION   COLUMN   |------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 1 -2.04 -0.025 -0.024 -0.029                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |
| 1 -2.04 -0.025 -0.024 -0.029                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |
| 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 4 1.00 0.0391 0.0026 0.0059 0.1164 5 1.97 0.0026 1.0102 0.0108 0.1621 0.2672 6 3.00 0.0914 0.0210 0.0332 0.2301 0.3632 7 4.00 0.1162 0.01325 0.0041 0.2426 0.4226 8 6.00 0.1075 0.0495 0.0030 0.2640 0.4475 9 8.10 0.2036 0.0613 0.1250 0.2590 0.4073 10 10.12 0.3045 0.0013 0.1732 0.2293 0.4886 11 12.15 0.4455 0.0947 0.2250 0.2125 0.5050 12 14.17 0.5389 0.1023 0.2737 0.1498 0.5078 13 16.19 0.6113 0.1033 0.2131 0.1652 0.5078 14 18.19 0.612 0.067 0.3349 0.0979 0.4916 15 20.21 0.7456 0.0419 0.3593 0.0979 0.4916 16 22.22 0.4090 0.0414 0.3573 0.0642 0.4876 17 24.24 0.8695 0.4424 0.4177 0.4464 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| 5 1.67 0.062k 2.0102 0.0166 0.1621 0.2672 6 3.ne 0.0714 0.0210 0.0332 0.2301 0.3632 7 4.3n 0.116r 0.0325 0.041 0.2926 0.4226 8 6.3n 0.1075 0.0495 0.0n33 0.2640 0.475 9 8.10 0.2036 0.0683 0.1250 0.2590 0.4763 10 10.12 0.3945 0.0013 0.1732 0.2293 0.4886 11 12.15 0.4455 0.0013 0.1732 0.2293 0.4886 11 12.15 0.4455 0.0037 0.2250 0.2125 0.5050 12 14.17 0.5385 0.1023 0.2737 0.1498 0.5078 13 16.19 0.6113 0.1043 0.3163 0.1652 0.5016 14 18.19 0.6112 0.0470 0.3349 0.0979 0.4916 15 20.21 0.7456 0.0479 0.3593 0.0642 0.4618 16 22.22 0.4040 0.0414 0.3579 0.0512 0.4795 17 24.24 0.8695 0.0424 0.4177 0.4486 0.4678 18 26.25 0.8933 0.0377 0.4764 0.0422 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 6 3.0e 0.0v14 0.0210 0.0332 0.2301 0.3632 7 4.3d 6.116 0.0325 6.0441 0.2426 0.4226 8 6.0b 0.1075 0.0495 0.0033 0.2640 0.475 9 8.10 0.2036 0.0443 0.1250 0.2590 0.473 10 10.12 0.3945 0.0413 0.1732 0.2233 0.4886 11 12.15 0.4455 0.0477 0.2250 0.2125 0.5050 12 14.17 0.5364 0.1623 0.2/37 0.1498 0.5078 13 16.19 0.6413 0.1643 0.3163 0.1652 0.5010 14 18.19 0.612 0.0667 0.3349 0.0979 0.4916 15 20.21 0.7456 0.0479 0.3543 0.0642 6.4818 16 22.22 0.4040 0.414 0.3579 0.0512 0.4795 17 24.24 0.8695 0.0477 0.4464 0.0022 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |
| 6 6.0h 0.1d75 0.0495 0.0d3 0.2640 0.4475 9 8.10 0.2036 0.0d83 0.1250 0.2590 0.473 10 10.12 0.3045 0.0d13 0.1732 0.2293 0.4886 11 12.15 0.4455 0.0477 0.2250 0.2125 0.5058 12 14.17 0.5389 0.1023 0.2137 0.1498 0.5078 13 16.19 0.6113 0.1043 0.3103 0.1652 0.5078 14 18.19 0.6012 0.3667 0.3349 0.0979 0.4916 15 20.21 0.7458 0.0479 0.3593 0.0642 6.4818 16 22.22 0.4090 0.0414 0.3573 0.0512 0.4795 17 24.24 0.8695 0.4424 0.4177 0.4464 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 9 8.10 0.2036 0.0063 0.1250 0.2590 0.0703 10 10.12 0.3005 0.0013 0.1732 0.2293 0.0886 11 12.15 0.4055 0.0747 0.2250 0.2125 0.5058 12 14.17 0.5389 0.1073 0.2737 0.1888 0.5078 13 16.19 0.6113 0.1043 0.3183 0.1652 0.5018 10 18.19 0.612 0.067 0.3309 0.0979 0.0916 15 20.21 0.7858 0.0479 0.3593 0.0979 0.0916 16 22.22 0.0090 0.0014 0.3593 0.0512 0.0795 17 24.24 0.8695 0.0624 0.4177 0.4887 0.4806 18 26.25 0.8933 0.0377 0.4764 0.0022 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| 10 10.12 0.305 0.0d13 0.1732 0.2293 0.0886  11 12.15 0.455 0.0957 0.2250 0.2125 0.5058  12 14.17 0.5389 0.1023 0.2737 0.1098 0.5078  13 16.19 0.6413 0.1043 0.3163 0.1652 0.5010  10 18.19 0.6413 0.1043 0.3593 0.0979 0.0916  15 20.21 0.7656 0.0479 0.3593 0.0662 0.4818  16 22.22 0.4890 0.0414 0.3579 0.0512 0.4795  17 24.24 0.8695 0.0424 0.4177 0.0487 0.4804  18 26.25 0.8933 0.0377 0.4404 0.0022 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 11 12-15 0-4-55 0-0-47 0-2250 0-2125 0-5050  12 14-17 0-5364 0-1023 0-2/37 0-1098 0-5078  13 16-19 0-6113 0-1063 0-2163 0-1652 0-5010  14 18-19 0-612 0-0647 0-3364 0-0979 0-916  15 20-21 0-7-56 0-0479 0-3553 0-0662 0-6818  16 22-22 0-0090 0-0414 0-3579 0-0512 0-4795  17 24-24 0-8695 0-0424 0-0177 0-0487 0-8806  18 26-25 0-8933 0-0377 0-4/64 0-0822 0-4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |
| 12 14.17 C.5389 O.1073 U.2/37 G.1898 O.5078 13 16.19 U.6113 D.1043 D.3163 O.1657 U.5016 14 18.19 O.512 0.3647 U.3349 D.0979 O.4016 15 20.21 O.7456 U.0479 D.3593 D.0642 G.4618 16 22.22 O.8090 O.0414 O.3979 O.0512 O.4795 17 24.24 O.8095 D.0424 D.4177 D.0487 D.4804 18 26.25 O.8933 O.0377 V.4764 O.0422 O.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |
| 18 18 19 0.6512 0.3667 0.3369 0.0979 0.4916 15 20.21 0.7456 0.0479 0.3593 0.0642 6.4818 16 22.22 0.6090 0.0414 0.3579 0.0512 0.4795 17 24.24 0.8695 0.0424 0.4177 0.4687 0.4806 18 26.25 0.8933 0.0377 0.4664 0.0422 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 15 20.21 0.7458 0.0479 0.3553 0.0642 6.4818<br>16 22.22 0.4490 0.0414 0.3579 0.0512 0.4795<br>17 24.24 0.8695 0.4424 0.4177 0.0487 0.4804<br>18 26.25 0.8933 0.4377 0.4464 0.0422 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |
| 16 22.22 0.6090 0.0414 0.3579 0.0512 0.4795<br>17 24.24 0.8695 0.0424 0.4177 0.0487 0.4884<br>18 26.25 0.8933 0.0377 0.4464 0.0422 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 17 24-24 0.8695 0.8424 0.4177 0.0487 0.4804<br>18 26-25 0.8433 0.4377 0.4464 0.0422 0.4773                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
| 17                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |

GE	ENGINEES 1 OF 1 1 OF 1		OPMENT CE	NTEKLAEN	C) PHOP	ULSION WING WTIN FISSIO WELLIII	TUNNEL FACILITY (PHT) AERODY E TAIL EFFECTS DATA R PLATE DATA	NAMIC MIND TUNNELLAT)
		FART MAC	2.5 F		SITION REE			
DINT	ALPHA	CNF	CH	C-3		VCPF		
<u> </u>	29.18	0.4455	0.0353 6,0365	0.4277	0.0394	0.4733		
3				0.4262	0.0354			
•	31.18	0.4470	0.0312	6.425R	0.0348	0.4747		
5	32.16_	0-9022	0.0295	0.4288	0-0327	_0.4752		
6	33.19	0.9151	0.0310	80t	0.0340	0.4789		
-	36.20	0. Y363	0.0295	0.4437	0.0320	0.4755		
9		0.9363 0.9365		3.4577				
0	40.70	0.9736	0.0204	6.4764	0.0205	8.4797		
11		1.0134		0.4855		0.4791	·	
12	44.22	1.0000	0.0157	0.4985	0.0150	0.4772		
13	40-24	1-0516		1.5233				
14 15	47.35 59.25	1.1024	0.0110	U.5266	0.0108 0.0056	0.4795		
16	52.26	1.1-89	0.0036	0.5575	0.0031	0.4852		
17	54.27	1-1493	0.0016	U.5553	0-0014	0.4832		
18	56.29	1.1477	-0.0012	0.5572	-0.0010	0.4855		
19	<u> </u>		-0-0009	<u> </u>	_0_00 <u>0</u> 8	.O. ARAG	· · · · · · · · · · · · · · · · · · ·	
					<del></del>			
		<del></del>		<del></del>				
								<u></u>
	•						<del></del>	·
	_							

E	1 OF		LOPHENT C	ENTEDIALU		<u>JLSION WIND TUNNE</u> PTIN MISSILE TAIL	EFFECTS DATA	AERODYNAMIC MIND JUNNEL (AT)
	1 OF	1				SPLITTER PLAT	E DATA	
							• •	
		LPART_MAG	M RE10-6	Cone Thay	SITION			
	2	203 0.92	2.5	F11 F	4EE		•	
OINT	ALPHI	Chf	Ch	Cà	KCPF	YCPF		
1	58.1		• • • • • • • • • • • • • • • • • • • •		-0-0002	0.4849		
2	54.17		-0.0024		-0.0022	0.4671		
3	59.6		-0-0031		-0.0029	0.4902		
•	60.1		1955 marin arrangement		-0.0022	0.4910		•
_5_	60.7		-0-0054	6.5365		0.4914		
6	61.10				-0.0656	0.4902		
<u>.                                    </u>	62-19		-0041			0.4896		
	63.10				-0.0091 -0.0112	0.4935		
10	66.2				-0.0112	0.4948	· · · · · · · · · · · · · · · · · · ·	<del></del>
11	68.2			0.5553		0.4997		
12	7c.2			The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	-0-0212	0.4978		
13	72.2				-0-0235	0-5039		
14	74.2	2 1.2479	-0.0346	0.6:10	-0.0268	0.4996		
<u> 15</u>	76.2			<u> </u>	-0-0309	6.5052		
16	78.2				-0.0338	0.5068		
17	80.2				-0-0369	D.5082	<u>.</u>	
36	85.2				-0-0-05	0.5094		
78	84.2		<u>-2.0534</u>		-6-4433	0-5144		
20 21	87.2				-0.0+76 -0.0503	0.5152		•
حـــــ		I TARSIA	-0-4057	V=0310	- ENSASIT		<del></del>	<del></del>
							······································	
					<del> </del>	- <del></del>	· · · · · · · · · · · · · · · · · · ·	
			<del></del>			<del></del>		
			<del></del>				· · · · · · · · · · · · · · · · · · ·	
1926								
					#II 57			
			· · · · · · · · · · · · · · · · · · ·					

E	ENGINEE 1 OF 1 1 OF 1		LOPMENT CI	INTER LAED	MAI	ULSION_HIND.JI PTI≈ MISSILE SPLITTER :	TAIL EFFECTS DATA	AERODYNAMIC 41ND TUNNEL1411
	• • • • • • • • • • • • • • • • • • • •	<del></del>						
		PART MAG 204 U.94	. <u>H.P.LC-6</u> .		SITION HEE	•		
INT		CNF	Сн	C4		YCPF		
<del>}</del> _	45-10 46-12	1.1942	-G.U616		-0.0515	0-5164		
3	91.09.	_lale43	-0.0769		-0-0598	_0_5189		
•	92.13		-0.6772		-0.0650	0.5160		
5_	<u>93.13</u> 94.14		-0-0798 -0-0-39		-0.0672 -0.0704	0.5169		
7	90.10	1.1765	-0.6586 -0.6586		-0.67.0	0.5128		
8	94.15	1.2143	-0.0955		-0.0766	0.5088		
9	100-13		<u>-0. 1775</u>		-0-0508	0-5060		
10 11	107.14		-0.1026 -G.1008		-0.0842	0-5053 0-5017		
S	105.16		-6.1111		-0.0916	0.5002		<del></del>
13	100.16		-6-1155		-0.0953	24942		
14 15	117.14		-0.11#3 -0.1206		-0.0953 -0.1012	0.4993		
16	114.19		-0.1216		-0.1036	0.4982		
	116.20	1.1547	-0-1244	0-5755	-0-1065	0-4941		
10	117.19	1.1607	-0.12+6	0.5712	-0.1073	922		
							·	
			<del></del>			<del></del>		
							•	
								•
			-					
								<del>-</del>
		-					· · · · · · · · · · · · · · · · · · ·	
					<del></del>		····	

TEST PAPT FACE PRIDE	TEST PAPT FACE HAID-6.COSE JBANSTION   2 zon 0.60 2.5 F36 FREE		0F 1				<del></del>	LRTI~ MISS. SPLIT	ILE TAIL EFFECTS DATA
INT ALOMA CWY CH CH CD KCOF YCPF  1	ALPHA CWF CH CH ACDF YCPF  -2.03 -6.0271 0.0013 -2.0276 -0.0092 0.2758  -0.59 -0.0159 -1.0000 -9.0014 -0.0007 0.0929  1.00 0.002 -0.0005 -0.0000 0.0162 0.0100 -0.0104 1.7459  1.00 0.001 -0.0001 0.0100 -0.0104 1.7459  2.93 2.0175 -1.0003 0.0100 -0.0008 0.0230  3.05 0.0270 -0.0027 -0.0002 0.0200 -0.0008 0.0593  4.05 (0.055 -0.0012 0.0250 -0.0008 0.0593  4.07 0.0027 -0.0012 0.0050 -0.0007 0.05378  0.07 0.0023 -1.0020 0.0453 -0.0070 0.05573  10.00 0.1761 -0.0004 0.0721 -0.0260 0.4040  12.12 (2.2361 -0.0052 0.295 0.3589  14.14 0.296 -0.0072 0.1055 0.0265 0.3589  15.15 0.3593 -0.0074 0.1279 -0.0179 0.3768  10.17 1.200 -0.0075 0.1279 -0.0179 0.3768  22.22 (.201 -0.0075 0.1293 -0.0184 0.0218 0.306  22.22 (.201 -0.0075 0.1293 -0.0184 0.3275  22.22 (.201 -0.0075 0.1293 -0.0184 0.3275  22.22 (.201 -0.0075 0.1353 -0.0184 0.3173  22.22 (.201 -0.0075 0.1353 -0.0184 0.3173  22.22 (.201 -0.0075 0.0055 0.0055 0.3389  22.22 (.201 -0.0075 0.0073 0.1752 -0.0139 0.3198  22.22 (.201 -0.0075 0.0073 0.1752 -0.0139 0.3198  22.22 (.201 -0.0075 0.0073 0.1752 -0.0139 0.3198  22.22 (.201 -0.0075 0.0055 0.2055 0.3087  27.22 (.201 -0.0055 0.2055 0.2055 0.3087  27.22 (.201 -0.0055 0.2055 0.2055 0.3087  27.22 (.201 -0.0055 0.2055 0.2055 0.3087  27.22 (.201 -0.0055 0.2055 0.2055 0.3087								
2 -0.69 -0.015 -0.0003 -2.0076 -0.0009 0.0009 2 -0.0005 -0.0109 -0.0001 0.0009 -0.0009 3 0.02 -0.0005 -0.0101 0.0108 -0.0108 -0.0108 1.7659 5 2.09 0.0175 -0.0001 0.0108 -0.0108 0.8393 7 0.05 0.076 -0.0002 0.0200 -0.0008 0.8393 7 0.05 0.076 -0.0002 0.0200 -0.0008 0.8393 8 0.07 0.1297 -0.0002 0.0403 -0.0007 0.5378 9 0.07 0.1297 -0.0004 0.0553 -0.0007 0.5378 10 10.00 0.161 -0.0004 0.0721 -0.0200 0.4049 11 12.12 0.2361 -0.0005 0.0295 -0.0205 0.3589 12 10.16 0.290 -0.0075 0.1055 -0.0205 0.3589 13 16.15 0.3393 -0.0075 0.1059 -0.0205 0.3589 14 10.17 (0.003 -0.0017 0.1077 0.1377 -0.0178 0.3784 15 10.17 (0.003 -0.0017 0.1075 0.00017 0.3784 16 10.17 (0.004 0.0017 0.1077 0.1377 0.0178 0.3274 17 2.20 0.0000 -0.0017 0.1377 -0.0179 0.3274 18 22.20 0.0000 -0.0017 0.1377 -0.0179 0.3274 19 27.22 0.0000 -0.0017 0.1075 -0.0130 0.3198 19 27.22 0.0000 -0.0007 0.2002 -0.0130 0.3198 19 27.22 0.0000 -0.0007 0.2002 -0.0130 0.3198 19 27.22 0.0000 -0.0007 0.2002 -0.0130 0.3198	-2.03 = 0.027	\•							•
2 -0.9E -0.9E5 -0.0U00 -w.0U14 0.0007 -0.0029 3 0.027 -0.0025 -0.0000 w.0022 0.0009 -0.0024 4 1.04 0.0001 -0.0001 0.6106 -0.0164 1.7656 5 2.06 0.0076 -0.0002 0.0200 -0.0004 0.9093 7 0.05 0.0076 -0.0002 0.0200 -0.0004 0.9093 7 0.05 0.0076 -0.0002 0.0200 -0.0004 0.9093 8 0.07 0.0293 -0.0290 -0.0290 -0.0004 0.9093 9 0.07 0.1297 -0.0002 0.0200 -0.0004 0.9093 10 10.09 0.161 -0.0004 0.0721 -0.0225 0.0016 11 12.12 0.251 -0.0005 0.0005 0.0004 0.0004 11 12.12 0.251 -0.0005 0.0005 0.0005 0.0004 11 12.15 0.0007 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 11 10.17 0.000 0.0005 0.0005 0.0005 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006 0.0006	-0.95 -0.015 -0.0205 -0.0200	; !~!		_					•
\$ 1.04 0.000   0.0010   0.0100 -0.0164   1.7459    \$ 2.90 0.0174 -0.0002   0.0230 -0.0006   0.9393    \$ 3.05 0.0274 -0.0002   0.0230 -0.0006   0.9393    \$ 4.05 0.0255 -0.0002   0.0240 -0.0006   0.9393    \$ 6.07 0.0003 -0.0070   0.0245   0.0207   0.5378    \$ 9 0.7 0.1297 -0.0004   0.0721 -0.0295   0.6573    \$ 10 10.00 0.161 -0.0004   0.0721 -0.0295   0.6573    \$ 11 12.12 0.2361 -0.0065   0.0095 -0.0277   0.3788    \$ 12 14.14 0.200 -0.0072   0.1959 -0.0225   0.3869    \$ 13 15.15 0.3393 -0.0076   0.1177 -0.00179   0.3266    \$ 14 10.17 0.200 -0.0076   0.1177 -0.00179   0.3274    \$ 20.26 0.0004 -0.0075   0.1752 -0.0133   0.3198    \$ 17 24.22 0.00096 -0.0016   0.1172 -0.0133   0.3198    \$ 17 24.22 0.00096 -0.00076   0.1752 -0.0133   0.3198    \$ 17 27.22 0.7005 -0.0075   0.2005 -0.0006   0.3007    \$ 19 27.22 0.7005 -0.0005   0.2005 -0.0008   0.30096    \$ 19 27.22 0.7005 -0.0005   0.2005 -0.0008   0.30096    \$ 19 27.22 0.7005 -0.0005   0.2005 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2005   0.2006 -0.0008   0.30096    \$ 10 0.0005 -0.0005   0.2006 -0.0006   0.3006    \$ 10 0.0005 -0.0005   0.2006 -0.0006   0.3006    \$ 10 0.0005 -0.0005   0.2006 -0.0006   0.3006    \$ 10 0.0005 -0.0005   0.2006 -0.0006   0.3006    \$ 10 0.0005 -0.0005   0.2006 -0.0006   0.3006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006    \$ 10 0.0005 -0.0005   0.2006 -0.0006	1-0 0.0001 -0.0001 0.6106 -0.0106 1.7755 2.00 0.0176 -0.0003 0.0270 -0.0006 0.8393 3.05 0.0276 -0.0007 0.0270 -0.0006 0.8393 4.05 0.0276 -0.0007 0.0553 -0.0007 0.5378 6.07 0.0003 -0.0007 0.0553 -0.0007 0.5378 8.17 0.1297 -0.0008 0.077 -0.0205 0.4008 12.12 0.2381 -0.0005 0.0008 0.0008 0.4008 12.12 0.2381 -0.0005 0.0008 0.0008 0.4008 13.15 0.3393 -0.0008 0.0008 0.0008 0.4008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 13.17 1.0008 0.0008 0.0008 0.0008 0.4008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 13.17 1.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.0008 0.00	2							
5	2.04 0.0175 -0.0003	3							
0 3.05 0.027a -0.0002 0.028 -0.0084 0.6993 7 4.05 (.055 -0.0012 0.028 -0.0275 0.6616 8 0.07 0.0003 -F.0076 0.6653 -0.0007 0.5376 9 0.07 0.1297 -0.002 0.072 0.0255 0.2573 10 10.09 0.161 -0.0006 0.072 0.0260 0.004 11 12.12 0.2361 -0.0065 0.0072 0.159 -0.0260 0.004 11 12.12 0.2361 -0.0065 0.0072 0.159 -0.0265 0.3788 13 16.15 6.3593 -0.007 0.1299 -0.0265 0.3589 14 18.17 (.200 -0.0075 0.137 0.0179 0.3276 15 23.26 6.4004 -0.0075 0.137 -0.0179 0.3276 16 27.22 0.0096 -0.0072 0.152 -0.0133 0.3198 17 24.22 0.0096 -0.0073 0.1752 -0.0133 0.3198 17 24.22 0.0096 -0.0073 0.1752 -0.0100 0.3007 19 27.22 0.7062 -0.0059 (.2185 -0.0084 0.3095	3.05 0.027a -0.0007 0.027a -0.008a 0.8393  4.05 0.045u -0.0012 u.0298 -0.0275 0.6615  6.07 0.1297 -0.0138 u.0293 -0.0295 0.8573  10.09 0.1761 -0.0065 0.2095 -0.0277 0.3788  12.12 0.2361 -0.0065 0.2095 -0.0277 0.3788  14.14 0.296 -0.0072 0.1059 -0.0278 0.3366  15.17 (20e -0.0074 0.1377 -0.0179 0.3278  23.26 6.464a -6.0072 u.1553 -0.0179 0.3278  27.22 0.5097 -0.0073 0.1752 -0.0133 0.3198  24.22 0.5095 -0.0073 0.1752 -0.0114 0.3173  25.28 0.6064 -0.0077 0.2082 -0.0114 0.3173  27.28 0.7067 -0.0059 0.2085 -0.0088 0.3087  27.28 0.7067 -0.0059 0.2085 -0.0088 0.3087	•							
7	4.05	<u> </u>							
8	6.07	7							
9 8.77 0.1297 -0.0032	8-07 0.1297 -0.0432	8							
10 10.09 0.1/61 -0.0065 0.2095 -0.0272 0.3788  11 12.12 (.2251 -0.0065 0.2095 -0.0275 0.3788  12 10.14 0.290 -0.077 0.1758 -0.0255 0.3589  13 15.15 0.3393 -0.0378 0.1203 -0.0218 0.3366  14 10.17 (.200 -0.0074 0.1377 -0.0179 0.3274  15 20.20 0.0000 -0.0172 0.1553 -0.0148 0.3207  16 27.22 0.0074 -0.0073 0.1752 -0.0133 0.3198  17 20.000 -0.0000 -0.0000 0.2000 -0.0000 0.3007  18 25.20 0.000 -0.0000 0.2002 -0.0100 0.3007  19 27.20 0.7007 -0.0059 (.2185 -0.0084 0.3090	10.09 0.1161 -0.0046 0.0721 -0.0260 0.4049  12.12 0.2361 -0.0065 0.0495 -9.0277 0.3788  10.14 0.2946 -0.0072 0.1195 -0.0245 0.3589  15.15 0.3953 -0.0075 0.1209 -0.0218 0.3366  18.17 1.4200 -0.0076 0.1377 -0.0179 0.3274  23.26 0.4954 -0.0072 0.1752 -0.0133 0.3198  24.22 0.5046 -0.0073 0.1752 -0.0133 0.3198  24.22 0.5046 -0.0067 0.2082 -0.0100 0.3067  27.28 0.7067 -0.0059 0.2185 -0.0084 0.3098	_				<u>v.0593</u>	-0.0295	0.4573	
12	1e,14					0.0721	-0.0260		
13	19.15								
10	10.17 (200 -0.3074 0.1377 -0.0179 0.3274 20.26 (204 -0.4072 1.1553 -0.0148 0.3207 27.27 (2077 -0.0073 0.1752 -0.0133 0.3198 24.2- 0.6090 -0.0010 0.1935 -0.0114 0.3173 25.20 0.6160 -0.3067 0.2062 -0.0100 0.3067 27.28 0.7062 -0.0059 (2165 -0.0084 0.3096								
15 23.26 Gaega - F. 2017	23_26								· · · · · · · · · · · · · · · · · · ·
16 27.22 (.5477 -9.0073 0.1752 -0.0133 0.3198 17 24.24 0.6096 -6.0076 0.1935 -0.0114 0.3173 18 29.28 0.6040 -0.0007 0.2002 -0.0100 0.3007 19 27.28 0.7062 -0.0059 0.2165 -0.00084 0.3096	27.22 (-5-77 -0.0073 0.1752 -0.0133 0.3198 24.24 0.6096 -0.0070 0.1935 -0.0114 0.3173 25.28 0.6144 -0.0059 0.2082 -0.0100 0.3087 27.28 0.7062 -0.0059 (-2185 -0.0084 0.3094								
18 25.28 C.6744 -0.0059 U.2185 -0.0084 0.3094	25.28 (.6/44 -0.0059							0.3198	
19 27.28 C.7u6; -0.0059 (.2)45 -0.0084 0.309a	27.28 C.7u62 -0.0059 (.2)85 -0.0084 0.309e								
		<del>y</del>	27.28	C. / ubi	-0.0059	<u> </u>	-0-0084	0.1096	
						<u></u>			
									•
									•

OINT AL  2 28 5 29 6 36 7 31 8 32 9 33 16 14 11 36 12 38 13 40 14 42 15 44 16 46 17 48 18 50 19 52 20 54 21 56	2 LPHs	209 U.BU  CNF 0.7144 0.7025 0.7740 0.8151 0.8544 U.9702 0.4776 0.4776 0.4776 0.7584 0.7533 0.9714 0.7533 0.9714 0.7533	2.5 CH -0.0029 -0.0049 -0.0049 0.0016 0.0029 0.0094 0.0274 0.0261 0.0261 0.0264	F3e	-0.009 0.003 0.0019 0.0032 0.0101 0.0325 0.0295 0.0256 0.0257 0.0257 0.0257 0.0257 0.0257 0.0257	VCPF 0.3038 0.3028 0.3010 0.3010 0.2981 0.2961 0.2934 0.2895 0.2751 0.2834 0.2862 0.2862 0.3067 0.3163				
OINT AL  2 28 5 29 6 36 7 31 8 32 9 33 16 14 11 36 12 38 13 40 14 42 15 44 16 46 17 48 18 50 19 52 20 54 21 56	2 LPHa 8-18 9-19 6-20 1-24 2-20 3-27 6-34 8-30 0-30 2-31 4-33 6-3-3 8-31 19-32 12-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32 19-32	209 U.BU  CNF 0.7144 0.7025 0.7740 0.8151 0.8544 U.9702 0.4776 0.4776 0.4776 0.7584 0.7533 0.9714 0.7533 0.9714 0.7533	2.5  CM -0.0137 -0.0029 -0.0049 -0.0049 -0.0049 -0.0274 -0.0274 -0.0274 -0.0274 -0.0274 -0.0274 -0.0274	F3e	REE  XCPF -0.0050 -0.0038 -0.0024 -0.0009 0.0032 -0.0101 0.032 -0.0256 0.0257 0.0257 -0.0257 -0.0257 -0.0257	0.3038 0.3028 0.3010 0.3010 0.2981 0.2981 0.2934 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.3087				
OINT AL 28 28 5 29 6 30 7 31 6 32 39 11 36 12 38 13 40 15 44 16 66 17 48 19 52 54 21 56	LPHA 8-14 9-17 0-20 1-24 2-25 3-27 6-34 8-30 0-30 2-31 4-33 6-35 8-31 9-32 12-32 13-35 16-35	CNF 0.7346 0.7625 0.7708 0.8151 0.8544 0.9702 0.9376 0.9376 0.9284 0.9533 0.9716 0.9716 0.9761 0.9761 0.9776 0.9771	CM -0.0029 -0.0029 -0.0009 0.0009 0.0019 0.0029 0.00274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274 0.02274	C::	xCPF -0.0050 -0.0038 -0.0024 -0.009 0.0032 0.0019 0.0325 0.0255 0.0255 0.0257 0.0256 -0.0019 -0.0019	0.3038 0.3028 0.3010 0.3010 0.2981 0.2981 0.2934 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.3087				
5 29 6 36 7 31 8 32 9 33 16 44 11 36 12 38 11 34 12 48 15 44 16 66 17 48 18 50 19 52 20 54 21 56	8-1h 9-1y 6-20 1-24 2-2b 3-27 6-34 8-30 0-30 2-31 4-33 6-35	0.7346 0.7025 0.7760 0.8151 0.8544 0.9702 0.7376 0.7376 0.7376 0.7533 0.9716 0.9761 0.9761 0.9761 0.9761 0.9761	-0.0937 -0.0029 -0.0009 -0.0016 -0.0029 -0.0026 -0.0276 -0.0276 -0.0274 -0.0274 -0.0274 -0.0274 -0.0274	0.2532 0.2349 0.2340 0.2517 0.2517 0.2732 0.2733 0.2721 0.2650 0.2728 0.2727 0.2327 0.2327	-0.0050 -0.0038 -0.0024 -0.0009 0.0019 0.0032 -0.0101 0.032 0.0255 0.0257 0.0257 0.0257 0.0257 -0.019	0.3038 0.3028 0.3010 0.3010 0.2981 0.2981 0.2934 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.2834 0.3087				
5 29 6 36 7 31 8 32 9 33 16 34 11 36 12 38 13 40 14 42 15 44 16 46 17 48 18 50 20 54 21 56	9.1 v 6.20 1.24 2.25 3.27 4.27 6.30 8.30 0.30 2.31 4.33 6.35 8.31 9.32 9.32 9.32 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.33 9.35 9.35 9.35 9.35 9.35 9.35 9.35 9.35 9.35 9.35 9.35	0./025 0.7740 0.0151 0.0544 0.9/02 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376 0.0376	-0.0029 -0.0019 -0.0019 -0.0019 -0.0016 -0.0029 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026 -0.0026	0.2309 0.2309 0.2453 0.2577 0.2577 0.2730 0.2730 0.2751 0.2650 0.2728 0.2728 0.2728 0.2728 0.2727	-0.0038 -0.0324 -0.0009 0.0032 0.0019 0.0032 0.0101 0.032 0.0255 0.0257 0.0257 0.0257 0.0257 -0.0019 -0.0019	0.3028 0.3010 0.3010 0.2981 0.2996 0.2895 0.2895 0.2834 0.2854 0.2854 0.2862 0.3087 0.3116				
6 36 7 31 6 32 9 33 16 44 11 36 12 39 13 40 14 42 15 44 16 66 17 48 19 52 20 54 21 56	6.20 1.24 2.25 3.27 3.27 6.34 8.30 0.30 2.31 4.33 6.35 8.31 9.32 9.23 9.23 9.32 9.33 9.33 9.33 9.33	0.776 0.8151 .0.8564 0.9702 c.8776 0.87376 0.87376 0.8736 0.9716 0.9736 0.9716 0.9761 0.9761 0.9761 0.9777	-0.0419 -0.0004 0.9002 0.0016 0.0029 0.0094 0.0274 0.0267 0.0254 0.0267 0.0264 -0.0019 -0.0019 -0.00124 -0.00124	0.23d0 0.2453 0.2517 0.2517 0.2517 0.2650 0.2726 0.2726 0.2726 0.2726 0.2327 0.2327	-0.0024 -0.009 -0.003 -0.003 -0.003 -0.003 -0.003 -0.025 -0.025 -0.025 -0.0019 -0.0127	0.3010 0.3010 0.2981 0.2981 0.2895 0.2895 0.2834 0.2834 0.2854 0.2854 0.2862 0.3087 0.3116				
6. 32 9 33 16 34 11 36 12 38 13 40 14 42 15 44 16 66 17 48 18 50 20 54 21 56	2.25 3.77 4.27 6.34 8.30 0.30 2.31 4.33 6.35 9.32 9.32 9.32 9.32	0.8151 0.8544 0.9702 0.9376 0.8961 0.9284 0.9533 0.9714 0.9761 0.9761 0.98771	-0.000M 0.900Z 0.001b 0.004y 0.0094 0.0274 0.0261 0.0261 0.0264 0.0264 -0.001y -0.001y -0.0124 -0.0124	0.2453 0.2517 0.2577 0.2650 0.2650 0.2650 0.2728 0.2473 0.2650 0.2728 0.2477 0.2477	-0.009 0.003 0.0019 0.0032 0.0101 0.0325 0.0295 0.0256 0.0257 0.0257 0.0257 0.0257 0.0257 0.0257	0.2951 0.2961 0.2934 0.2895 0.2751 0.2834 0.2856 0.2862 0.2909 0.3007				
9 33 16 34 11 36 12 38 13 40 14 42 15 44 16 66 17 48 18 50 20 54 21 56	3./7 4.27 6.34 5.30 0.30 2.31 4.33 6.35 9.32 9.32 9.32	0.9/02 C.dy/0 0.73/6 0.8991 0.8061 0.9284 0.7533 0.971F 0.976 0.9761 0.9834 0.4837 1.0206	0.0016 0.0029 0.0094 0.0274 0.0261 0.0247 0.0254 3.0244 -0.0019 -0.0019 -0.0124	0.2577 0.2630 0075.0 2005.0 2005.0 2005.0 2005.0 2005.0 2005.0	0.0019 0.0032 0.0101 0.0305 0.0295 0.0297 0.0256 -0.0019 -0.0127	0.2961 0.2936 0.2895 0.2834 0.2834 0.2856 0.2862 0.3087 0.3116				
16 39 11 36 12 38 13 40 14 42 15 44 16 66 17 48 14 50 19 52 20 54 21 56	6.34 8.30 0.30 2.31 4.33 6.35 8.31 9.32 9.32 4.33	0.9376 0.8991 0.8061 0.9286 0.9286 0.9233 6.9716 6.9761 0.9834 6.9977	0.0049 0.0074 0.0274 0.0261 0.0267 0.0254 3.0269 -0.0019 -0.00124 -0.0124	0.2032 0.2700 0.2073 0.2511 0.2650 0.2728 0.2357 0.2357 0.3021	0.0032 0.0101 0.0305 0.0295 0.0297 0.0297 0.0297 0.0297 0.0297 0.0297	0.2934 0.2895 0.2751 0.2834 0.2854 0.2862 0.2909 0.3087 0.3114				
11 36 12 39 13 40 14 42 15 44 16 46 17 48 19 52 20 54 21 56	6.34 8.30 0.30 2.31 4.33 6.34 8.31 10.32 10.32 14.33 16.35	0.7376 0.6791 0.8061 0.7284 0.7284 0.7533 0.9714 0.776 0.776 0.7761 0.7776	0.0094 0.0274 0.0261 0.0267 0.0264 0.0264 -0.0019 -0.0019	0.2700 0.2651 0.2650 0.2650 0.2729 0.2457 0.3021	G.u101 g.u305 0.0295 0.0295 0.0297 0.6256 -0.0019 -0.0027	0.2895 0.2751 0.2834 0.2854 0.2862 0.2909 0.3087 0.3114				
13 40 14 42 15 44 16 46 17 48 19 50 19 52 20 54 21 56	0.30 2.31 4.33 6.34 8.31 9.32 92.32 4.33	0.8061 0.9286 0.9533 6.9717 6.9761 0.9836 6.9927	0.0261 0.0247 0.0247 0.0254 0.0254 -0.0019 -0.0019 -0.0124	0.2013 0.2011 0.2050 0.2729 0.2727 0.2757 0.3021	0.0295 0.0256 0.0257 0.0256 -0.0019 -0.0096 -0.0127	0.2834 0.2854 0.2862 0.2909 0.3087				
15 44 16 46 17 48 19 50 19 52 20 54 21 56	2.31 4.33 6.34 8.31 9.32 92.32 4.33	0.9284 0.9533 6.971+ 6.9761 0.9834 6.9977	0.0247 0.0254 0.0264 -0.0019 -0.0019 -0.0124 -0.0124	0.2650 0.2729 0.2327 0.2357 0.3031	0.0256 0.0257 0.0257 0.0256 -0.0019 -0.0019 -0.0127	0.2854 0.2862 0.2909 0.3087				
15 44 16 46 17 48 19 50 19 52 20 54 21 56	8.31 9.32 9.32 9.32 4.33	0.9533 0.9718 0.9718 0.9761 0.9634 0.9977 1.0206	0.0254 -0.0264 -0.0019 -0.0091 -0.0124	0.2729 0.2527 7542.0 1205.0 0.3071	0.0257 0.6256 -0.0019 -0.0094 -0.0127	0.2862 0.2909 0.3087 0.3114				
16 46 17 48 19 50 19 52 20 54 21 56	6.34 8.31 9.32 9.32 9.32 9.33 9.35	6.971E 6.957E 6.9761 0.9836 6.9977 1.0206	0.0744 -0.0014 -0.0041 -0.0124 -0.0142	0.2527 0.2457 -0.3021 -0.3041	-0.0019 -0.0019 -0.0127	0.3087		· · · · · · · · · · · · · · · · · · ·		
17 48 19 50 19 52 20 54 21 56	8.31 10.32 12.32 14.33 16.35	G. Y>7e G. 9761 O. Y834 G. YY77 1.0206	-0.0019 -0.0091 -0.0124 -0.0142	0.2957 1505.0 1605.0	-0.0019 -0.0094 -0.0127	0.3087				
19 52 20 54 21 56	2.32 4.33 6.35	0.9634 6.9917 1.0206	-0.u124 -0.u142	0.3091	-0.0127					
20 <u>54</u> 21 56	6.35	1.0<06	-0-4142			0.3143				
21 56	6.35	1.0206								
					0 <u>-0143</u> _ -0.0165	-0-3181 0-3189		 		
	59		-0.0180		-0-0175	0-3201		 ··		
			22			2011				
							· · · · · · · · · · · · · · · · · · ·	 		· · · · · · · · · · · · · · · · · · ·
					<del></del>			 		
<del>-</del>								 	- · · · · · · · · · · · · · · · · · · ·	
					***			 		
							· <del></del>	 		

.

--

. ...

	ENGINEER 1 OF 1	ING VEVE	LOPMENT_CE	MIERIAED	C) · PROPI	JLSION.mino 113514 missi	) T <u>unmel Facility(PWI)                                    </u>	AERODYMANIC MIND TUNNEL(AT)
HEET	1 OF 1					SPLITI	R PLATE DATA	
					<u> </u>			
	7557	DART MAC	H_RX10=6_0	TOUE TRAN	CITION			
	5	510 0.60	2.5		HEE			
BOILT	AL PHA	CNF	Ch	Cd	* COE	YUPF		
1	59.20		-0-0143		-0-01AZ	0-3207		
5	54.24	1.0173		0.3273	-0.0209	0.3217		
3	60.23		-0.026		0 a0221_	0.3733		
*	61.24		-0.0242		-0.0236	0.3238		
_5_	63.26		-0-0255 -0-0267		-0-0248	0.3265		
7	69.25		-0-0267		-0.0259	0-3264		
8	54.75		-0.0311		-0.6300	0.3263	· · · · · · · · · · · · · · · · · · ·	
9	69.25		-0.0329		-0.6317	0.3297		
10	10.26		-0-0343		-0.0331	0.3316		
_11	72.26	1.0367			0_0353	0.3331	·····	
15	74.26		-0.0367		-C-0374	0.3340		•
13	76.27		-0.0443		-0-0345	0.3375		
15	76.24		-0.0475		-0-0449	0.3367		
16	42.27		-0.0513		-0.0442	0.3425		.,
17_	89.25		-0,0552		-0-0517	0.3440		
18	86.78		-0.0566		-0.0546	0.3451		
19_		1-0146	-0_uell	0.3710	-0_0568	0-3453		
							<del></del>	<del></del>
					•			
				·				
							• •	
					·	<del> </del>	<del></del>	<del></del>
						•		
						·		
-								
				•				
			<del>,</del>					
			•					

1 OF   SPLITTER PLATE DATA   SPLITTER PLATE DATA		1 OF 1				MA	IN MISSILE TAIL EFFE	CTS DATA	AERODYNAMIC AIND TUNNEL (AT)
2 211 0-by 2-5 F36 FREE  (NT ALPMA CNF CM CM CM CM CM CM CM ACPF VCPF  AB.13 1.0266 -00.0040 0.3575 -0.0570 0.3675  0 9-14 1.0222 -0.0040 0.3544 -0.0595 0.3472  1.90.16 1.9189 -0.4432 0.3559 -0.4620 0.3493  0 91.17 1.0137 -0.9656 0.3544 -0.0649 0.3493  0 91.17 1.0137 -0.9656 0.3544 -0.0649 0.3496  0 92.17 1.0197 -0.9579 0.3544 -0.073 0.3516  0 93.16 1.0002 -0.4703 0.3541 -0.073 0.3546  0 94.14 0.9912 -0.0725 0.3524 -0.0740 0.3536  2 94.14 0.9912 -0.0725 0.3524 -0.0740 0.3536  2 99.15 0.9035 -0.0528 0.3522 -0.0990 0.3578  2 99.15 0.9035 -0.0528 0.3522 -0.0991 0.3637  1 100.16 0.9766 -0.0560 0.3557 -0.0991 0.3637  2 104.15 0.9795 -0.0580 0.3555 -0.1001 0.3639  3 106.15 0.9796 -0.0560 0.3556 -0.1001 0.3639  5 110.15 0.9715 -0.1155 0.3576 -0.1101 0.3668  5 110.15 0.9715 -0.1155 0.3577 -0.1192 0.3667  7 114.15 0.9052 -0.1210 0.3577 -0.123 0.3676  8 116.17 0.9523 -0.1212 0.3574 -0.123 0.3676							-ACLIICH FERILLIAN		
2 211 0-by 2-5 F36 FREE  (NT ALPMA CNF CM CM CM CM CM CM CM ACPF VCPF  AB.13 1.0266 -00.0040 0.3575 -0.0570 0.3675  0 9-14 1.0222 -0.0040 0.3544 -0.0595 0.3472  1.90.16 1.9189 -0.4432 0.3559 -0.4620 0.3493  0 91.17 1.0137 -0.9656 0.3544 -0.0649 0.3493  0 91.17 1.0137 -0.9656 0.3544 -0.0649 0.3496  0 92.17 1.0197 -0.9579 0.3544 -0.073 0.3516  0 93.16 1.0002 -0.4703 0.3541 -0.073 0.3546  0 94.14 0.9912 -0.0725 0.3524 -0.0740 0.3536  2 94.14 0.9912 -0.0725 0.3524 -0.0740 0.3536  2 99.15 0.9035 -0.0528 0.3522 -0.0990 0.3578  2 99.15 0.9035 -0.0528 0.3522 -0.0991 0.3637  1 100.16 0.9766 -0.0560 0.3557 -0.0991 0.3637  2 104.15 0.9795 -0.0580 0.3555 -0.1001 0.3639  3 106.15 0.9796 -0.0560 0.3556 -0.1001 0.3639  5 110.15 0.9715 -0.1155 0.3576 -0.1101 0.3668  5 110.15 0.9715 -0.1155 0.3577 -0.1192 0.3667  7 114.15 0.9052 -0.1210 0.3577 -0.123 0.3676  8 116.17 0.9523 -0.1212 0.3574 -0.123 0.3676			2427 ****			FITTOM		*	
89.14		S	S11 0-61	2-5	F36 F	REE		<del></del>	
89.14						KCPF	YCPF		
90.16	<u> </u>	86-13	1.0264	=0.0587	0.3575	-0.60370			·
91.17 1.0137 -0.0659					0.3559	-0-6520	7-7-6 - TPAF		
1		91.17	1.0137	-0.9658	0.3544	-0.0649	3496		
7 94.14 0.9772 -0.0776		42.17	1.0090	0.N <u>519</u>	4.3540	Qa#6Z3			
9 96.16 (.9070 -0.070) (.3532 -0.0790 0.3578 9 98.15 (.9035 -0.0528 (.3552 -0.0842 0.3608 1 100.16 (.9025 -0.0528 (.3550 -0.0991 0.3637 1 102.16 (.9025 -0.0528 (.3550 -0.0991 0.3623 2 104.15 (.9025 -0.0580 0.3566 -0.1001 0.3639 3 106.15 (.9725 -0.0580 0.3566 -0.1001 0.3639 4 107.15 (.9725 -0.1021 0.3566 -0.1049 0.3674 4 107.15 (.9725 -0.1155 0.3556 -0.1101 0.3668 5 110.15 (.9715 -0.1155 0.3556 -0.1101 0.3668 5 110.15 (.9702 -0.1150 0.3577 -0.1192 0.3667 7 114.15 (.9564 -0.1190 0.3577 -0.1192 0.3667 8 116.17 (.9523 -0.1212 0.3524 -0.1273 0.3701					0.3541	-0.0703	0.3540	`	
9 99.15 0.9035 -0.0528 0.3562 -0.0002 0.3608 0 100.10 0.9760 -0.0572 0.3557 -0.0991 0.3637 1 102.16 0.9765 -0.0560 0.3565 -0.1001 0.3623 2 104.15 0.9796 -0.0560 0.3565 -0.1001 0.3639 3 106.15 0.9796 -0.0560 0.3556 -0.1049 0.3674 6 109.15 0.9715 -0.115 0.3556 -0.1101 0.3668 5 110.15 0.9715 -0.115 0.3577 -0.1192 0.3667 7 114.15 0.9049 -0.1150 0.3577 -0.1192 0.3667 8 116.17 0.9523 -0.1212 0.3524 -0.1273 0.3676					9245	-0.0740	3536		
100.16									
1 102-16	0		0-9/40	=0-05Z3	0-3-57	-0-0491	1.3437		
2 104.15	1	102-16	C.9025	-0.1536	0005	-0.0952			
6 109.15	2	104.15	C. 979c	-0.0960	U.3565	-0.1001	0.3639		
5 110.15 0.9716 -6.1115 0.3589 -0.1147 0.3693 6 112.15 0.9702 -0.1156 0.3577 -0.1192 0.3667 7 114.15 0.9645 -0.1190 v.3547 -0.1233 0.3676 8 116.17 0.9523 -0.1212 0.3524 -0.1273 0.3703	3	166.15	0.9735	-0.10/1				<del></del>	
6 112.15 0.9702 -0.1156 0.3577 -0.1192 0.3667 7 114.15 0.9649 -0.1190 0.3524 -0.1233 0.3676 8 116.17 0.9523 -0.1212 0.3524 -0.1273 0.3701	•	109.15	U.9641	-0.1005	0.3551	-0.1101	0.3668		
7 114.15 0.5045 -0.1190 v.3547 -0.1233 0.3676 8 116.17 0.9523 -0.1212 0.3524 -0.1273 0.3701	-	110-15	0.9715	-0-1113		-0.1167	0.3697	<del></del>	
8 116.17 0.9523 -0.1212 0.3524 -0.1273 0.3701	ř	114.15	0.4044	-0-1190	u-35e7	-0-1233	0-3676		
9 117 14 0.9441 -0.1270 0.3505 +0.1289 0.3704									
					<del></del>				<del></del>
									<del></del>
					<del></del>				
								· · · · · · · · · · · · · · · · · · ·	
				-					
					<del></del>	·			
						· <del>···</del>	<del></del>		

SHEET 1 OF 1

	JESI			CONF. IRAN	SITION	
	2	515 0.80	2.5	F36 F	RFE	
POINT	ALPIA	CNF	CH	· Cn	(COF	YCPF
1	110.00		-0.1147			0-3701
2	114.06		-u.11y3		-0-1334	0.3715
	120.25		-0-1510		-0.1350	0.3716
	121.06		-0.1224		-0.1367	0.3708
5	122.26		-0.14.7			0.3698
	123.05		-9-1255		-0-1402	0.3708
	124.05		-G-125n		-0-1416	0-3695
	126.00		-0.1677		-0.1453	0.3701
	125.05		-0.1307		ual491	0.3698
	130.05		-0-1326		-0-1527	0.3704
	132.00		-0-1356		-0-1561	G-3696
12	134.06		-0.1379		-0.1595	0.3726
	135-17		-2-1-03		-0-1523	0-3714
14	138.05		-0-1442		-0.1741	0.3777
	139-16		-0.1503			0.3817
16	142.06		-0.1619		-0-1924	0.3899
	144.09		1076_			0-4004
18	146.04		-6.1716		-0.2171	0.4071
	147.05		-0-1711			0.0092
				<del></del>		
				•		
				<del></del>		<del>,</del>

ARNOLD ENGINEERING DEVELOPMENT CENTER (AEDC) PROPULSION DING TUNNEL FACILITY (PWT) AERODYNAMIC WIND TUNNEL (AT)

PAGE 1 OF 1 HARTIN MISSILE TAIL EFFECTS DATA

٠

SPLITTER PLATE DATA

Æ	ENGINEE! 1 OF 1 1 OF 1	RING DEVE	LOPMENT_CE		MAI	TIV MISSILF TAIL	EFFECTS DATA	AERODYNAMIC WIND TURMEL (AT)
	1ESJ.	PAPI PAC 213 0.60			SITION			
	ALPHA	CNF	-0-1648	Cr		YCPF		
2	148.95		-0.1679		-0.2218	0.4092		<del></del>
ž	149.90		-0.1634		-0.2262	0.4112		
	150.97		-0-1590		-0.2277	0.4089		
<u> </u>	151a97_		-0-1533 -0-1460		<del>-0.2296</del>	0.4061	· · · · · · · · · · · · · · · · · · ·	
7	152.90		-0-1480 -0-1430		-0.2320	0.4103		
8	155.99		-0-1321		-0.2394	0.4117		
9	158.00	0.4711	-0.1245	0.2344	-0.2459	0.4161	·-··	
	159.44		-0.1098		-0.2532	0.4184		
	162-00		_0_ <u>u967</u>		-0.2623	0-9226-0		
3	164.01		-0.007# -0.u767		-0.2733	0.4284		
•	166.03		-0.0652		-0.3026	0.4376		
5	170.04	0.1726	-0.0550	0.0762	-0.3183	0.0411		
6	172.06		-0.0-40		-0.3348	0.4464		
Z	173.16. 176.10		<u>-0.0377</u> .		-0.3460 -0.3857	0.4549		
9	177.09		-0.0221 -0.0170		-0.4229	0.5335		
					<del></del>			
					<del></del>			
			101					
							•	

6E	1 OF 1		LOPMENT C	ente <u>o laeu</u>	<u>C1 PHOP</u>	HTIN MISSILE	TUNNEL FACILITY (PHT) TAIL EFFECTS DATA	AEHOOYNAMIC WIND TURNEL !	<u> </u>
ET_	1 OF 1		·-·			SPLITTER	PLATE DATA		<del></del> -
		PART PAL	H.RX10-6		S1110%				
	2	214 0.60	2.5	F36 F	HEE				
	ALPHA	CNF	Сн	CA		YCPF	74 ±,	•	ė. edi
<u>.                                    </u>	179.00	0.017m	-0.0123	0.0116	-014314	0.6502			d.
3		GAULY		U-0172	-0.5535	1.0376			
4 5	180.99	-0.0039 -0.0113	0.VGQ0 0.VG35	-0.0035	-0.0129	-0.907Z			
	183.01	-0.UZ13	0.0074	-0-0050	-0.3469	0-2362			
7	184-01	-0.4514_ -0.4504	0-0115		-0.3610 -0.3534	0.3030	<del></del>	· · · · · · · · · · · · · · · · · · ·	
	·								
						<del> </del>			
							•		
	·-··-	<del></del>					· · · · · · · · · · · · · · · · · · ·		
							·		
	-								
		-					· · · · · · · · · · · · · · · · · · ·		
								· · · · · · · · · · · · · · · · · · ·	
					·				
				· · · · · · · · · · · · · · · · · · ·					
									·-··
				<del></del>			-		
							<del></del>		

	1 OF 1				MV	TIN MISSILE	UNNEL FACILITY(PMT) TAIL EFFECTS DATA PLATE DATA	
								•
	TEST	PART MAC	n Palo-6	CONF TRAN	51T10N			
	2	215 0.65			REE			•
POINT	ALPHA	ENF	CH	Ce	KCPF	YCPF		
		-0.0304	6.0001		-0.0026	0.4706		
2	-0.91	-0.015/		-0.6068	0.0147	0.4343		
	1.04	-0-006a	-C.0003	-0-0001	0 <u>-0516</u> -0.0931	0-0110 1-4057		
3	2.0+		-0.0004			0-6547		
6	3.04		-0.,007		-0.0273	0.6284		
_7	4.05		-0.0012		-0.4301	0.5524		
6	6.07		-0.J0J7		-0.0394	0.4701		
10	# <u>.07</u>		-0.0043 -0.0052		-0-0349 -0-0306	0-3921		
_11	12-11		-0.0052 -0.0055		-0-0295	0.3731		
12	14.13	0.2655	EACU.D-		-0.0292	0.3426		•
	10.15		-2-06-2		-0.0266	0.3279	<del> </del>	<del> </del>
14	18.16		2660-0-		-0-0223	0.3195 0.3147		
16	55.55		-C.0093		-0.0173	0.3125		
_17	24.25		-0.0093		-0-0155	0.3128		
16	56.59		-0.0098		-0.0139	0.3084		
19	27.29	0.0364	-0-3CHG	0.2117_	-0-0127	0-3040		
			•					
						·	<del></del>	<del></del>
						·	<del></del>	
								· · · · · · · · · · · · · · · · · · ·
					-			
					<del></del>		·	
							***************************************	· · · · · · · · · · · · · · · · · · ·

- ----

<del></del>	
	-
	•
	•
	•
	- 1
	,
	,
	_
	•
	•
	1
	. !
	- (

3E	1 OF 1		LOPPENI. L		MA	ILSION WIND TUNNEL FACILITY(PHT) HYIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC .aind TUNNEL(611
						· · · · · · · · · · · · · · · · · · ·	
	IESI. _	PARI .MAC 217 0.65			SITION		
DINT	ALPHA	CNF	Cn	C-		VCPF .	· A
1	28.15		-0.0071		-0.0100	0.3622	
5	29.74		-0.0065	0.2237		0.3013	
3	39.24_		0.0059		-0.0076_	. 0.2969	
•	31.20		-0.0055		-0.0063 -0.0050	0.2965	
·	33.27		-0.0030		-0.0035	0.2923	<del></del>
,	34.28	4506.0			-0.0014	0.2917	
8	36.70	0.7463	0.0630	U.7504	0.0033	0.2876	
ě	38.32	0.9431	0.417#	G-2570	0.0193	0.2780	
10	+0.31	0.6797	0.02+3	0.2431	0.0276	0.2764	
ii_	42.34	0.9242		0.2005		0.2819	
12	44.35	0.4563	4550.0	0.2703	0.0234	0.2827	
13_	96.36	0.4046	0.0232	0.2756		0.2857	
14	4R.33		-0.0019	4.2416		0.3044	
15	_50.33_		-0.0069		0-0192	0.3074.	<del></del>
16	52.35		-0.0131	0.3071		0.3118	
11	_54.35_		0.0153		0_0152	0.3129	
18	56.37		-0.0174 -0.0185		-0.0169 -0.0178	0.3160	
14	3/43/	1-0304	-0.0163	Un-1200	-040174	043163	<del></del>
			**			<del></del>	
				•			
			<u> </u>				
							·
		<del></del>					
			<del></del>				······································
					<del></del>		
						<del></del>	<del></del>
			<del></del>			·· <del>···································</del>	
							,

Æ	1 OF 1		COPPESS 3		MAI	TIN MISS	ILE TAIL EFFECTS DATA TER PLATE DATA	AERODYNAMIC #IND_TUNNEL(AT)
		PARI MAL		CUNF IRAN	SITION			
INT	ALPHA	CNF	CH -	Cn	) CPF	YCPF		,
1	59.20	1-0165			-0.0194	0.3188		
5	59.25	1.0263			-0-0506	0.3168		
<u> </u>	61.26	le@il	-0.0225 -0.0237		-0.0218	0.3200		
3	62.26		-0-0248		-0.0239	0.3225		
6	63.26		-0.0242		-0.0252	0.3220		
1_	64,75	1.0951	-0-4275	0.3387	-0.0263	0.3241		·
8	66.27		-0.0305		-0.0291	0.3253		
9	69.27		<u>-C-1366</u>		-0-0312	0.1262		
0	70.26		-0.0341		-0.0324	0.3289		
<u>ų –</u>	71.39				<u>=0.u335</u>	0.3306		
13	74.26		-0.0367		-0.0365	0.3316	•	
14	76.28		-0.0441	0.3253	-0-0-12	0.3357		
15	85-29		-C-0-73		-0-0439	0.3365		
16	42.24		-0.0509		-0.0459	0.3384		
<u> </u>	84.30		-0-0557		-0.0511	0.3408		
18	86.31		-0-9544		-0.0543	0.3430		
19	87.30	1.0439	-0.0510	<u> </u>	-0-0558	0.3441	<del></del>	
		<del></del>		· · · · · · · · · · · · · · · · · · ·				
						•		
				· <del></del>				
				20				<u></u>
							· · · · · · · · · · · · · · · · · · ·	
			·					

	1 OF	eping vevi 1 1	LLOPHENT CI	NTEHLALD	C) PHUP	JLSIUM WIND TUNNEL EAGILITY(PWI) TIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYMANIC DIND TUNNEL (41)
						,	
<u> </u>	<u>TE</u> S	T PART MA	CH BX10-6_(		SITION		
ŽINT	ALPHA		Сн	Сн	* *xCPF		<b>u</b>
<u>-1</u>	89.14 89.14			U-36U3	-0-0570	0.3456	
<u> </u>	90.17	1.0400	-0-4634	0.3017	-0-4014	D. 3478	- <del>11 - 12 - 12 - 12 - 12 - 12 - 12 - 12</del>
•	91.11			0.3546	-0.0539	0.3493	
<u> </u>	<u> 92.17</u> 93.17			0.3575	-0-0667 -0-0701	0.3508	
<u>.                                    </u>	79.17			4.3617	-0-0725	0.3537	
6	96.11			0.3567	-0.6789	0.3563	
9	98.17 100.17			0.3620	-0.0537 -0.0561	0.3620	
11	102.17		-0-4942	0.3577	-0-0948	0.3598	
12	104.1	0.4743	-0.0468	0.3617	-0.0994	0.3638	
13	105-17			<u> </u>	-0-10-2	0.3659	<del></del>
14 15	108.17		-0.1ue2 -0.1123	0.3034	-0.1097 -0.1146	0.3655 0.3679	
16	112.1				-0.1182	0.3688	
	114.1		-0.1211	G.3610	-0-1231	0-3669	
19	116.10	0.9665	-0.1224		-0.1268 -0.1286	0.3698	
11	-11/41	6.3637	- 121234	- 444201	- Walzan		
						•	
						•	•
			<del></del>	<del></del>			
			- <del>-</del>				
		<del> </del>					
			<del> </del>		·		

E	ENGINER 1 Of 1 1 Of 1	RING DEVE	LOPMENT C	ENTERLAED	C1 PROPI	11510N =1 (TIN #155 SPLIT	NO TUNNEL FACILITY (P=T) ILÉ TAIL EFFECTS DATA TER PLATE DATA	AERODYNAMIC HIND TUNNEL (47)
	76 67	<del></del>						· · · · · · · · · · · · · · · · · · ·
	5	220 0.65			REE			
	ALPHA	CNF	CH	Co		YCPF	· · · · · · · · · · · · · · · · · · ·	
	118.01 119.01		-0-1243		-0.1319 -0.1336	0.3713		
	120.01	0.7000	-0-1230	0.3349	-0-1355	0.3686		
	121.07		-n.1250		-0.1371	0.3681		
	122.07		<u>-0.125a</u> -0.1262	<u> </u>	-0-1388 -0-1405	0.3680	<del> </del>	
	174.00	0.6462	-0-1277	0.326d	-0.1422	0.3661		
	126.06		-v-1295		-0-1458	0.3686		
	130.06		-0.1323 -0.1336		-0.1493 -0.1529	0.3682		
ĭ	132.07	0.0/32	-6-1360	0.3229	-0.1559			
Ž	134.07	0.6646	-1.1375	50SE.u	-0.1590	0.3703		
	136-98		-0-1-00		-0-1634	0-3711		· · · · · · · · · · · · · · · · · · ·
	138-06		-n.1436		-0.1700 -0.1799			
	142.05		-0.1562		-0.1880	0.3827		
			0 <u>-1039</u> .	6-3211	-0.2012			
			-0.1673		-0.2144 -0.2196	0-4048		
	1411							
				<u></u>				
							**************************************	
				<del> </del>				
		-						

	1 OF 1					3FL4116H	PLATE DATA		
		PART MAC	W HX10-0-1	CUNF_TRAN	511104	· · · · · · · · · · · · · · · · · · ·			
		221 0.65			REE			<del> </del>	
	ALPHA	CHF	СН	C4	WE ACPF		• અ હો		1 (15)
	147-90		-0-1077		-0-2193	0.4057			
:	1-8-97		-0.1672		-0.2230 -0.2252	0.4064	•		
	150.97		=0.1646_ -0.1607		-0.2272	0.4055		<del></del>	<del></del>
	151.97		-0-1549		-0.2294	0.4055			
	152.98		-0.1503		-0 -2322	0.4076			· · · · · · · · · · · · · · · · · · ·
	153.96		-0-1497		-0-2339	0.4090			
1	155.99		-0.1333		-0.2378	0.4079			
6	157.99		-0-1222			0-4109			
, _	160.00		-0.1099		-0.2516	0.4166			
Ĺ	162-01		-0.4793		-0-2610	0.4170			
2	164.02	6.3246	-0.0688	0.1397	-0.2718	0.4246	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
	166-03	0.2/30	-0-0786	W-1175	=0.2877	0-4302			
	168.04	5.26.2	-0.0576	0.0954	-0.3015	0.4255			•
	170.04		-0-0564			0.+343			
5	172.07		-0.0-52		-0.3357	0.4336			
	174-08		Q. <u>0333</u>		-0.3631	_O.+423			
8	176.09		-0.0227		-0.3R29	0.4331			
9	177-10	0.0046	-0-0176	0.0194	0.3967	0.4327	<del></del>	<del></del>	<del></del>
			-						
-								······································	
				<del></del>	<del></del>				
				· · · · · · · · · · · · · · · · · · ·			•		
						<del></del>			

• • • • • • • • • • • • • • • • • • • •						•			
								· · · · · · · · · · · · · · · · · · ·	
		·	*						
PAGE	1 OF 1		LOPPENT C	ENILRIAED	MAI	TI- MIS	SILE TAIL EFFECTS DATA	AERODYNAHIC .=1ND_TUNNEL_(4T)	· •
SHELT	1 OF _1				<del></del>	SPLI	TTER PLATE DATA		
		.PARI_MAG	M. HA10=6_	CUNE_IHA					
	S	255 0.65	2.5	F36 F	4EE				
	ALPHA 178-00	CNF	Cn =0.0122	Co	793X	YCPF			
5	174.90	6.0167	-0.0050	0.0096	-0.4757	0.5235			-
•	180.95	-0.0030	0.0003	0.0017	-0.3805	-0.5563		· · · · · · · · · · · · · · · · · · ·	
	162-01	-0.0096	0.0047	-0-0029	-D.3016	0.3057			<del></del>
7	164.04	-0-0315	0.0121	-0.0126	-0.3953	0.3990	· · · · · · · · · · · · · · · · · · ·		
8	186.01	-0.0592	0.0219	-0.02+1	-0.3702	0.4057		•	
	-								
	·			<del></del>	<del></del>				
									·
							•		
		id.	70%						
	<del></del>								
					· · · · · · · · · · · · · · · · · · ·				
						<u></u>			
					<del></del>				
									•
	<del></del> -								<del></del>
	_								· · · · · · · · · · · · · · · · · · ·
			<del></del>						
	-								
								The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	

3E	ENGINEE 1 OF 1 1 OF 1		LOPHENI C	ENTERLAED	<b>₩</b> ▲	ULSIUM MIND JU HTIM MISSILE T SPLIITER P	AIL EFFECTS DATA	AERODYNAMIC IND. TUNNEL (AT)
			<del> </del>					
	IESI	DAM TEAG Seu Ess		CONF TRAM	SITION			
		223 0.92	C+3	r30 r				
TNT		Cref	Cm	Ce	* xCPF		<b>13</b> 49	نقيد
<u>.                                    </u>		-0-4334			0.0003	0.6121	<del></del>	
Š	-0.97		-0.0003	-0-0103	0.0174	0.4823		
<del>!</del> —	1.04	-0-00P1.		-0-0 <u>-0-</u>	-0.1232	0-1708		
:	2.04		-0.0006 -0.0006		-0.0540	0.4711		
<del>-</del> -	3.04		-0.0006		-0.0316	0.5722		
7	4.95		-0.000e		-0-0278	0.5794		
6	6.67		-0.0627	U-0359	-0.0358	0.4643		
9_	8.00		-0-0044		-0-0369	0.4227		
10	10.16		-0.0058		-0.0346	0.3770	· · · · · · · · · · · · · · · · · · ·	
11_	12.12		-0.0u13		-0.0330	0.3584		
12	14.13		-0.0094		-0.0333	0.3373		
13_	15.10		-0-4106		-0-033B	0.3237		<del></del>
14	18.16		-0.0114		-0-0279	0.3173		
15 _	20.20_		-0-0113		-0-0239	0.3113		
16 17	22.20		-0.0115		-0-0550	0.3093		
18	26.30		-0.0129	1-2.142	-0.0195	0.3084		<del></del>
19	27.34		ES10.00		-0.0177	0.3057		
•								
	400			-				
								•
							·	
_		<del></del>						
						<del></del>	<del></del>	
								•
								•
		_					•	
								•

	1ESJ		M HA19-6_	CONF TRAN	S1110N		
	5	224 0.46	2.5	F36 F	HEE		
THIC	ALPHA	CMF	CH	Co		YCPF	
<u> </u>	28.17		-0-0102		-0-G141	0.3060	
ź	30.24		-6.2207 -betve7		-0.0116	0.3020	•
•	31.26		-0-0000		-0.0098	0.2983	<del></del>
	32.27		-0-000			0.2962	
	33.26	0.6/27	-7.0000	V-2585	-0-0069	0.2963	
	34.24		-C-LLAD		-0-60-4	0.2941	
	36.33	0.4364	0.0129	6.5045		0.2866	
	40.34	0.410p	<u> </u>	<u>0.2569</u> 0.2560		0.2788 0.2789	
	42.36		U+(1777 	0.2500 <u>0.2608</u>		0.2789	
<u> </u>	44.37	0.4660		0.2781	0.0210	0.2879	
<u> </u>	46.36		6-2149		0.0202	0.2915	
•	45.35		一日・ロビッカ		-0.0058	0.3077	<del></del>
<u> </u>	50.35		-0-0134		0 <u>_u138</u>	0.3121	<del></del>
,	52.37 54.39		-0.015-		-0.0155 -0.0168	0.3157	•
/ 8	55.50		-0.0145		-0.0178	0.3188	
_	57.40				-0-0190	0-3194	
							•
							· · · · · · · · · · · · · · · · · · ·

GE	ENGINEE 1 OF 1 1 OF 1		LOPMENT CI	NJER (AED	C) PROPI	TIN MISSIL	<u>D TUNNEL FAC:</u> LE TAIL EFFEC ER <u>PLATE DAT</u>	TS DATA	AERODYNAMIC WIND TUNNEL (AT)	
							_			
	TEST	PART WAS	H PALO-6_1	ONE TRAN	51110N		_			
	5	225 6.96			REE				•	,
PÓINT	ALPHA	CNF	CH	Cp	T *CPF	YCPF		R 4		
	58.22	1.0590	-0-0227	0.3371	-0-0215	0.3197				
2	59.29	1.0577	-6.0233		-0.0550	0.3214			•	•
_3	61.29	1.0726	-0.0243		-0.0228 -0.0233	_0.320A	<del>- , , , , , , , , , , , , , , , , , , ,</del>			
•	62.29		-0.0250		-0.0733	0.3217				
6	63.29	1.0725	-0.0256		-0.0239	0.3242				
	64.31	laur3a	-0-4269		-0-0769	0.3256				
d	06.30	1-6000			-0.0275	0.3272				•
_9	68.29		-0-0335		-6.0310	0-3284			<del> </del>	
10 11	70.31 72.31	1.0074	-0.0340 -0.0373	0.3604	-0.0313 -0.0341	0.3314				•
15	74.31		-0.0403		-0.0366	0.3334			··	
13	70.31		-0-0625		-0-EU-0-	9455-0				
14	78,33		-0.0454		-0.0412	0.3367			•	
_15	80.33		-0.0484		-0.0433	0.3385 _				
16	82.33		-0.0524	0.3412		0.3409			•	
_17	_64_33	<u>1-1206</u>	-0.0571 -0.0613		<del>-0.0510</del>	.0-3-14	<del></del>		· · · · · · · · · · · · · · · · · · ·	
16	86.34 87.34		-0.0613		-0.0545 -0.0564	0.3440				
13	- HIA-18-	1412.15	-0.400.33	UR3-113	-UAU-3134					
							•			
						<del></del>		· · · · · · · · · · · · · · · · · · ·		
		•	-						-	
								<del></del>	<del>~</del>	
							<del></del>		· · · · · · · · · · · · · · · · · · ·	
									-	
							1			
							<del></del>		· · · · · · · · · · · · · · · · · · ·	

	ENGINEE 1 OF 1 1 OF 1		LOPMENT C	ENTER (AED	44	KTIN MISSIL	. IUNNEL FACILIT E TAIL EFFECTS R PLATE DATA	DATA	LERODYNAMIC_HIND_TUNNELIATI
		•							
	IESI	284 U.96		CUYF IRAN F36 F	SITION PEE	<del></del>			
NY	ALPHA 84.15	CNF	-0-0655	Ç5	XCPF -0_05/6	YCPF	<del></del>		
<u>-</u>	84.16	1.070/	-0-00-0	0.3723	-0.0594	0.3453			
<u> </u>	91.21	1.0724	-0.0567		-0.0619 -0.0635	0.3465	<del></del>	··	
	92.21	1.4641	-0.0699	<u>0.3578</u>	-0-0657	0.3476			,
,	93.20 94.20	1.0586		0.3703 4.3095	-0.0677 -0.0702	0.3497			
!	96.15	1.0-13	-0.0779	0.35H3	-0.0748	0.3537			
,	98.19	1.0257	-0. u P 25		-0.0802	0-3561		<del></del>	
	100.19	1.0300		0.3701 0.3595		0.3593			
	104.19	1.0166	-0.0769	0.3693	-0.0471	0.3626			
	105.19	1.0155	-0.1035	0.3725	-0.1082	0.3651			
5	110.15	1.0132	-9-11-4	3731مئـــــ	0.1129	0.3663	<del></del>		
	112.15		-0.1145	0.3717	-0.1170 -0.1217	0.3669			
1	115.20	1.0014	-0.1264	0.3711	-0.1262	0.3706			
	117.20	0.4464	-0.1479	0.3708	-0-12 <del>4</del> 1	0.3714			
		•							
							-		
					· -			· · · · · · · · · · · · · · · · · · ·	
					<del> </del>				
	<u>-</u>		<del></del>				<del></del>		
									· · · · · · · · · · · · · · · · · · ·
					• • •		<u> </u>	<del></del>	•

<u>L</u>	ENGINEE 1 OF 1 1 OF	RING UEVE	LOPMENT C	ENTERIALD	MA	TIV MISSI	O JUNNEL FACILITY (PHI). LE TAIL EFFECTS DATA ER PLATE DATA	AERODYNAMIC #1ND TUNNEL (41)
<u> </u>			<del></del>	~		SPLAII	ER PLAIR DATA	
							<del>,,,,</del>	
	TEST	PART MAC	H RX10-6	CONF TRAN	SITION			
	S	227 0.92			REE			
-	ALPHA	CNF	Сн		* ACPF	web\$	<u> </u>	
1	118.00		-0-1228		-0-1324	0-3742		
2	119.00	0.4526	-0.12-2	0.3447	-0-1342	0.3724		
	120-01				-0.1356	0-3704		
• •	121.07		-9.1265 -0.1279		-0.1375 -0.1395	0-3704		
	123.07		-0.12H4		-0.1410	0-3704		
7	124.06	0-9171	-0-1410	0.3398	-0-162B	0.3705	<del></del>	
8	126.06		-0.1327		-0.1466	0.3717		=
	128.00			0.3342	-0-1498	0-3719		
0 1	130.00		-0.1362		-0-1530 -0-1556	0.3710		
_	134.07		-0.1377		-0.1584	0.3681		
Ĺ	136-66	0.0050	-0-1396	0.3166	-0-1514	0.3085		
•	138.07		-0.1412		-0.1652	0.3698		
	139.12				-0-1529	0-3701		
	142.08		-0.1473 -0.1537		-0-1775 -0-1901	0.37 <b>26</b> _0.3846		
5	146.00		-0.1662		-0.2080	0.3961		
	147-06		-0.1705		-0-2140	7.3985		
							-	
				<del></del>				
							<u>.</u>	
							<u> </u>	·
				<del></del>				
				<del></del>		<del></del>	<del></del>	
_								

	1 OF 1				MAI	ITIN MISSI	LE TAIL EFFECTS DATA	AERODYNAMIC - IND TUNNEL (AT)
EL	I OF I					SPLITT	ER PLATE DATA	
							•	
							-	
	JES1_ 2	24.u.4 <u>4.</u> 24.u 425		CONETRAN	\$111 <u>0%</u>  HEE			
		EE- 007E	£.5		WEE		· ·	
	ALPHA	CNF	Ch	C=	KCPF	YCPF		
	147.90		-C-1717		-0-2160			<del></del>
2	148.97 149.96		-0.1703	0.3114 <u>0.3</u> 059	-0.2193	0.4013		
	150.96		-0.1643		-0.2235	0.4015		· · · · · · · · · · · · · · · · · · ·
	151.97_		-0-1600		-0.2267	B.4041		·
6	152.98		-0.1558	6.2769	-0.2292	0.4075		
	153.97		-0-1510		-0-2317	0.4051	<del></del>	<del></del>
	155.99 157.99		+0.1+u+ -0.1280		-0.2356 -0.2413	0.4020		
	160.00		-0.1151		-0.2479	0.4057	<del></del>	
	162.00	0.+100	-2-1110	Val 096	-0-2706	0-4137		-
15	164.01	6.3547	-0.1602	0.1470	-0.2825	0.4145		
	106.02		-C-0871		<u>-0.2346</u>	0.9210		
	168.03		-0.6741		-0.3073	0.4205		
	172.07	0.1020	-0-0013	0 - 0 - 0 - 3 T	-0.3194 -0.3392	0.4550 0.4550		
	174.08	C-1625	_0.0363	0.0615		0.4039		
	176.10	0.0637	-9.0244	0.0278	-0.3825	0.4363		
19	177.11	0.0504	-0.0192	0.0285	-0.3512	0.4075		
				•				
			<del></del>					
				•	•			•
								<del></del>
					<del></del>		,,	
				<del></del>				· · · · · · · · · · · · · · · · · · ·
		<del></del>		-			· · · · · · · · · · · · · · · · · · ·	
			-					

PAGE	ENGINEE 1 OF 1		LOPHENI C	ENTERLAEDC	MA	ITIN MISSIL	E TAIL EFFE		AERODYNAMIC MIND TUNNEL (41)	
				<u>-</u>			THE STATE STATE			
<u> </u>		<del> </del>						<u>-</u>		
				CONF. LHANS						
	5	250 0.25	2.5	F36 FR	ΕE					
	ALPHA	CNF	Cm	Cr		YCPF				.3
	177.97			0.005	-0-37-10		<del></del>	<u>. i i</u>		•
2	179.04		-0.0045	<u> 0.0054</u>		0.3710			•	
4	161.04	0.0050	-0-0014	0.0011	-0.2578	0.2026				
5	102.05		0.4625_	-0-0430	-0-5364	0.6279			<del> </del>	
6		-0.0173		-0.0068		0.3915				
		-0.0536		-0.0119		0.4185				
9				-0.0-01				<del> </del>		
						-		<del></del>		
						•				
							<del></del>			-
_				<del></del>						
				·					· · · · · · · · · · · · · · · · · · ·	
		<del></del>			•		·	<del></del>		
									······································	
						_				
		-		-						
				<del></del>						
					<b></b> .		<del> </del>			
								•		
			-					<del></del>		
						,				
	<del></del>				···-		<del></del>			

ĜΕ	1 OF 1		<u></u>	ENTEHIALD	C) PHOPI	-TIN MISSI	LE TAIL EFFECTS DATA	AERODYNAMIC WIND TUNNEL (AT)
						·· · · · · · · · · · · · · · · · · · ·		<del></del>
	1E\$1 2	<u> </u>			5 <u>1710n</u> Pee			
DINT	AL PHA	CNF	Cr	C-1		YCPF		
2	-2.03		-0.0005	-0-6144	0.1005	0.545B 0.7138	·	
_3	0.02	-0-0005	-G.O.OA	-0.0025_	0.8667	2.7667		
•	1.05		-0.0011	0.0051	-0.0986	0.1972		
5	- 3.05		-0.0014	0.0136	-0.0416	0.4153		<del></del>
7	9.00	0-0-77	-0-0019	0.0207	-0-0194	0.4338		
8	6.07		-0.00+4		-0.0496	0.4308		
<u>9</u> 10	19.10		-0.0064 -0.0080		-0.0467 -0.0437	0.3692		
<u>ii                                    </u>	12.13		-0-0106		-0-0441	0.3567		
12	14.15		-0.0131		-0.0434	0.3380		
13 14	19.17		-0.0150 -0.0161		-0.0434	0.3174		
15	20.22		-0.0199		-0-0396	0-3144		
16	22.25		-0.0212		-0.0372	0.3131		
17	20.30		-0 <u>-022</u> -0.3231	0891	-0.0332	0.3130		······································
19	27.32		-0.0229		-0.0314	0.3097		
					· · · · · · · · · · · · · · · · · · ·	<del></del>	· · · · · · · · · · · · · · · · · · ·	
							<del></del>	
		•						
				<del> </del>				
		=	•	<del></del>		<del></del>		
								· · · · · · · · · · · · · · · · · · ·

				<del></del>	.,	SPLII	ILE TAIL EFFECTS DATA TER PLATE DATA
-		EAPT MAG 231 G.Vb	+ F¥10-6.1	ONE_IRAS	SITION		•
Olnt	ALPHA	CNF	Ch	C ²		YCPF	
1	28.16		-0-0245		-0.u334	0.3136	
2	29.24	0.7771	-0.0253	0.2420	-0.0326	G.3125	
_3	30.25			0.2501	-0-0315	0.3093	<u> </u>
•	31.27		-0.0253	0.2543	-0.0302	0.3076	
-5	33.26	0.6/03	-0.0251 -0.0237	U-2068 C-2736	-0-0259 -0-0264	0.3065	
7	34.29	0.9224	-0-0211	0.2-00	-0.0229	0.3036	
8	36.32	0.9572	-0.0120	9.2538	-0.0126	0.2965	
9	38.34	0.9587	0.0033	0.2770	6.0035	0.2889	
10	40.36	0.9065	0.0119	0.2/59	0.0123	0.2065	
<del>11</del>	92.38	0.9010	0.0146	0_2618	0-01-9	0.2473	<del></del>
13	•4.35	0.9963	0.0147	1042-0	0.0147 2.0136	0.2906	
14	48.40	1.6284	0-0126	0.3050	0.0122	0.2966	······································
15	50.34	1-0224	-0.0096		-0-0094	0.3108	
16	52.39	1.0345	-0.0141		-0.0136	0.3117	,
.17	50001	1.0560_			-0-017B	0.3161	
18	56.43	1.0950			-0.0200	0.3193	
19	57.00	1.LOGA	-0.0231	C_3593.	-0×05n8	0.3195	<del></del>
							•
					·		······································
_							
							•
				· ·		· <del></del>	
			•		-		•

	OF I		<u>ELOPMENT</u>		MA	RTIN MISSIL	TAIL EFFECTS DATA	1) AERODYNAMIC WINE	TUNNEL (AT)
	OF_1	· <del></del>	<del></del>		·	SPLITIE	R PLATE DATA		
				<del> </del>	_				
	TEST	PART PA	CH RX10-6	CUNE TRA	MITION			•	
	5	234 0.5			REE				
LT.	ALPHA	CNF	CH	С÷	L COF	YCPF			
	59.24		-0.0238		-0.0216				
	54.30		-0.0250	0.3555	-0.0226	0-3220			
	60.29			U-3590	-0.6234	0.3234			
	61.31		-0.0271		E450.0-	0.3250			
	62.31 63.31		-0-0244		-0-0254 -0-0263	0.3247 0.3255			•
	64.30		-0.0107		-0.0273	0.3261			
	66.31	1-1310	-0.0324	6.3705	-0.0291	0.3274	•		
	69.31		<u>-0.v351</u>		-0-0309				
	70.33		-0.036A		-0-0355	0.3302			
	72.33		-0.0394		-0-0359	0.3317			
	76.33		-0.3444		-0-0375	0.3352			
	78.34	1.1552	-0-0-66	0.3095	-0.0403	0.3372			
	80.34	1.1539	-0-0484	0.3911	-0.0420	0.3392			
	82.35		-0.0515		-0.0448	0.3406			
		1.1606	-0-4559	0-3760	-0-0481	_0.3411		~~	
	85.36		5000.0-		-0.0515 -0.0539	0.3430			
	.07.33			W 2 3 11 3 11	-040334	UA3633			
				•					
				<del></del>					<del> </del>
								•	
						<del>-</del>			<del> </del>
				•					•
	<del></del>								
								•	
									<del></del>

TEST PAPI MACH PAID = CONF TRANSITION   2 235 0.00 2.5	it.	1 OF	1	LUPEEHI !	<u>Centep (alu</u>		ULSION WIND TUNNEL FACILITY (PMT) RTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC_WIND_TUMNEL_(41)
2 235 0.00 2.5 F36 FREE  OINT ALPHA CN6 CH CH CH ACPF VCPF  1	LR.I	1 07	<u> </u>			. <del> </del>	SPLITTEN PLATE DATA	
2 235 0.wa 2.5 F36 FREE  OINT ALPMA CNF CH C4 ACPF VCPF  1 48.16 1.1.31 -C.1056 0.3416 -0.0518 0.1450 2 69.15 1.1.35 -C.1050 0.3433 -0.0549 0.3463 3 90.16 1.1.37 -0.4977 0.3499 -0.0515 0.3483 4 91.21 1.1305 -0.0123 0.3400 -0.0640 0.3486 5 92.21 1.1196 -0.0123 0.3410 -0.0640 0.3486 6 93.21 1.1104 -0.0156 0.3412 -0.0656 0.3498 7 94.21 1.1104 -0.0156 0.3412 -0.0576 0.3598 9 94.19 1.0726 -C.0075 0.3884 -0.0630 0.3567 9 94.19 1.0726 -C.0075 0.3884 -0.0908 0.3569 10 100.20 1.0416 -0.0525 0.3472 -0.0855 0.3580 11 102.20 1.0438 -0.0476 0.3413 -0.0900 0.3618 12 104.14 1.0606 -0.1630 0.3598 -0.0954 0.3609 13 106.19 1.0644 -0.1671 0.3413 -0.0900 0.3618 14 104.20 1.0627 -0.1137 0.3582 -0.1752 0.3661 15 110.20 1.0627 -0.1110 0.3402 -0.1752 0.3661 16 112.20 1.0627 -0.1110 0.3402 -0.1752 0.3668 17 114.21 1.0613 -0.1217 0.3402 -0.1135 0.3668 18 116.21 1.0765 -0.1100 0.3401 -0.1207 0.3679		-	<u>-</u>				•	
POINT ALPMA CM								
1 \$P_016	•	S	235 0.40	2.5	F36 F	REE		
2 b9.15 1.135	TAIO	ALPHA	CNF	CH	C+	ACPF	YCPF	
3 901E 1-137 -0.0797 0.3449 -0.055 0.3483  4 91.21 1.1305 -0.0723 0.3440 +0.0640 0.3486  5 92.21 1.119E -0.0737 0.3714 -0.0660 0.3486  6 93.21 1.110E -0.0756 0.3712 -0.0676 0.3498  7 98.21 1.110E -0.0764 0.3712 -0.0676 0.3507  8 96.20 1.0709 -0.0764 0.3709 0.3507  8 96.20 1.0709 -0.0765 0.3709 -0.0754 0.3534  9 98.19 1.0726 -0.0755 0.3000 -0.0908 0.3569  10 100.20 1.071E -0.0725 0.3772 -0.0855 0.3580  11 102.20 1.000 -0.0530 0.3598 -0.0954 0.3618  12 104.19 1.0006 -0.1630 0.3598 -0.0954 0.3609  13 106.19 1.0000 -0.1630 0.3598 -0.0954 0.3609  14 104.20 1.0727 -0.1139 0.373 -0.0908 0.3633  15 110.20 1.0657 -0.1170 0.3702 -0.1152 0.3633  16 112.20 1.0723 -0.1217 0.3712 -0.1153 0.3668  17 114.21 1.0765 -0.1300 0.3701 -0.1173 0.3658  18 116.21 1.0765 -0.1300 0.3701 -0.1173 0.3658	1							
4 91.21 1.1305 -0.0723 0.3940 -0.0640 0.3486 5 92.21 1.1196 -0.0739 0.3914 -0.0660 0.3496 6 93.21 1.1196 -0.0756 0.3912 -0.0576 0.3498 7 94.21 1.1094 -0.0764 5.3883 -0.0630 0.3507 8 96.20 1.0749 -0.0027 0.3869 -0.0754 0.3534 9 98.19 1.0726 -0.075 0.3864 -0.0908 0.3569 10 100.20 1.0916 -0.0525 0.3872 -0.0855 0.3588 11 102.20 1.0816 -0.0525 0.3873 -0.0900 0.3618 12 104.19 1.0864 -0.1671 0.3913 -0.0900 0.3618 13 106.19 1.0844 -0.1671 0.3598 -0.0954 0.3634 14 108.20 1.0727 -0.1139 0.3734 -0.1752 0.3633 15 110.20 1.0657 -0.1170 0.3734 -0.1752 0.3661 16 112.20 1.0723 -0.1217 0.3712 -0.1135 0.3648 17 114.21 1.0765 -0.1277 0.3712 -0.1137 0.3658 18 116.21 1.0765 -0.1300 0.3791 -0.1207 0.3679	2							
5								
6	5							<u> </u>
7 99.21 1.1.71 =0.0764 5.3nH3 =0.0630 0.3507 8 96.20 1.0747 =0.0020 0.3569 =0.0754 0.3534 9 98.19 1.0726 =0.0075 0.3n64 =0.0908 0.3569 10 100.20 1.0016 =0.0025 0.3H72 =0.0855 0.3580 11 102.20 1.0036 =0.0476 0.3913 =0.0900 0.3618 12 104.19 1.0006 =0.1030 0.3598 =0.0954 0.3609 13 106.19 1.0044 =0.1071 2.3669 =0.1066 0.3634 14 100.20 1.0027 =0.1137 0.3934 =0.1952 0.3633 15 110.20 1.0057 =0.1170 0.3932 =0.1957 0.3661 16 112.20 1.0723 =0.1217 0.3912 =0.1135 0.3668 17 114.21 1.0765 =0.1257 (.3521 =0.1173 0.3658 18 116.21 1.0765 =0.1300 0.3961 =0.1207 0.3679	6							
9 98-19 1-0-26 -0-2075 0-3064 -0-0008 0-3569  10 100-20 1-0-16 -0-0-25 0-3+72 -0-0455 0-3560  11 102-20 1-0-32 -0-0-175 0-3413 -0-0900 0-3610  12 104-14 1-0-0-0 -0-1630 0-3598 -0-0954 0-3699  13 106-19 1-0-64 -0-1671 0-3569 -0-1006 0-3634  14 104-20 1-0-25 -0-1170 0-3402 -0-1952 0-3633  15 110-20 1-0-57 -0-1170 0-3402 -0-1957 0-3661  16 112-20 1-0-57 -0-127 0-3412 -0-1135 0-3668  17 114-21 1-0-1257 0-3412 -0-1173 0-3658  18 116-21 1-0765 -0-1300 0-3401 -0-1207 0-3679	. 7	94.21	1,1471	-0-0764	6.3nH3	-0.0570	0.3507	
10 100.20 1.0416 -0.0525 0.3872 -0.0855 0.3580  11 102.20 1.0636 -0.0476 0.3513 -0.0900 0.3618  12 104.14 1.0600 -0.1630 0.3598 -0.0954 0.3609  13 106.14 1.0644 -0.1671 0.3598 -0.1052 0.3634  14 104.20 1.0657 -0.1136 0.3434 -0.1752 0.3633  15 110.20 1.0657 -0.1170 0.3402 -0.1097 0.3661  16 112.20 1.0723 -0.1217 0.3412 -0.1135 0.3648  17 114.21 1.0716 -0.1257 0.3921 -0.1173 0.3658  18 116.21 1.0765 -0.1300 0.3461 -0.1207 0.3679	é							
11 107-70 1-403e -0-476 0-3913 -0-0900 0-3610  12 104-19 1-0e66 -0-1630 0-3598 -0-0954 0-3609  13 106-19 1-0e64 -0-1671 0-3569 -4-1006 0-3638  14 104-20 1-4057 -0-1139 0-3934 -0-1752 0-3633  15 110-20 1-4657 -0-1170 0-3902 -0-1097 0-3661  16 112-20 1-4723 -0-1217 0-3912 -0-1135 0-3648  17 114-21 1-4714 -0-1257 6-3521 -0-1173 0-3658  18 116-21 1-4765 -0-1300 0-3961 -0-1207 0-3679	-9-							
12 104.19 1.0e0c -0.1030 0.3698 -0.0954 0.3609 13 106.19 1.0e6c -0.1071 2.3669 -0.1066 0.3638 14 104.20 1.0e29 -0.1139 0.3934 -0.1752 0.3633 15 110.20 1.0e57 -0.1170 0.3902 -0.1097 0.3661 16 112.20 1.0723 -0.1217 0.3912 -0.1135 0.3668 17 114.21 1.0715 -0.1257 (.3921 -0.1173 0.3658 18 116.21 1.0765 -0.1300 0.3961 -0.1207 0.3679	-							
13 106.19 1.00aa -0.1071								
15 110.20 1.0657 -0.1170 0.3×02 -0.1097 0.3661 16 112.20 1.0723 -0.1217 0.3×12 -0.1135 0.3648 17 114.21 1.071+ -0.1257 0.3521 -0.1173 0.3658 18 116.21 1.0765 -0.1300 0.3×61 -0.1207 0.3679								
16 112.20 1.0723 -0.1217 0.3v12 -0.1135 0.3648 17 110.21 1.071± -0.1257 0.3921 -0.1173 0.3658 18 116.21 1.0765 -0.1300 0.3v61 -0.1207 0.3e79								
17 114.21 1.471F =0.1257								
18 116.21 1.0765 -0.1300 0.3961 -0.1207 0.3679								
								· · · · · · · · · · · · · · · · · · ·
							•	
							<del> </del>	
								•
					<del></del>		· · · · · · · · · · · · · · · · · · ·	
		<del> </del>				· · · · · · · · · · · · · · · · · · ·		<u></u>
	<del></del>		<del> </del>					

OINT 2	TEST 2	PARL MAC 236 0.58					LER. PLAIL MAIA	
2						•	•	
2			H HELO-4	COME TRAN	SITION			
2		E30 0.70			REE .			
2	ALPHA	CNF	CH	C ₇	*CPF	YCPF		
	116.03		-G-1280	11-3/14	-0.1276	0-3703	•	
3	114.71		-0.1294	0.3/03	-0.1742	0.3698	•	· · · · · · · · · · · · · · · · · · ·
			-0.1310		-0-1306			
	121.06 122.07		-0.1330 -0.13-3		-0.1325 -0.1342	0.3690		
	123.05		-0.1304		-0.1358	0.3698	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
	124-07		-0.1377		-0-1379	0.3696		
. 6	124.00	1.0039	-0.1-11	0.3725	-0-1-05	0.3711		•
	128.97		-0.1439		-0.1439	0.3689		
	130.07		-0.1455		-0.1473	0.3691		
	132-01		-0.1467 -0.1468		-0.1510 -0.1552	0.3692		
	130.07 136.07		-2-1515			0.3685		
	130.97		-9.1547		-0.1650	0.3722		** - Turner   1
	140.07					0.3816		
	142.06		-0.1763		-0.1999	0.3881		
			-0-1446		-0-2003	0.3950		
	146.67		-G.1+30		-0.2042	0.3961		
19	19(3)(	N.O.L.C.	- PHAIDUD		-0.2070	U_3482		
								·
							•	
					<del></del>			<del></del>
							<del></del>	<del></del>
						•		
							•	
	•							
					<u></u>			
							<del></del>	<del> </del>

IFSI_PART_WALH RAID=6 CUMF THANSITION	E	ENGINEE 1 OF 1 1 OF -1		LOPMENT C	ENTERIAED		PTI+ MISSILE	TUNNEL FACILITY TAIL EFFECTS OF PLATE DATA		AERODYNAMIC #IND T	IMMEL (47)
2 237 6.50 2.5				· · · · · · · · · · · · · · · · · · ·						······································	
DINT ALPHA CMF CH CH CH CH CH CH CH LAND CMF CMF CMF CMF CMF CMF CMF CMF CMF CMF		iest	PART MAC	H RX10-6	CUNF THAN	SITION					
1 + 7.49		5	237 6.90	2.5	36 F	REE					
144.96   0.807/2   -0.1032   0.3376   -0.2162   0.3965     149.96   0.8178   -0.1789   0.365   -0.2163   0.4022     150.96   0.7725   -0.1060   0.305   -0.2155   0.3992     5.   151.97   0.7225   -7.81822   0.2256   -0.2267   0.3981     6.   157.96   0.725   -7.81822   0.2256   -0.2267   0.4032     7.   153.96   0.8056   -0.1597   0.2618   -0.2267   0.4032     8.   155.97   0.6069   -0.1597   0.2613   -0.2298   0.4013     9.   157.98   0.5072   -0.1105   0.2262   -0.2478   0.3984     16.   16.00   0.4057   -0.1139   0.1177   -0.2675   0.4054     1   16.00   0.4057   -0.1139   0.1177   -0.2675   0.4054     1   16.00   0.3032   -0.1007   0.1077   -0.2753   0.4061     1   16.00   0.3032   -0.1007   0.1077   -0.3013   0.4075     1   16.00   0.2082   -0.1007   0.0077   -0.3013   0.4075     1   16.00   0.2082   -0.0073   0.0077   -0.3013   0.4075     1   17.00   0.116   -0.0603   0.0075   0.3394   0.4065     1   17.07   0.116   -0.0603   0.0075   0.3395   0.3395     1   17.17   0.0075   0.0075   0.0087   -0.3305   0.3056     1   17.17   0.0075   0.0075   0.0087   -0.3305   0.3056     1   17.17   0.0075   0.0075   0.0087   -0.3305   0.3062     1   17.17   0.0075   0.0075   0.0087   -0.3515   0.3661     1   17.17   0.0075   0.0075   0.0087   -0.3515   0.3661     1   17.17   0.0075   0.0075   0.0087   -0.3515   0.3661     1   17.17   0.0075   0.0075   0.0087   -0.3515   0.3661     1   17.17   0.0075   0.0075   0.0075   0.0075   0.3661     1   17.17   0.0075   0.0075   0.0075   0.0075   0.3661     1   17.17   0.0075   0.0075   0.0075   0.0075   0.3661     1   17.17   0.0075   0.0075   0.0075   0.0075   0.3661     1   17.17   0.0075   0.0075   0.0075   0.0075   0.3661     1   1   1   1   1   1   1   1   1					Cn	ACPF	VCPF	<del></del>			<del></del>
3 149.95 (a.8176 -0.1789 6.3269 =0.2188 0.4022  1 150.96 (a.7729 -0.1666 0.30.95 -0.2155 0.3992  5 151.97 (a.725 -0.1661 0.2456 -0.2187 0.3381  6 157.96 (a.7237 -0.1661 0.2418 -0.2287 0.4032  7 153.36 (a.8256 -0.1575 0.2287 -0.2383 0.4653  8 155.97 (a.6291 -0.1505 0.227 -0.2392 0.4018  9 157.48 (a.9572 -0.1655 0.2227 -0.2392 0.4018  10 160.00 0.445 -0.1274 0.2.15 -0.2576 0.4075  11 162.91 (a.4257 -0.1139 0.1777 -0.2675 0.4058  12 164.02 (a.3022 -0.1007 0.1475 -0.2773 0.4061  14 164.02 (a.3022 -0.1007 0.1233 -0.2881 0.4075  15 170.05 0.1716 -0.0803 0.0767 -0.3118 0.4075  15 170.05 0.1716 -0.0803 0.0767 -0.3184 0.4006  17 174.09 0.1117 -0.0350 0.0387 -0.3852 0.3863  18 176.11 0.0005 -0.0234 -0.0075 0.0265 -0.3803 0.3866  19 177.11 0.0005 -0.0234 -0.0017 0.0015 -0.3866								<del></del>			
150.96   0.7729   -0.1666   0.30.65   -0.2155   0.3962											
5 151.97 0.725 -0.1224 0.2956 -0.2187 0.3981 6 152.96 0.7c37 -0.1001 0.2918 -0.2267 0.4032 7 152.96 0.0250 -0.1597 0.2763 -0.2298 0.4633 8 155.97 0.0c91 -0.1595 0.2250 -0.2292 0.4018 9 157.98 0.0072 -0.1055 0.2250 -0.2292 0.4018 10 100.00 0.495 -0.1274 0.2255 0.2275 0.4058 11 100.00 0.495 -0.1274 0.2215 -0.2275 0.4058 12 104.01 0.3257 -0.1199 0.1727 -0.2773 0.4061 13 104.02 0.3322 -0.1007 0.1475 -0.2773 0.4061 14 104.02 0.3022 -0.1007 0.1475 -0.2773 0.4061 15 106.04 0.246 -0.073 0.0977 -0.3013 0.4075 15 170.05 0.1918 -0.0603 0.0767 -0.3314 0.4006 16 172.07 0.146 -0.475 0.0599 -0.3305 0.3954 17 174.09 0.1114 -0.0350 0.0367 -0.3442 0.3803 18 176.11 0.005 -0.0236 0.0245 -0.3353 0.3802 19 177.11 0.0033 -0.0182 0.0182 0.0184 -0.33613 0.3861								<del></del>			
7 153.96 0.0250 -0.1595 0.226 -0.2398 0.4633 8 155.97 0.6291 -0.1595 7.227 -0.2392 0.4618 9 157.98 0.5572 -0.1405 0.2227 -0.2392 0.4618 9 157.98 0.5572 -0.1405 0.2220 -0.2278 0.3984 10 100.00 0.445 -0.1274 0.215 -0.2575 0.4051 1.52.01 0.4257 -0.1139 0.1727 -0.2675 0.4058 12 164.01 0.3022 -0.1007 0.1475 -0.2773 0.4061 1.166.02 0.3022 -0.1007 0.1475 -0.2773 0.4061 1.166.02 0.3024 -0.0071 0.1233 -0.22881 0.4075 14 166.02 0.3024 -0.0071 0.1233 -0.22881 0.4075 15 170.05 0.1146 -0.0603 0.0767 -0.3163 0.4076 15 170.05 0.1146 -0.0675 0.5599 -0.3305 0.3054 17 174.09 0.1146 -0.0350 0.0367 -0.3363 16 176.11 0.4045 -0.0234 0.0367 -0.3363 17 174.09 0.1146 -0.0235 0.0364 -0.3462 0.3803 19 177.11 0.003 -0.0234 0.0245 -0.3630 0.3802 19 177.11 0.003 -0.0182 0.6194 -0.3615 0.3861	5	151.97	0.7425	-0.1t24	0.2456	-0.2187					
8 155,97 0,0c91 -0.1505 0,c227 -0.2392 0.010 9 157.98 0,5572 -0.105 0.3985 0.3985 0.4075 0.576 0.277 0.2778 0.3985 0.4075 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.675 0.67											
9 157.98 0.5672 -C.1605 0.2260 -0.2478 0.3986 10 100.00 0.0005 -0.1274 0.2115 -0.2576 0.075 11 102.01 0.4257 -0.1139 0.1727 -0.2675 0.4054 12 100.01 0.3032 -0.1007 0.1075 -0.2773 0.4061 14 166.02 0.3032 -0.0071 0.1233 -0.2881 0.4075 14 100.00 0.2006 -0.0737 0.0077 -0.3013 0.4076 15 170.05 0.1916 -0.0003 0.0767 -0.3188 0.4066 16 172.07 0.1036 -0.0075 0.0509 -0.3305 0.3956 17 170.09 0.1116 -0.0350 0.0387 -0.3402 0.3803 18 176.11 0.0005 -0.0234 0.0245 -0.3630 0.3602 19 177.11 0.0003 -0.0187 0.0194 -0.3615 0.3661								<del>- ,</del>			
10 100.00 0.0765 -0.1276 0.2015 -0.2576 0.0075 11 102.01 0.4257 -0.1139 0.1727 -0.2675 0.058 12 100.01 0.3032 -0.1007 0.1075 -0.2773 0.0061 14 100.02 0.3022 -0.0071 0.1233 -0.2881 0.4075 14 100.00 0.2006 -0.0737 0.0077 -0.3013 0.0076 15 177.05 0.1716 -0.0003 0.0767 -0.3106 0.0066 10 172.07 0.1036 -0.0475 0.0509 -0.3305 0.3056 17 174.09 0.1111 -0.0350 0.0285 -0.3682 0.3803 19 177.11 0.005 -0.0230 0.0225 -0.3601 0.3661											
11 162-01 0.4257 -0.1139 0.1727 -0.2675 0.4051 12 100-01 0.3032 -0.1007 0.1075 -0.2773 0.4061 13 160-02 0.3022 -0.0871 0.1233 -0.2881 0.4075 14 160-00 0.2006 -0.0737 0.0077 -0.3013 0.4076 15 172-05 0.1176 -0.0603 0.0767 -0.3136 0.4006 16 172-07 0.1036 -0.0475 0.0509 -0.3305 0.3054 17 172-09 0.1116 -0.0350 0.0387 -0.3462 0.3803 18 176-11 0.0005 -0.0230 0.0245 -0.3630 0.3802 19 177-11 0.0003 -0.0182 0.0182 -0.3155 0.3661								······································		***************************************	
14 166.02 0.3024 -0.0071 0.1233 -0.2881 0.4075 14 108.04 0.2446 -0.073 0.0777 -0.3013 0.4076 15 170.05 0.1916 -0.0063 0.0767 -0.3146 0.4006 16 172.07 0.1436 -0.0475 0.0569 -0.3305 0.3054 17 174.09 0.1018 -0.0350 0.0187 -0.3442 0.3803 18 176.11 0.0045 -0.0234 0.0245 -0.3030 0.3802 19 177.11 0.0033 -0.0182 0.0194 -0.3661											
1											
15 170.05 0.1916 -0.0603 0.0767 -0.3146 0.4006 16 172.07 0.1436 -0.0475 0.0569 -0.3305 0.3954 17 174.09 0.1016 -0.0350 0.0387 -0.3442 0.3803 18 176.11 0.0645 -0.0234 0.0245 -0.3630 0.3802 19 177.11 0.0003 -0.0182 0.0194 -0.3615 0.3661										<del></del>	
10 172.07 C.1+36 -0.0475 G.0569 -0.3305 0.3956 17 174.09 0.1016 -0.0350 0.0387 -0.3462 0.3803 18 176.11 0.045 -0.0234 0.0245 -0.3638 0.3802 19 177.11 0.0003 -0.0182 0.0194 -0.3615 0.3661											
17 174.09 0.1L1t -0.0350 0.0387 -0.3642 0.3803 16 176.11 0.0645 -0.0234 0.0245 -0.3630 0.3802 19 177.11 0.0003 -0.0182 0.0194 -0.3615 0.3661											<del></del>
19 177-11 0-0-0182 0-0184 -0-3615 0-3661											
											•
	9	177.11	0.0203	-0-0162	0.0154	-0.3615	0-3661				
										•	
	_										
			<del></del>	<del></del>	<del></del>		<del></del>	<del></del>			
								-		· · · · · · · · · · · · · · · · · · ·	
			<del></del>						<del></del>		
					· · · · · · · · · · · · · · · · · · ·						

3E	ENGINE: 1 OF 1		LOPMENT C	ENTEH (AED)		PT1 - =1551	D_IUNNEL.FACILITY1PHT1 LE TAIL EFFECTS DATA ER_PLATE_DATA	AERODYNAMIC HIND TUNNEL (AT)
				4				
	. JEST	L PAPT PAC	H_RX16-6_	CONF_ 1PAN	SIT104			
	2	240 1.10			MEE			
DINT	ALPHA	CNF	СН	C+	xCPF	YCPF		
1	Z_04.			-0.6152		0.5764		
2	-0.46	-0.0166	0.6601	-0.0112		0.7021		
3	<u>9.93</u> 1.06	-0.0054 0.0106	-0.0002 -0.0015	-0.0049 -0.0006		-0.0577		
5	2.05	0.0225	-0-0014		-0-1-55	0-2747		
6	3.06	0.0344	-0.4025	0.0124	-e.0720	0.3587		
7_	9.06	0-0493	-0-0035	1.01.01	-0-0703	0-3862		
5	6.08	U. 005e	-U.VU5#	0.0359 : 0:15		0.4150		
10	19.12	<u></u>	_ <del>0_005</del> 5_	<u>160-15-</u> 0.0608		0.3948		
10 11	12.12				-0-0543	0.3572		
<u> </u>	14.14		-0.G173	U. 0986	-0.0589	0.3367		
13	10-14			0.1155		0.3257		
14	18.21		-0.0214		-9.0524	0.3219		
15	20.24		-0 <u>-0215</u>			0.3164		
17.	24.29		-0.u232		-0-0461	0.3179		
18	26.33	0-6174	-0-0316	0.2143	-0.0457	0.3165	•	
19	27.35	C. TONA	22دىم0-	0.2240	-0-0454	0.3160		
				<b>.</b>				
		·····			<del></del>			
								·
								•
								<del></del>
					,	_		
					<del> </del>	··	• • • • • • • • • • • • • • • • • • • •	<del></del>
						1		

	1 OF 1				MAI	TIN MISSI	O TUMMEL FACILITY (PMT) LE TAIL EFFECTS DATA ER PLATE DATA	
	TEST	PART MAC	H PE10-6	CONE_TRAS	S1110N	· · <del>- ·</del> · · · · · · · · · · · · · · · · · ·		
_	5	241 1.10			REE			
OINT		CNF	Сн	C9		YCPF		
5	26.25		-0.0330 -0.0340		-0.0441	0.3153		<del></del>
	30.25		-0-U349		-0-0+35	0.3141		
	31.27		-0.0360		-0.0431	0.3141		
	32.29 33.29	0.8703	-0.0372 14c0.0-	0-2721	-0.0427 -0.0423	0.3126 0.3142	· · · · · · · · · · · · · · · · · · ·	
	34.31		-0-0391			0.3146		
В	36.33		-0.0-10		-0.0411	0.3160		
9	_36_35_		<u>-0.041</u> 8.		-0.0345			
G 1	40.38		-0.0331 -0.0214		-0.0303 -0.0194	0.3135		•
2	44.42		-0.6115		-0.0103	0.3068		
13		1.1253	-0-0020	5.3416	-0-0619	0.3036	·	
1.	48.46		-0.0026		-0.0023	0.3054		
15	50.47 52.49		-0.0041 -0.0047	0.3592	-0-0036 -0-0040	0.3096		
17		1.2216	-G_0167	0.3071	-0-6137	A-3169		
10	56.52	1.2395	-0.0241	U.3984	-0.0194	0.3217		
19	57.52		-0-4271	0.4036	-0.0217	n.3232	· <del>····································</del>	<del></del>
					•			
				<u> </u>	· · · · · · · · · · · · · · · · · · ·			
							<del></del>	
		-						•
			<del></del>	<del></del>				
					···· · <del>-</del> · · · · · · · · · · · · · · · · · · ·			
			· · · · · · · · · · · · · · · · · · ·			-		

i E	1 OF	1			MAI	ULSION BIND TUNNEL FACILITY(PMI) PTIM MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYMAMIC AIND TUNNEL (67
	tes	14 TARA 11			SITION		
PO1NT	ALONA	CNF	Сн	CH	xCPF	YCPF	
	56.29				-0.0210	0.3226	
2	54.30				-0.6724	0.3229	
3	6.30				-0.0236	0.3236	
•	61.37				-0.0247	0.3256	
	<u>62.36</u> 63.36				-0-0258 -0-0270	0.3250	
6	03.30				-0-0270	0.3260	
-	64.39				-0.0298	0.3296	<del></del>
9	65.39				-0-0324	0.3303	
10	70.46				-0.0345	0.3317	
ii_	72.4	1.3431	-0-0-75	0.0336	-0-0364	0.3326	
15	74.40		-0.0496	0.4368	-0.0382	0.3345	
.13	76.61		-C-4523		-0-03-9	0.1351	
1.	74.4		-0.3544		-0.0416	0.3372	
_15	80.4		-0-0576		-0-D-34	0.3362	<del></del>
16	82.4		-0.0503		-0.0456	0.3398	
_17 18	B4.44		-0.0661		-0-0+77 -0-0509	0.3426	
19		1.3911			-0-0524	_0.3427	
			- 11 4 1 1 1 1		-11211.75		•
		<del></del>					
						· · · · · · · · · · · · · · · · · · ·	<u> </u>
							•
		<del></del>					· · · · · · · · · · · · · · · · · · ·

TEST PART PACH PAID = 6 CUNF TRANSITION   2 243 1-10 2-5 F36 FREE		ENGINEE 1 OF I		LOPMENT C	ENTERLAED	C) <u>PROF</u>	<u>PULSION WIN</u>	D TUNNEL FACIL LE TAIL EFFECT	SIY(PET)	AERODYNAMIC_win	D TUNNEL (41)
2 243 1.10 2.5 F36 FREE  INT ALPMA CNF Cn Cv KCPF YCPF					<del></del>						
2 243 1-10 2-5 F36 FREE  INT ALPMA CMF Cn CH KCPF YCPF - 8t-23 1.325: -0.0709 0.6535 -0.0535 0.3621  5 8v-22 1.325: -0.0709 0.6535 -0.0532 0.3432  6 90-25 1.3173 -0.0773 0.6535 -0.0588 0.3452  8 90-25 1.3173 -0.0773 0.6535 -0.0588 0.3452  8 90-26 1.3065 -0.0701 0.6535 -0.0588 0.3456  9 90-26 1.3074 -0.0010 0.6536 -0.0023 0.3470  1 96-26 1.3001 -0.0633 0.6546 -0.0630 0.3466  1 96-26 1.2001 -0.0017 0.6501 -0.0077 0.3408  2 98-26 1.2721 -0.0752 0.6573 -0.00710 0.3519  3 100-25 1.2731 -0.0069 0.6073 0.3519  3 100-25 1.2731 -0.0069 0.6073 0.3516  5 104-25 1.2742 -0.1131 0.6590 -0.0735 0.3546  5 104-25 1.2742 -0.1131 0.6603 -0.0520 0.3558  6 106-26 1.2001 -0.1165 0.6630 -0.0019 0.3562  9 112-26 1.2002 -0.1205 0.6650 -0.0104 0.3662  9 112-26 1.2002 -0.1205 0.6651 -0.0104 0.3662  1 116-26 1.2746 -0.1306 0.6651 -0.0104 0.3664  1 116-26 1.2746 -0.1306 0.6651 -0.0104 0.3664  1 116-26 1.2746 -0.1306 0.6651 -0.0104 0.3664  1 116-26 1.2746 -0.1306 0.6651 -0.0104 0.3664  1 116-26 1.2746 -0.1306 0.6651 -0.0107 0.3634											
2 243 1.1u 2.5 F36 FREE  DINT ALPHA CWF Cm CH XCOF VCPF 4 84.23 1.325x -0.0709 0.0535 0.3621 5 89.22 1.325x -0.0730 0.4540 -0.0552 0.3432 6 90.25 1.3173 -0.0730 0.4540 -0.0552 0.3432 8 92.26 1.3325 -0.0730 0.4553 -0.0688 0.3452 8 92.26 1.3325 -0.0171 0.4530 -0.0623 0.3464 9 93.26 1.3325 -0.0014 0.4530 -0.0623 0.3470 10 99.26 1.3325 -0.0619 0.4554 -0.6742 0.3884 11 99.26 1.3221 -0.079 0.4591 0.6977 0.3498 12 98.26 1.2221 -0.0521 0.6977 0.4533 13 100.25 1.2231 -0.0049 0.4599 -0.0750 0.3533 14 107.27 1.2245 -0.1171 0.4599 0.60785 0.3544 15 106.25 1.2247 -0.1111 0.4599 0.60785 0.3558 16 107.27 1.2245 -0.1105 0.4503 -0.0052 0.3558 17 168.26 1.2891 -0.1185 0.4503 -0.0919 0.3592 18 112.26 1.2889 -0.1289 0.4091 0.4500 -0.0919 0.3592 19 112.26 1.2889 -0.1306 0.4650 -0.0110 0.3608 22 112.27 1.2245 -0.1306 0.4650 -0.0110 0.3608 22 112.28 1.2794 -0.1185 0.4553 -0.0101 0.3608 22 112.28 1.2794 -0.1185 0.4553 -0.0101 0.3608 22 117.28 1.2794 -0.1185 0.4553 -0.0101 0.3608 22 117.28 1.2794 -0.1185 0.4553 -0.0101 0.3608 22 117.28 1.2794 -0.1185 0.4559 -0.0117 0.3634		TEST	PART MAC	H 9215-6	CUMF TOAM	SITION					
8	-		243 1.10	2.5	F36 F	REE					
\$ 81.23	DINT	· AL PHA	CNF	Cn		x CPI	YCPF	<del></del>		<del></del>	
6 90.25 1.3173 -0.0750 0.4532 -0.0578 0.3448  7 91.26 1.3137 -0.0773 0.4535 -0.0588 0.3452  8 92.26 1.3045 -0.0711 0.4535 -0.0588 0.3464  9 93.26 1.3045 -0.0014 0.4536 -0.023 0.3470  10 90.26 1.3041 -0.0839 0.4544 -0.652 0.3486  11 96.26 1.2931 -0.0079 0.4541 -0.0677 0.3098  12 96.26 1.2931 -0.0079 0.4551 -0.0077 0.3498  13 100.25 1.2931 -0.0060 0.4550 -0.0750 0.3533  14 102.27 1.2944 -0.1017 0.4590 -0.0765 0.3533  15 100.25 1.2937 -0.0060 0.4503 -0.022 0.3564  15 100.26 1.2947 -0.1131 0.4514 -0.0273 0.3563  17 100.26 1.2947 -0.1131 0.4514 -0.0273 0.3563  18 10.26 1.2947 -0.1135 (0.4530 -0.0199 0.3592  19 112.26 1.2806 -0.1239 0.4615 -0.01014 0.3508  20 119.27 1.2248 -0.1306 0.4550 -0.1014 0.3508  21 116.26 1.2747 -0.1410 0.4553 -0.1014 0.3508  21 116.26 1.2747 -0.1410 0.4553 -0.1016 0.3508  22 117.26 1.2747 -0.1410 0.4559 -0.1128 0.3662		81-23	1.325E	-0-0709	0.4535	-0.0535	0.3421				
7 91.26 1.3137 -0.0773 0.4535 -0.0588 0.3452 8 92.26 1.33v5 -0.071 v.4533 -0.0804 0.3454 9 93.26 1.3v7a -0.usia v.4533 -0.0623 0.3470 10 94.26 1.3va -0.0433 v.4544 -0.6542 0.3884 11 94.26 1.2va -0.usia v.4544 -0.6542 0.3884 11 94.26 1.2va -0.usia v.4544 -0.0577 0.3484 11 94.26 1.2va -0.usia v.4544 -0.0571 0.3519 13 100.25 1.2va -0.usia v.4544 -0.0570 0.3533 14 102.27 1.2va -0.101 v.4503 -0.0750 0.3533 15 104.25 1.2va -0.101 v.4503 -0.0520 0.3558 16 104.25 1.2va -0.113  0.454 -0.073 0.3564 17 106.26 1.2va -0.113  0.451 -0.0573 0.3563 18 110.26 1.2va -0.113  0.451 -0.0573 0.3563 19 112.26 1.2va -0.1300 0.4050 -0.0104 0.3608 20 114.27 1.2va -0.1300 0.4050 -0.0104 0.3608 21 114.28 1.2va -0.1300 0.4050 -0.1107 0.3634 22 117.28 1.2va -0.146 0.4659 -0.1107 0.3634 22 117.28 1.2va -0.146 0.4659 -0.1128 0.3661	5										
8	7										
10	180	42.26	1.3085	-0-0141	V.4534	-0-0604	0.3464				<del></del>
11	-							•			
12 98.26 1.2721 -0.0721 0.55-7 -0.0712 0.3519 13 100.25 1.2931 -0.0769 0.4569 -0.0750 0.3533 14 107.27 1.2946 -0.1217 0.4569 -0.0765 0.3558 15 104.25 1.2937 -0.161 0.4603 40.0520 0.3558 16 106.26 1.2947 -0.1131 0.4514 -0.073 0.3563 17 168.26 1.2941 -0.1135 0.4514 -0.0919 0.3592 18 110.26 1.2969 -0.1306 0.4650 -0.0919 0.3602 19 112.26 1.2869 -0.1306 0.4650 -0.1014 0.3608 20 114.27 1.2038 -0.1362 0.4553 -0.1061 0.3624 21 116.26 1.2796 -0.1416 0.4651 -0.1107 0.3634 22 117.26 1.2796 -0.1416 0.4659 -0.1128 0.3663											
10 107.27 1.2vec -0.1017 0.4590 -0.0785 0.3546 15 104.25 1.2v37 -0.1061 0.4603 -0.0v20 0.3558 16 106.26 1.2v4c -0.1131 0.4512 -0.0073 0.3558 17 108.26 1.2v91 -0.1185 0.4630 -0.0v19 0.3592 18 110.26 1.2v90 -0.1239 0.4612 -0.0988 0.3602 19 112.26 1.2v90 -0.1306 0.4650 -0.1014 0.3608 20 114.27 1.2v3c -0.1302 0.4653 -0.1061 0.3624 21 116.26 1.2v9c -0.1416 0.4651 -0.1107 0.3634 22 117.26 1.2v9c -0.1460 0.4659 -0.1128 0.3661											
15											
16 106-26 1-299								<del></del>			
17											
19 112.26 1.200 -0.1306 0.4050 -0.1014 0.3608 20 114.27 1.203c -0.1302 0.4053 -0.1061 0.3624 21 116.26 1.2706 -0.1416 0.4651 -0.1107 0.3634 22 117.26 1.2706 -0.1444 0.4659 -0.1128 0.3641		168.26								_	
20 110-27 1-203t -0-1302 0-053 -0-1061 0-3624 21 116-26 1-2794 -0-140 0-051 -0-1107 0-3634 22 117-26 1-2796 -0-1400 0-0659 -0-1128 0-3601										<del></del>	<del></del>
71 116.26 1.2796 =0.1416 0.4659 =0.1128 0.3634 22 117.26 1.2796 =0.1444 0.4659 =0.1128 0.3641											
		116.26	1.279#	-0.1416	0.4651	-0-1107	0.3634				
	22	117.26	1,2746	-0-1666	0.4659	-0.112A	0.3641				
								_			
					<del></del>						
											•
							<del> </del>				. <del> </del>
										•	
											<del>-</del>
							_				
										····	
			<del> </del>	<del></del> -	· · · · ·			<del></del>	<del> </del>	<del></del>	

	1 OF 1	ING. LEVE	LOPMENT CI	NTEKLALU		ULSIUN WIND TUNMEL PTIM MISSILE TAIL ( SPLITTER PLATE	FFECTS DATA	AERODYNAMIC WIND TUNNEL (eT)
							-	
	<del></del>		<del></del>	-				
			M_PX10-6					
	2	244 1.16	2.5	F36 - F	MEE			
OINT	ALPHA	CNF	Сн	Ce		YCPF		
<u> </u>		1.2739	-2-1969		-0-1153			
	119.05		-0.1471 -0.1510		-0.1174 -0.1187	0.3673 0.3643		
	121.10		-0.1533		-0.1207	0.3645		
5			-0-1544		-0-1223	0.3648		
6	123.09		-6.1757		-0-1241	0.3653		
7	124.16		=0.1573		-0-1200	0.3659		
ь	126.16		-0.1606		-0-1300	0.3664		•
9	128-10		-0-1035		-0-1343	0-3677		
10 11	130.09		-0-1726		-0-1-72	0.3697		
12	134.06		-0.1799		-0.1562	0.3759		
<u> </u>	136.09		-0.1561		-0.1642	0.3795		
1.	138.08		-0.1000		-0.1680	0.3807		
15	140.00		-0-18-6		-0.1717	0.3810		
16	147.09		-0.1835		-0.1756	0.3821		
17	146.11				-0.1834	0.3662 0.3667		
18	147.10		-0-1756		-0.1918	0.3889	,	
					72.1.1.1.1			
			· · · · · · · · · · · · · · · · · · ·			······································		
	<del></del>				<del></del>			

RNOLD AGE MEET	ENGINE 1 OF 1 OF	PING DEVE	LOPMENT C	ENTERLAED	MA	RIIN MISSIL	LIUNNEL FACII E TAIL EFFECT R PLATE DATA	S. DATA	AERODYNAMIC WIND THRMEL (AT
	<del></del>				r) 91				
	IES	PART_MAL 245 1.10		CONF. TRAN F36 F	SITION HEE	· · · · · · · · · · · · · · · · · · ·			
POINT	ALPHA	CNF	Ch	C+	» Cof	. YCPF	<del> </del>	··	
1	197.89	0-6780	-0.1710	U-3+06	-0.1948	0.3879	<del></del>	·	
5	148.90		-0.1674		-0.1984	0.3885			
	150.98		-0.1646		-0.2021	-0-39 <u>00</u> -0-3912	· · · · · · · · · · · · · · · · · · ·		
	151.99	0.7484	-0-1000		-0.2092	0.3915			
6	152.98	0.7142	-0.1522		-0.2130	0.3932			
	153.98		-0.1389		-0.2171 -0.22+6	0.3929		<del></del>	
9	157.13		-0.1334		-0.2302	0.3924			
10	160.01		-0.1177		-0.2429	0.3958			
# _	162-02		-0-1060			0.4013			
12	154.03 156.05		-0.0943 -0.1822		-0.2637	0.3990			
19	168.05		-0.0702		-0.2872	0.3861		<del></del>	
15	170-07		-0-1562		-0-3664	0.3786		<u> </u>	······································
15	172.09		-0.0464		-0.3164	0.3747			
17	<u>174.11</u> 175.13		-0.0351		-0-3335 -0-3472	0.3562			
<u> </u>	177.13		-0.1191		-0-3-91	0.3493			<u></u>
		<del></del>							<del></del>
				<del></del>					
									•
				<del></del>	<del></del>	<del></del>		<del></del>	
	-					·			
						<del></del> -			
		·· <del>···································</del>		· · · · · · · · · · · · · · · · · · ·					· · · · · · · · · · · · · · · · · · ·
	-								

										•
AHNOLD	ENGINE	ERING WEYE	LOPHENT C	ENTERIALD	C)PROP	ULSION #1	ND TUNNEL FACIL	174(PbI)	AERODYNAMIC WIND TUNNEL 1472	
PAGE	1 OF				44	RTIN MISS	ILE TAIL EFFECT	S DATA		
4111 10.12										
	TFS	I PART MAL	H RX10-6	CONF TOAS	SITION					_
	S	246 1.10	2.5	F36 F	REE				•	
POINT	ALPHA	CNF	Ch Ch	CH	#CPF	YCPF	7			
2	179.04	0.0350	-0-0114	6.0645	-0.3756	0.2707			,	
3	161.00	0.0146	-0.0020	2000.00	-0.2975	-0.0129		· · · · · · · · · · · · · · · · · · ·		
	162.06	0.0601	0.0015	-0.4454	10.3333 -	36.2666				
6	183.07	-0.0091	0.0055	-C-0104	-0.6126 -0.5048	1.1512				
8	186.09	-0.0436	0.0145	-0.0251	-0.4455	0.5734				_
								·····		_
						•		<del></del>	· · · · · · · · · · · · · · · · · · ·	
					<del></del>					—
			· · · · · · · · · · · · · · · · · · ·							
		······································		<del> </del>			<del></del>			
	·						· · · · · · · · · · · · · · · · · · ·			
							•			
										_
		<del></del>			· · · · · · · · · · · · · · · · · · ·	<del></del>				
									·	<del></del>
							<del></del>	<del></del>	•	
			<del></del>							—

#EET 1 OF SPLITTER PLATE DATA    TEST   PART   WACH RAID == COMF   THANSITION		NGINEE	RING LEVE	LOFMENT	CENTERIAL	GC1 PROP	ULSION MISSI	TUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA	AERODYNAMIC, WIND TUMNEL (6T)
2 247 1.24 2.5 F36 FHEE  OINT ALPHA CMF CH CH CH ACPF VCPF  1 = 2.03 - 0.0315 0.3012 - 0.2015 - 0.0300 0.6817  2 -0.96 -0.0165 0.0004 - 0.0141 - 0.0236 0.6545  3 0.09 - 0.0005 - 0.001 - 0.0007 - 0.0014 - 0.0236 0.6545  5 2.00 0.0220 - 0.0015 0.0024 - 0.0013 - 0.2956  5 2.00 0.0220 - 0.0015 0.0022 - 0.0091 0.1291  0 3.05 0.0347 - 0.0021 0.0077 - 0.005 0.7217  7 4.06 0.0041 - 0.0021 0.0077 - 0.005 0.7217  9 0.11 0.1266 - 0.0010 0.0047 0.0133 - 0.0586 0.31245  10 10.13 0.1747 - 0.0094 0.0672 - 0.0539 0.3157  11 12.14 0.2267 - 0.0116 0.0779 - 0.0527 0.3158  12 14.17 0.2364 - 0.0116 0.0779 - 0.0527 0.3285  14 18.22 0.4058 - 0.0116 0.0179 0.0490 0.3285  15 10.00 0.000 0.000 0.0000 0.0000 0.0000 0.3194  16 18.22 0.4058 - 0.0147 0.1263 0.0000 0.3194  16 18.22 0.4058 - 0.0147 0.1263 0.0000 0.3126  17 24.32 0.5959 - 0.0231 0.1647 - 0.0032 0.3085  19 27.35 0.0005 - 0.0280 0.0280 0.3125									
2 247 1.20 2.5 F36 FHEE  **OINT ALPHA CMF			·····					· · · · · · · · · · · · · · · · · · ·	
OINT ALPHA									
1 -2.03 -6.0315									
2 -0.46 -0.4165	DINT .								
4 1.05 0.0001 -0.0007 -0.0024 -0.0413 -0.2956 5 2.06 0.0220 -0.0015 0.0027 -0.0691 0.1291 6 3.05 0.0347 -0.0021 0.0077 -0.0005 0.2217 7 4.06 0.0231 +0.0027 0.0154 -0.0566 0.3245 8 0.05 0.0041 -0.0044 0.0313 -0.6585 0.3717 9 0.11 0.1246 -0.0044 0.0027 -0.0557 0.3766 10 10.13 0.1744 -0.0094 0.0622 -0.0539 0.3557 11 12.14 0.2270 -0.0116 0.0779 -0.0522 0.3333 12 14.17 0.2644 -0.0147 0.6036 -0.6517 0.3205 13 15.19 0.3314 -0.0164 0.1243 -0.0490 0.3194 14 18.22 0.4046 -0.0147 0.1263 -0.0462 0.3114 15 20.75 0.4068 -0.0147 0.1263 -0.0462 0.3126 16 27.28 0.5340 -0.0231 0.1647 -0.0432 0.3085 17 24.32 0.5955 -0.0283 0.1631 -0.0428 0.3127 18 26.35 0.6055 -0.0283 0.1647 -0.0428 0.3125 19 27.35 0.6095 -0.0289 0.2165 -0.0419 0.3141	5								
\$ 2.00	3								
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	•							•	-
7									· · · · · · · · · · · · · · · · · · ·
9	7								
10	8								• •
	9								
12 14.17 0.284 -0.0147 0.6936 -0.6517 0.3285 13.16.19 0.3432 -0.0147 1.1098 -0.0440 0.3194 14.18.22 0.4054 -0.0147 0.1263 -0.0062 0.3114 15.20.75 0.4082 -0.0203 0.1461 -0.6433 0.3120 16.27.28 0.5940 -0.0231 0.1647 -0.0432 0.3085 17.24.32 0.5955 -0.0280 0.2061 -0.0425 0.3127 18.26.35 0.6595 -0.0280 0.2061 -0.0425 0.3125 19.27.35 0.6095 -0.0289 0.2165 -0.0419 0.3141	-								
13 15.19 0.393E -0.010= 1-1798 -0.0490 0.3194  14 16.22 0.495E -0.0187 0.1263 -0.0462 0.3114  15 20.75 0.496E -0.0703 0.1401 -0.4433 0.3120  16 27.28 0.5340 -0.0731 0.1647 -0.0432 0.3085  17 24.32 0.5955 -0.0755 0.1583 -0.0428 0.3127  18 26.35 0.6595 -0.0780 6.2061 -0.0425 0.3125  19 27.35 0.6095 -0.0789 6.2164 -0.0419 0.3141									
15									······································
16									
17 24.32 0.5959 -0.0255 0.1963 -0.0428 0.3127 18 26.35 0.6595 -0.0280 6.2061 -0.0425 0.3125 19 27.35 0.6695 -0.0289 6.2164 -0.0419 0.3141								<del></del>	
18 26.35 0.6595 -0.0780 6.2061 -0.0625 0.3125 19 27.35 0.6895 -0.0289 6.2165 -0.0619 0.3161									
								•	•
	19	27.35	0.6495	-0.0289	3.2155	-0.0419	0-3141	<u> </u>	
		<del></del>							
						<del>,</del>			
			<del></del> -					<del></del>	
								7	
					<del></del> _	· · · · · · · · · · · · · · · · · · ·		•	• •
						<u></u> .			
						•			

. .

Æ	1 OF 1		- C	JIER LAEM	<b>#4</b> (	GTIN MISSILE	TAIL EFFECTS	DATA	AERIU TRARIL		
						<del></del>	•			•	
			n PX16-6_0			<del></del>	·				
	2	248 1.20	2.5	-36 F	*EE						
THE	ALPHA	CNF	Cr	Ce		YCPF					
2	29.25		-0.029E		-0-6416	0.3136		·		<del></del>	
3	30.25		-0-0323		-0.0412						
•	31.24	0.8141	-0.0337		-0-0408	0.3111					
5	32.29		-0-0343		-0-0-05	_0.3117		<del></del>	<del></del>	<del></del>	
6	33.30	0.0//3	-0.0351 -0.0358		-0.0400	0.3130					
8	36.34	0.4691	-C. 1376		-0.03dA	0.3159					
9	39.35	1.6435	-0-0360	0.3259	-0.0379	0.3184	<del></del>	····	· · · · · · · · · · · · · · · · · · ·		
10	40.38		-0.0363		-0.0357	0.3206					
15 17	-92.49		<u>-0.0356</u> -0.0305		-0.0271	0.3213					
13	44.42		-0-0304		-0-0211	0.3192					
1.	48.47		-0.0193		-0.0165	0.3184					
15	50.47		-0.0156			0.3177				<del> </del>	
16 17	52.50		-0.0145		-0.0160	0.3188					
10	54.52 54.51		<u>-0.;275</u> -0.;354		-0.0224	0.3271	· · · · · ·				
19	57.52		-0-4490		-0-0309	0.3292	<u>.                                    </u>			-	
								<del></del>			<del></del>
										<del> </del>	
				<del></del> -					<del></del>		
					•						
											•
									·· <del>·············</del>	<del></del>	
									<del></del>		
										<del></del>	

GŁ	1 OF 1		LUKERI L		MA	HTIN MISSI	LE TAIL EFFE ER PLATE DAT	ECTS DATA	AU	CONTH. DIMANYCOS	
				<u> </u>	<del> ,</del> ,.			· 			
	<u>TESI</u>	249 1.20	M RA10-6	<u>COME IRAN</u> F36 F	SITION	<del>~</del>					
OINT	ALPHA	CMF	CH A 1257	Ce		YCPF	•				
<del>,</del>	59.29 59.36	1.2054	-0-4353		-0.02A0 -0.0297	0.3302					
3	60.36	1.2/54	<u>-0_0397</u>		-0.6312	_0.3300					·
•	61.36	1.2673			-0.0328	0.3317					
<u>.</u>	<u>- 52.37</u> 63.38	<u></u>			-0.0337	0.3320 0.3331					
	64-39		-0-4-77		-0-0361	0.3331					
8	66.40	1.3465	-0.0517		-0-0384	0.3336					
9	05.00		-0.0550		-0-0-06	0.3345				<del> </del>	
10	70.42		-0.0544		-0.0429	0.3359					
14 14	72.42		<u>-0.6615</u> -0.0652		-0.044Z -0.0456					<del></del>	
13	76.43		-0-05MC	U-4776	-0-04A2	0.3390					
14	78.43	1.4221	-0.4095	V-4449	-0.0491	0.3410					
15	80.49		-0-0717		-0.0501	0.3421					
16	82.45		-0.0726 -0.0735		-0.0503 -0.0505	0.3436					
18	86.48		+C-0755	V-5017	-0.0522	0.3468	·				
19_			-0-u766		-0.0529	0.3472					
	33							-		_	
—									· · · · · · · · · · · · · · · · · · ·	<del></del>	
						. 65					
									•		
			<del></del> -								
				~ *** · · · · · ·							
			<del></del>						<del></del>		
									1		,

GE	1 OF 1	STAG NEAF	LOPMENT CE	NTEPLAED	C) PROPI	ULSION WIND TUNNEL FACILITY (PWI)	AEHODYMAMIC JUMMEL (AT)
EET.	1 OF 1					SPLITTER PLATE DATA	
	1561	CART MAC	h AX10-6.(	CONE TOAN	STYTON		
		250 1.20	2.5		HEE		
POINT	ALPHA	CNF	Сн	Cé	xcef	YCPF	
1	h8.22	1.9356	-0-041-		-0.0567	0-3677	
5	N4.24	1-4347	-0.0531	0.4794	-0.0579	0,3481	
_3	91.29	1.4395			-0.0593	0.3481	<del></del>
5	92.29	1.4403	-0.0673 -0.0691		-0.0606 -0.0619	0.3493	
6	93.76		-0.0406		-0.0630	0.3494	
7	94,29	1.4464	-0.6915		-0.0637	0.3504	
8	95.30		-0.09-0		-0.0652	0.3513	·
10	98.29		<u>-0.0962</u> -0.0968		-0.0672 -0.0698	0.3531	
11	102.29		-0-1024		0.0730	0.3531 0.3543	
12	104.30		-9-10-7		-0.0758	0.3554	
13	105.30		-0-1090		-0.0401	0-3567	<del></del>
14	108.29		-0.1161 -0.1223		-0.4860	0.3582	
15 16	110 <u>.29</u> 112.29		-0.1269		-0.0915 -0.0975	0.3628	
iz_	114.30	1-3667	-0.1340		-0-1025	0.3651	
18	116.29		-0.1412	0-4751	-0.1093	0.3679	
19_	117.26	1-2-37	-0.1443	0.4731	-C-1124	0.3686	
						<u></u>	
							······································
_							<del></del>
						<del></del>	
			<del></del>			<del></del>	
			•				
		•					

_							
_		<del></del>				<u> </u>	
1 ()	f mG1 mf f	PING VEVE	OPMENT (	FN164 (AF)	sC1 0000	ULSION WIND TUNNEL FACILITY (POT)	AERODYNAMIC WIND TUMMEL (AT)
Ė	1 OF 1		LVI.ZBILL	ALT DETCHAN		ATIN MISSILE TAIL EFFECTS DATA	
<u> </u>	1 OF 1				<del></del>	SPLITTER PLATE DATA	
		PAPI MAC					
	5	251 1.20		10.745.7	FREE		
MT	120.05	CNF	Сн -0.1525	C6	xCPF -0-1181	VCPF 0-3078	
<u>-</u>	121-10		-0.1544		~0.1705	0.3690	· · · · · · · · · · · · · · · · · · ·
3	122.11	1.273¢	-0-1560		-D.1725	0.3696	
	123.10 124.16		-0.1573 -0.1587		-0.1262	0.3696	
	150-11		-0-1614		-0.1301	0.3710	
	129.09		-C.1662		-0.1364	0.3738	
5	130.05		-0.1700 -0.1707		-0.1420 -0.1463	0.3756	
<u> </u>	134.10		-0.171e		-0.1507	0.3757	
1	136-10	1.1071	-6.1724	0-4163	-0.1558	D-3760	
3 3	139.10		-0-1732 -0-1750		-0.1616 -0.1691	0.3779	
-	1.2.10		-0-1775		-0.1761	0.3841	
5	144.10	0.9596	0.1731	0.3666	-0.1204	0.3#42	· · · · · · · · · · · · · · · · · · ·
6 7	146.12	0.9640	-0.1660		-0.1859 -0.1893	0.3843 6.3847	
	19/413	<u> </u>	-VelD34		-241047		
				· · · · · · · · · · · · · · · · · · ·			
							<del></del>
				<del> </del>			
			*			· · · · · · · · · · · · · · · · · · ·	•
_				·			
		<del></del>					
				<u> </u>			
						•	

5£	1 OF 1		LURELNI C	ENIERIAED		PTIN MISSILE 1	INNEL FACILITYS		AERODYNAMIC WIN	TUNNEL (AT)
EI_	1 OF 1					SPLITER	LATE DATA	•		
_								· · · · · · · · · · · · · · · · · · ·		<del></del>
				CUNF TRAN						
	S	258 1.20	£1.3	F36 F	REE					
NT"	ALPHA	CHF	CH	CH	CPF		· u	*		1. 45
	147.93 140.93	0.8521	-0.1625 -0.1592	0.3103	-0-1907 -0-1940	0.3848	<del></del>		····-	
	109.92	0.7589	_0_1554	0.3128_	-0-1970	0.3838				
•	150.97	0.7551	-0.1513	L+5+68	-0.2004	0.3639				
	152.98 152.99	0.6970	-0.1474 -0.1433	G-2755	-0.2030	0.3835				
<b>,</b>	153.98	[-6565	-0-1340		=0-2091	0.3643		_		
3	154.06	0.5765	-0-1244	r.2244	-0.2167	0.3831				
	158-00		-0-1201		-0.2249	S862				
0 1	160.01		-0.1099	0.1031 <u>0.1581</u>	-0.2342 -0.2444	0.3901			•	
5	164.04		-0.0446	0.1348		0.3878	•		,	
3	166.05	6.2897	-0.0775	2-1396	-0.2575	0.3782	<del> </del>			
•	168.07		-0.0661		-0.2-04	0.3740				
5	170-08		-0.0548		-0.29 <u>53</u> -0.3094	0.3702 0.3485				
	174-12		-0-0328		-0.3219	0.3451			1	
8	176.15		-0-0550		-0.3332	0.3331	•			•
9	177.15	0-0220	-0-6171	0-0159	-0-3241	0.3053				
<del>-</del> -	-				<del></del>					
										•
										<del></del>
				<del> </del>						
			•							
		··	<del></del>						<del></del>	<del></del>
				<del></del>					<del>, ,</del>	
		<del></del>		<del></del>		<del></del>				<del></del>
							<u> </u>			

)_TUNNEL(4T)	AERODYNAMIC WIND IU	NNEL FACILITY (PMT) AIL EFFECTS DATA LAIE DATA	TIN MISSIC	C) PROPI MAF	ENTER (AEU	OPMENT C		ENGINEE 1 OF 1 1 OF 1	GE
3000				SITION	CONF TRAN	H RX10-6	PART MALI	7651	
				PEE			257 1.30	2	
<del></del>		<del></del>	YCPF	xCPF	Ca	Cm	CNF	ALPHA	POINT
			0.6695	-0-0328	-0.0222		-0-0332		
			0.6056	-0.0204		0.0004		-0.97	2
			·0 · 3835	-0-1264	-0.0027	-0.0004		1.06	4
	·		0.2225	-0.0812	0.0045	-0.0017	0.0204	2.06	5
			0.3091	-0.0696	L.0103	-0.0023		3.08	6
	<del>- •-</del>	<del></del>	0.3958	-0.0633		-0.0053		6.10	8
			0.3796	-0.U507	0.0-35	-0.0674	andets.	_8.11_	9
			0.3591	-0.4568		-0.0100		10.13	10
	<del></del>		0.3516	<u>-0.0561</u> -0.0544		-0.0128 -0.0156		_12 <u>-1</u> E_ 14.19	15 77
			0.3250	-9-0517	2.1119	-0-0176	Ca3999	16.21	13
	<del></del>		0.3172	-0.0459		-0.0198		14.23	14
<del></del>		<del></del>	0.3136	-0.0469		-0.0220		20.20	15
			0.3130	-0.0458	i.lb53	-0.už13		24.32	_iĭ
			0.3129	-0.0-53		-0-6296		26.35	16
		····	0-3129	-0.0452	0.2161	-G. C312	0.6907	27,37	19
								·	
					<del></del>		<del></del>		
					····				
							·		
				1000					
			-						
		<del></del>		<del></del>					
<del></del>	<del></del>	<del></del>				<del></del>	<del></del>		

		•					
				<del></del>			
<del></del>			L	<del> </del>	<del></del>		
ARYOLD	ENGINEL	PING NEVE	LOPMENT C	ENTERCALO	C). PROP	PULSION MIND TUNNEL FACILITY (PHT) AERODYNAMIC MIND TUNNEL (AT)	
PAGE	1 OF 1				**	MANTIN MISSILE TAIL EFFECTS DATA	
SHEET	1 0F 1					SPLATTER PLATE DATA	
						· · · · · · · · · · · · · · · · · · ·	
	TEST			CUNE_IRAN			
	≥.	258 1.30	2.5	F36 F	HEE		
POINT	· ALPHA	CNF	C+	C→		PF YCPF	
2	14.12		-0.0136 -0.0150		-0.0555 -0.0566	A 0044	
3	15.1£		-9-162		-0.0532		
•	16.14	0.3.51	-0.0174	0.1684	-0-0520	0.3236	
<u> </u>	17.16 10.17		-0.4143 -0.4194		-0.0574 -0.0492		
7	19.15		-0-u203		-0-6477		
ę.	21.21		-0.1225		-0.0460	0.3130	
9	23.23		-0-4251				
16	25.26 26.39		-0.0276 -0.0272		-0.0451 -0.0450	6.3129 	
12	29.31		-0.0330		-0.0446		
13_	31.35		-0-4355				
14	33.37 _35.40_		-0.3375		-0.0431 -0.0423		
16	37.44		-0.0394 -0.0005		-0.0409		
<u> </u>	39.40	1.0967	-0-0-12		-3-0394	0-3186	
10	41.48		-6.0-11		-0.0375		
19	42,50	1-1199	-0-0412	0.3581	-0-0367	0.3198	
-							
			_	_			
						<del></del>	
						•	
				<del></del>	<del></del>		
		. —				•	
					* *******		

		<del></del>	<del></del>					•			·- <del></del>	
			<del></del>					<u>:</u>	· - · · · · · · · · · · · · · · · · · ·	<del> </del>	<del></del>	<del></del>
	<u>engineli</u> 1 of 1		OPMENT C	enter (aeu	C) PROP	FTIN MISSI	LE TAIL EFF	CILITYIPHTI	AE	RODYNAMIC =	IND_TUNNELL	<b>AI)</b>
EI	1_0f _1					SPLITI	ER PLATE D	TA				
											•	
	IESI	PAPT MAC	H PAlúmb		SITION					•		
INT:	ALPHA	CAF	Сн	Cr	XCPF	YCPF		1				<del></del>
<u> </u>	1.34	10001			-0.0376	0.3190		,			<del></del>	
3	42.42	1.1236	-0.0399 -C.0371		-0.0355 -0.0321	0.3105 0.3195						
•	46.47	1.1006	-0.0330	0.3748	-0.0280	0.3175						
5	48.49		0.0310		-0.0257	0.3174		····				
6	50.50 52.52	1.2191	-0.1292 AFFu.u-		-0.0274	0.3172						
	54,53	1.2503	-0.63nm	v.+v+1	-0.6310	0.3232						
9	56.54		-0.60.46		0-0339_	4.3251	<del></del>					<del></del>
10	57.57	1.2441	-0.0457	4.4224	-0.0353	0.3264						
					<del></del>	<del></del>					· · · · · ·	
												•
												•
		<del> </del>					<del></del>					<del></del>
							<u>'</u>					
						-						
							-				····	
				_								
			-				•					
			· · · · · · · · · · · · · · · · · · ·					<del></del>		· · · · · · · · · · · · · · · · · · ·		
			<del></del>		<del></del>					• • • • • • • • • • • • • • • • • • • •		
	<del></del>				·····			<del></del>			· - · · · ·	
					<del></del>				•			
						<del></del>		•		<del></del>		<del></del>
						•						
								<del></del>				

	1 OF 1			155	AM	ATIN MISSILE	TUNNEL FACILITY!	TA		-
<u> </u>	1_0F1		<del></del>				PLATE DATA	<b></b>		··
							•			·
	TEST	PAPT MAC	Cr. PX10-6	CONFIRAN	SITION					
	5	260 1.30	2.5		REE					
NT	AL PHA	CNF	CH	C =	<b>⊀CPF</b>	YCPF				<del></del>
	59.31	1.2825	-0-0411	0.4150	-0-0320	0.3747				
61	59.34		-6.6434	0.4621		0.3259				
	_00.34_		-0.0461			0-3276				
	61.41		-0.04M7 -0.0312		-0.0371 -0.0387	0.3285				
	63.40		-0.0532		-0.0399	0.3298		<del></del>		
<u></u>		1.3451	-2,4252		-0.0011	0.3300		·		
•	66.42	1.3699			-0.0-26	0.3323				
<u> </u>	-68.42		<u>=6-0-15</u>		-0.0442	0-3326				
) L	76.43		-0.0652 -0.0656		-0.0463 -0.0483.	0.3334				
	74.44		-0.UARY		-0.04H1	0.3353				
	76.46		-0-4560		-0.0469	0.3351				
	78.47	1.4014	-0.06=6	0.4451	-0.0469	0.3354				
<u> </u>	80.47					0.3362				<del></del>
:	82.49		-0.0769		-0.0512	0.3376	-			
•	86.52		-0.0775		-0.0510 - -0.0516	0.3390				
					-0-0534	0.3389				
			<del></del>							
				-						
			<del></del>						<del></del>	
										•
	•				··				• • • • • • • • • • • • • • • • • • • •	
					<del></del>		W.		· · · · · · · · · · · · · · · · · · ·	
										<del></del>

GE	ENGINEER 1 OF 1 1 OF 1	ING UELE	LOPHENT CI	ENTERIAEU		TIN MISSILE	TUNNEL FACILITY TAIL EFFECTS PLATE DATA		AERODYNAMIC MIND TUNNEL (4T)	
	IEST	PART MAC 261 1.30	H RX10=6		SITION					
OINT	ALPHA	CNF	CH	Co	* SACPF	YCPF	اب	3	f 4	3
	MB . 24		-0-0×70		-0.0582	0.3022				
5	89.26		-0.0013		-0.0581	0.3410				-
3	91.32		-0.udbb		-0-0576 -0-0573	0.3410				
5	92.33		-0-0a75			Q-34DA				
6		1.5091			-0.0591	0.3420				
7	94.33	1.5085	-0.0914		-0.0608	0.3622			<u> </u>	
8	46.33		-0.0705		-0.0641	0.3442				
9_	_99.13_		-0-0776		-0.0663	0.3459				
0	100.33		-0.1030		-0.0689	0.3469				
1	102.33		-0-1055		-0.0716	0-3481				
13	104.32		-0.1103		-0.0750 -0.4818	0.3501	-			
4	105.33		-0.1234		-0.0866	0.3545				
			-0.1179		-0-0856	0-3581				
16	111.00		-0.1120		-0.0573	0.3598				
17	119.33		-0-1276		A. 0459	0.3626				
10	116.33		-0.1365		-6.1017	0.3603				
19	117,30		-0,1391	0.4462	-0-1035	0.3619				
						<del>-</del>	<del></del>			
									•	
						<del></del>	···			
			•							
			~						· · · · · · · · · · · · · · · · · · ·	

D_ENGINEERING_UEVALOPMENT_CENTER(ALDC)	<del> </del>					·	
1 OF   SPILITER PLATE DATA   SPILITER PLATE DATA	<del></del>		·				•
1 OF   SPILITER PLATE DATA   SPILITER PLATE DATA			·		· · ·		
TEST PART PACK RA10-6 CONF TRANSITION  2 262 1.30 2.5 F.16 FREE  NT ALPHA CMF CM CM CM 1.323 -0.1394 0.4072 -0.1064 0.3653  110.00 1.3233 -0.1406 0.4033 -0.1064 0.3655  120.01 1.3068 -0.125 0.4103 -0.1091 0.3664  121.12 1.2047 -0.1400 0.4722 -0.1127 0.3647  122.13 1.2047 -0.1510 0.4060 -0.1122 0.3651  123.13 1.2055 -0.1510 0.4060 -0.1122 0.3651  123.12 1.2717 -0.1510 0.4060 -0.1123 0.3651  124.12 1.2717 -0.1510 0.4060 -0.1123 0.3651  124.12 1.2717 -0.1510 0.4060 -0.1123 0.3651  125.12 1.2717 -0.1510 0.4060 -0.1123 0.3651  126.12 1.2717 -0.1510 0.4060 -0.1230 0.3658  127.11 1.2241 -0.1577 0.4059 -0.1273 0.3660  137.12 1.1510 -0.1577 0.4059 -0.1322 0.3669  134.13 1.331 -0.1577 0.4167 0.4167 0.3669 0.3659  134.13 1.331 -0.1507 0.4167 0.4167 0.3669  136.13 1.351 -0.1509 0.4157 0.4157 0.4166 0.3687  136.11 1.0007 -0.1607 0.4167 0.3007 -0.1672 0.3753  146.12 1.0167 -0.1607 0.5007 -0.1672 0.3753  146.13 0.4937 -0.1655 0.3369 -0.1773 0.3768  147.15 0.4969 -0.1596 0.3369 -0.1773 0.3768	E 1 OF 1		loement_cf	YIER (ALD		HTIN MISSILE TAIL EFFECTS DATA	AEPODYNAMIC WIND TUNNEL (4T)
2 262 1.30 2-5	1 A VI					The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	
2 262 1.30 2-5	YEST	C PART MAC	w 0x10-6 f	OLE TRAM	:12704		
118.09		262 1.30	2.5	36 F	EE		
119,00	INT - ALPHA						
120,01							
	3 120-01	1.3464	-0.1-25	6.4703	-0-1091	0.3646	····
123-12 1.2717 -0.1510 0.6650 -0.1201 0.3651 124-12 1.2717 -0.1525 0.6659 -0.1201 0.3666 126-12 1.2564 -0.1569 0.6659 -0.1236 0.3658 126-11 1.2241 -0.1567 0.6395 -0.1322 0.3684 132-12 1.1506 -0.1597 0.6395 -0.1322 0.3684 132-12 1.1606 -0.1595 0.6262 -0.1315 0.3690 134-13 1.1351 -0.1609 0.6262 -0.1325 0.3666 136-13 1.4575 -0.1609 0.6457 -0.1622 0.3666 136-13 1.4575 -0.1609 0.351 -0.1522 0.3763 169.11 1.0000 -0.1731 0.3966 -0.1522 0.3753 169.12 1.0000 -0.1731 0.3966 -0.1632 0.3758 164-13 0.4537 -0.1655 0.3609 -0.1725 0.3755 164-15 0.6986 -0.1594 0.3398 -0.1773 0.3786 167.15 0.8985 -0.1595 0.3398 -0.1773 0.3768							
124_12   1.2717 -9.1525   0.4659 -0.1234   0.3656     176_12   1.256 -0.1549   0.6590 -0.1234   0.3656     129_11   1.2241 -0.1560   0.4589 -0.1275   0.3667     130_12   1.1931   0.1577   0.3955 -0.1322   0.3664     132_12   1.1666   0.1595   0.4262   0.3135   0.3649     134_13   1.1361   0.1607   0.4166   0.1622   0.3666     134_13   1.1361   0.1607   0.4166   0.1627   0.3666     136_13   1.056   0.1624   0.3951   0.1522   0.3763     169_11   1.0697   0.1671   0.3667   0.1672   0.3751     169_12   1.0167   0.1697   0.3607   0.1672   0.3751     164_13   0.2537   0.1655   0.3809   0.1755   0.3785     147_15   0.8753   -0.1565   0.3398   -0.1788   0.3768     147_15   0.8753   -0.1565   0.3298   -0.1788   0.3768     169_11   0.1697   0.1697   0.3567   0.3768     169_11   0.1697   0.1697   0.3567   0.3785     169_11   0.1697   0.1596   0.3398   -0.1788   0.3768     147_15   0.8753   -0.1565   0.3298   -0.1788   0.3768							
120_11							
130.12 1.1931 -6.1577 0.4395 -0.1322 0.3684  137.12 1.1666 -6.1595 6.4282 -0.1375 0.3636  134.13 1.1361 -0.1607 0.4165 -0.1422 0.3666  134.13 1.1975 -0.1609 (4.4957 -0.1466 0.3697)  135.12 1.0066 -0.1624 0.3951 -0.1522 0.3763  150.11 1.0067 -0.1731 0.3966 -0.1632 0.3753  142.12 1.0147 -0.1697 0.3007 -0.1672 0.3753  144.13 0.4937 -0.1655 0.3609 -0.1725 0.3785  145.15 0.6989 -0.1594 0.3398 -0.1773 0.3760  147.15 0.8753 -0.1565 0.3298 -0.1788 0.3768							
132.12 1.1606 -G.1595 G.4282 -G.1315 G.369G  134.13 1.1501 -G.1607 O.4166 -G.1622 G.3686  136.13 1.4575 -G.1609 G.4557 -G.1666 -G.3697  136.12 1.0666 -G.1626 G.3551 -G.1522 G.3763  149.11 1.0607 -G.1731 G.3666 -G.1632 G.3758  147.12 1.0147 -G.1697 G.3607 -G.1672 G.3751  144.13 G.4537 -G.1645 G.3609 -G.1773 G.3785  145.15 G.8753 -G.1596 G.3788 G.3768							
134-13 1-1341 -0.1607 0.4166 -0.1422 0.3666 136-13 1-4475 -0.1609 4.4457 -0.1466 0.3667 134-12 1.0666 -0.1624 0.3451 -0.1522 0.3763 140-11 1.0607 -0.1731 0.3866 -0.1632 0.3758 147-12 1.0147 -0.1697 0.3607 -0.1672 0.3758 144-13 0.4537 -0.1655 0.3609 -0.1725 0.3765 146-15 0.4989 -0.1594 0.3398 -0.1773 0.3766							
136.13 1.uv/5 -0.1609 (.e.u57 -0.1466 0.3467  137.12 1.0066 -0.1624 0.3751 -0.1522 0.3703  140.11 1.0067 -0.1731 0.3666 -0.1632 0.3758  147.12 1.0147 -0.1697 0.3607 -0.1672 0.3751  144.13 0.2537 -0.1655 0.3609 -0.1725 0.3785  145.15 0.0986 -0.1594 0.3398 -0.1773 0.3786  147.15 0.0753 -0.1565 0.3298 -0.1788 0.3768							
1+0-11 1-0-07 -0-1731 0-3966 -0-1632 0-3758  1+7-12 1-0147 -0-1697 0-3607 -0-1672 0-3751  1+4-13 0-9537 -0-1645 0-3609 -0-1725 0-3785  1+6-15 0-6989 -0-1594 0-3398 -0-1773 0-3780  147-15 0-6753 -0-1565 0-3298 -0-1788 0-3768	3 136,13	1.44/5					
147.12 1.0147 -0.1697 0.3607 -0.1672 0.3751 144.13 0.4537 -0.1645 0.3609 -0.1725 0.3785 146.15 0.8989 -0.1594 0.3398 -0.1773 0.3786 147.15 0.8753 -0.1565 0.3298 -0.1788 0.3768							
104-13 0.9537 -0.1065 0.3609 -0.1725 0.3785 146-15 0.8989 -0.1594 0.3398 -0.1773 0.3780 147-15 0.8753 -0.1505 0.3298 -0.1788 0.3768							· · · · · · · · · · · · · · · · · · ·
145.15	7 -104-13					0.3785	
167.15 0.8753 -0.1565 0.3298 -0.1788 0.3768	8 145.15	0.8989	-0-1594	0.3398	-0-1773		
	9 147.15	0.8753	-0.1505	D.329A	-0-1788	0.3768	
							•
							•
		· · · · · · · · · · · · · · · · · · ·					
	··						
							<del>,</del>
		•					
				•		<del></del>	
•							
						- · · · · · · · · · · · · · · · · · · ·	•
					<del></del>		

TESI 2 INT ALPHA 1 147-91 2 148-97 3 149-99 4 150-99 5 152-00 6 153-00 7 153-99 8 156-01 9 158-01 0 160-02 1 162-03 12 164-05 13 166-07 4 165-07 170-89 167-17	LPMA CMF Cm Cm ACPF YCF 7.91	767 754 753 : : : : : : : : : : : : : : : : : : :
2 INT ALPHA 1 147-91 2 148-97 3 149-99 4 150-99 5 152-00 6 153-00 7 153-99 8 156-01 9 158-01 0 160-02 1 162-03 1 164-05 3 166-07 5 170-89 16 176-16	2 203 1.3u 2.5 F30 FREE  LPMA CNF CM C0	767 754 753 : : : : : : : : : : : : : : : : : : :
INT ALPHA 1 147-91 2 148-97 3 149-99 4 150-99 5 152-00 6 153-00 7 153-99 8 156-01 9 158-01 0 160-02 1 162-03 1 164-05 3 166-07 4 166-07 170-09 174-13 18 176-16	LPMA CMF Cm Cm ACPF YCP 7.91 0.8463 -0.1561 0.3188 -0.1821 0.31 8.97 0.8159 -0.1507 0.3060 -0.1850 0.37 9.99 0.7053 -0.1475 0.2747 -0.1878 0.37 0.99 0.7061 -0.1441 0.27820 -0.1906 0.37 2.00 0.7225 -0.1491 0.2711 -0.1938 0.37 3.00 0.6724 -0.1305 0.2599 -0.1971 0.37 3.99 0.6556 -0.1324 0.2779 -0.2087 0.37 6.01 0.5751 -0.1240 0.2249 -0.2084 0.37	767 754 753 : : : : : : : : : : : : : : : : : : :
1 147.91 2 148.97 3 149.99 4 150.99 5 152.00 6 153.00 7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 165.07 5 170.09 16 172.12	7.91	767 754 753 : : : : : : : : : : : : : : : : : : :
2 148.97 3 149.99 4 150.99 5 152.00 6 153.00 7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 1 164.05 3 166.07 5 170.89 1 77.12 1 74.13 1 176.16	8.97	754 753 : : : : : : : : : : : : : : : : : : :
3 149.99 4 150.99 5 152.00 6 153.00 7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 1 162.03 1 166.07 4 166.07 5 170.09 1 174.13 18 176.16	9.99	753
4 150.99 5 152.00 6 153.00 7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 166.07 5 170.09 174.13 174.13 18 176.16	0.99	730
5 152.00 6 153.00 7 153.00 8 156.01 9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 166.07 15 170.09 16 172.12 17 174.13	<u>2.00                                   </u>	
6 153.0u 7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 165.07 5 170.09 16 172.12 17 174.13 18 176.16	3.00	
7 153.99 8 156.01 9 158.01 0 160.02 1 162.03 12 164.05 13 166.07 14 166.07 15 170.09 16 172.12 17 174.13 16 176.16	<u>3.99                                   </u>	
8 156.01 9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 166.07 5 170.09 17.12 17.13 18 176.16	6.01 0.5751 -0.1240 0.2244 -0.2084 0.37	
9 158.01 0 160.02 1 162.03 2 164.05 3 166.07 4 166.07 5 170.09 17 174.13 18 176.16		
0 160.02 1 162.03 2 164.05 3 166.07 4 166.07 5 170.09 16 172.12 17 174.13	<u>veri megayo, "vellor verulu "perlir vel</u>	768
1 162.03 2 164.05 3 166.07 4 166.07 5 170.09 16 172.12 17 174.13 18 176.16		
106.07 160.07 170.09 16 172.12 17 174.13 18 176.16		769
4   166.07   5   170.05   6   172.12   7   174.13   10   176.16		
5 170.09 6 172.12 17 174.13 18 176.16		
6 172.12 17 174.13 18 176.16		
7 174.13		
8 176.16		
		1169 1955
		510
	JAN WANTER - WANTER WANTER WATER	
		· · · · · · · · · · · · · · · · · · ·
	•	1
	•	
	·	

€E	1 OF 1		L0PME41_C		441	1114 MISSI	ID JUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA LER PLATE DATA	AERODYNAMIC WIND TUNNEL (41)
	IESI	PAPT MAC	<u> 2.5</u>		211107 HEE		· · · · · · · · · · · · · · · · · · ·	
OINT	ALPHA	CNF	CH	CH	t- KCPF	YCPF	- J	ñ 185
<u> </u>	118-07	1.0093	-0.1189	0.5518	-0.1091	D-5065		
	119.13	1.0072	-0.1206	0.5461	-0.1114	0.5046		
	120.14. 121.10		<u>-0.121#</u> -0.1237		-0.1129	0.5045 0.5012		
5	122.14	1.0798	-0.1221		0.1136	0.5070		
	123.15	1.0694	-0.1233	0.5375	-0,1153	0.5026		
	124.15	1.0673	-0.1293 -0.1292	<u> </u>	-0.1211	0.4975		
	128.10	1.0075	-0.1334	0.5320	-0.1211	0.4922		
	130.16	1.0632	-0.1351	0.5340	-0.1247	0.4930		
	132-15	1.0735	<u>-0.1356</u>		-0-1263	0.4946		
	134.16	1.0543	-0.1362		-0.1311	0.4900		
	130-17	1.0293	-0.1356 -0.1357	0.5076	-0-1318 -0-1352	0-4931		
-	140.17	0.9937	-0-1360		-0-1368	0.4911		
	147.15	0.4693	-0.1361	0.4753	-0-1404	0.4903		
_17	144.16				0.1445	0.4894		
18	146.19	0.9354	-0.1362 -0.1362		-0.1480	0.4883		
	171410	NAZIVI	-041302	365383	-112.1502			
								<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>
							***************************************	

							The graph of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of t
			<del></del>				
				<del></del>			
	ENGINEE 1 OF 1		<u>Lopment C</u>	ENTERLACO		ULSION WIND TUMMEL FACISITY (PMT) HTIN MISSILE TAIL EFFECTS DATA	AERODYNAMIC MIND TURNEL (AT)
	105		<del>,</del>			SPLITIER PLATE DATA	
						-	
	1561	DART MAL	M AKISTS	CONE TON	677704	•	
	<u>\$</u>	270 0.42			KEE		
POINT	ALPHA	CHF	C+	Сь		YCPF	
2	149.11	P.8742	-0.1377	6.4345 6.4325	-0-1540 -0-1532	0.4859	<del></del>
3	150.11		-0.1363		-0-1532 -0-1556	0.486 <b>8</b>	
•	151.12		-0.1367		-0-1572	0.4830	•
_5	152.13		-0.1375		-0-15a5	0.4825	
7	153.13		-0.1360		-9.1600 -0.1611	0.4827 8.4803	
6	156,14		-0.13/4		-0-1541	0.4829	· · · · · · · · · · · · · · · · · · ·
ÿ	158.13		-0.1325		-0-1504	0.4841	·
10	160.14	0.7565	-0.1390	u - 3696	-0-1633	0.4873	
11	102.14		-0.1e03		-0-2053	0-5045	· · · · · · · · · · · · · · · · · · ·
12	164.14		-0-1-37 -0-1753		-0-2416 -0-3111	0.5072 0.5150	
13	164,13		-0-1754		-0-3256	0.5166	
	170.13		-0-1322		-0.3538	0.5080	<u> </u>
10	172.15		-6-1059		-0.3915	0.5064	
17	174.16		-0-0816		-0-4039	9-4631	<del></del>
16	176.18		-0.6543 -0.4419		-0-4297	0-4541	
19	177.14	<u> </u>		News 44	-0.4354	0.4372	······································
		lie I		<del>~~ · · · · · · · · · · · · · · · · · · </del>	<del></del>		
					,		
		•					
					•		
			<del></del>				
						······································	•
			<u> </u>				<u> </u>

						<u> </u>	· · · · · · · · · · · · · · · · · · ·
							•
							•
		DING DEVE	LOPPENI C	ENTER LAED	C) PROP	ULSION DIND JUNNEL FACILITY (PAT)	AERODYNAMIC IND TUNNEL (AT)
	1 OF 1				44	RTIN MISSILE TAIL EFFECTS DATA	•
SHEET	1 OF 1					SPLITTER PLATE DATA	
	TEST	PARI MAC	4-0129 M	COME THAN	STITOM	•	•
	5		2.5	FII F	HEE		
00147	. ALPHA	CNF	Сн	C:		YCPF	
1		0.4722			-0.4326	0.3901	
S	179.05	0.0452	-0.0197	0.0138	-0.4355	0.3050	
	180.05	-0.0045	6-0646	-0.0061	-0-4149	_0 <u>.2564</u> 	
5	182.00	-0.0366	0.6165	-0.0180	-0.4491	0.4899	
6	183.07	-0.0635	0.0274	-0.0323	-0.4312	0.5086	
	100.07	-NAUYER	U_U_U_	-0-14-63	-V-9-10-7	. U. 9.7 V B	
						·	
	<del></del>						
					=	·	
					<del></del>		
			<u> </u>				
						•	•
						· · · · · · · · · · · · · · · · · · ·	
				<del></del> .			•
		,					•
			- <del></del>				
<del></del>							
				•			
			•				

-2-04 -0-0565 -6-0230 -0-0330 0.4081 0.5851 2 -0-94 -0-0466 -0-0114 -0-04103 0.4443 0.5851 2 -0-94 -0-0466 -0-0114 -0-0423 -2-6445 -1-2636 3 -0-06 0.0407 0.0030 0.0120 0.1349 0.4516 5 -2-05 0.0561 0.0112 0.0249 0.2000 0.4447 5 3-11 0.4066 0.0400 0.0362 0.2255 0.4296 7 4-11 0.122 0.0333 0.0447 0.4472 8 6-13 0.2124 0.0333 0.0443 0.4479 0.4647 8 6-13 0.2124 0.016 0.1006 0.1464 0.4752 9 6-14 0.2950 0.6561 0.1006 0.1464 0.4752 0 10-16 0.3994 0.3633 0.1991 0.1584 0.4985 1 12-16 0.3995 0.0633 0.1991 0.1584 0.4985 1 12-16 0.3995 0.0712 0.2854 0.1258 0.4993 2 13-34 0.5659 0.0712 0.2854 0.1258 0.5903 3 16-24 0.7185 0.4785 0.4785 0.4789 0.5908 4 16-26 0.8132 0.0787 0.4139 0.3968 0.5090 5 20-28 0.9975 0.9020 0.4466 0.8904 0.5141 6 22-33 1.0096 0.0776 0.5174 0.5760 0.65125 7 24-33 1.0096 0.0745 0.5023 0.6681 0.5125 7 24-33 1.0096 0.0746 0.5023 0.6681 0.5125 8 26-33 1.0079 0.042 0.5490 0.0394 0.5081 9 27-32 1.1666 0.0422 0.55560 0.0374 0.44934	TEST PART MACH RAIG-6 CONF TRANSITION  2 272 0.90 2.5 F11 FMEE  (NT ALPMA CNF CM C6 ACPF VCPF  -2.90 -0.0565 -0.0230 -0.0330 0.0011 0.5851  2 -0.94 -0.0266 -0.0119 -0.0103 0.0041 0.5851  3 -0.06 0.0267 -0.0129 -0.0023 -2.065 -1.2010  5 -2.05 0.0561 0.0112 0.0229 0.2000 0.0407  5 -2.05 0.0561 0.0112 0.0229 0.2000 0.0407  5 -2.05 0.0561 0.0112 0.0249 0.2000 0.0407  5 -3.11 0.0066 0.000 0.0362 0.2255 0.0206  6 -3.11 0.0066 0.000 0.0362 0.2255 0.0206  7 -0.11 0.1220 0.0010 1.000 0.1964 0.0752  8 -0.13 0.2120 0.0016 0.1000 0.1964 0.0752  9 -0.10 0.0390 0.0561 0.1001 0.1964 0.0752  9 -0.10 0.0390 0.0561 0.1001 0.1964 0.0752  1 12.16 0.0390 0.0565 0.0551 0.1290 0.1990  1 12.16 0.0390 0.0712 0.2755 0.1258 0.5963  1 15.26 0.7105 0.0767 0.0767 0.2755 0.1059  1 18.20 0.0132 0.0767 0.0165 0.0968 0.5000  2 -0.0975 0.0975 0.0980 0.0968 0.5000  5 -20.20 0.9975 0.0920 0.0517 0.0968 0.5000  5 -20.20 0.9975 0.0920 0.0517 0.0763 0.5125  7 -20.33 1.0096 0.0770 0.5174 0.0763 0.5125  8 -20.33 1.0096 0.0770 0.5174 0.0763 0.5125  8 -20.33 1.0096 0.0770 0.5174 0.0763 0.5125  8 -20.33 1.0090 0.0077 0.05174 0.0763 0.5125  8 -20.33 1.0090 0.0070 0.052 0.5500 0.0994 0.5001  9 -27.32 1.1066 0.0022 0.5560 0.0374 0.4934	TRANSITION  FREE  Ch		1 OF 1		LOPMENT C	ENTER (AEU	PHOP.	ATIN MISSILE	TAIL EFFECT	S DATA	AERODYNAMIC	winoTunnel.com
2 272 0, we 2.5	2 272 0.96 2.5 F11 FMEE  INT ALPMA CNF CN Ch 4CPF YCPF 1 -2.00 =0.0565	FMEE  CE	<u>. I </u>				<del></del>		3FLL11EK	PLAIR DAIR	<del></del>		•
2 272 0.90 2.5 F11 FMEE  DINT ALPMA CNF CN Ch 4CPF VCPF  1 -2-10 -0.0565 -6.1230 -6.0330 0.4081 0.5851  2 -0.94 -0.0266 -0.0117 -0.0103 0.443 0.6847  3 0.06 0.0119 -0.0036 0.0120 0.1349 0.4516  5 2.05 0.0561 0.0112 0.2049 0.2000 0.4447  6 3.11 0.0666 0.0200 0.0362 0.2255 0.296  7 4.11 0.122a 0.0303 0.0543 0.2479 0.4477  8 6.13 0.2120 (.4616 0.1009 0.1964 0.4752  9 8.10 0.2955 0.0561 0.1009 0.1964 0.4752  9 8.10 0.2955 0.0561 0.1063 0.1697 0.4945  10 10.10 0.3994 0.0633 0.1691 0.1584 0.4065  11 12.16 0.3975 0.0671 0.2555 0.1258 0.5043  12 13.30 0.5659 0.0712 0.2856 0.1258 0.5043  13 16.26 0.4150 0.0766 0.3662 0.1099 0.3966 0.5000  15 20.28 0.9075 0.9020 0.4666 0.0904 0.5161  16 22.30 1.0945 0.0776 0.5174 0.0763 0.5125  17 24.33 1.0979 0.0432 0.5490 0.0394 0.5001  18 26.33 1.0979 0.0432 0.5560 0.0374 0.4434	2 272 0.90 2.5 F11 FHEE  DINT ALPMA CNF CN Ch 4CPF YCPF  1 -2.30 -0.0565 -0.0230 -0.0330 0.4081 0.5851  2 -0.94 -0.026 -0.0119 -0.0129 -0.0023 -2.6645 -1.2036  4 1.09 0.0267 0.0030 0.0120 0.1349 0.4516  5 2.09 0.0561 0.0112 0.0249 0.2000 0.4667  6 3.11 0.0066 0.0200 0.0362 0.2255 0.2266  7 4.11 0.1220 0.0303 3.0543 0.2479 0.4477  8 6.13 0.2120 0.0416 0.1008 0.1964 0.4752  9 A.10 0.2950 0.0561 0.1008 0.1964 0.4752  9 A.10 0.2950 0.0561 0.1008 0.1964 0.4955  11 12.16 0.5075 0.0075 0.2533 0.1891 0.1584 0.4985  11 12.16 0.5075 0.0075 0.2534 0.1258 0.5043  13 16.20 0.7165 0.0075 0.2554 0.1258 0.5043  14 16.20 0.7165 0.0077 0.4139 0.3063  15 20.22 0.9075 0.0712 0.2854 0.1258 0.5043  16 22.30 1.0096 0.0070 0.4139 0.3068 0.5090  17 24.33 1.0962 0.0176 0.5174 0.0763 0.5125  17 24.33 1.0962 0.0176 0.5023 0.0501	FMEE  CE					50v5 35v					* * * * * * * * * * * * * * * * * * * *	
1 -2.0u -0.0565 -6.0230 -0.0330 0.4081 0.5851 2 -0.04 -0.0267 -0.0114 -0.0199 -0.0623 -2.6445 -1.2634 3 0.00 0.0267 0.0036 0.0120 0.1349 0.4516 5 2.05 0.0561 0.0112 0.0249 0.2000 0.4447 6 3.11 0.0866 0.0200 0.0362 0.2255 0.4296 7 4.11 0.122 0.0333 3.0543 0.2479 0.4477 8 6.13 0.2120 0.0333 3.0543 0.2479 0.4477 8 6.13 0.2120 0.0333 0.1943 0.2479 0.4477 8 6.13 0.2120 0.0333 0.1941 0.1964 0.4752 9 8.14 0.2956 0.0516 0.1009 0.1964 0.4752 10 10.16 0.3994 0.0533 0.1991 0.1584 0.4985 11 12.16 0.3975 0.0075 0.2536 0.1329 0.4983 12 13.30 0.5659 0.0712 0.2854 0.1258 0.5043 13 16.24 0.7165 0.0767 0.4139 0.3662 0.1269 0.5083 14 18.26 0.8132 0.0767 0.4139 0.3968 0.5090 15 20.28 0.9975 0.0767 0.4139 0.3968 0.5090 16 22.33 1.0096 0.0776 0.5523 0.6681 0.5183 17 24.33 1.0062 0.0765 0.5023 0.6681 0.5183 18 26.33 1.0079 0.042 0.5490 0.0394 0.5001 19 27.32 1.1666 0.0922 0.5560 0.0374 0.4934	1 -2.0u -0.0565 -0.0210 -0.0330 0.4081 0.5851 2 -0.94 -0.0267 -0.0119 -0.0119 -0.0130 0.443 0.6687 3	0.330											
2 -0.94 -0.0cb -0.0119 -0.0103 0.0443 0.0867 3 0.06 0.0019 -0.0099 -0.0023 72.6455 -1.2636 4 1.09 0.0cb 0.0030 0.0120 0.1349 0.4516 5 2.09 0.0561 0.0112 0.0249 0.2000 0.4647 6 3.11 0.0ccb 0.0000 0.0352 0.2255 0.4296 7 4.11 0.1220 0.0303 0.0194 0.477 0.4477 8 6.13 0.2120 0.0161 0.1006 0.1964 0.4752 9 A.10 0.2555 0.0551 0.1653 0.1697 0.4945 10 10.10 0.3994 0.0633 0.1697 0.4945 11 12.16 0.5075 0.0075 0.2538 0.1329 0.4993 12 13.30 0.5659 0.0712 0.2550 0.1256 0.5943 13 16.24 0.7165 0.4765 0.4765 0.3642 0.1369 0.5943 14 18.26 0.8132 0.0767 0.4166 0.3642 0.1369 0.5083 15 20.28 0.9975 0.076 0.3642 0.4665 0.8994 0.5508 16 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 17 28.33 1.0962 0.4766 0.5523 0.6681 0.5130 18 26.33 1.0979 0.0432 0.5560 0.0374 0.4934	2 -0.94 -0.0co -0.011 -0.012 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0023 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -0.0020 -		DINT	ALPHA	CNF	Cr	Ch	ACPF	YCPF	<del></del>	•	· · · · · · · · · · · · · · · · · · ·	
3	3	0023 -2.6645 -1.2636 0120 0.1349 0.4516 0249 0.2000 0.4647 0362 0.2255 0.4296 0543 0.4479 0.4477 1006 0.1964 0.4752 11463 0.1897 0.4945 11991 0.1584 0.4985 .2534 0.1329 0.4993 .2535 0.1256 0.5043 .4139 0.3968 0.5083 .4139 0.3968 0.5090 .4616 0.0904 0.5161 .5174 0.0763 0.5125 .5623 0.4681 0.5130 .5623 0.4681 0.5130	_								<del></del>		
4 1.09 0.0267 0.0036 0.0120 0.1349 0.4516 5 2.05 0.0561 0.0112 0.0249 0.2000 0.4647 6 3.11 0.0666 0.0200 0.0362 0.2255 0.4296 7 4.11 0.122 0.0333 0.543 0.2479 0.4477 8 6.13 0.2120 0.046 0.0200 0.1964 0.472 8 6.13 0.2120 0.046 0.1008 0.1964 0.4752 9 A.14 0.2955 0.0561 0.106 0.1964 0.4955 10 10.10 0.3994 0.0633 0.1991 0.1584 0.4985 11 12.16 0.5075 0.0075 0.2534 0.1329 0.4985 12 13.30 0.5659 0.0712 0.2854 0.1329 0.4993 13 16.24 0.7165 0.0767 0.4139 0.5083 14 18.26 0.8132 0.0767 0.4139 0.3968 0.5090 15 20.28 0.9075 0.0767 0.4139 0.3968 0.5090 16 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 17 24.33 1.0962 0.0746 0.5523 0.0681 0.5130 18 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 19 27.32 1.1266 0.0422 0.5560 0.0374 0.4934	4 1.09 0.0c67 0.0036 0.0120 0.1349 0.4516 5 2.09 0.0561 0.0112 0.0249 0.2000 0.4447 6 3.11 0.0086 0.0000 0.0362 0.2255 0.4296 7 4.11 0.1222 0.0330 0.0543 0.2479 0.4477 8 6.13 0.2120 0.0416 0.1008 0.1964 0.4752 9 A.10 0.2955 0.0551 0.1663 0.1897 0.4945 10 10.16 0.3994 0.0633 0.1991 0.1584 0.4985 11 12.16 0.5975 0.0075 0.2534 0.1329 0.4983 12 13.30 0.5659 0.0712 0.2854 0.1258 0.5943 13 16.26 0.7165 0.3662 0.1369 0.5083 14 18.26 0.8132 0.0767 0.4139 0.0968 0.5083 15 20.28 0.9075 0.0777 0.4139 0.0968 0.5090 15 20.28 0.9075 0.0770 0.5174 0.0763 0.5125 17 24.33 1.0979 0.0432 0.5490 0.0394 0.5081 18 26.33 1.0979 0.0432 0.5490 0.0394 0.5081	0120 0.1349 0.4516 0249 0.2000 0.4447 0362 0.2255 0.4296 0543 0.479 0.4477 1100 0.1964 0.4752 1463 0.1697 0.4985 1191 0.1584 0.4985 12534 0.1329 0.4983 12554 0.1256 0.5043 1462 0.1369 0.5083 14139 0.3968 0.5090 14139 0.3968 0.5090 14156 0.0904 0.5141 15174 0.0763 0.5125 15023 0.0681 0.5130 15023 0.0681 0.5130	<u>.</u>									•	
3.11 0.0000 0.0362 0.2255 0.4296 7 4.11 0.1224 0.0303 0.0543 0.2479 0.4477 8 6.13 0.2120 0.0416 0.1000 0.1964 0.4752 9 8.14 0.2255 0.0551 0.1663 0.1697 0.4985 0 10.16 0.3994 0.0633 0.1991 0.1584 0.4985 1 12.16 0.5075 0.0075 0.2534 0.1329 0.4993 2 13.30 0.5659 0.0712 0.2854 0.1258 0.5043 3 16.24 0.7165 0.0760 0.3642 0.1369 0.5083 4 18.26 0.8132 0.0767 0.4139 0.3968 0.5090 5 20.26 0.9075 0.9020 0.4666 0.0904 0.5141 6 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 7 24.33 1.0962 0.0746 0.5623 0.0681 0.5130 8 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 9 27.32 1.1265 0.0422 0.5560 0.0374 0.4934	3.11 0.0000 0.0362 0.2255 0.4290 7 4.11 0.1224 0.0303 0.0443 0.2479 0.4477 8 5.13 0.2120 0.0416 0.1000 0.1964 0.4752 9 8.14 0.2950 0.0551 0.1463 0.1697 0.4965 0 10.16 0.3994 0.3633 0.1991 0.1584 0.4985 1 12.16 0.5075 0.0075 0.2534 0.1329 0.4993 2 13.30 0.5659 0.0712 0.2754 0.1258 0.5043 3 16.24 0.7105 0.0766 0.3662 0.1369 0.5083 4 18.26 0.8132 0.0767 0.4139 0.3968 0.5090 5 20.28 0.9075 0.000 0.466 0.0904 0.5141 6 22.30 1.0096 0.0776 0.5174 0.0763 0.5125 7 24.33 1.0979 0.0432 0.5690 0.0394 0.5001 9 27.32 1.1665 0.0422 0.5560 0.0374 0.4934	0362 0.2255 0.4296 0543 0.2479 0.4477 1006 0.1464 0.4752 1163 0.1697 0.4985 11641 0.1584 0.4985 12534 0.1329 0.4993 12754 0.1258 0.5043 13642 0.1369 0.5083 14139 0.3968 0.5090 14139 0.3968 0.5090 14139 0.0763 0.5125 15023 0.0681 0.5125 15023 0.0681 0.5001	•	1.09	0.0267	0.0036	0-0120	0.1349	0.4516			•	
7	7	0543 0.7479 0.4477 .1008 0.1964 0.4752 .1463 0.1697 0.4985 .2534 0.1329 0.4985 .2534 0.1258 0.5043 .2454 0.1258 0.5043 .3642 0.1369 0.5043 .4139 0.3968 0.5090 .4139 0.0968 0.5090 .4156 0.0904 0.5121 .5174 0.0763 0.5125 .5023 0.6681 0.5125 .5023 0.6681 0.5130	•								· _ ,		
9	9	1463	1	4.11	0.1220	0.0303	3-0543	0.7479	0.4677				<del></del>
0 10.16 0.3794 0.0633 (.194) 0.1584 0.4985 1 12.16 0.5475 0.4675 0.2534 0.1329 0.4993 2 13.30 0.5659 0.0712 0.2854 0.1258 0.5043 3 16.24 0.7165 0.4766 0.3642 0.1069 0.5083 4 18.26 0.8132 0.0767 0.4139 0.0968 0.5098 5 20.20 0.9075 0.9020 0.4666 0.0904 0.5141 6 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 7 24.33 1.0962 0.4766 0.5623 0.6681 0.5130 8 26.33 1.0979 0.0432 0.5490 0.0394 0.5081 9 27.32 1.1669 0.0422 0.5560 0.0374 0.4934	0 10.16 0.3994 0.0633 0.1991 0.1584 0.4985 1 12.16 0.5475 0.4675 0.2536 0.1329 0.4993 2 13.30 0.5659 0.0712 0.2754 0.1258 0.5043 3 16.24 0.7165 0.4766 0.3662 0.1369 0.5083 4 18.26 0.8132 0.0767 0.4139 0.3968 0.5090 5 20.20 0.9975 0.9020 0.4666 0.0904 0.5161 6 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 7 24.33 1.0962 0.4766 0.5623 0.6681 0.5130 8 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 9 27.32 1.1665 0.0422 0.55560 0.0374 0.4934	-1541 0.1584 0.4985 -2534 0.1329 0.4993 -2454 0.1258 0.5043 -3642 0.1369 0.5083 -4139 0.3968 0.5090 -4666 0.0904 0.5161 -5174 0.0763 0.5125 -5623 0.6681 0.5130 -5690 0.0394 0.5001											
12.16	12-16	2536 0.1329 0.4993 -2454 0.1258 0.5043 -3642 0.1369 0.5083 -4139 0.3968 0.5090 -4666 0.0904 0.5161 -5174 0.0763 0.5125 -5623 0.6681 0.5130 -5490 0.0394 0.5001			0.3494	0.0633			0.4985			· · · · · · · · · · · · · · · · · · ·	
3 16.74 6.7165 0.0767 0.3642 0.1369 0.5083 4 18.26 0.8132 0.0767 0.4139 0.0968 0.5098 5 20.26 0.9175 6.9020 0.4666 0.0904 0.5161 6 22.30 1.0046 0.0770 0.5174 0.0763 0.5125 7. 24.33 1.0962 0.0746 0.5623 0.0681 0.5136 8 26.33 1.0979 0.0432 0.5490 0.0394 0.5081 9 27.32 1.1265 0.0422 0.5560 0.0374 0.4934	3	3642 0.1369 0.5083 .4139 0.3968 0.5090 .4556 0.0904 0.5161 .5174 0.0763 0.5125 .5623 0.0681 0.5130 .5490 0.0394 0.5001			0.5475	0-4075	0.2536	0.1329_	0.4993				·
	15 20.28 0.9075 0.0020 0.4666 0.0904 0.5141 16 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 17 24.33 1.0962 0.0746 0.5623 0.0681 0.5130 18 26.33 1.0979 0.042 0.5470 0.0394 0.5001 19 27.32 1.1265 0.0422 0.5560 0.0374 0.4934	-6656 0.0904 0.5161 -5174 0.0763 0.5125 -5023 0.0681 0.5130 -5490 0.0394 0.5001		15.36	0.5659	0.0712	0.2854	0-1256					
5 20.20 0.9075 0.0020 0.4066 0.0904 0.5141 6 22.30 1.0096 0.0770 0.5174 0.0763 0.5125 7 24.33 1.0962 0.0746 0.5623 0.0681 0.5130 8 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 9 27.32 1.1265 0.0422 0.5560 0.0374 0.4934		-6656 0.0904 0.5161 -5174 0.0763 0.5125 -5023 0.0681 0.5130 -5490 0.0394 0.5001		18.26	0.8132	0.0767	0.4139	0-0968	0.5090				
7 24.33 1.0962 0.0746 0.5623 0.0681 0.5130 18 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 19 27.32 1.1265 0.0422 0.5560 0.0374 0.4934	7 24.33 1.0962 0.0746 0.5623 0.0681 0.5130 18 26.33 1.0979 0.0432 0.5490 0.0394 0.5001 19 27.32 1.1265 0.0422 0.5560 0.0374 0.4934	-5623		20.20	0.9975	0.0020	0.4656	0.0904		<del> </del>	<del></del>	<del></del>	<del></del>
8   26.33   1.0979   0.0432   0.5490   0.0394   0.5081   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934   0.4934		.5490 0.0394 0.50 <b>0</b> 1		24.33	1.0096	0-0770	0.5623	0.0763	0.5125				
			8	26.33	1.0979	0.0432	0.5490	0.0394	0.5001				
			9	21.32	1.1005	0.0022	0.5560	0-0374	0.4934	<del>·</del>	<del></del>		
			,										
									<del> </del>	<del></del>		······	
							<del></del>		<del></del>				
										····			<del></del>
					•								
												<del></del>	
								<del></del>					
									-				· · · · · · · · · · · · · · · · · · ·
				——									

Ė	enginees 1 of 1 1 of 1	ING MEYE	LOPMENT CE	NTERCAEDO	PPOPI MAI	PTIN MISSILE	TUNNEL EACILIY TAIL EFFECTS PLATE DATA	LY (PHT)	AFRODYNAMIC SIND. TUNMEL(AT)
			625.				<del></del>	· · · · · · · · · · · · · · · · · · ·	
	S IFPT	273 U.96	2.5		SEE		<del></del>		
<u> St</u>	ALPHA	CNF	Çh	E3	* ACPF	YCPF		2> L	, op
1	24.17	lalage		La5643	0-0336	0.4914	<del></del>		
2	29.23	1.1672	0.0361 0.0354	0.5768	0.0309	0.4865			
<del></del> -		1.1756	0.9331	0.5608	0.0277	0.4857			
51	32.25	101742	0.0313	U-5008	0.0262	0.4654			
ь	33.26	1.1713	0.0303	0.5797	0.0254	0.4866			
_1	34.25	1.1006	0.4245	6.5759	0.0250	0.4677			
6	36.25	1-1711	0.0220	0.5572	0.0185	0.4843			
10	40.25	1.1597 1.1531	0.0151	0.5557	0-0146	0.4847	<del></del>		<del></del>
11	42.27	1.1557	0-0124	0.5538		0.4841			
15	44.27	1.1720	0.0074	J.5678	0.0980	0.4845			
13	46.28	1.1732		0.5595		0.4854			
1.	49.29	1.2021	0.3033	0.5833	7500.0	0.4652			
	50.29		10000		-0-6301	0-4848			
)6	52.31		-0.0030		-0.0024	0.+888			
17	_ <u>5</u> 4.31_ 55.33	l_c0l3_	-0.0113		-0.0046	0.4857			<del></del>
19	57.35		-0-0644		-0-0075	0-4911			
			<del></del>					<del> </del>	
					<del> </del>				
									·
						<del></del>			<del></del>
			· · · · · · · · · · · · · · · · · · ·		<del></del>				
							··		<del></del>
		·········						<del></del>	

1 58.1e 1.1273 -0.0043	E	ENGINED 1 OF 1 1 OF 1				PA	WTIN MISSILE	UNNEL FACILITY TAIL EFFECTS PLATE DATA	DATA	AERODYNAMIC -IND TUNNEL (41)
2 274 0.90 2.5 fil fREE  INT ALPMA CM+ CM CM RCPF YCPF  1 58.10 1.273 -0.6043 0.5502 -0.0034 0.4880  2 59.22 1.131+ -0.0050 0.5533 -0.0050 0.4889  3 66.21 1.1441 -0.0050 0.5551 -0.0089 0.4889  6 61.21 1.1305 -0.0102 0.5551 -0.0089 0.4804  5 62.22 1.1394 -0.0102 0.5551 -0.0089 0.4804  5 62.22 1.1394 -0.0107 0.5505 -0.0094 0.4915  7 64.23 1.1094 -0.0124 0.5017 -0.0138 0.4915  8 66.20 1.1031 -0.0197 0.5727 -0.0165 0.4928  8 66.20 1.1031 -0.0197 0.5727 -0.0165 0.4928  9 68.20 1.1785 -0.0232 0.5837 -0.0197 0.4953  0 70.24 1.1910 -0.0261 0.5922 -0.0219 0.4972  1 72.26 1.2337 -0.0314 0.6072 -0.0258 0.5002  2 74.25 1.2392 -0.0354 0.6207 -0.0298 0.5008  3 76.26 1.2543 -0.0301 0.6017 -0.0350 0.5036  5 80.29 1.2749 -0.0400 0.6010 -0.0209 0.5006  6 62.20 1.2749 -0.0400 0.6010 -0.0360 0.5036  5 80.29 1.2810 -0.0523 0.6014 -0.0066 0.5130  7 84.30 1.2940 -0.0523 0.6014 -0.0065 0.5136  8 8 63.1 1.2945 -0.0527 0.6723 -0.0479 0.5176  9 87.33 1.3003 -0.0043 0.6049 0.6059 0.5188					<del></del> ,			·		
1 58-10 1-1273 -0.0063			274 U.98	2.5	COME_TRAM				<del></del>	
7       59.22       1.1314       -0.0050       0.5533       -0.0050       0.4889         3       66.21       1.141       -0.0071       0.5559       -0.0063       0.4804         4       61.21       1.1305       -0.0107       0.5555       -0.0089       0.4801         5       62.22       1.1396       -0.0107       0.5545       -0.0108       0.4915         6       63.72       1.1024       -0.0124       0.5017       -0.0108       0.4915         7       64.23       1.1496       -0.0139       0.5421       0.4918         8       66.24       1.1031       -0.0127       0.5127       -0.0165       0.4924         9       68.24       1.1785       -0.0232       0.5237       -0.019       0.4972         10       70.24       1.1910       -0.0261       0.5922       -0.0219       0.4972         11       72.26       1.2137       -0.0314       0.6472       -0.0286       0.5002         12       74.25       1.2543       -0.0356       0.5036       0.5036         13       76.26       1.2543       -0.0466       0.6321       -0.0365       0.5036         15       80.27	OINT		_	-						
3 66.21 1.1341 -0.9071 0.5559 -0.0063 0.4901 4 61.21 1.1365 -0.0102 0.5551 -0.0089 0.4864 5 62.22 1.1396 -0.0107 0.5565 -0.0099 0.4901 6 63.72 1.1424 -0.0124 0.5617 -0.0138 0.4915 7 64.23 1.1496 -0.0139 0.5665 -0.0121 0.4910 8 66.24 1.1631 -0.0147 0.5727 -0.0165 0.4924 9 68.24 1.1785 -0.0232 0.5637 -0.0147 0.4953 10 70.24 1.1910 -0.0261 0.5922 -0.0219 0.4972 11 72.26 1.2137 -0.0314 0.6072 -0.0258 0.5002 12 74.75 1.2582 -0.0356 0.6200 -0.0269 0.5008 13 76.26 1.2543 -0.0060 0.6072 -0.0269 0.5008 14 78.20 1.2789 -0.0460 0.6060 0.6060 0.5036 15 00.29 1.2614 -0.0667 0.6530 -0.0360 0.5036 16 62.20 1.2643 -0.0523 0.6014 -0.0466 0.5136 17 04.30 1.2966 -0.0528 0.6028 0.5036 18 06.31 1.2965 -0.0528 0.6029 0.5188	<u> </u>									
6 63.22 1.139e -0.0102	5									
5 62.22 1.1396 -0.0107 0.5595 -0.0094 0.4915 6 63.72 1.1024 -0.0124 0.5017 -0.0138 0.4915 7 64.23 1.1096 -0.0139	•									
7 64.23 1.109£ -0.0139		62.22	1.1396	-0-0107	0.5545	-0.0094	0.4901			
8 66.24 1.1031 -0.0147 0.5727 -0.0165 0.4924 9 68.24 1.1785 -0.0232 0.5837 -0.0197 0.4953 10 70.24 1.1910 -0.0261 0.5922 -0.0219 0.4972 11 72.26 1.2137 -0.0314 0.6372 -0.0258 0.5002 12 74.25 1.2382 -0.035h 0.6200 -0.0289 0.5008 13 76.26 1.2543 -0.036h 0.6201 -0.0320 0.5008 14 78.26 1.2764 -0.0466 0.6321 -0.0320 0.5036 15 80.24 1.2814 -0.0487 0.6530 -0.0365 0.5036 16 82.26 1.2643 -0.0523 0.6614 -0.0366 0.5130 17 84.30 1.2994 -0.0523 0.6614 -0.0463 0.5130 18 86.31 1.2445 -0.0622 0.6723 -0.0479 0.5178 19 87.33 1.3003 -0.0664 0.6764 -0.0495 0.5188										
9 68.24 1.1785 -0.0232 0.5837 -0.0197 0.4953 10 70.24 1.1710 -0.0261 0.5922 -0.0219 0.4972 11 72.26 1.2137 -0.0314 0.6972 -0.0258 0.5002 12 74.25 1.2382 -0.0356 0.6200 -0.0289 0.5008 13 76.26 1.2543 -0.0356 0.6201 0.6371 -0.0320 0.5039 14 78.28 1.2787 -0.0408 0.64530 -0.0365 0.5036 15 80.29 1.2814 -0.6887 0.6530 -0.0368 0.5096 16 82.28 1.2843 -0.0523 0.6614 -0.0466 0.5130 17 84.30 1.2994 -0.0578 0.6614 -0.0468 0.5130 18 86.31 1.285 -0.0622 0.6723 -0.0479 0.5178 19 87.33 1.3403 -0.0644 0.6746 -0.0495 0.5188					<u> </u>	<u>-0.0121</u>				
10	-				0.5/2/	-0-0167				
11 72.26 1.2137 -0.0314 0.6572 -0.0258 0.5002  12 74.25 1.2582 -0.0358 0.6200 -0.0269 0.5008  13 76.26 1.2543 -0.0401 0.6321 -0.0320 0.5039  14 78.26 1.2789 -0.0400 0.6421 -0.0365 0.5036  15 80.27 1.2814 -0.0487 0.6530 -0.0360 0.5036  16 62.28 1.2893 -0.0523 0.6014 -0.046 0.5130  17 84.30 1.2990 -0.0574 0.6664 0.6664 0.5130  18 86.31 1.2985 -0.0622 0.6723 -0.0479 0.5178  19 87.33 1.3003 -0.0664 0.6745 -0.0495 0.5188					0.5922	-0.0219				
13 76.26 1.2543 -0.4401 0.6321 -0.0320 0.5039 14 78.28 1.2789 -0.0400 0.6040 -0.0365 0.5036 15 80.29 1.2814 -0.4887 0.6530 -0.0360 0.5096 16 82.28 1.2843 -0.0523 0.6614 -0.046 0.5130 17 84.30 1.2990 -0.0574 0.6664 -0.0443 0.5149 18 86.31 1.2995 -0.0622 0.6723 -0.0479 0.5178 19 87.33 1.3403 -0.4664 0.6746 -0.0495 0.5188										
16 78.28 1.27Ay -0.0466 0.6467 0.536 0.5036 15 80.29 1.2814 -0.6487 0.6530 -0.0360 0.5096 16 82.20 1.2893 -0.0523 0.6614 -0.006 0.5130 17 84.30 1.2940 -0.0576 0.6644 0.5149 18 86.31 1.2945 -0.6622 0.6723 -0.0479 0.5178 19 87.33 1.3803 -0.664 0.6746 -0.0495 0.5188										
15 80.27 1.2014 -0.467 0.6530 -0.0360 0.5096 16 82.20 1.2043 -0.0523 0.6614 -0.0006 0.5130 17 84.30 1.2950 -0.0574 0.6664 -0.0443 0.5149 18 86.31 1.2465 -0.0622 0.6723 -0.0479 0.5178 19 87.33 1.3403 -0.4664 0.6746 -0.0495 0.5188			1.2543	-0-2403	0.6371	-0.0320				
16 62.20 1.2043 -0.0523 0.6614 -0.0006 0.5130 17 06.30 1.2960 -0.0576 0.6664 -0.0463 0.5169 18 06.31 1.2465 -0.0622 0.6723 -0.0479 0.5178 19 67.33 1.3003 -0.0664 0.6746 -0.0495 0.5188										
17										
18 86.31 1.2995 -0.0022 0.6723 -0.0479 0.5176 19 87.33 1.3003 -0.0044 0.6746 -0.0495 0.5188										
	18		1.2945	-0.0022	0.6723	-0.0479	0.5178		-	
	19	87.33	1.3403	-0-6044	0-6746	-0-0495				
				•	•		•			
							<del></del>			· · · · · · · · · · · · · · · · · · ·
							<del></del>		<del></del>	
										•
							·····			
							•			
		<del>-                                    </del>			<del></del>		<del></del>	<del></del>		
		_								

E 1	0F 1 0F 1			THE STATE	MAI	KTIN MISSIL	E TAIL EFFECT	S DATA	AERODYNAM		
	JESI		P RX10-6 (			•					
	2	275 v.40	2.5	F11 F	REE						
	ALPHA	CNF			V 3		<del></del>	D 5			• 3
IMI .			CM	Cn	÷0.0503	YCPF					- ~
?	69.13		-0.0544		-0.0525	0.5175	<del></del>				
3	90.17		-Jat-60		-0-0556	0.5186					
•	91.16		-0.0712		-0.0561	0.5195					
5	92.18	1.2271	-0-0770	_4.6342	-0.0628	0.5168					
6	93.17		-0.0744		-0.064A	0.5164					
7	74.19		-0.4-31		-0.0676	0.5168					
8	96-19		-0464		-0.0716	0.5153					
9	96.19		-0-1550			0.5117	<del></del>		<del></del>	·	
	100.20		-0.0967		-0.0790	0.5101		·			•
	102.21 194.22		-0.1035 -0.1084		-0-0827 -0-0664	0.5050			<del></del>		
	106.23		-0-1134		E840.0=	0.5055					
	136.23		-0.1125		-0.0905	0.5049			<del></del>		
		1.2.2.			-0-0943	0.5018					
	112.25		-0.11e7		-0.0960	0.5031					
		1.2642			-0-1004	0.4997				• • •	
	116.27	1.2259	-0-12-6	9-0144	-0.1017	0.5008	,				
9	117.27	1,2207	-0-1276	0.6058	-0-1045	0.4963					
		<del> </del>		<del></del>		· <del>······</del>	······································		<del></del>		
		<del></del>						·-		<del></del>	-
										<del>.</del>	
									<del></del>		
						<del></del>					
	_							·			<del></del>
					<del></del>					····	
		<del></del>								<del></del>	

D ENGINE 1 OF 1		LOPHENT CI	ENTER (AED)	44	ULSION MINO TUNNEL FACILITY (PHT) RILA MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC WIND TUNNEL (AT)
	<u> </u>	PX10-6		SITION		
T ALPHA	CAF	CH	Ct		YCPF	
119.13		-0.1221		-0.1070 -0.1088	0.4954	
120-13		-0.1732		-0-1109	0.4933	
121.14	1.1315	-0.1268	0.5594	-0.1170	0.4944	
122-15		-0-1281		-0-1131 -0-1140	0.4925	
124.15	1.1.0/	-0.1311	2-5637	-0-11-9	0.4947	· · · · · · · · · · · · · · · · · · ·
126.15				-0-1175	0.4905	
126.17 136.18		-0.1354 -0.1-05		-0.1150 -0.1193	0.4935	
132.17	1_1615	-0-1422	0.5629	-0.1225_	0-4846	
134.18		-0-1433		-9.1236	U.4878	
136.19 138.20		-0-1474 -0-1457	0.5529	-0-1271 -0-1265	0.4632	
140-19	1_1555_	-9,1515	0.5506	-0.1313	0.4852	
142.20		-0.1503		-6.1300	0.4878	
144.22		-0-1546		-0-1350 -0-1404	0.4870	
147.22		-0-1634		-9-1414	0.4895	
		<del></del>				
						······································
			_			
· · · · · · · · · · · · · · · · · · ·						
	<del></del>					
						<del></del>

			فكن بنطبت يدهد	HIERCARD		TIN MISSIL	TUNNEL FACILITY (PUT) AFRODYNAMIC WIND TUNNEL (6T) E TAIL EFFECTS DATA
	1 OF 1					SELLITE	R PLATE DATA
	1631	PAPI MAC	H_EX10-6_4	CONF IRAN	SITION		
	5	277 0.98	2.5	-11 F	MEE		
POINT	ALPHA	CNF	CH	CH		YCPF	
<u> </u>	148-04		-0-1514		-0-1401	0.4680	
2	1-9-11	1.2053	-0.1688		-0.1400 -0.1410	0.4881	
•	151.12	1.1237			-0.1421	0.4873	
5	152-13	_1.1623_	-0-1657		-0-1-26	0.4884	
6	153,12		-0.1634		-0.1441	0.4874	
8	154.12		-0.1675		-0.1593	0.4955	
9	154-10_	0.4625	-C-1705		-0-1771	0.4981	
10	160.11		-0.1938		-0.2053	0.5098	
15 17	162-11		-0-1d51 -0-1724		<u>-0.2149</u> -0.2268	0.5075 0.5041	
13_	166-13		-0-1557		-0.2377	0.4994	
14	169.12		-0.1-04		-0.2529	0.4868	•
15	170-11	_ <u> </u>			-0-2712	0-4790	
16 17	172.13		-0.1027		-0.2990	0.4661	
18	176.14	0.1-61	-0.0569	0.0622	-0.3946	0201	
19	177.19	0.1169	-0.0452	0.0412	-0.3932	0.3583	
							•
	<del></del>			<del> </del>			
						<del></del>	
							·
			<del></del>				
							r
					<del></del>		<del></del>

•E	ENGINEE 1 OF 1 1 OF 1		LOPPENT C	ENTERTALO	MA	ULSION WIND TUNNEL FACILITY (PMT)  TIN MISSILE TAIL EFFECTS DATA  SPLITTER PLATE DATA	AERODYNAMIC WIND TUNNEL (AT)
		• •					
	7567	0407 #46	- Oblo-6	CUMF IRANS	17104		
		279 1.10			EE .		
VAT	ALPHA	CNF	CH	C+	# TCOF	YCPF	;; La _{1,2}
1		-0-0-5-		-0.0309	0.4365	0.6384	
5	-0.96	-0.0160	-0.0147	-0.0155	0.8959	0.4687	
_3	0.04	0.0001		-0.0028			
•	1.06	0.0-03	0.0000	0.0001	0.0012	0.2002	
<u> </u>	2.06	0.055		0.0233_ C.0387	0-1101	0.3381	
7	3.07	0.1303	0.0175	0.0539	0.1846	0.4052	
6	6.16	0.2071	0.0250	5040.0	0-1769	0.4355	
9	P.13	0.2414	0.4.39	0.1339	0.1506	D.4594	
10	10.14	0.3836	0.0515	0.1539	0-1344	0.4794	
11	11.27	0.439E	0.0539	0.2113	0.1225_	0.4805	
12	14.19	0.5035	0.0579	0.2557	0.0992	0.4897	•
13	16.21	C.6026	3-45-35	4.3375	0.0672	0.4945	
14 15	18.24	0.7760	0.0510	U.3846	0.0784	0.5008 0.5015	
15	22.79	0.9542	0.0608	0.4540	0.6638	0.5072	
17	24.30	1.0391	0.4582	6.5305	0.0560	0.5106	
10	26.34	1.1157	0.0557	6.5690	0.0499	0.5099	
16	27.39.	1,1093	0-0374	C.5567	0.0339	0,5023	<del></del>
					<del></del>		
					-		•
		_					
					•		•
		<u> </u>			<del></del>		
		Vir				-	
				<del></del>			
						······································	

E	1 OF 1		LOPMENT	enteriae	MAI	ALSION WIND TUNNEL FACILITY (PATENTIAL MISSILE TAIL EFFECTS DATE	MT) AERODYNAMIC MIND IUNNELLAI)
1_	<u>. oe. 1</u>					SPLITIER PLATE DATA	
- 64	TEST	PART MAC	H 6x10-6	CONF IRA	NSITION		
	5	250 1.10	2.5	F11	FREE		
THIC	ALPHA	CNF	CH	Cr	<b>ECPF</b>	YCPF	
2	29.25	1.1076	0.0312	0.5722		0.5016	
1	30.25	1.2196		G.6107		0.5006	
•	31.26	1.2502	0.0313	0.6291	0.0251	0.5031	
5	32.26	1.2001	0.0327	24500		0.4993	
6	33.18	1.3254	0.0325	0.6482		0.4972	
7	34.20	1.3/19	0.0141	<u>64563</u> 651660		0.4901	
•	39.29	1.9692	0.0161	0.60/5		0.4896	
10	40.30	1.4363	0.30-0	U.730A		0.4908	
11	_\$Le\$2.	1.0394	0.0627	وكنتاء نسب			
12	44.31	1.4567	-4.0045		-0.0031	0.4882	
13	46.32 48.33	1.0161	-0-0079 -0-0136		-0.0056	0.488	
15	50.34		0.0130 114		-0.0788	0.4ABA	
16	52.35		-0.0191		-0.0129	0.4902	
17	_54.37.				-0-0149	0.4903	······································
19	56.38		-0.0256		-0.0178	0.4909	
15	57.3b	1.5002	<u>-0.ú275</u>		-0-0184	0.4938	<del></del>
		-					
							<del></del>
						<del></del>	<del></del>
							·
							· · · · · · · · · · · · · · · · · · ·
							<u> </u>
						. <u>.                                   </u>	

		L			MA1	TIN MISSILE	TUNNEL FACILITY (PHT) TAIL EFFECTS DATA PLATE DATA	AERODYNAMIC WIND TUNNEL (4T)
		•						
	766	LPARI MAC	h 8210-6	CONE TOAM	SITION			<del></del>
	5	281 1.10			REE			
TNT	ALPHA	CNF	Сн	C#	Tros	YCPF		\$ 40°
1	59.18		-0.0261		-0-0178	0.4906		
Z	54.25		-0.0245	0.7227	-0-0194	0.4910		
3	60.25	1.9796_	9.0297_	4.7204	-0.0201	0.4910		
•	61.27		-0.9314	C.7301	-0.0211	0.4914		
5	62.20		-0au334	<u>0.7348</u>		0-4926		
0	63.76		0.0359	0.7399	-0.0239	0.4922		
7	66.27		-0.0379	C 7545	-0-0251 -0-0263	0.4564		
2	65.26				-0-0270	0-4988		
0	70.29		-0.0462	0.7036	-0.0302	0.4981		
1	72.20			¥-7695		0.4997		
2	74.30		-0.6526	6.7734	-0.0340	0.5027		
3	75.31	1,5947	-0-0569	0-77ea	-0.0369	0.5042		
•	78.31		-0.0601	U.7188	-0.0391	0.5066		
5	_F0.32		Qaubab .		-0.0420	0-5079		
16	62.33		-0.0683		-0-0-47	0.5108		
18	84.34 46.40		-0-0713 -0-0753		0~0 465	_0.5121		
9	87.35		-0-0780		-0.0499 -0.0518	0.5152		
	VIA			441147	-484-716	NATION		
	_							
								·
								,
								<del></del>
			•					
						<del></del>		
							<del></del>	<del></del>
					<del></del>			
								•

F (2

	1 OF 1 1 OF 1		FLOPSEN		4/	MTI 4 MISSI SPLITI	F TAIL SEE	FCTS DATA		AERODYNAMIC.	TWO TUNNEL	(AT)
				· <del>-</del>			·					
·	IESI 2	I.I SHS		F11	FREE					······································	•	-
NT .	ALPHA	CHF	CH	CB		YCPF						•
_	69.15		<u>-0.579</u>		5 -0.0530 5 -0.0556	0.5147	<del></del>					
	90.21		-0-00		7 -0-0576	0.5161						
	91.72		-9.064		1 -0.0605	0.5144						
	92.23		-0.05		<u>-0.0623</u> -	0.5146				<del></del>	•	<del></del>
	94.22		-0-030		FARRAS-	0-5146						
	96.23		-0.10		-0.0699	0.5125						
	98,23		-6.10		20-0722_	0.5112				···		<del></del>
	100.24		-0.110 -0.11		1 -0.0763	0.5085						
	104.25		-0.12		1 -0.0514	0.5055				· · · · · ·		
	106.26		-0-12		7 -0.0540		•					
	108.27		-0.13		8 -0.0658	0.5032						-
	110 <u>.26</u>		-0.13	540 <u>.767</u>	0 -0.0898 2 -0.0898	0.5017 0.5035						
	114.29		-0-13		0 -0.0916							
	116.30		-0.14	01 U.750	0 -0.0933	. 0.4994	•					
	117.32		-0-14	<u>05 0.796</u>	9 -0.0940	0.4998						
												•
				****		<del></del>			<del></del>			
												-
											· · · · · · · · ·	
		-										
										•		

GE	ENGINE 1 OF 1 1 OF 1	RING ULVE	LOPMENT C	ENTERLAED	PROP	ULSION @IND TURNEL FACILITY TIN #ISSILE TAIL EFFECTS DO SPLITTER PLATE DATA	(PHI) AERODYNAMIC HIND, TUNNEL (AT)
				•		Description of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of t	
	7651	PART HAL	H #X30-6	CONF TRAM	S1710W		
	5	283 1.10			REE		
DINT	· ALPHA	CNF	Сн	Ca	* RCPF	YCPF	,
<u>   i                                 </u>	110-06	1-5486	-0-1446	G.7960	-0.0952	0.4959	
2	119.17	1.4590	-0.1447	0.7449	-0.0965	0.4969	
-	121-16	1.4013	<u>-6.1951</u> -0.1473		-0.0974 -0.0994	0-4947	
	122.19	1.9739	-0-1-80	0.7285	-0-1004	0.4943	
6	123.16	1.4049	-0.1.66	0.7217		0.4927	
<del></del> _	124.1ë 125.30	1.9591	-0.1503 -0.1501		-0.1030	0.4922	
_5_	128-19		-0.1501 -0.1594		-0-1004	0.4918	
10	130.14	1.4545	-9.1575	0.7186	-0.1083	0.4941	
<del>!!-</del>	132.20		-0.1524		-0-1116	9-4922	<del></del>
13	134.20		-0.1651		-0.1130 -0.1150	0.4919	
14	136.21		-0.1043		-0.1171	0.4921	-
15_	140,23	1.9.103	-0-1712	0. 7006	-0.1197	0.4926	
16	142.23		-0.1729		-0.1727	0.4937	
18	144.24		- <del>0.1757</del>		-0.1272 -0.1326	0.4944	
19	167.25		-0.1757		-0-1355	0.4946	
							•
						<del></del>	
				,			1
						•	· · · · · · · · · · · · · · · · · · ·
						<del></del>	· · · · · · · · · · · · · · · · · · ·
		<del></del>	<del></del> -		<del></del>		
		•					

			··							•
<del></del>							<del></del>	· · · · · · · · · · · · · · · · · · ·		
	<del>, </del>	····	<del> </del>							
A D D D	CACTAGE	0140 4544	OPH NT	ENTERIAL	.C. BOOD	U 510N -1N0	TUNNEL FACTI	******	AERODYNAMIC .IND TUNNEL (AT)	
PAGE	1 OF 1		CHE PLICE.		MA	RTIN MISSILE	TAIL EFFECT	S DATA	ALAUU INAMA G	
AIRE						100				
	TEST	PART MAC	M. RX10-6.	CONF TRA	SITION					
		.584 1-10			HEE					
POINT	ALPHA 148-05	CNF	CH		4CPF -0.1353	YCPF				
	149.12	1.2652	-0.1/25	0.6265	-0.1367					
	150-11	1.2467				0.4949				
	151.12 152.13	1-1935			-0-1443	0.4980				
6	153.12	1.1444	-0.1559	0.5612	-0-1-76	0.4992				
	154.12 155.12		<u>-0.1650</u> -9.1662		-0.1525 -0.1666	0.4968		<del> </del>		
		0.7/93				0.5034				
	160.12		-0.1732			0.5020				
	164.12	0-5113	-0.1529	0.3594	-0-20 <del>-2</del> -0-2150	0.4925				
					-0.2244		<u> </u>			
								***		
									•	
								·		
			<del>-</del>							

•										• •		17
4040LD	CNGINES	The DEVA	. 004547 . 05	NTER LAED	F) 8939	u 5104 -7	NO TUNNEL FA	CT. TTV/B-T1	ACRAC	WNAME - THE	911111151 AA 93	- <del></del>
PAGE	1 OF 1	-ING MEYE	LUP TENLL LA	CHIER LAEL	<b>₽</b> A1	TIN MISS	ILE TAIL EFFE	ECTS -DATA	AERUL	ANTIC STATE	INMELICIALI	· · · · · · · · · · · · · · · · · · ·
SHEET	1.0E1					SPLIT	TER PLATE DA	TA				<del></del>
					-							
	TEST.	285 1-10	# PX10-6		SITION			<del> </del>			····	
POTHT	ALPHA	CNF	Cr -	CH		YCPF				<del></del>		
	168.12	0.5123	-0.1263	0.2461	-0.2464	0.4816		<del></del>	<del>_</del>			
3	170.13 172.13	0.4130	-0-1044	0-1420	-0.2661	0-4650						
•	174.14	0.2313	-0.0733	0.0990	-0.3167	0.4297						
<u> </u>	176-16 177-17	0.1162	-0-0530 -0-0424	0.0001	-0.3550 -0.3653	0.3680				· · · · · · · · · · · · · · · · · · ·	<del></del>	<del></del>
										· <u> </u>		
							•					
				-		<u> </u>						
						······································						
							<del></del>	<del></del>		<del></del> ,		
			<del></del>					<del></del>				
						· · · · · · · · · · · · · · · · · · ·						
										· · · · · · · · · · · · · · · · · · ·		
								· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·		
					•							
										···		<del></del>
				*			-					
												•
		-										
···		<del></del>	<del></del>									
								····		<del></del>	<del></del>	

TEST PART MACH RAID-6 CO. TRANSITION 2 267 1-20 2-5 F11 FREE  INT ALPHA CNF CH CE ACPF YCPF 1 -2.04 -0.4047 -0.4217 -0.0310 0.4647 0.781 2 -0.06 -0.0151 -0.0165 -0.0182 0.9026 1.2117 3 0.06 0.9131 -0.9055 -0.0000 0.0034 0.0176 -0.0064 4 1.07 0.0663 0.0000 0.0034 0.0176 -0.1064 5 2.08 0.9765 0.9976 0.0550 0.0595 0.1208 6 3.08 0.1074 0.0156 0.0057 0.1460 0.1653 0.3723 7 4.09 1.1412 0.0009 0.0557 0.1460 0.1888 8 6.12 0.2190 0.0795 0.0795 0.1460 0.1888 8 6.12 0.2190 0.0795 0.0795 0.1460 0.1888 9 H.13 0.3056 0.0360 0.127 0.1388 0.4279 9 H.13 0.3056 0.0380 0.127 0.1122 0.4491 10 10.16 0.3936 0.0380 0.127 0.0366 0.4639 11 12.16 0.4990 0.0003 1.2313 0.0255 0.4731 12 14.20 0.5016 0.0433 0.2780 0.0785 0.4781 14 16.25 0.7714 9.0429 0.3743 0.0556 0.4859 15 20.27 0.8556 0.037 0.0507 0.4856 16 22.31 0.9346 0.047 2.4602 0.0507 0.4877 17 24.32 1.0132 0.4050 0.0451 0.5077 0.5016		1 OF 1	RING DEVE	LOPPENT.C	ENTERLAED		TIN MISSIL	TUNNEL FACIL <u>*</u> T E Tail Effects R <u>Plate Data</u>		AFRODYNAMIC_WIND_TUNNEL_(AT
2 267 1,20 2.5 F11 FREE  INT ALPMS CMF Cn Cc ACPF YCPF  1 -2.09 -0.4917 -0.1217 -0.0310 0.4447 0.7281  2 -0.96 -0.4917 -0.1217 -0.0310 0.4447 0.7281  3 -0.96 -0.4917 -0.1217 -0.0010 0.4447 0.1281  3 -0.96 -0.4917 -0.0010 -0.0014 0.4917 -0.0316  4 1,07 0.493 0.0000 0.0040 0.0170 0.1823  5 -2.08 0.4075 0.9917 0.4025 0.4995 0.1288  6 3.08 0.1074 0.0150 0.000 0.1453 0.3723  7 4.09 6.137 0.0009 0.4037 0.1388 0.3773  8 A.12 0.2196 0.0795 0.037 0.1388 0.2276  9 B.13 0.3354 0.0386 0.127 0.01020 0.0450  10 10.10 0.3932 0.0386 0.127 0.0006 0.4430  11 12.18 0.4359 0.0386 0.1271 0.0006 0.4430  12 14.20 0.5016 0.0433 0.2718 0.0755 0.4731  18 18.25 0.7714 0.025 0.3774 0.0075 0.4850  18 18.25 0.7714 0.025 0.3774 0.0075 0.4850  18 18.25 0.7714 0.0026 0.3774 0.0075 0.4850  18 22.31 0.9366 0.0072 0.0072 0.0075 0.4850  18 22.31 0.9366 0.0072 0.0072 0.0087  18 22.31 0.9366 0.0072 0.0072 0.0087  18 22.31 0.9366 0.0072 0.0072 0.0087  18 22.31 0.9366 0.0072 0.0087 0.0087  19 27.37 1.1305 0.0081 0.0081 0.5085 0.0013  10 27.37 1.1305 0.0081 0.0081 0.5085 0.0085		****		H 0110.4	FD-E PHAN	17704	-			•
									<del></del>	
7 -0.46 -0.0151 -0.0165 -0.0162 0.9026 1.2117 3 0.06 0.00131 -0.0005 -0.0004 0.0176 -0.1023 4 1.07 0.0463 0.0004 0.0004 0.0004 0.0176 0.1623 5 2.08 0.0155 0.0116 0.0605 0.0004 0.0178 0.1623 6 3.08 0.1074 0.0156 0.0000 0.1453 0.3723 7 2.09 1.0215 0.0209 0.0057 0.1000 0.1283 6 6.12 0.2196 0.0795 0.037 0.1000 0.0279 9 8.13 0.3055 0.0306 0.127 0.0000 0.0279 9 8.13 0.3055 0.0306 0.127 0.0000 0.0403 11 12.18 0.0000 0.0000 0.127 0.0000 0.0403 12 14.20 0.5016 0.0033 0.2710 0.0705 0.4701 13 14.22 0.0516 0.0033 0.2710 0.0705 0.4701 14 18.25 0.7714 (0.025 0.3774 0.0067 0.4850 15 20.27 0.0510 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	POINT	ALPHA	CNF	Cn	Cé	ACPF	YCPF		, ,	
3 0.08 0.0131 -0.0055 -0.0006 0.0030 0.0010 0.01023 1-07 0.00603 0.0000 0.0000 0.0033 0.3723 5 2.08 0.0265 0.0016 0.0000 0.0000 0.01453 0.3723 7 3.09 0.1074 0.0156 0.0000 0.1457 0.1460 0.3723 8 6.12 0.2196 0.0000 0.0000 0.0000 0.0270 0.1480 0.2729 9 8.13 0.3054 0.0000 0.0000 0.0000 0.0270 0.0000 0.0270 10 10.16 0.3000 0.0000 0.0000 0.0000 0.0000 11 12.18 0.0000 0.0000 0.0000 0.0000 0.0000 12 14.20 0.5016 0.0000 0.0000 0.727 0.0006 0.0000 12 14.20 0.5016 0.0000 0.727 0.0006 0.0000 13 16.25 0.7714 0.0000 0.0000 0.0000 0.0000 14 18.25 0.6714 0.0000 0.0000 0.0000 0.0000 15 20.27 0.0000 0.0000 0.0000 0.0000 0.0000 15 20.27 0.0000 0.0000 0.0000 0.0000 0.0000 17 24.12 0.0000 0.0000 0.0000 0.0000 0.0000 18 26.37 1.0000 0.0000 0.0000 0.0000 0.00000 19 27.37 1.1305 0.0000 0.0000 0.0000 0.00000								<del> </del>		
- 1.07 0.0463 0.0000 0.0000 0.0000 0.1653 0.1623 5 2.08 0.0174 0.0156 0.0000 0.1453 0.3723 7 - 2.09 0.1274 0.0156 0.0000 0.1453 0.3723 7 - 2.09 0.1274 0.0156 0.0000 0.1453 0.3723 9 8.13 0.3054 0.0145 0.0145 0.0145 0.0000 0.1453 9 1.13 0.3054 0.0145 0.0145 0.0122 0.4629 10 10.16 0.359 0.0300 0.127 0.01122 0.4629 11 12.18 0.4190 0.0003 0.2113 0.1625 0.4731 12 14.20 0.5016 0.0033 0.2180 0.0175 0.4701 13 16.22 0.6151 0.0056 0.0033 0.2180 0.0145 0.4850 14 18.25 0.7114 0.0000 0.0000 0.0000 0.0000 0.0000 15 20.27 0.8552 0.0000 0.0000 0.0000 0.0000 0.0000 15 20.27 0.8552 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000										
5 2.08 0.6765 0.0076 0.6255 0.6995 0.2266 0.5955 0.2266 0.3080 0.1076 0.00150 0.30723 7 4.09 6.1232 0.0000 0.1257 0.1260 0.2986 0.2079 0.2037 0.1386 0.2079 0.2037 0.1386 0.2079 0.2037 0.1386 0.2079 0.2037 0.1386 0.2079 0.2037 0.2038 0.2079 0.2038 0.2038 0.2038 0.2079 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038 0.2038										
7 4.09 (6.1837 0.0000 0.1000 0.1000 0.1000 0.4279  8 6.12 0.2196 0.0000 0.1000 0.1122 0.8001  10 10.16 0.3936 0.0336 0.172 0.0136 0.4225 0.4731  11 12.16 0.4800 0.0033 0.2131 0.4255 0.4731  12 14.20 0.5016 0.0033 0.2100 0.0705 0.4701  13 16.25 0.511 0.0000 0.0000 0.0000 0.4850  14 10.25 0.7714 0.0000 0.0000 0.4850  15 20.27 0.8552 0.6051 0.0037 0.4052 0.4050  16 22.31 0.0000 0.0007 0.3000 0.5000 0.0077  17 24.32 1.0132 (1.380 0.5000 0.5000 0.0077  18 26.37 1.0000 0.0001 0.5070 0.0013 0.5015  19 27.37 1.1305 0.0000 0.5510 0.0013 0.5015  19 27.37 1.1305 0.0000 0.5550 0.5000			0-0765	0.0076	U-0245	_0.4995	0.3208			
8										
9 8.13 0.3654 0.4363 0.1372 0.1122 0.4649  10 10.16 0.3535 0.0360 0.127 0.0366 0.4639  11 12.18 0.4990 0.0903 0.2113 0.6225 0.4731  12 14.20 0.5016 0.0433 0.2780 0.0765 0.4781  13 14.25 0.6151 0.0433 0.278 0.0566  14 18.25 0.6151 0.0433 0.0556 0.4853  15 20.27 0.4855 0.658 0.472 0.605 0.4927  16 22.31 0.9366 0.4072 0.605 0.4927  17 24.32 1.6132 0.3551 0.3571 0.3570 0.0013  18 26.37 1.906 0.4551 0.570 0.0013  19 27.37 1.1305 0.4922 0.5655 0.4375 0.5802										
12 14 0.4819 0.4913 0.2113 0.6225 0.4731 12 14.20 0.5916 0.0433 0.2110 0.0745 0.4761 13 16.22 0.6751 0.0356 0.2274 0.0657 0.4855 14 18.25 0.7714 9.4229 0.3743 0.0556 0.4853 15 20.27 4.8554 0.6588 0.4214 0.6536 0.4927 16 22.31 0.9346 0.0472 0.4662 0.4503 0.4977 17 24.32 1.0132 (.1989 0.4062 0.4067) 0.5470 0.0413 0.5015 18 26.37 1.0960 0.4041 0.5470 0.0413 0.5015 19 27.37 1.1305 0.402 0.5555 0.4375 0.5302			0.3054							
12 14.20 0.5010 0.0433 0.2780 0.0745 0.4850 14 16.22 0.6711 0.0450 0.3274 0.0067 0.4850 15 16.25 0.7714 0.0450 0.323 0.0556 0.4853 15 20.27 0.8554 0.6555 0.4723 0.0556 0.4927 16 22.31 0.9346 0.0472 0.45082 0.0504 0.4977 17 24.32 1.0132 0.0450 0.45082 0.0504 0.4977 18 26.37 1.0906 0.0451 0.5470 0.0413 0.5015 19 27.37 1.1305 0.0452 0.5555 0.0375 0.5502	10									
14 16.25 0.0714 9.0425 0.3743 0.0556 0.4853 15 20.27 9.8554 0.6654 0.4214 0.6556 0.4853 15 20.27 9.8554 0.6654 0.4214 0.6556 0.4857 16 22.31 0.9366 0.0472 0.4662 0.6504 0.4977 17 24.32 1.0132 (.1469 0.4651 0.5470 0.0413 0.5015 18 26.37 1.0956 0.0451 0.5470 0.0413 0.5015 19 27.37 1.1305 (.0424 0.5655 0.0375 0.5502	11									<del></del>
14 18-25 0.7714 9.0429 0.3743 0.0556 0.4853 15 20.27	13.									
16	14									
17 24.32 1.0132 ()ee9 0.5082 0.0077 0.5016 18 26.37 1.0900 0.0451 0.5470 0.0413 0.5015 19 27.37 1.1305 ()e22 0.5655 0.0375 0.5302	15									
18 26.37 1.0406 0.0451 0.5470 0.0413 0.5015 19 27.37 1.1305 6.0424 0.5655 0.0375 0.5302								•		
	18							,		
	19									
					•					
										<del></del>
				<u> </u>				·	·	
									•	
· · · · · · · · · · · · · · · · · · ·							<del></del>			
			•							-
							·			
	_									

E !	ENGINEER 1 OF 1 1 OF 1	RING WEYE	I OPMENI C	ENTERLAED	-446	RTIM MISSILI	JUNNEL FACIL Tail Effect Plaie Data	S-DATA	AERODYNAMIC_HIND_IUNNEL_CAT
					<u>:</u> _				
	7 <u>F51</u> 2	28= 1.20			SITION REE				
INT	ALPHA	CNF	CH	Ç2	xCPF	YCPF			
<u> </u>	26.17	1-1567	0.0410	u-5607	0-0354	0.5007			
Ş	29.25	1.1955	0.0361	0.5463	0.0319	0.4986			
4	31.27	1.2367	0 <u>_</u> 0_0366_ 0.0331	0.6203	0.0268	0.5016			
5	32.27	1.2671	0-0269	0.0203	0.0228	0.5016			
6	33.29	1.2454	0.0275	0.6444	0.0212	0.4975			
1	39.29	1.3221	0.0225	u-6539	0-0170	0.4946			
8	36.31	1.3615	0.0206	0.6720	0.0153	0.4934			
9	38.32	1.3535_	0.0142	0.6568		0.4914	<del></del>	<del></del>	
10 LL	40.32	1.4375	0.0021 -0.0019	0.7602 0.7127	0.0015	0.4871			
12	44.33	1.4744	-0.0069	0.7246	-0.0046	0.4915	<del></del>		
13	46.35	1.4852	-0-0105	0.7246		0-4913			
1 •	44.35	1.5031	-0.0144		-0.0099	0-4897		-	
15	_50.36_	1.5653_			-0-4114	0.4898			<del> </del>
17	52.37	1.5169	-0.0211		-0.0139 -0.0164	0.4906			
18	56.40		-C. 0289		-0.0189	0.4921	<del></del>	<del></del>	
19	57.42		-0-0318		-0-0208	0.4920			
						***************************************			
								<del></del>	
							·		
			-						•
							<del></del>	<del></del>	
						···	<del></del>		
		<del> </del>							<del></del>
		<del></del>							

16E	I OF		LGPYENT	CENTER LAED	44.6	HTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC #IND TUNNEL(4T)
				CUME TRAN			
	2	289 1.20	2.5	F11 F	HEE		
POINT	ALPHA	CNF	CH	Cr	KCPF	· YCPF	52 ₇
	_56_19		-0-u320		-0-0209	0.4927	
5	59.77		-0.0348		-0.0227	0.4927	•
	61.27		<u>-0-0-1</u> 0060-0-		-0.0216 -0.0233	0.4965	
5	02.26		-0.0395		-0-0254		
6	63.26		~0.u+00		-0.0257	0.4957	, , , , , , , , , , , , , , , , , , , ,
	64.28		-0.0907		-0.0260	0.4972	
8	66.29		-0.0443		-0.0781	0.4975	
9 10	<u>68.29</u> 70.30		<u>-0.0465</u> -0.0495		-0 <u>-0295</u> -0-0312	0.5092	
11	72.30		-0-1525		-0-0332	0.50ZA	
_1 <u>2</u> _	74.31		-0.0551		-0.03-9	0.5033	
13.	75.33		-0.U=97		-0-0377	0.5045	
14	74.33		-0.0038			0.5063	
<u>_15_</u>	_6C_33	1.5767	Qayle 74	6.5029	-0-0+27	0.5092	
16 17	64.35		-9.0/27 -0.0736		-0.0461 -0.0476	0.5104	
18	86.38		-0.0401		-0.0523	0.5183	
19	87.37		-0-0520		-0.0535		
_				•		<del></del>	······································
						<del></del>	·
						•	
	<del></del>						
						•	
							•
							•
							,
							·

GE	1 OF 1	ING DEVE	LOP-LNT CE	MIERKAED		TIN MISSI	E TAIL EFFEC	TS DATA	AERODYN	MIC_=IND_TUMNEL(4)	<u> </u>
EI_	1_0F1_	<del></del>				SPLIŢII	ER PLATE DATA		~ <u>~~~~~</u>		
	7447	PART MAI	M RX10=5 C	Out Ton	E1110-						
		290 1.20			REE		····				
TALO	ALPHA	CMF	Сн	СH		YCPF					
<del>-}</del> -	78-10	1.530r 1.547¢	-0.4526 -0.0861		-0.0540	0.5189 0.5184	· · · · · · · · · · · · · · · · · · ·	<del></del>	<del></del>		
3	10.21	1.3216			-0.0596	0.5197					
•	41.22	1.5240	-0.0745	0.7917	-0.0518	0.5176					
5	92.23	1.5305			-9.06-1	0.5162					
7	99.23	1,5344			-0.0562	0.5152					
8	96.25		-0-1102		-0.0708	0.5124					
9_	98.25	1.5566	-0-1117			0-5112				<del></del>	
10	100.25		-0.1213		-0.0771	0.5092					
	102.25_		-0-1236		-0-0708	0.5079		<del></del>			
12	104.2e		-0.1790 -0.1320		-0.0520 -0.0535	0.5049					
14	105.29		-7-135-		-0.0945	0.5053				<del></del>	
15	109.34		0_1355	Q_7959_		0.5047				·	
16	112.29	1.5776	-0.1393	0.7429	-0.0683	0.5025					
	119-31-		-1-1-30	C. 7922	-0-0905	0-5012				<del></del>	
10	116.32		-0.1426		-0.0913	0-5018	•				
14	111,33	1.2011	-0-16-3D	W. (523.	-1011454	. #=3011					
				<del></del>	·						
					<del> </del>		<del></del>	<del></del>	··		
						•					
			· · · · · · ·								
										·	
									·		
				•		·					
		<del></del>	<del> </del>		<del></del>		······································				
										· <del></del>	

						•		
					•			
							<del></del>	
		ING DEVE	LOPMENT CE	MTERLALD	C) PRUP	ULSION I	NO TUNNEL FACILITY (PHT)	AERODYNAMIC WIND JUNNEL (AT)
	1 Of 1 1 OF 1				MAI	9714 4155) <u> </u>	ILE TAIL EFFECTS DATA	
	1651	PART MAC	₩ RX10-6_0	ONE TRAN	SITION			
	5	291 1.26			HEE			
DINT	ALPHA	CNF	Ch	CH		YCPF		
<del>]</del>	118.10 119.17	1.5576	-0.1474	0.7689	-0-0935 -0-0455	0.4969		
	120.10	1.5923	-C-1981	0.7055		0.4963		
•	121.16	1.5377	-0.1442		-0.0973	0.4956		
5	122.18	1.5264	-0.1503 -0.1522		-0.0965	0.4941		
7	124.14		-0.1526		-0-1001	0.4942		
B	126.19	1-5103	-0.1544	U.7464	-0.1023	0.4942		
9	124.19		-0:1593		-0.1055	0.4947		
1	130.19		-0.1597 -0.1632		-0.1064 -0.1092	0.4942	-	
15	134.21		-0-1054		-0.1116	0.4940		
13	136.22	1.4744	-0-1076	J-7782	-0-1138	0.6940		
14	134.22		-0.1700		-0.1169	0.4920		
16	140.23		-0.1713_ -0.1774		-0-1206 -0-1261	0.4929	<del></del>	
17	199.24		-0-1826			0.9977		
18	146.20	1.3207			-0.1410	0.5005		
19	147.26	1.4726	-0.1H30	0.640	-0-1416	<u>_0_5020</u>		
								• •
					•			

							··.				1200	٠.٠.
			•				<del> </del>	<del></del>			<del></del>	···
<del></del>		<del></del>			<del></del>							<del></del>
										**-		
		ING DEVE	LOPSENT	CENTERLAEI	PROP	ULSION NIN	D TUNNEL FA	CILITY	·	ERODYNAMIC	ND TUNNELLAT	1
GE 1 OF EFT 1 OF							LE TAIL EFF ER PLATE DA					
	557	DART MAG	. 0.14-4	CONF TRA								-
		565 1.50			FREE	•			<del></del>			<del></del>
OINT ALP		CNF	Cm	C→		YCPF						
1 148.			-0.1825		-0.1432	0-4981						
2 149.			-0.1504		-0.1449 -0.1508	0.4989						
4 151.			-0.1647		-0.1521	0.5023			1	·	<del> </del>	
5 152.	12			_0.5720.	-0-1538				<del></del>			
6 153. 7 154.			-0-17H6		-0.1562 -0.1591	0.5002						
8 156			-0-1700		-0-1500	0.4959						
9 158.			-0.1624		=0.1718	0.4941			•			
10 160.			-0.1521		-0.1770	0.4919						
11162.					0.1922_	-0-489B						
12 164. 13 166.			-0.1305 -0.1197		-0.1900	0.4623						
14 168			-6.1069		-0.2120	0569				•		
15 170		0.0110	-0.0542	7-1953	-0-2292	0.4435				<u> </u>		
16 172			-0.0786		-0.2512	0.4302						
17 174					-0.2799	0.3916				<del></del>	·	<del></del>
18 176. 19 177.			50+0.0- 51E0.0-		-0.3027 -0.3206	0-3415						
1710.		NAT THE	-040376		-44.32.00		<del></del>				<del></del>	
									11			
<del></del>							<del></del>	<del></del>		·	<del></del>	
							·					·
							W.A.				<del></del>	
									<del></del>	<u> </u>		
								-		<del></del>	<del></del>	
						•						
			= =				-					
							<del></del>				·	

			<del></del>							<del></del>
ARNOLD	ENGINEE	PING CEVE	LOPMENT C	ENTERLAED	CI PHO	ULSION VI	NO TUNNEL FACI	LLITY(PHI)	AERODYNAMIC WIND JUNNEL (41)	
PAGE	1 OF 1				H	AHTIY MISS	ILE TAIL EFFEC	CTS.OATA		
SHEET	1 OF 1					SPLII	TEH PLATE DATA	·		<del></del>
								<del></del>		·
	TEST	PART PAC	H #X10-6	CUNF TRAN	51TIO4					
	5	293 1.20	2.5	F11 F	HEE					
POINT	ALPHA	CNF	CH	Co	ACP	F YCPF		<del></del>		
	177.98	0.luge	-0.0336	U-0295	-0.3350	0.2932	·			
2	179.05	0.0675			-0.3505 -0.3224					•
•	141.06	0.0020	-0.0007	-0.0169	-0.3+62	-A. 2293				
5	182.06	-0.0272	0.067	-0.0271	-0.3181	0.9963				<del></del>
7		-0.0276	0-0200	-4-0-07	-0-3071	0.6474				
8					-0-2709					
								<del></del>		
								<del> </del>		
										<del></del>
		<del></del>			· · · · · · · · · · · · · · · · · · ·	<del></del>				
	-				-					
				····						
<del> </del>			· · · · · · · · · · · · · · · · · · ·							
		· · ·						· .=		
							<del></del>			
								- <del></del>		<del></del>
				-						
									· · · · · · · · · · · · · · · · · · ·	
		· · · · · · · · · · · · · · · · · · ·	•					····		

LET	1 OF 1			L. I. I. I. I. I. I. I. I. I. I. I. I. I.	P. P. P. P. P. P. P. P. P. P. P. P. P. P	ALTIA MISS	ND TUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA	AFRODYNAMIC WIND TUNNEL (AT
	i_OFi					SPLIT	TER PLATE DATA	
					-	<del> </del>		
	IESI	JAM. IRAB UE.1 405		COMF TRANS	<u>sition</u> Kee		<del></del>	
101NT	ALPHA	CWF		CH	ACPI	YCPF		
1		-0.0-30			0-9158			
2		0.0044		-0.0164 -0.0029	1.0561	1.7495		
	1.06	0.0566	0.U302	0.0102	0.0637	0.1805		
_5	2.07	0.0071	_0.0461	<u> 1-0261</u>	0.0595	0.2992		
6	3.07	0.1211	0-6114	0.0-08	0.0971	0.3366		•
	6-12	0.1537	0-0526	0.0553	0.1175	0.3705		<del></del>
9	_ 5.13_		0.4299	0.1337_	0.09aZ_	0.4400		
10	10.15	C-3400	0.3305	0.1756	0.0783	0.4508		
11	12-16	0-9146	0.0315	0.2228	0.0557	0.4653		
13	13.31	0.530+	0.0326 N.0344	0.2=64 0.3126	0.0615	0.4681		
10	14.25	0.7485	0.03-5	0.3572	0-0461	0.4773		
15_	20.28	0.0375		0.4428	0.0417	0.4809		
16	24.33	0.4164	0.03.0	0.4419	0.0369	0.4809 0.4886	•	
17	26.3P	1.0665	0.6353	0-5228	0.0365 0.0331	0.4904		
19	27.38				0-0333	0.0943		
							•	•
			***************************************					
					<del> </del>			<del> </del>
								······································
						<u></u>		

	1 OF 1	- ING DETE	LDP#ENI CI	EN IER Lativ	MA	ULSION WIND TUNNEL FACILITY(PWT) HTT: MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC INO TUNNEL (41)
<u></u>	I VE I					SPLITTER PLATE DATA	<del></del>
			H. BA10-6.				
	e	29- 1.30	2.5	F11 F	HŁE		
INT	ALPHA	CNF	CH	C ₇₇	#CPF	YCPF	
1	29.17	1,1199	0-9413	9-5501	0.6760	0.4912	
2	24.25	1.1566	0.0313	6-2045	0.0270	0.4922	
3	_32-20_	laleti	<u>Caudey</u>	_9.2067_	0.0260	0.4939	
	31.28	1.2193.		6.5445	0.0234	0.4917	
_	37.24	1.2774	0.u25#	0.6325	2020*0	0.4949	
•	34.24	1.3.03	0.5229	0.6410	0.0202	0.4979	
8	30.30	1.3351	0.0170	0.6545	0.0128	0.4902	
9	35.32	1.3657	Carlel	1.6594	0.0103	0.4890	
0	49.33	1.3955	6.0058	0.0011	0.0042	0.4681	
L	42.34	1.4223	-0.0009	_ Gabyy4_		0.0916	
5	44.34	1.4500	-0.5069	0.7566		0.4867	
3_	45.31	1-4051	-0-ulio	5.7177	-0.0075	0-4899	
5	47.47 50.30	1.0000	-0.0136 -0.0185	0.7224	-0.009Z -0.0124	0.484.0 FRA4.0	
6	52.39	1.5124	-0.3217		-0.0143	0.4910	· · · · · · · · · · · · · · · · · · ·
<del>.</del> _	54.44	1.5151	2450-0=		-0-0158	0.4944	
6	56.42	1.5239	-0.6281		-0.0164	0.4955	
19	57.43		-0-1367	2.7580	-0.0201	0.4964	
						<del></del>	
			<del></del>				
						•	
			<del></del> .				
		<del></del>					<del></del>
				<del></del>			
						•	
						······································	

	I OF I		TOPPENT CI	MIERIAED	<b>4</b> ∆	ATIN MISSILI	TUNNEL PACILITY (PHI) = E TAIL EFFECTS DATA R_PLAIE DATA	AERODYNAMIC WIND TUNNEL (4T
					P 2 2 2 2 1 1		<u> </u>	
	5	SAV 1.30	<u> </u>		REE		•	
NT	ALPHA	CNF	Сн	Co		YCPF		· · · · · · · · · · · · · · · · · · ·
	58.2C 59.77	1.5274	-0-04-8	<u> </u>	-0-022A	0-5001		
	60.20				-0.0229			
	61.28	1.5444	-0.0395	6.7648	-0.0756	0.4983	-	
_	63.29		-0.001t4 -0.0409		0 <u>-0267</u>	0.4985		
,	64.29		-0.0463	0.7/12		0.4966		
)	66.30	1.5651	-0.0445	6.7854	-0.0274	0.5008		
	68.31		-0-096b		-0-0287	0-5031		
1	70.32		-0.0443		-0.0315	0.5042		
	74.32		-0-0504 -0-0546		-0.0322 -0.0348	0.5070		
1	76.33			1.7470	-0.036A	0.5095		
	78.34		-0.0517		-0.0345	0.5113		
25	80.35 61.46		-0-0549		-0-0417	0.5169		
	84.38		-0-0411		-0.0430 0.0453 -			
	66,36	1.5326	-0.9/63	u. 7 × 36	-0.0511	0.5178		
	67.36	1.5/90	+6_val9	C.7934	-0-0535	0-5188		<del></del>
		•						
					<del></del>	<del></del>		
	·							
						- — —		
_							<del></del>	<del></del>
							<del></del>	
_							<del></del>	

AGE	ENGINEED 1 OF 1 1 OF 1	ING DEVE	LOPMENT CE		MA	NISION WIND TUNNEL FACILITY (PWI) PTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC MIND TUNNEL (AT)
		PARI_PAG 257 1.3u	P B		5111 <u>0</u> N		
POINT	2 ALPHA	CNF	CH	F11 F		YCPF	
	88.18	_	-0.0860	_	-0.0562	0-5194	
5	89.17		-0.0665		-0.0578	0.5181	
	90.22		-0.0497 -0.0406		-0.0585 -0.0592	0.5178	
5	92.23	1.5251	-0-0940		-0.0592	0.5191 0.5185	
6	93.23	1.5291			-0.0536	0.5171	
	94.23		-0-4452	Alk Tar	-0-66-9	0.5169	
Ą	96.24	1.5354	-0.1676		-0.0701	0.5146	
<del>9</del>	99.25		-0-1119 -0-1161		0.0721 -0.0750	0.5153 0.5142	
ii	102.26		-0-1225		-0-0788	0.5141	
12	104.26		-0.1273		-0.0817	0.5138	
_13	106.28		-0-1294		<u>-0.0628</u>	0.5135	
10	108.29		-0.1341		-0.0854	0.5091	
<u>15</u> 16	112.36 112.30		-0.1356 -0.1371		-0.0561 -0.0473	0.5076	
iř	114.32		-0.1370		-0-0:19	0.5076	
18	116.33	1.5556	-0.1432	0.7867	-0.0918	0.5044	
	117.33	1.5544	-0-1445	0.765H	-0-0929	0.5056	
							·
							•
				-			
							· · · · · · · · · · · · · · · · · · ·
						"	
							······································

E	EMFINE 1 OF 1 OF	1	FF 064F41 C	ENTER(AED	MA	TIN MISSIL	) TUNNEL FACILITY (PHT) LE TAIL EFFECTS DATA R. PLATE DATA	AERODYNAHIC .WIND .TUNNEL.14T
		7 DADT na	4. 5430-4	5W 5 730				
	153	29A 1.3	LH PX10-5 u 2.5		STITUS		· <del></del>	
INT	ALPHA		Cr	C-		YCPF		
	127.12		-0.1479		-0.0956	0-5002		
•	121.16		-0.1465 -0.1515		-0.0957	0.4982		
<del>-</del>	123.19		-0.1511		-0.0989	0.4970		
_	124.19		Cal521_			0.4973		
8	120.15	1.5070	-0.1567	6.7516	-0.1013	0.4987		
9_	124.20		-0.1572		-0-1049	0.4958	<del></del>	
0	132.21		-0.15~4 -0.1614		-0.1077 -0.1095	0.4954		
با اک	134.21		-U-10133		-0-1116	0.4950		
3			-0-1676		-0.1150			
•	134.22	1.4336	-0.16F8	6.7365	-6.1177	0.4927		,
_	190.24		-0-1714		-0-1226	0.4941		
16	142.25		-9-1775		-0.1296	0.4937		
rī —	122,20		-0.1794			0.4968		
19	146.20		-0.1743 -0.1796		-0.1392 -0.1418	0.4976		
	- 44   44		-9111				,	
		<del></del>					· <del></del>	
						<del></del>		
							· · · · · · · · · · · · · · · · · · ·	
							•	
								•
		<del></del>					<del> </del>	
						. ———		

indlu Mge Meet	1 OF	ering Geve 1 1	LOPMENI C	ENTEHSAED	C) PROPI	ULSION WIND TUNNEL FACILITY (PWI) HTIN MISSILE TAIL EFFECTS DATA SPLITTER PLATE DATA	AERODYNAMIC WIND TUMMEL (AT)
							· · · · · · · · · · · · · · · · · · ·
	TES	T PAPT MAL	H PA10-6	CONF. TRAN	SITION		
-	5	249 1.30			HEE		
VINT	ALPHA	CNF	CH	Ce	ACPF	YCPF	<del></del>
_i_	198-07		-0-1799		-0-1436	0.4975	·
2	149.15		-0.1763	9.0056		0.4970	
3'	150-11		-Ual761_		-0-1972	0.4947	
-	151.12		-0.17j4 -0.10pd		-0.1466 -0.1499	0.4952 -0.4952	
- 3	153.12		-0.1662		-0.1521	0.4931	
	154.13		-0.1036		-0-1547	0-4915	
0	156.13	0.4773	-0.1552	i017	-0.1588	0.4926	•
9	155.13			0.4916		0.4881	
10	160.14		-0-1362		-0.1674	0.4789	
<del>_1</del> 1	162-13		<u>-0-1207</u>		0-1738	_0_0721	
12	164.14		-0.1191 -0.1063	0.3060	-0.1904 -0.1977	0.4636 9.4617	
14	168.14		-0-04-3		-0.1986	0.4559	
	170-15		-0.4553		-0-2167	0.4362	· · · · · · · · · · · · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _ · _
16	172.15		-0.0736	U-1274	-0-2-10	0.4171 -	
_17	_174+10		-0.0594		0.2600	0-3908	·
16	176.17				-0.2804	0.3512	
19	117.17	0_1167	-0-0332	0.0346	-0.2949	0.2967	
						•	
						·	
						<del></del>	
		<del></del>		<del></del>		<del></del>	<del></del>
							· · · · · · · · · · · · · · · · · · ·
						•	
			•				
							<del></del>
						•	
							<del></del>
			<del></del>				

## APPENDIX C TEST 3

E E	1 NF 1			LANGLEY H	ESEAHLH C	ENTEH (NAS MAHTIN M	A) ISSILE TAI	UNITA IL EFFECTS	MY PLAN N UATA	IND TUNK	EL (UPST)		
				<del></del>		<del></del> .	· - · · <del>- · · - · · - · · · · · · · · ·</del>	<del></del>		<u>.</u>			
	TEST	PAUT U	441U-	6 PAI	CUNF	L MEL	1 UELZ .	JEL3 DEL4	THANSIT	UN			
	<u> </u>	10 5.	3.0	<u> </u>	1 v v f 35_ 0	• 0	0 0	0	FIXE				
12×I	ALPHA	HFTA	CV	CL 4	CY	CLY	CLL	CA	CAR	CAF	KCP		
¬ı —	-3.58		-0.70.73						0.1234	0.5660	-2.4292		
<del></del>	-7.02	C 1	-10-24/5		-1-02/1		-0.0652	J. 3846 5. 3862	C-1207		-2.5272		
	0.10	Carl.	-6.71-7			-0.0136		0.3477	v.1143		-2.6831 -8.0433		
<u> </u>	-i.i.	7, 1		-6.3061			-0.7656	3.3656	0.1192	0.2664	-1.9079		
6	2.15	Lat	0.7750	-(.m50+	-0.0070		-0.061H	0.3649	u.1193		-2.1497		
7	4.64	6.0		-1.7792		U		7.3430	0.1276		-5.5527		•
	4.37	(		-22			-0.0637	)117	0.1432		-2.1895	·····	
y lj	10.51	C. v1		-3.7.95			-0.0577 -0.0577	0.4235 0.4350	0.1602		-2.0822 -1.9553		
<u> </u>	17.17	0.01		-500050				8450	0.1517		-1.0122		
15	14.47	Cosi		-4.11375				0.4755	0.1490		-1.7030		-
13	17.19	1.01		-6.4931				0.4315	0.1490		-1.6385		
14	14.45	2.00		-1.1127				03+5	0.1461		-1.5944		
15	21.55	Love		-4.100,				J.4417	0.1420		-1.55/9		
16 17	0.09	6.03	-0.457	-9.474				0.4504	0.1361		-1.5518 -6.1032		
• •					-200151	764.731	-007077		****	0.2030	-011036		
											<del></del>		
							·- <del>-</del>			·	·		
								<del></del>				<del></del> -	~
								- <u>-</u>					
_									<del></del> <del></del> -	<u> </u>			
			•									-	
				<del></del>					·				
							<del></del>						

					<u> </u>							
	1 OF 1			LAYOLEY A	ESEMBLA CI			UNITA		INU TUNN	EL (UPST)	-
r. T	1 0 1											
_	7551	1441 -	ALT HATTE	e Pel	LUMF	L LEL	1 666	DEL3 DEL4	THANSITI	UN		
	3		36 4.0		1-0+35 0		0 0	00				
	ALPHA	of la	C'4	CLA	CY	CFA	CLL	CA	CAH	CAF	ACP:	
1	- 4.56	, ue			-0.6793		-1-8469	7.3805	0.1255		-7.4308	<del></del>
7	-2-31	1001	-0-41c	1.14(1	<b>=(.</b> 9259 =0.0251	6-0000	-0.0mm	7.354	4-1166		-2.5263 -2.6467	
.7 •	1, 60 9	0.01	-6.12.1		-0.4445	1-0429		0.3001	V-1195		-6.4580	•
5	1.1.	0.51		- '		0.0503	-9.0641	C-3432	0.1191		-1.9624	
<u> </u>	2.14	0.91		-: - 40 36			-2.0724	\$1 × E • 6	0.1130_		-7.1671	
7	4.27	6.0	027-	-1 -r6/2			-0.0563	dbnE.c	0-1279		-2.2633	
<u> </u>	5.3t	-0-01		-3./51-			-0-6647	0.3463	0.1377		-2.2125 -2.1304	
6	17.59	-6.01		-407140			-0.0547	0.3998	0.1418		-1.9629	
1	12.75	-( 0]		-4.1757		V-1327	-4.0570	1.3469	C.1419		-1.7953	~
2	14.94	-6.01		-5.4524		C.1376	-0.0595	10-044	0.1504	U.2590	-1.6930	
3		-6-115		-00/293			-0.U50d	0.4057	0.1490		-1.6166	
<u>*</u>	19.45	-0.02	4,44,	-7.7)4-	-0.0905		-0.0611	0.4075	3-1-61		-1.5770 -1.5703	
3 5	23.74	-0.06		-10-2/64			-3.0595	0.4117 0.4196	0-1-60		-1.5086	
ý—		LONA			-0.0347		-0.0050		0.1207		-5.1047	***************************************
								•				
				<del></del> -			<del></del>	<del></del>				<del></del>
		· · ·										
						-						
										-	<del>_</del>	
											<del></del>	
					·							

	1 OF 1			LawoLEY W	ESEAW(n C		ASSILE TA			INU TUNK	LL (UPWT)		
	resi	PAHT &		h Phl	Curef	i vki	I CELZ		THANSIT				
		<u>. (1 č.</u>	ro 3.4	-5.0 M	1 • uf 35 0	.0	0 0	<u> </u>	FIXE	<u> </u>			
141	ALPHA	HETA	CN	CL.	Cv	CLY	CLL	CA	CAH	CAF	ACP		
1	-3.51	0.01	-1.7001		-0.0045	0.0013		V-3551	0-1523	0.2528	-2.1680		
7	-7-06	( , )	-1.4/14	701 4	-0.0104	1.0222	-0.0547	0.3515 J.3541	0.0475	0.2540	-2.7559 -7.4559		
-	0.1	0.0	-9-0477		-0.0176	0.0210	-C.0541	0.3561	0.1006		-4.2223		
<del>-</del> -	1.13	U.U -	3.1550		-0.0145	(00) 15	-0.754A	0.3533		0.25+1		<del></del>	
6	2.12	0.0	Acsf.	-1 -774"	-9.611M	r.01e3	-0.0545	0.1520	0.0976	U.2550	-1.0241		
7 -	4.74	0.0	5.162	-1.3470	-0.5177	0.0261	-3.(539	0.35-4	6.1034		-1.9336		
H	4, 10	0.7	1.1564	-2.61/1	-0.0007	C . T. 4 3 P	-3.3492	3.3654	0.1103	0.2551	-1.9040		
4	4.00	-(1	1.5471	-5-4-3-	-6.611.	7.03.7	(1002	2.35/2	0.1136	0.2536	-1.8163		
U	102	-6.01	7.1914		-6.6225	0310	-0-6470	0.3565	0.1135		-1.6901		
1	12.44	-1.001		1/13	-6.0444	1.129	-1.6446	V.3739	C-1136		-1.5085	•	
<u>3</u> -	14,-1	-0.01	3.17.1	-4.7541	-0.6744	6.6776	-0.6508	3.3759	6.1152_		-1.5185		
•	10.40	-6.71	****	-+ 1 5 1	-11-11-77	(.5475	-C.0532	0.3740	0.1166		-1.4890 -1.4870		
<del>-</del>	21.63	-0.05		-7.5.16.1	-0.07e0		-V-055n	0.453h	0.1136		-1.5012		
6	23.70	-0.03		-6.9665	-0.6455		-0.0542	0.4159	0.1104		-1.5295		
7	0.9e	0.01	-0.0373	0.1713	-0.0172		-0.0551	0.3571	4501.0		-4.7196		
				_									
		-						•					
						<del></del>							
			<del></del>										
							· <del></del>			<del></del>			
								·					
											<del></del>	<del></del>	
						<del></del> -							
			<del></del>										

GE E E T	1 OF 1			LANGLEY M	ESE_HCH C		A) ISSILE TAI			IND TUNN	EL (UPat)	
	11,51	PEGT P	ALP VATUE	h Pn1	LUNA		.l itle .	EL3 VÉLG	TRANSIT!	ION		
		22 4.	90_ j•u	0.0.4			0 0		F TYE			
1410	ALPRA	HE TA	(4	CL"	<u>CY</u>	. CLW	cr <u>r</u>	CA	C44	CAF	XCP	
1	-3.73		-1.07246			-0.0-12		9.35A7	0.1040		-2.1440	
- 1	-1.15	( · · · ·	-0.43/6	*****	1.0007	-1.01570	-1.0547	0.3555	0.1008		-7.2724 -7.4343	<del></del>
-	-0.07	0.0	-0.5-21	(ialoue	-4-0166	-0.0455	-0.0552	0.35mm	0.1007		-4.2860	•
-5	0.46	0.91	7.1434	-1,00 100	T-7. 0110"	-0.6248	-0.25.7	v. 3561 "	0.1005		-1.4200	
6	1.96	0.6	6.333-	-3.403.	-d. Uü34	-1.03-1	-6.0544	0.3564	5660.0		-1.8085	
7	4.10	0.0				-0.0246		0.3641	€-1055		-1.6932	
8	K.1+	0.0		=7 a 1270		-6.774		0.3745	0.1119		-1.8565	
4	÷ 31.	0.01	1764			- • :53		1. 3474	J.1163		-1.7706	
10	10.34	- 10 · 0 F		3.55	<u>-0.023+</u>	-1.orec	-0.0503	. 0.3574	1199		-1.6836	<del></del>
11	12.54	0.01	2.4444			04-22		0.3849	9.1107		-1.6003	
12	14.45	0.61	3.177-	-4 7 -		-1.05-1	-0.6475	0.3962_	0.1151 0.1119		-1,5381	
14	14.16	0.UC	4.376]			-0.000		0.4076	6.1117		-1.4970 -1.4792	
15	e1.11	U.UE				-v.1315		U-4138	1.1639		-1.4726	
16	23.30	5.0c					-0.0446	0265	3.0459		-1.4855	
17	-0.00	U. 31					-0.0512	0.3565	0.1023		-3.5449	
•								******				
										-		
										<u> </u>		
					<del> </del>						<del></del>	
								•				
-							<del></del>				<del></del> .	
												<del></del>
												<del></del>
				_								
				<del></del>							·	

1 -3.61 0.01 -0.333 0.927 -0.0156 0.0126 -0.0325 0.2602 0.0576 0.2126 -1.7491 2 -1.36 0.0 -0.3132 0.957 0.0025 -0.0177 -0.0321 0.2769 0.0676 0.2043 -1.8163 3 -0.36 0.01 -0.157 0.0159 -0.0125 0.0177 -0.0318 0.2763 0.0676 0.2043 -1.8163 4 -0.36 0.01 -0.0155 0.0055 -0.0125 0.0175 -0.0318 0.2763 0.0676 0.2764 -7.5333 5 1.76 0.0 0.1673 -0.2227 -0.0200 0.0175 -0.0366 0.2758 0.0676 0.2076 -7.5333 5 1.76 0.0 0.1673 -0.2227 -0.0200 0.0175 -0.0366 0.2758 0.0676 0.2022 -1.3869 6 2.22 0.0 0.0135 -0.4739 -0.0135 0.0135 -0.0308 0.2779 0.0076 0.2103 -1.5116 7 4.32 0.0 0.4135 -0.4739 -0.0135 0.0130 -0.0308 0.2779 0.0076 0.2166 -1.5636 6 6 3.3 0.0 0.4472 -1.1150 -0.0295 0.0370 -0.0356 0.2665 0.0677 0.219 -1.5235 9 7.63 0.0 0.0 0.0 0.0077 -0.0155 0.0173 -0.0356 0.2666 0.0677 0.219 -1.5235 0 10.50 0.0 1.7773 -2.4416 -0.0255 0.0173 -0.0379 0.3349 0.0690 0.2567 -1.4002 1 17.57 -0.01 2.227 -3.1164 -0.0214 0.0376 -0.0379 0.3316 0.0698 0.2655 -1.3546 2 16.67 0.0 2.7110 -3.6763 -0.064 0.0370 -0.0641 0.3316 0.0696 0.2655 -1.3546 3 10.77 -0.01 3.2750 -0.0507 -0.0537 0.0506 0.0506 0.2666 -1.3553 3 10.77 -0.01 3.2750 -0.0507 -0.0537 0.0506 0.0506 0.0576 0.2568 -1.3738 5 296 0.01 5.7100 -7.5745 -0.0577 0.0756 0.0556 0.0576 0.2568 -1.3738 5 296 0.01 5.7100 -7.5745 -0.0577 0.0757 0.0556 0.0576 0.0591 0.3509 -1.4537				!	LANGLEY H	ESEARCH C	ENTEN ( -AS	41	UNITA	HY PLAN	IND TUNN	EL (UPUT)	
TFS  Part =20m =210=0   Fm1   CUMF   L   Utl1   Utl2   Dtl3   Dtla TMANSITION					<del></del>		MAUTIN M	ISSILE TA	L EFFECTS	DATA		<del></del>	
3												·	
3 23 3 0 23 3 0 23 3 0 2 45 0 2 46 0 2 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0													
OINT ALPHA   META   CN   CL   CV   CLN   CLL   CA   CAB   CAF   RCP     -3.0    0.01   -0.4353   C.7363   -0.6150   0.0124   -0.0325   0.2602   0.0576   0.2126   -1.7491     -1.54   G.0   -0.3137   0.0157   -0.0127   -0.0321   0.2763   0.0076   0.2093   -1.8163     -0.19   0.0   -0.0157   0.0557   -0.0127   -0.0318   0.2763   0.0076   0.2087   -1.9904     -0.19   0.0   -0.0175   0.0557   -0.0126   0.0175   -0.0318   0.2750   0.0676   0.2087   -7.5333     -1.74   0.0   0.16.3   -0.2227   -0.0200   0.0135   -0.0364   0.2750   0.0676   0.2087   -1.3608     -1.74   0.0   0.16.3   -0.4739   -0.0136   (.0130   -0.0308   0.2779   0.0676   0.2108   -1.5116     -2.22   0.0   0.3135   -0.4739   -0.0135   (.0130   -0.0308   0.2779   0.0676   0.2108   -1.5116     -3.32   0.0   0.497   -1.715   -0.0179   0.0277   -0.0345   0.2895   0.0677   0.2108   -1.5636     -3.32   0.0   0.497   -1.515   -0.0179   0.0277   -0.0345   0.2895   0.0677   0.2219   -1.5235     -3.33   0.0   0.0   0.1773   -2.4016   -0.0275   0.0176   -0.0345   0.2895   0.0677   0.2219   -1.5235     -3.33   0.0   0.0   0.1773   -2.4016   -0.0275   0.0176   -0.0376   0.3549   0.0676   0.2665   -1.4082     -3.47   0.0   2.7110   -3.4743   -0.044   0.0370   -0.0441   0.3316   0.0476   0.2465   -1.3546     -3.47   -0.01   3.270   -4.5000   -0.0427   0.0500   0.0501   0.3702   0.0076   0.2668   -1.3538     -3.47   -0.01   3.270   -4.5000   -0.0427   0.0500   0.0500   0.0076   0.2668   -1.3538     -3.47   -0.01   3.270   -4.5000   -0.0437   0.0150   0.3702   0.0500   0.0076   0.2668   -1.3538     -3.47   -0.01   3.270   -4.5000   -0.0577   0.0500   0.0500   0.0076   0.2766   -1.3766     -3.47   -0.01   5.7100   -0.0737   -0.0577   0.0560   0.0100   0.0500   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076   0.0076													
-3.4  0.01			27 30	99 3.0	4700 0	140133 0	• •	<u> </u>		KARY	<u> </u>		
2 -1.5# G.0 -0.3132													
3													•
5 1.74 U.0 0.1c.3 -(-2220.0200 0.0135 -0.0364 0.2758 0.0676 0.2062 -1.3869 6 2.22 0.0 0.3135 -0.6739 -0.0135 (.0130 -0.0308 0.2779 0.0676 0.2103 -1.5116 7 4.32 U.0 0.6492 -1.1150 -0.0295 0.0270 -0.0354 0.2692 0.0576 0.2166 -1.5634 6 6.34 0.0 0.0 0.0000 -0.0179 0.027 -0.0345 0.2696 0.0677 0.2219 -1.5235 9 7.43 U.0 1.3014 -1.0000 -0.0255 0.0360 -0.0379 0.3349 0.0699 0.2267 -1.6452 10 10.50 0.0 1.773 -2.4616 -0.0275 0.0173 -0.0379 0.3349 0.0690 0.2351 -1.6402 11 17.57 -0.01 2.227 -3.(144 -0.0214 0.0374 -0.0420 0.3163 0.6698 0.2465 -1.3544 12 16.67 0.0 2.7110 -3.6763 -0.0644 0.0374 -0.0641 0.3316 0.0676 0.2665 -1.3544 13 15.77 -0.01 3.2701 -4.5000 -0.0437 0.0379 0.0506 0.0676 0.2568 -1.3553 14 14.40 -0.01 3.2701 -4.5000 -0.0537 0.0546 0.0676 0.2568 -1.3736 15 20.00 -0.01 5.7160 -7.5795 -0.0597 0.0596 0.0100 0.0591 0.3509 -1.4537	•	0.46	n.91.	-1012-1	20.4124	-0-0167	5. 11.5	-0.031H	0.0763	0.0076	3.20m7	-1.9704	
6													
7 4.32 U.U 0.6442 -1.6150 -U.0295 U.0370 -0.0354 U.2762 0.0576 0.2166 -1.5636 6 6.34 0.U 0.6444 -1.5615 -U.0179 U.077 -0.0345 0.2696 0.0677 0.2219 -1.5235 9 7.43 U.U 1.511 -1.575 -0.0255 0.0257 0.0370 U.0990 0.227 -1.5235 10 10.50 0.U 1.773 -2.4416 -0.0275 0.0173 -0.0379 0.3344 0.0696 0.2351 -1.4002 11 17.57 -0.01 2.227 -3.0144 -0.0214 0.0374 -0.0420 U.3163 0.0698 0.2465 -1.3544 12 14.67 0.U 2.711U -3.4743 -0.0444 0.0374 -0.0450 U.3163 0.0698 0.2465 -1.3544 13 15.77 -0.01 3.2701 -4.5007 -U.0327 U.0145 -0.0501 U.3504 0.0676 0.2528 -1.3738 14 14.49 -0.01 3.2701 -4.5007 -U.0327 U.0145 -0.0501 U.3504 0.0676 0.2528 -1.3738 15 20.04 -0.01 3.4 -0.0577 0.0577 0.0574 -0.0550 0.0012 0.3762 0.0634 0.3564 -1.4035 16 23.17 -0.01 5.7140 -7.5744 -0.0547 0.0694 -0.0556 0.4100 0.0591 0.3509 -1.4537				0. 1135	4734	-0.0135	(.0130						
9			_	20.4045	-1.(15)	-0-1-295					0.2166	-1.5634	
10 10.50 0.0 1.773 -2.4616 -0.0275 0.0173 -0.0379 0.3349 0.0696 0.2351 -1.4002 11 17.57 -0.01 7.7257 -3.(144 -0.0214 0.0374 -0.0420 0.3163 0.6696 0.2465 -1.3544 12 14.67 0.0 2.7110 -3.4743 -0.044 0.0370 -0.0441 0.3316 0.0676 0.2465 -1.3553 13 15.77 -0.01 3.770 -4.5007 -0.037 0.0195 -0.0501 0.3702 0.0676 0.2678 -1.3736 14 14.67 -0.01 3.770 -0.0577 0.0577 0.0576 -0.0501 0.3702 0.0676 0.3688 -1.4035 15 20.97 -0.01 4.479 -0.3711 -0.0333 -0.0370 0.0560 0.4100 0.3762 0.0436 -0.3764 -1.4035 16 23.17 -0.01 5.7140 -7.5795 -0.0597 0.0596 0.4100 0.0591 0.3509 -1.4537				1-3-14	-1-2015	-0.0175					0.2219	-1.5235	<del></del>
12 16.67 0.0 2.7110 -3.4763 -0.0644 0.0370 -0.0641 0.3316 0.0676 0.2640 -1.3553 13 15.77 -0.01 3.7703 -4.5005 -0.0437 0.0195 -0.0501 0.3504 0.0676 0.2628 -1.3738 14 14.45 -0.01 3.4 3 -5.4734 -5.0557 0.0754 -0.0561 0.3702 0.3643 0.3068 -1.4035 15 20.45 -0.01 4.45 4 -0.3711 -0.0371 -0.0371 -0.0547 0.0056 0.4100 0.3764 0.3764 -1.4276 16 23.17 -0.01 5.7144 -7.5794 -0.0547 0.0096 -0.0556 0.4100 0.0591 0.3509 -1.4537	1	0.50	0.0	1.17/3	-7.4616	-C.C275	0.0173	-0.0379			0.2351	-1.4002	
13 15.77 -0.41 3.7701 -4.5005 -0.0437 0.4145 -0.0501 4.3504 0.0676 0.2578 -1.3736 14 14.45 -0.61 3.4 3 -5.4734 -5.4557 (.4754 -0.054) 0.3762 0.3634 0.368 -1.4035 15 24.45 -0.41 4.45 9 -0.371 -0.4333 -0.5154 -0.0556 0.4100 0.3764 -1.4276 16 23.17 -0.41 5.7144 -7.5744 -0.4597 0.0696 -0.0566 0.4100 0.3591 0.3599 -1.4537													
16 14.46 -0.61 3.4 3 -5.4734 -5.4557 (276 -0.654) 0.3762 (268 -1.4035) 15 24.46 -0.01 4.47 4 -0.371 -0.4333 -0.5160 -0.6560 0.475 0.462 0.3764 -1.4276 16 23.17 -0.01 5.7140 -7.5744 -0.0547 0.0646 -0.0556 0.4100 0.3539 -1.4537				3.275)	-4.5005	-4-3-37	- 6.0145						
16 23.17 -0.01 5.71-J -7.5790.0597 6.0696 -0.0566 0.0100 6.0591 0.3509 -1.4537	1	H.4P	-0.61	3 3	-5.4734	-7.05-7	1. 37-4	-0.0541	0.3762	0.0434	0.3048	-1.4035	
				6.44 9	-10-3771	-0.4333							
												·	
												•	
				<del></del>	<del></del>				<del></del>				<del></del> .
						<del></del> :							
· · · · · · · · · · · · · · · · · · ·													
						<del></del>			<del></del>				
·													
·		<del></del> -											
						·							
<del> </del>	_												
				<u></u> .	<del></del>		· - ·						

	1 OF 1			Laidley M	ESEARCH C			UNITAL IL EFFECTS		IND TUNN	EL (UPaT)	-	
	TEST		ach Hali-		CUNF			DEL3 DEL4	THANSIT				
	3	24 3.	45 3.0		1=0F35 0	0.0	0 0	0 0	FIXE	)			
2014T	ALPHA	HETA	<u>(N</u>	CL×	CA	CL ~	CLL	CA_	CAR	CAF	ACP		
3	-3.51 -2.10	0.0	-0.5537	0.545n		-0.0500		0.2772	0.0576		-1.7446		
-5	-1.07	0.0	-0.1715	0.3375		-(-(-1)		0.2737	0.0677	0.2060	-1.9371	-	
•	-0.02	6. u	-G.01 ++			-J.C??#		0.2732	0.0677		-4.0990	•	
5	1-03	6.0	C. 15cu	-0.2023	-3.0009	-0.07.50	-0.0311	0.2741	0.0677		-1.3309		<del></del>
9.	2.01	0.61	0.2857	-0.4372		-0.0006	-0.0309	0.2763	0.0676	0.2057	-1.5249		
7	4.11 6.15	0.0	0.6244	-1.4420		-6.6637		0.2403	0.0676	0.2164	-1.5354 -1.4898		
9	4056	0.0	1.4510	-1. 7545	11-60-15		-0.03nb	0.2442	6.3698		-1.4352		
10	10.30	0.0	1.752-	-2.4027		-0.0445	-0.0427	0.3075	0.0496		-1.3712		
11	17.34	0.01	2.14-4	-6.4657	-4-0117		-9.0415	0.3167	0.0698		-1.3293		<del></del>
15	14.4F	C.01	2.67.5	-3-4-100		-0.3556	-0.0455	0.3310	0.0576_		-1.3092		
13	16.58 15.71	0.01	3.1500	-4.4134	-0.0011	-1.1245	-0.0547	U.3470 C.3441	0.0655		-1.3141 -1.3236		
15	20.7E	0.01	406475	-70/000	-0.0011		-0.0405	0.3819	0.0591		-1.3412		
16	55.49	0.01	4.9700	-0.7000		-0.07.02		0.4009	6.05.4		-1,3655		
17	-0.01	0.0	0.0005	0-1543	-0.0631	-de0.0364	-0.0357	0.7736	6.0634	6.5105	109.6080		
16	-0.01	0.0	0.0005	5-15-3	-0.0031	-0.0354	-0.0367	0.7 <u>736</u>	0.0655	0.5081	108.6000		
								•					
					• • • •								
									<u> </u>				
							•						
		<u> </u>		· · · · · · · · · · · · · · · · · · ·				• -					<u> </u>
								<del></del>					
	·												
						•					•		
					<del></del> -		<del></del>	<del></del>				<u>.</u>	
•			-										
									<del></del>			<del></del>	
				<del></del>								<del></del>	
	•												
						•					·		
									•				
			,										

	1 OF 1					ENTERCAS MARTIN M		IL EFFECTS	DATA				
EET	1 OF 1												
		<del></del>								<del></del>			
		2011290						54.71					
	3		63 3.0		1-0F35 0		0 0	VEL3 VEL4					
			03 340		140733 (	,,,,			. 73461	·			
OINT	ALPHA	HETA	CN	CL H	CY	CLN	CLL	CA	CA9	CAF	KCP .		
5 1	-1.75	0.0	-0.4575	0.6599	0.0042	-0.0772		0.2572	0.0498		-1.4424		
3	-0.73	6.6	-0.0977	L-1744		-0.01-0		107442	0.0498		-1.8207		
	0.34	6.0	0.04-9	-0.6290	F200.0			0-2444	0.0495	0.1990	-0.5922		
5	1.35	0.0	U-1-4-5		-0-0257		-0.0330	0.2505	0.0525	7.1900	-1.1224		
<del>,</del>	- <del>? • 35</del>	0.0	7.5541	-6-4053	-6.0011	-0.0159 -0.0137	-0.0318	0.2501	0.3525 _ 0.525 _		-1.1981 -1.2706		<del></del>
ė	6.46	0.5		-1-21-5	-6.0027		-9-0376	0.2639	0.0525	0.2114	-1.2645		
4	A.53	0.0				-6.0763		0,2737	0.0525		-1.2395		
10	10.56	0.0			-0-0150		0.0423_	0.2843	0.0525		-1.2173		
-11 12	12.61	0.0	7.0461	-7-5645	0.0042		-0-0479	0-246H	0.0525		-1.2328 -1.2601		
13	15.76	0.0		-3.HY4.		-6.1133		0.3244	0.3496		-1.3054		
10	1A.Ac	16.7			-6.0107	-4-1054	-0.0444	0.3474	0.0470	0.2954	-1.3550		
15	50.30	6.01				-1.9440		3.3634	0.043		-1.3971		
16	23.07	0.01		-0-0133		-0.0664		0.3453	0.0399		-1.4303 -0.2745		
•••	••••		***************************************	-000.03	***************************************		00000			0020-0	-002143		
									<del></del>				
				-									
										<del></del>			
•													
									·				
												· · ·	
						<del> </del>			<del></del>	<del></del>			<del></del>
								- <del></del>					<del> </del>

	1 OF 1			LAMGLEY A	ESEARCH C	ENTERLAS M ALTHAM	A) ISSILE TA	UNITAR	DATA	IND TUNN	EL (UPat)	
									· 			
			151 196 5			-					<u> </u>	
	TEST 3	54 4°	43 3.0		CUNF		0 0	DEL3 DEL4				
						·						
101	4LPHA -2.97	P.O	-n.4534	CLM	CY	-0.0C-0	CLL -0-0345	CA 5.2559	CAB	CAF	*1.4489	
Ž	-1.47	0.5	-0.2347		-0.0050		-9.0349	0.7516	0.0496		-1.6037	
3	<i>■1.</i> , 46	0.0	-0.05-5	7.100+	-0.0119	C-U1-0	-0.0337	5.2207	0.0444	J.2009	-1.8592	- '
	0.59	0.0	0.0504		-0.0190	0.0275	-0.0333	<u> </u>	0.0525	J-1994	-0.3769	
5	2.60	0.0	0.3244		-0.0265		-0.0330	0.2521	0.0525 0.0525	0.1996	-1.0909 -1.1665	
7		0.0	0.5350	-0.3020	-0.0119		-0.0366	0.2540	0.0525		-1.2608	<del></del>
8	6.72	0.6	1.000	-1.7670	-0.6106	4.0166	-0.0375	5.7647	0.0525	ē.2122	-1.2925	
4	5.70	(1-11		-1.0000		-0-0021	-0.C+37	0.2710	0.0725		-1.2669	
11	12.47	-0.VI		-7-1413	-0.0274	-3-0450	-0.0427	0.2840°	0.0525	7.2315	-1.2526 -1.2721	
12	14.95	0.0		-3.4513			-0.0474	0.3112	0.0525 0.0525	0.2587	-1.3281	
13	17.91	-0.41	3,1,76	-4.3523	-9.072-	-0.00-0-	-0.0530	0.3320	4.4448		-1.3914	
1+	19.11	-0.01	3.7/146	-4.336	-0.0749	-0.0005	-6.7545	0.3504	U-0470	0.3034	-1.4403	
15.	21.13	-0.01				-1.00054		G-3744	0.0443		-1.4796	
- <u>16</u>	23.29	-0.01	0.0547	-7.623.1	-0.0312	-0.0099	-0.0562	0.3973 0.250A	0.0416	0.3557	-1.5978 -0.3543	
	<b>4.</b> 37			-446114	0,0100		-0.0333	***************************************		4.2030		
			•									
				·····	-							
								<del></del>		<del></del>		<del>-:</del>
								-				
				<del></del>				<del></del>	<del></del> .			
				<del></del>								~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
						<del></del>			ww- <del></del>	<del> </del>		
					<u> </u>							

	1 OF 1						ISSILE TAI			······································			
	7EST		ALM HATU-0		CONF 140F35 0		0 -50	0 -20		N			
INT	ALPHA	BETA	CN	CLM	CY	CLA	CLL	CA	CAR	CAF	XCP		
J	-1.66		-2-21/52			-0.0210		1.1550	0.1481		-3.6149		
₹	-2.13		-2-11-2		-0.0763	-0.0321	-0.0474	1.0540	0.1525	0.9447	-3.8166	<del></del>	<u> </u>
•	-0.01		-1.4470		-0.0503	0.0010		1.0106	0.1553		-4.1557		
5	-0.03		-10-519			-0.0171		1.0117	0.1553	0.8564	-4.1590		
6	1.04		-1.7000			-0.02-3		0.9701	C-1580		-4.3849		
7	5.43		-1.51.59			-0.0119		0.9379	0.1623		-4.6558	•	
<del>- 3</del>	6.25		-1-1-47		-0.0409	0-6166	-0.0501	0.7647	C.1680		-5.5341 -7.8036		
10	9.37	-	-0.1735					0.6851	0.1693		-24.5326		•
11	10.49	0.02	0.4325		-0.056+		-0.0577	0.4057	0.1652	0.4405	8.1409		
12_	12.66	0.02	1.1375			-0.0644		0.5303	0.1708	0.3595	1.9391		
13	14.44	0.02	111-			-0.0716		0.4542	U.1709	0.2833			
14 15	17.00	C. U.3	3.1240		-0.0375	-0.1933	-0.0462	0.3986 V.3528	0.1666	0.2278	0.0617 -0.1750		
16	21.44	0.03	3.71/1			-G.1570		0.3156	0.1610		-0.3001		
17	23.72					-0.1501		5005.0	C.1636		-0.4282		
_I#	-0.03	0.01	-1-9054	7.4203	-0.0085	-c.0710	-0.0472	1.0100	0.1554	0.8546	-4.1567	<del></del>	
			<del></del>					·					
_						_							
							<del></del> _						
									<del></del>				
	•											· · · · · · · · · · · · · · · · · · ·	
											<u> </u>		
							<del></del>					<del></del>	
							·						

.,,;

The second section

2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 10 10 11 12 12 14 13 16 14 15 21 15 21	7EST 3	PETA	CN -7-301e -2-030v -1-6-72 -1-6-71 -1-6-71 -1-7-50 -2-4-74	0.8 dl CLM 7.5603 7.101- 6.70dy 6.3910 6.013c 5.7073 4.3535 3.4640 6.4922 1.0491	-0.0032 -0.0131 -0.0232 -0.01077 -0.0296 -0.0296 -0.0237 -0.0231 -0.0313	CLN -0.0275 -0.0753 -0.0753 -0.0543 -0.0543 -0.066 -0.0745 -0.0745 -0.0477 -0.0467 -0.0469	CLL -0.0434 -0.0427 -0.0427 -0.0460 -0.0455 -0.0553 -0.0581	CA 1.0304 0.9761 0.4384 0.4379 0.4576 0.4576 0.4579 0.512 0.7447 0.6596 0.5194 0.5194 0.605		CAF 0.9161 0.8638 0.825 0.7804 0.7601 0.6208 0.6208 0.6208 0.6608 0.3017 0.3015	ACP -3.5054 -3.7146 -3.9150 -4.1449 -4.4877 -4.7586 -6.0102 -9.9441 74.6689 4.8491 1.3543 8.6068	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3 	2	CN -7.301e -2.03ev -1.6371 -1.6371 -1.4501 -1.759 -0.4174 0.0000 1.7790 2.7601 2.0030	0.8 dl CLM 7.5603 7.101- 0.7047 6.3410 6.3410 6.3435 3.4040 7.4422 1.5207 1.0491	1-0f35 0 CV -0.0100 -0.0131 -0.0232 -0.0160 -0.0077 -0.0246 -0.0235 -0.0235 -0.0235 -0.0231	CLN -0.0875 -0.0720 -0.0543 -0.0543 -0.0543 -0.0543 -0.0543 -0.0545 -0.0547 -0.0547 -0.0547 -0.0547	CLL -0.0434 -0.0438 -0.0427 -0.0463 -0.0458 -0.05530 -0.0562 -0.0581 -0.0529 -0.0476	CA 1.0304 0.9761 0.9384 0.8379 0.8576 0.6576 0.547 0.6696 0.5909 0.5194 0.6695 0.9302	Can 0-11-3 0-11-3 0-11-9 0-1175 8-1176 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	CAF 0.9161 0.8638 0.825 0.7804 0.7601 0.6208 0.6208 0.6208 0.6608 0.3017 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3 	2	CN -7.301e -2.03ev -1.6371 -1.6371 -1.4501 -1.759 -0.4174 0.0000 1.7790 2.7601 2.0030	0.8 dl CLM 7.5603 7.101- 0.7047 6.3410 6.3410 6.3435 3.4040 7.4422 1.5207 1.0491	1-0f35 0 CV -0.0100 -0.0131 -0.0232 -0.0160 -0.0077 -0.0246 -0.0235 -0.0235 -0.0235 -0.0231	CLN -0.0875 -0.0720 -0.0543 -0.0543 -0.0543 -0.0543 -0.0543 -0.0545 -0.0547 -0.0547 -0.0547 -0.0547	CLL -0.0434 -0.0438 -0.0427 -0.0463 -0.0458 -0.05530 -0.0562 -0.0581 -0.0529 -0.0476	CA 1.0304 0.9761 0.9384 0.8379 0.8576 0.6576 0.547 0.6696 0.5909 0.5194 0.6695 0.9302	Can 0-11-3 0-11-3 0-11-9 0-1175 8-1176 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	CAF 0.9161 0.8638 0.825 0.7804 0.7601 0.6208 0.6208 0.6208 0.6608 0.3017 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3 	2	CN -7.301e -2.03ev -1.6371 -1.6371 -1.4501 -1.759 -0.4174 0.0000 1.7790 2.7601 2.0030	0.8 dl CLM 7.5603 7.101- 0.7047 6.3410 6.3410 6.3435 3.4040 7.4422 1.5207 1.0491	1-0f35 0 CV -0.0100 -0.0131 -0.0232 -0.0160 -0.0077 -0.0246 -0.0235 -0.0235 -0.0235 -0.0231	CLN -0.0875 -0.0720 -0.0543 -0.0543 -0.0543 -0.0543 -0.0543 -0.0545 -0.0547 -0.0547 -0.0547 -0.0547	CLL -0.0434 -0.0438 -0.0427 -0.0463 -0.0458 -0.05530 -0.0562 -0.0581 -0.0529 -0.0476	CA 1.0304 0.9761 0.9384 0.8379 0.8576 0.6576 0.547 0.6696 0.5909 0.5194 0.6695 0.9302	Can 0-11-3 0-11-3 0-11-9 0-1175 8-1176 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	CAF 0.9161 0.8638 0.825 0.7804 0.7601 0.6208 0.6208 0.6208 0.6608 0.3017 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3 	2	CN -7.301e -2.03ev -1.6371 -1.6371 -1.4501 -1.759 -0.4174 0.0000 1.7790 2.7601 2.0030	0.8 dl CLM 7.5603 7.101- 0.7047 6.3410 6.3410 6.3435 3.4040 7.4422 1.5207 1.0491	1-0f35 0 CV -0.0100 -0.0131 -0.0232 -0.0160 -0.0077 -0.0246 -0.0235 -0.0235 -0.0235 -0.0231	CLN -0.0875 -0.0720 -0.0543 -0.0543 -0.0543 -0.0543 -0.0543 -0.0545 -0.0547 -0.0547 -0.0547 -0.0547	CLL -0.0434 -0.0438 -0.0427 -0.0463 -0.0458 -0.05530 -0.0562 -0.0581 -0.0529 -0.0476	CA 1.0304 0.9761 0.9384 0.8379 0.8576 0.6576 0.547 0.6696 0.5909 0.5194 0.6695 0.9302	Can 0-11-3 0-11-3 0-11-9 0-1175 8-1176 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	CAF 0.9161 0.9638 0.4225 0.7804 0.76021 0.6208 0.5408 0.4605 0.3317 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3.7H 2.2e 1.73 1.16 0.49 1.91 1.91 0.32 7.45 1.61 1.63 1.63 1.63 1.63 1.63 1.63 1.63	0.05 0.05 0.01 0.01 0.01 0.01 0.01 0.01	-7.301e -2.03ev -1.6371 -1.6371 -1.6501 -1.750 -0.4374 -0.4155 -1.1750 2.7601 2.6030	7.5601 7.5603 7.101- 6.7054 6.3410 6.013c 5.7073 6.3535 3.4640 7.4422 1.0204 1.0204	-0.010 -0.0032 -0.0131 -0.0232 -0.0160 -0.0077 -0.0296 -0.0296 -0.0235 -0.0235 -0.0237 -0.0313	-0.0875 -0.0753 -0.0753 -0.0563 -0.0565 -0.0331 -0.029 -0.0735 -0.0477 -0.0647 -0.0699	-0.0434 -0.0438 -0.0427 -0.0463 -0.0468 -0.0458 -0.0530 -0.0562 -0.0562 -0.0581 -0.0529	1.0304 0.4781 0.4384 0.4579 0.4570 0.6596 0.5909 0.5194 0.6605 0.5302	0-11+3 0-11+3 0-11-5 0-1175 0-1175 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	0.9161 0.8638 0.4225 0.7804 0.7021 0.6208 0.5408 0.4605 0.3317 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
1 -3 2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 1 10 10 11 12 12 14 13 16 14 15 21	3.7H 2.2e 1.73 1.16 0.49 1.91 1.91 0.32 7.45 1.61 1.63 1.63 1.63 1.63 1.63 1.63 1.63	0.05 0.05 0.01 0.01 0.01 0.01 0.01 0.01	-7.301e -2.03ev -1.6371 -1.6371 -1.6501 -1.750 -0.4374 -0.4155 -1.1750 2.7601 2.6030	7.5601 7.5603 7.101- 6.7054 6.3410 6.013c 5.7073 6.3535 3.4640 7.4422 1.0204 1.0204	-0.010 -0.0032 -0.0131 -0.0232 -0.0160 -0.0077 -0.0296 -0.0296 -0.0235 -0.0235 -0.0237 -0.0313	-0.0875 -0.0753 -0.0753 -0.0563 -0.0565 -0.0331 -0.029 -0.0735 -0.0477 -0.0647 -0.0699	-0.0434 -0.0438 -0.0427 -0.0463 -0.0468 -0.0458 -0.0530 -0.0562 -0.0562 -0.0581 -0.0529	1.0304 0.4781 0.4384 0.4579 0.4570 0.6596 0.5909 0.5194 0.6605 0.5302	0-11+3 0-11+3 0-11-5 0-1175 0-1175 0-1191 0-1289 0-1289 0-1288 0-1288 0-1288	0.9161 0.8638 0.4225 0.7804 0.7021 0.6208 0.5408 0.4605 0.3317 0.3015	-3.5054 -3.7146 -3.9150 -4.1467 -4.4677 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
2 -2 3 -1 6 -0 5 0 6 1 7 4 8 6 9 10 10 11 12 12 14 13 16 14 15 21 15 21	2.26 1.73 1.16 1.41 1.41 1.00 1.79 1.32 2.5 1.675 1.03	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.02 0.02	-2.03ev -1.62v2 -1.6371 -1.6501 -1.7501 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.4374 -2.437	7.5663 7.101- 6.705- 6.3410 6.413c 6.413- 6.413- 6.412- 6.412- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.413- 6.	-0.0032 -0.0131 -0.0232 -0.0160 -0.0077 -0.0296 -0.0235 -0.0235 -0.0237 -0.0321	-0.0720 -0.0720 -0.0543 -0.0543 -0.0742 -0.0331 -0.0299 -0.0745 -0.0447 -0.0467 -0.0647	-0.0430 -0.0427 -0.0463 -0.0458 -0.0458 -0.0582 -0.0581 -0.0529 -0.0476	0.9761 0.9384 0.8979 0.6576 0.6212 0.7447 0.6696 0.5909 0.5194 0.4605 0.4302	0.1143 0.1175 0.1175 0.1176 0.1191 0.1289 0.1289 0.1288 0.1288 0.1289	0.8636 0.7825 0.7804 0.7606 0.7621 0.6208 0.5408 0.4605 0.3906 0.3317 0.3015	-3.7146 -3.9150 -4.1449 -4.4077 -4.7586 -6.0102 -9.9441 74.6669 4.0491 1.3543	
3 -1 5 0 6 1 7 4 8 6 9 10 10 11 12 14 12 14 13 16 14 16 21 16 2:	1.73 1.16 1.48 1.41 1.00 1.09 1.71 1.32 1.53 1.63 1.63	0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.02	-1.6371 -1.6371 -1.4501 -1.259 -0.4374 -0.4374 0.0474 0.155 1.1759 1.7790 2.7601 2.7601	7.101- 0.7049 6.3910 6.013c 5.7073 6.3935 3.4040 6.9209 1.0491 0.5583	-0.0131 -0.6232 -0.0160 -0.0077 -0.0246 -0.0235 -0.0235 -0.0235 -0.0211	-0.0720 -0.0543 -0.0543 -0.0642 -0.0331 -0.029 -0.0745 -0.0449 -0.047 -0.047	-0.0427 -0.0463 -0.0458 -0.0530 -0.0562 -0.0563 -0.0581 -0.0529 -0.0476	0.4384 0.4379 0.4576 0.6512 0.7447 0.6596 0.5194 0.6605 0.6605 0.6302	0.1159 0.1175 0.1176 0.1176 0.1289 0.1289 0.1288 0.1288 0.1288	0.H225 0.7804 0.7400 0.7021 0.6200 0.5468 0.4605 0.3317 0.3015	-3.9150 -4.1467 -4.4077 -4.7586 -6.0102 -9.9441 74.6609 4.0491 1.3543	
5 0 6 1 7 4 8 7 9 1 10 10 11 12 12 14 13 16 14 15 21 16 2:	0.16 0.48 1.91 0.00 0.32 2.45 1.61 6.75 1.03	0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.02 0.02	-1.6371 -1.4501 -1.250 -2.4374 -0.4374 0.6455 1.1759 1.7759 2.7661 2.7661	6.3410 6.3410 6.013c 5.7073 6.3433 3.4640 7.4422 1.9207 1.0441	-0.0232 -0.0160 -0.0077 -0.0265 -0.0235 -0.0217 -0.0321 -0.0313	-0.0543 -0.0566 -0.0422 -0.0331 -0.0299 -0.0745 -0.0747 -0.0647 -0.069	-0.0463 -0.0468 -0.0458 -0.0530 -0.0562 -0.0553 -0.0581 -0.0529	C.8479 C.4576 O.6212 O.7447 O.6696 C.5907 U.5194 B.4605 B.4302	0.1175 0.1176 0.1191 0.1289 0.1289 0.1288 0.1288 0.1288	0.7804 0.7400 0.7021 0.6208 0.5408 0.4605 0.3906 0.3317	-4.1449 -4.4977 -4.7586 -6.0102 -7.9441 74.6689 4.0491 1.3543	
6 1 7 4 8 6 9 5 10 10 11 12 12 14 13 16 15 21 16 2:	0.32 0.32 0.32 0.32 0.33 0.33 0.33 0.33	0.01 0.01 0.01 0.01 0.01 0.02 0.02 0.02	-1.4501 -1.250 -2.4059 -2.4055 -2.4374 0.4155 1.1404 1.7290 2.2601 2.7601	6.3710 6.013c 5.7075 6.7335 3.4660 7.4722 1.9207 1.0491 0.5583	-0.0160 -0.0077 -0.0260 -0.0290 -0.0339 -0.0235 -0.0217 -0.0321	2540.00 2540.00 2540.00 2540.00 2540.00 7740.00 7460.00	-0.0468 -0.0458 -0.0530 -0.0562 -0.0553 -0.0581 -0.0529 -0.0476	0.4576 0.4212 0.7447 0.6696 0.5909 0.5194 0.4605 0.4302	0.1176 0.1191 0.1739 0.1289 0.1304 0.1288 0.1288 0.1288	0.7400 0.7021 0.6200 0.5408 0.4605 0.3906 0.3317	-4.4877 -4.7586 -6.0102 -9.9441 74.6689 4.0491 1.3543	
7 8 9 10 10 10 11 12 14 13 16 15 21 16 21	0.00 0.09 0.32 0.32 0.51 6.75 0.99	0.01 0.01 0.01 0.02 0.02 0.02	-0.437# -0.437# -0.437# -0.6155 1.1454 1.7790 2.7601 2.6030	5.7073 6.7073 3.4040 7.4922 1.0207 1.0491 0.5583	-0.029 -0.029 -0.033 -0.0235 -0.0217 -0.0321 -0.0313	-0.0331 -0.0299 -0.0245 -0.0449 -0.0477 -0.0447	-0.0530 -0.0562 -0.0553 -0.0581 -0.0529 -0.0476	0.7447 0.6596 0.5907 0.5194 0.6605 0.4302	0.1739 0.1289 0.1304 0.1288 0.1288 0.1289	0.6208 0.5408 0.4605 0.3906 0.3317 0.3015	-6.0102 -9.9441 74.6669 4.0491 1.3543	
8 9 10 10 10 11 12 14 13 16 15 21 16 21	0.09 0.32 0.45 0.61 0.75 0.99 1.03	0.02 0.02 0.02 0.02 0.02	-0.437# 0.0004 0.6155 1.1909 1.7290 2.2601 2.030	4-3535 3-464n 2-4722 1-5207 1-0491	-0.0294 -0.0335 -0.0235 -0.0217 -0.0321 -0.0310	-0.0299 -0.0745 -0.0449 -0.0477 -0.0647	-0.0562 -0.0553 -0.0581 -0.0529 -0.0476	0.6596 0.5909 0.5194 0.6605 0.6302	0.1269 0.1304 0.1268 0.1266 0.1267	0.4605 0.3906 0.3317 0.3015	-9.9441 74.6689 4.8491 1.3543	
10 10 11 12 12 14 13 16 14 16 15 21	0.32 2.45 6.75 6.75 1.99	0.01 0.01 0.02 0.02 0.02	7.0444 7.4155 1.1959 1.7290 2.7401 2.4030	3.4640 2.4922 1.9207 1.0491	-0.0335 -0.0235 -0.0217 -0.0321	-0.02.5 -0.04.9 -0.04.77 -0.05.47 -0.09.9	-0.0553 -0.0581 -0.0529 -0.0476	0.5909 0.5194 0.4605 0.4302	0.1304 C.1288 0.1288 G.1287	0.4605 0.3906 0.3317 0.3015	74.6689 4.0491 1.3543	
10 10 11 12 12 14 13 16 14 16 15 21	0.32 2.45 6.41 6.75 8.99 1.03	0.01 0.02 0.02 0.02 0.02	0.6155 0.6151 0.657.1 0.000.5	1.5207 1.5207 1.0491 0.5583	-0.0235 -0.0217 -0.0321 -0.0319	-0.0449 -0.0477 -0.0547 -0.0999	-0.0581 -0.0529 -0.0476	0.5194 8.4605 8.4302	0.1268 0.1268 G.1267	0.3906 0.3317 0.3015	4.0491 1.3543	
11 12 14 13 16 15 21 16 2:	6.75 9.99 1.03	0.05 0.05 0.05 0.01	1.1454 0657.1 1045.5 0604.5	1.5207	-0.0217 -0.0321 -0.0313	-0.0477 -0.0447 -0.0999	-0.0529 -0.0476	0.4605 0.4302	0.128s 6.1287	0.3317	1.3543	<u> </u>
12 14 13 16 14 16 15 21 16 23	6.75 6.75 7.99 1.03	0.05	1.7230 2.7401 0.000	0.5583	-0.0321	-0.0547	-0.0476		G-1287	0.3015		
14 16 15 21 16 21	1.03 3.26	0.02	2030				-0.0500	8-4066				
15 21 16 21	1.03 3.26	Gibe		0.0500	-0-0299					0.2781	0.2470	
16 2:	3.26		3 4147					0.3816	0.1240	0.2576	0.0181	
						-0.1515		0.3617	0.1223	0.2394	-0.1301	
	0.14		3.41+7	6.7422	-0.0214	-0.1906 -0.0798	-0.0536	0.8994	0.1774	0.2185	-0.2846 -4.1481	<del></del>
	****		-10(3.0	001722	-00000	-0.0175	-0.0403	000,334	001113	00.017		
							<del></del>			***************************************		
							<u>.</u>					
						-						
					•	_				•		
				·		<del></del>					<del></del>	<del></del>
												•
									<del></del>			
				•						-		
						<del></del>	<del></del>		<del></del>	<del></del>		<del></del>
								-			•	
_ •			_									
							:					
								-				

				A-OLEY H	ESEAHCH C			UNITA		IND TUNN	EL (UPat)		
	1 OF 1					H FITHAP	ISSILE TA	IL EFFECTS	DATA			<u>.</u>	
Ţ	1 OF 1			-			•						
						<del></del>			<del></del>	<del></del>			
			ACH RATE-		CUNF	L DEL	I WELZ		THANSIT				
		24 3.	45 3.0	J. 0 B	1-0F35 (	0.0	0 -50	0 -20	FIXE	ــــــ			
NT	ALPHA	HFTA	CN	CL4	CY	CL4	CLL	CA	CAB	CAF	ACP		
	-3.56	0.0	-1.437E	5.2795	0.0061	-n.0507	-0.0313	U.8240	0.0567	0.7573	-3.4169		
1	-2.13	0.,	-1.57+>	5.0103	0.0113	-0.0954	-7.031.	0.7750	0.0667	0.70A3	-3.6809		
5	-1-11	0.0	-1.4616	5-4754	0.0163	-0.1519	-0.0363	0.7396	0.9467	0.6729	-3.9086		
<u>-</u>	-0.06 v.97	0.u	-1.2745	5.1372	0.021 <u></u>		-0.0361 -0.0358	0.7049	_0.068 <u>6</u>	0.6006	-4,1943		
\$	1.96	0.0	-0-4643	4.4510	0.0003			0.6347	0.0688	0.5659	-5.0334		
;	4.06	0.0	-0.5071	3.7100	0.0024			0.5603	0.0710		-7,3178		•
Ä	6.12	0.01	-0.0914	2.4213	-0.0077			0.4913	0.0710	0.4203	-31.7674		
•	. 5. Jh	0.0	0.3003	5-33-3	-9.00-5		-0.03-3	J-467	0.0731	0.3756	7.6733		
0	10.75	0.0	0.4469	1.9108	0.0075		-c.0373	0.4282	0.0731	0.3551	2.7741		
5	14.41	0.01	1.4370	1.6690	-0.0092		_	U.+1A1 0.+169	0.0731	0.3450	1.5026	••	
3	16.54	0.01	1.4376		-0.00			- 3.4162-	0.0731	0.3431	0.6683		<del></del>
	14.66	01	7.2810	0.9471	-0.0635		-0.3478	0.4181	0.0709	9.3472	0.4151		
5	20.71	0.01	2.7401	0.4371	U-010-	-0.2750		0.4200	0.0-85	0.3512	0.2325		
ь	27.A4	0.01	3.7597		-0.0191			0.4173	0.0667	0.3506	0.0737		
7	-0.00	0.0	-1.5556	5-1205	0.0247	-0.1213	-0.0360	0.7021	0.0668	9.6333	-4.1941		
								<del></del> -			<del></del>	···	
								•					
								. <b></b>					
								•					
		-	•										
			···	<del></del>							<del></del>		
			<del></del>							<del></del>	<del></del>		
		•											
				71									

			T.	ANGLEY A	ESEAHCH C	ENTERTOAS	Δ1	UNITA	RY PLAN	IND TUNN	EL (UP # T)	
	OF 1					MANTIN M	ISSILE TA	IL EFFECTS	. DAYA	<del></del>		
					<del></del>		<del></del>				<del></del>	
	YEST	PART P	ACH 4310-7	PH1	CONF	L VEL	1 DEL?	DEL3 DEL4	TRANSIT	ON		
	3	30 4.	6.5 3.0	0.0 #	1-0F35 0	.0	0 -20	0 -20	FIXE			
INT		BFTA	CN	CLM	CY	CLN	. CLL	CA	CAH	CAF	XCP	
	-3.27	0.0	-1-0545	5.5276	0.0110	-0.0744	-0.0274	0.7465	0.0-85	0.6980	-3,3939	
<u> </u>	-1.75	0.0	-1.774-	5.79/2	-0.011A	-0.0450	-0.0200	0.4979 U.6657	V-0485	0.6494	-3.7073 -3.9374	
	0.31	0.0	-1.0203	4.450#	-0.0027		-0.0329	0.6299	0.0485	0.5P14	-4.3623	
<del>-</del>	1.33	0.0	-6.4531	4.1421	0.0025		-0.0326	0.5966	0.0465	0.5441	-4.8554	
5	7.33	G. U	-0.7190	3.0644		-0.0452	-0.0323	0.5617	0.0512	0.5105	-5.4435	
	4.40	0.0	-0.3653	3.1496	0.0153		-0.0315	0.4862	0.0512	0.4370	-9,6525	
	F.44	0.0	0.030	2.5521		-U.0837	-0.0375	0.4365	0.0512	0.3453	83.9528	
	10.54	0.0	0.654/	7-1865 1-9448		-0.0420	-0.0356	0.4074	0.0512	0.3627	6.0925 2.8404	
_	12.50	0.0	1.2112	1./491		-0.1278		0.4030	0.0512	0.3518	1.7297	
2	14.56	0.01	1.7353	1.5917	-u.0011	-0-17-5	-0.0401	0.4058	0.0539	0.3519	1.1920	
3	14.75	0.01	1.7056	1.354#	0.0091			0.4100	0.0512	0.3588	0.7943	
<u> </u>	14.44	0.61	2-1017	1-4717	-0.0067	-6.1530	-0.0377	0.4173	0.0512	0.3661	0.5099	
5	50.05	0.01	5-410	0.7937	0.0000	-t-1516		0.4244	0.0512	0.3732	0.3186	
<u> </u>	55.49	0.01	7.9576		-6.0090	-0.1314	-0.0486	0.4266	0.0457	0.3809	0.1472	
	0.54	0.0	-1.0400	4.4d24	-0.0026	-0.6333	-0.0330	0.6303	0.3485	0.5618	-4.2911	
			<del></del>									
					·	···						
			<del> </del>						<del></del>	<del></del>	<del></del>	<del> </del>
					<del></del>							
												·
								·			•	
					<del></del> -		<del></del>	<del></del>			<del></del>	
										<u>_</u>		
											•	

.

•

E	1 OF 1			LANGLEY H	ESEAHCH C	ENTEHINAS	A) 1551LE TA	UNITA Ti eesicts	HY PLAN L	IND TUNK	EL (UPST)	
	1 OF 1						1331LE IR	L EFFECTS	UNIA		<del></del>	
									•			•
	YEET	DASY M	LH HAIG-	6 2-1	CONF	A (15 a	1 05.3	DELJ DEL4	THANSITI	A-1		
	3		36 2.5			.0 Z	0 -50	50 -50				
_											111 11 11 11 11 11 11 11 11 11 11 11 11	<del></del>
DINT		RETA	CN	CL*	CY	CLM	CLL	<u>CA</u>	CAB	CAF	ACP	
2	-3.5E	0.05	-3.4478	12.3779	-0.0294	-0.0753	-0.0255	1.8509 1.7735	0.1788 0.1768	1.5947	-3.7976 -3.9420	
-	-1-95	6.35	-2.9217	11.9625	-0.0155	-0.0161	-3.0249	1.7215	U-1707	1.5403	-4.0735	
•	9.05	0.05		11.4710	-0.047-	0.0112	-0.0274	1.4675	0.1+08	1.4862		
5	1.07	0.05	-2.5245	11.0200	-0.0459	0.0707	-0.0245	1.6143	0.1927		-4.3618	
6	2.15			10-6137		0.3267	-0-0249	1.5612	0.1426		-4.5547	
7	••1•	0.04	-1.94.5		-0.045h	1550.0	-0.0331	1.4501	0.1-04		-5.0195	
9	5.20	0.04	-1.4436	4-5744	-7-05-8	0.0455	-0.0373	1.3145	0-1-25		-5,9434	
10	F.32	0-0-	-0.3651	7.5541 6.451	-0.0531	0.0627	-0.0450	1.0796	0.1#24 6.1843		-7.9644 -17.5252	
iř	12.49	0.03	0.2024	5.2776	-0.0007	-0.0501	-0.0437	1.0011	0.1562		24.0516	
12	14.54	0.03		. 5.4260		0.0661	-0.0329	0.9385	0.1492	0.7503	6.2991	·
13	10.77	0.03	1.3929		-0.0725	C-01-7		3. HR59	6.1863	0.0996	3.1469	
14	14.70	0.04	2.6241		-0.0776	0.0023		0.E384	0-1904	0.6520	1.8350	
15	\$1.03	(.03	2.6493	3050	-0.0040	0.0250		0.7927	0.1445	6-6025	1.1345	
16	23.26	0.03	7,3235		-0.0905		-0.0453	0.7417	J.1826	0.5591	0.6659	<del></del>
17	0.05	0.03	-6.1336	11.4000	-0.0655	0.0769	-0-0294	1.5655	0.1807	1.4050	-4.2004	
			<del></del>			<del>`</del> _					<del> </del>	
												<del></del>
			_									
					<del></del>				<del></del>		<del></del>	
											-	
	•											
											<del> </del>	
											•	
	<del></del>											
										•		

				LALULEY A	ESEAHCH C				RY PLAN .	IND TUNK	EL (UPeT)	
	1 OF 1			<u> </u>		-4112	INSTILE IN	IL EFFECTS	DATA	-		
									· · · · · · · · · · · · · · · · · · ·			
												•
	TEST			Inq &		L GEL	I DELZ		THAMSITI			
_ <u>.</u>	3	37 2.	to 3.0	45.0 d	140F35 6	<u> </u>	-20	20 -20	FIRED			
NT	ALPHA	RETA	CM	CL*	CY	CLN	CLL	CA	CAR	CAF	ACP	
	-3.63	0.00	-2.4451		-0.0147	-0.03#5	-0.05+9	1.4178	0.1247	1.4931	-3.6978	·
	-2.11	0.05	-2.6445	10.43		-0-0434	-0.0245	1.5444	0.1247	1.4701	-3,8674	<del></del>
	-I-05	0.05	-2.4950 -2.3041	4.0332	-0.0271	-0.0334	-0.0332	1.4442	0-1746	1.3696	-4.0215 -4.1862	
	1.07	0.05	-2-11-0	9.2572	-0.0305	-0.0195	-0.0367	1.3427	0.1362	1.2665	-4.3707	
	2.01	0.45	-1.4231	A-0733	-0.0350	-0.0113	-0.0364	1.3424	0.1263_	1.2161	-4.6141	
	4-17	0.05	-1.5401	A-1327	-0.0414	-0.0014	-0.0319	1.5316	0.1276	1.10.0	-5.2602	•
	4.30	0.04	-1-0550	7-05#3 6-1912	-7-0-02	-6.60+0 0.62<7		1.1080	0.127+	0.9431	-6.6369 -10.4024	<del> </del>
	13.45	0.04	-0-0726	5.3715	-0.0553	3.0275		0.9357	0.1310		-73.9896	
	17.58	0.04	0.4421		-0.0502	0.0193		0.4045	0.1310	0.7535	10.8294	
<u>.                                    </u>	14.73	0.04	7.4505		-0.0719	0.01-1	-0.0309	0.4445	0-1327	0.7118	4.5026	······································
	16.49	0.03	1.4799	3.7554	-0.0666	0.0169		0.4125	0.1326	0.6799	2.5343	
	21.15	0.03	2.4139	3.752m	-0.0546		-0.03=7	0-9046	0.1311	0.6338	1.6337	
	23.37	0.03	3.1266		-0.0714		-0.0451	0.7389	0.1278	0.6111	0.6783	
	. 0.02	0.05	-2.7992			-0.0145		1-440	0.1263	1.3177	-4.1911	
									·	····		
								. *				•
									•			
							•					
	<del></del>					<del></del>	··					
							:					
			<del></del>								<del> </del>	

			•	fa =	ormani					265	a v v			
6E	1 OF 1			AHGLEY H	ESEANCH C	ENTEP(AS	A) ISSILE TAI	UNITA LL EFFECTS	HY PLAN #	IND TUNN	EL (UPWT)			
EET	1 OF 1													
	7E51	HAHT W	ACH HX 10=5 95 3.0	PHI	CONF 1=0F35 0	L UEL	0 -50	20 -50			•			
A T 11 T		PFTA	•						CAB		XCP .	<del></del>		<del></del>
1	-3.45		-2.3642	B-5294	-0.0156	-0.0359	-0.0359	1.2929	0.0633	1.2295	-3.6077		<del></del>	
2	-1.90		-7.03-1		-0.0309	-0.0120	-0.0355	1.2740	0.0433		-3.8371			222
3	0.16	0.03	-1.4175 -1.7048	7-0556		C-01u7	-0.0300	1.1360	0.0633 0.0633	1.1215	-3.9923			
5	1.16	0.03	-1.5442		-0.0493	6.0272	-0.03-7	1.0855	0.0654	1.0211	-4.4536			
7	2.15	0.03	-1.3751		-0.0-31	-0.007A	-0.0292	1.0352	0.0654	0.8707	-4.7427	<del> </del>		
A	6.32	0.04	-7.5820	5.6219	-0-0507	0.0278	-0.0279	0 . H557	0.0675	0.7852	-9.6167			
10	10.45	0.05	9-145	4-3608	-0.0408	-0.0003		0.7990	0.0575		-24.9902 21.9457			
11	15.25	0.02	3.5459	3.7375	-0.0475	-C.0785	-0.0198	0.7555	0.0557	0.6858	6,8466			<del></del>
12	16.71	0.05	0.91er 1.2m72			-0.022A		0.7545	0.0675	0.6848	3.8632			
14	34.47	9.00	1.7041	3.2207	-0.0501	-0.0466	-0.031#	0.7845	0.0575	0.7173	1.8899			
15	20.en	0.02	2.5033			-6.0556 -0.1932		0.4059	0.0654	0.7405				
17	0.16	0.02				-0.0011		1.1312	0.0654		-4.2362			
18	0.15	. 0.03	-1.7263	7.2632	-0.6276	0.0002	-0.0349	1.1328	0.9654	1.0674	-4.2074			
								•				•		
									-					
													· · · · · · · · · · · · · · · · · · ·	
				•									•	
				•										
							<u> </u>							
	•	_	-											
												· <del></del>		
							•					· · · · · · · · · · · · · · · · · · ·		
			<del></del>											
												_	•	

				LANGLEY K	ESEARCH (	ENTEHLAS	A)	UnitA	HY PLAN	-IND TUNN	EL (UPUT)	
	1 OF 1					MANITA M	1991FF 1	ALL EFFECTS	DAIR		<del></del>	
				<u> </u>				·				
			ACH WATUE		CUNF	L VEL			TRANSIT			
	3	35 7.	36 2.5	45.0 6	1 + OF 34 (	0.0 2	0 -20	20, -20	FIXE	<u> </u>		<del></del>
INT	ALPHA	eETA.	C4	CLM	CY	CLN	CLL	Ç4	CAS	CAF	ACP	
1	-3.60	0.00		14.5746	0.0004		-0.0200	2.0603	0.1655	1.6948	-3.9173	
2	-2.07	0.05	-3.3434	13.7662		-0-0224	-0.0249	1.4738	0-1673	1.6065	-4.0567	·
3	0.0	0.05	-3.1717	13-7165	-0.000h	-0.0344	-0.0340	1.4171	0-16-1	1.7430	-4.1670 -4.2911	
5	1.06	0.05	=2.7791	12.2/2	0.0044	-0.0753	-0.0337	1.6523	0.1708 0.1724	1.6152	-4.4150	
6	7.06	0.05	-2.5926	11.8704	-0.0051	-0.0215	-0.0376	1.7283	0.1741	1.5542	-4.5593	
Ť	4.15	0.65	-2.13-1	10.67-3	-0.0032		-0.0372		0.1725		-4.9971	
B	6.23	0.64	-1.6000	4.3751	-0.0309	0.0230	-0.7452	1.4171	0.1742	1.2379	-5.8271	
4	4.30	0.00	-1.7521	#.V054	-11.0544	4.0227			0.1026	1.0436	-7.0665	
0	10.42	0.04	-C.43se	6.7553	-0.0445	0.0567	-0.7396	1.1317	SAAL.D	0.9475	-15.6229	
1	17.55	0.03	0.1961	503175	-0.4560		-0.0257	1.0334	0.1860		31.7977	
5	14.44	F0.0	0.7433	50000	-0.0507		-0.0243		0-1960	0.7700	6.5054	
3	14.67	0.03	1.3443	4.4133			-0.0188		0.1860	0.7027	3.2314	
14	14.15	0.03	5. 354	3.6990	-0.0565	1.0496	-0.0172	0.1797	0.1960	0.6437	1-0165	
15	21.16	6.03	2.4757	1.7/44					0.1859	0.5852	1.0940	
17 -	-0.0	6-04	-2.9645		-0.0795	£550.0-			-0-1826 -0-1708	1.6901	0.5811 -4.2980	<del></del>
	0.0	(00	-263633	150,05	-0.0163	-000553	-0.0273	1.0204	0.1100	1.0701		
						<del></del>						
							_					•
								<u> </u>				
												<del></del>
							<del></del>			<del></del>		<del></del>
					<del></del>			<del></del>		<del></del>		
							<del></del>	<del></del>				<del></del>
							•					
											•	

.,

				LANGLEY H	ESEANCH (	ENTERINAS	A)	ATI-U	HY PLAN	INO TUNN	EL (UP4T)	
	OF 1					WITTH P	ISSILE TA	IL EFFECTS	DATA			,
	. 07 1										•	
			<del></del>	<del></del>							<del></del>	•
						<del></del>	- 412.5	DE 9 LEA	300.5	12-2		<del> </del>
	3		ALH PX10- 60 3.0			0.0 2		50 -50	FTEE	104		
<del></del>			300		110.04			<u> </u>	•===	<b></b>		
POINT		HFTA	C_N	CLH			CLL	CA .	CAB	CAF	ACP	
. I	-3.41					-0.0516		1.7946	0-1145		-3.8392	
-	-2.07		-2.nn+1			-0.0554		1.7114	101100	1.5953	-4-0043 -4-1457	
•	0.02		-2.4705			-0.0502		1.5022	0.1176		-4.2826	
5	1.06		-2.2605	10.0770		-0.0504	-0.0401	1.5144	0.1193		-4.4678	
6	2.00		-2-0053				-0.0399	1.4525	_}•1;22•	1.3301		·
	4.17		-1.6553		-0.0344	0-0126	-0.0355 -0.0350	1.3201	0.1224 0.1272		-5.2827 -6.5909	
9	8. 16		-0.0005		-0.0501		-0.0343	1.0703	0.1304		-9.9376	<del></del>
10	10.44		-0.10u9	5.0557	-0.6547	0.01-2	-1.0243	0.9404	0.1337	7.8467	-56.0521	
11	12.56	0.0-	0.4147	50037-	-v. 056-		-0.0505	0.9169	0.1336		12-1471	
15	14,73	0.00	0.9237		-0.0553		-0.0189	0-6544	0.1337	0.7311	4.8269	<del></del>
13 14 ·	16.48 19.86	eu.0	1.4443	3-4002	-0.0528		-0.0176 -0.0281	0.8214 0.7615	0.1336 0.1337	0.6840	2.6283 1.6532	
15	21.16	0.13	2.5340			-0.4113		0.7523	0.1320	0.6203	1.0867	<del></del>
16	23.41	C. U3	3.1659		-0.U76b		-0.0292		0.1304	0.5892	0.6448	
17	0.02	0.00	-2.4758	10.6011	-0.0236	-0.0454	-0.0363	1.5804	0.1193	1.4611	-4,2819	_
											<del></del>	
								•				
			-			<del></del>						
						<del></del> .				<del></del>		
										<del></del>		<del></del>
-				•								
•	-											
			•	•			•					
				<del></del>							<del></del>	· · · · · · · · · · · · · · · · · · ·
												•

4	1 OF 1		(	A-16LEY R	ESEAHCH C		ISSILE TAI			IND TUNN	EL (UPAT)	
	1 01 1					Leal Fig. L	TRAILE IN	E EFFECTS	<u> </u>		<del></del>	<del> </del>
												<del></del>
	TEST		- WALU-		CUNF	L UEL			THANSITI			
	3	37 3.	y5 3.0	45.0 0	1-0F34 0	•0 2	-20	20 -20	FIXED		<del></del>	
THIO	ALPHA	OFTA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	ACP	• .
	-3.42		-7.4364	9.1510	0.0192	-0.0917	-0.0354	1.3882	0.0625	1.3257	-3.7603	
2	-1.40		-7-1247	#.494" #.4977	-0.0047	-0.0916 -0.05c1	-0.0350	1.2567	0.0546	1.1661	-3.9902	
3	0.15		-1.77.1	7.5742	0.01+5	-0.0448	~0.0243	1.1912	0.0646	1.1266	-4.3377	
5	1.le		-1.5702	7.247	-0.0101	-0.0314	-0.0343	1.1327	0.0557	1.0660	-4.6166	· · · · · · · · · · · · · · · · · · ·
6	7.19		-1.4013	6-8450	-0.0667	-0.0237	-0.0289	1.0771	0-0467	1.0104	-4.8880	
8	4.27	0.02	-1.02/6	5.1941	0.0006	-0.0-18	-0.0283	0.9733 0.4877	0.0667	0.9066	-5.9250 -8.5262	
9	~.42	6.96	-0-21-5	4.0366	-11-9693	-0.0165	-0.0217	0.8247	0.0710		-21.1322	
10	10.45	0.00	0.1730	4.2015	-0.0309	-0.0137	-0.0206	2.7676	6.0731	0.7145	24.2861	
11	12.52	0.02	1.5537	3.0756	-5.0213	-0-0270	-0.0195	0.7638	0.0731	0.6907	6.9995	
13	14.62	0.02	1.3554	3.6077	-0.0347	-0.0711 -0.0473	-0.0237	0.7510	0.0731 0.0731	0.6779	3.8902	
14	18.65	0.02	1.73	3.7902	-0.0214	-0.0496	-0.0263	0.7653	0.0710	0.6943	2.6150 1.8535	
15	50.49	0.00	2.1075	7.7413	-1.0197	-0.0746		0.7650	0.6710	0.6940	1.3562	~ · · · · · · · · · · · · · · · · · · ·
16	23.13	0.04	2.7327	2.4944	-0.0329		-0.0234	0.7499	0.3667	0.6632	0.9130	
17	0.17	0.03	-1.75-9	7.6590	-0.0001	-0.0444	-0.0293	1.1861	0.0667	1.1194	-4.3643	
					<del></del>		*	*				
											<del></del>	
									<del></del>			
					•				•			
						-				· -		
				<del></del>			<del></del>				······································	······································
•											· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
								·				
												<del></del>

	1 OF				ANGLEY M	LSEAHUM C	ENTERIVAS M NITHAM	A) ISSILE T	UNITAL ALL EFFECTS	RY PLAN	INU TUNN	EL (UPUT)	
	1 OF		-							•			
•			Au .		US ESTIMA	5-08 TO	VOLVE	AVEC				•	
		51		SUP HATU-		CUNF 1-0+34 (		1 UEL2	50 -50	THAMSIT			
N 1	-5.4		HFTA	-2.1136	6.005Y	C.0025	-0.0435	-0.0257	CA 1.2452	U. 0459	CAF	4CP -3.7878	
	-1.5		0.02	-1.4765	7.45/5	-0.0049	-0.0453	-0.0754	1.1677	0.0459		-3.9743	
	-11			-1-4703	7.0142	-1-0134	-0.0343	-0.0252		0.427		-4.2024	
	6.			-1.4417	6.0203	-2.00-3		-0.0249		0.0486	1.0061	-4.4721	
	1.5			-1.3132	6.6543	-0.0100		-0.0247		0.0486		-4.7664	
	4.6			-1.1270 -0.7mgh	5.2512	-0.00H0		-0.0244		0.0486		-5.2334 -6.7254	<del></del>
	6.6			-0.4159	4.5491	-0.0335		-0.0231	0.7947			-11.0316	
	4.		0.00	-0.13/5	4.905.	-0.0334	-U.u 145	-0.0773		0.6513	0.6972-	108.4000	
	10.		0.45	0.3010	3.7574	-0.0564		-0.0588		0.0513		12.4831	
	17.		0.02	0.6214	3-5045					0.0513	0.6653	5.6507	
	14.9		0.00	1.2426			-r.0145 -3.0550			0.0513	0.6738 0.6774	3.7138 2.5834	
	14.		0.02	1.6711			-0.0445		0.7272	0.0513	0.6759	1.7444	
	٤١.		0.02	2.0172	7.7700	-0.0363		-0.0159		0.0486	9.6716	1.2290	
	23.		0.00	2.5624	2.1147	-0.0429	-0-06-6	-0.0212	0.7054	0.0486	0.6568	0.8252	
,	0.9	9	0.02	-1.0002	0.5300	-0.0034	-0.0625	-0.0249	1.0570	0.0486	1.0084	-4.4837	
										<del></del>			
								-					
						• •							
						<del></del>							
												*	

				LANGLEY H	ESEANCH C	ENTENTAS	Al	UNITA	HY PLAN H	IND TUNN	EL (UPST)	·
AGE	1 OF 1					MARTIN M	ISSILE TA	IL EFFECTS	DATA			
HEET	1 OF 1											
<del></del> -			<del> </del>	<del></del>	<del>_</del>	<del></del>	<del></del>	····			<del></del>	<del></del>
			ACH HATU-					UEL3 DEL4	THANSITI	ON		
	3	39 2.	36 3.0	V.0 3	1=0134 0	.0	0 -50	0 -20	FIXE			····
POINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP.	
_ 1	-3.47	6.01	-2.4061	10.55.2	-0.01-5	-0.0646	-0.0335	1.2844	0.1410		-3,7585	
5	-2-14	0.01	-2-5005	9.4575	-0.0173	-0.6473	-0.0333	1.2705	9-1438		-3.9418	
3	-1.47		-2.0741	9.1343	-0.05AV	-0.0247	-0.6365	1-17-1	0.1400		-4.0908	
- 5	1.02		-1.AF22	9.3560	-0.0135	-0.0706	-0.0397	1.0874	0.1537	0.9337	-4,2623	•
•	2.05	0.02	-1.6523	7.0266	-0.6375	-0.0r17	-0.0325	1.0399	0.1564	0.4635	-4.7368	
7	4.17	0.01	-1.2011	6.7324	-u-0+04	0.015	-0.0425	0.9416	0.1635	0.7781	-5.6052	
8	4.76	0.06	-0.7345			0.0717		0.A424	0-1463	0.4761	-7.6538	
10	19.51		0.1994		-0.0377		-0.0483	0.6542	0-1431		-19.7466 P.5647	
11	17.59	0.02	101244	2-15-19	=0-0377	-6-027A	-0.0561	0.5551	0.1635	0.3911	1.9063	
iż	14.49	0.02	1.9243	1.0305	-0.0442	-0.0005	-0.0408	0.4713	0.1649	0.3064	0.5636	
13	17.09	0.02	2.4956	0.1575	-0.0357	-0.6500	-0.0357	0.4197	0.1664	0.2533	0.5636	
14	14.31	0.04	3-1121	-6.4663	-0.03-7	-0.0000	-9.0272	0.3769	0.1649	0.2119	-0.1571	
15	21.50	0.03	3.7550	-1-1444	-0.0334	-6.1231	-0.0291	0.3361	0.1607	0.1754	-0.3165	<del></del>
$-\frac{16}{17}$	-0.01	0.03	-3 (0-)3	4-1153	-0.0057	-0,0744	-0.0275	1.1306	0.1593 0.1508	0.1349	-0.4513	
• •	-4441		-100035	0.0136	-0.0323	-000734	-010327	201300	441340	4.7176	-405150	
_			<u>.                                    </u>		<del></del>						<del> </del>	
						<del></del>			_			
					•							
												·
											•	
				<del></del>								
										·		
				•								
					-	•						

1651 PART - 24 - PRIL - 6 PRI CUMF L CELL OBLS OBLS THANSITION  3	TEST PART = ALM PRIU-6		OF 1			ANGLEY M	ESEARCH C			UNITA IL EFFECTS		IND TUNN	EL (UPaT)		
3	3	ELT	OF 1		_									:	
3	3												•		
POINT ALPMA (EFA CN CLP CY CLN CLL CA CAS CAF KCP 1 -3.7v 0.01 -2.4514 9.004v -0.018m -0.0493 -0.0350 1.1393 0.1077 1.0316 -3.6544 2 -2.2e 0.01 -7.16vh 5.36v0 -0.0233 -0.0624 -0.0346 1.0776 0.1077 0.96v7 -3.8625 3 -1.21 0.01 -1.vnn 7.v1r3 -0.02v3 -0.0624 -0.0346 1.0776 0.1077 0.96v7 -3.8625 3 -1.21 0.01 -1.vnn 7.v1r3 -0.02v3 -0.0040 -0.0340 1.0312 0.10v3 0.v21v -4.0268 4 -0.14 0.01 -1.vnr 7.4467 -0.0195 -0.0647 -0.0380 0.9446 0.1125 0.8721 -4.2535 5 -0.04 0.01 -1.76v7 7.4467 -0.0195 -0.0647 -0.0380 0.9340 9.114 0.4247 -4.5100 6 1.92 0.01 -1.3616 6.0099 -0.0161 -0.0573 -0.0339 0.9340 9.114 0.4247 -4.5100 6 1.92 0.01 -1.3616 6.0099 -0.0167 -0.0573 -0.0330 0.4988 0.1173 0.7785 -4.8510 6 1.92 0.01 -1.3616 6.0099 -0.0127 -0.03546 -0.0370 0.6044 0.1205 0.0809 -6.0495 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6 0.000 6	ALPMA META CN CLP CY CLN CLL CA CAB CAF XCP  -1.7	_						L UEL					•		•
1 -7./V	-3./V 0.01 -2.4614	OINT											100	•	
3 -1.21	-1.21					9.0047									
-0.16 0.01 -1.75.7 7.6667 -0.0195 -0.0567 -0.0381 0.9466 0.1125 0.8721 -4.2535  5 0.40 0.01 -1.5600 6.7725 -0.0005 -0.0607 -0.0539 0.9344 0.1161 0.8267 -4.5100  6 1.92 0.01 -1.3410 6.0009 -0.0161 -0.0573 -0.0336 0.8958 0.1173 0.7785 -4.8510  7 4.02 0.01 -0.4210 5.0710 -0.0127 -0.0506 -0.0370 0.6064 0.1205 0.6839 -6.0495  8 6.00 0.01 -0.4727 4.6210 -0.0265 -0.0266 0.7138 0.1237 0.5901 -9.7774  9 8.22 0.01 0.0771 3.5514 -0.0265 -0.0364 0.0190 0.1237 0.5901 -9.7774  10 10.33 0.01 0.6562 2.4651 -0.0265 -0.0365 0.0190 0.1237 0.4953 67.0203  11 12.46 0.01 1.7351 1.6066 -0.0265 -0.0365 -0.0383 0.5392 0.1237 0.4155 3.7262  12 14.61 0.02 1.7646 1.9660 -0.0376 -0.0376 0.0278 0.0541 0.1253 0.3598 1.2991  13 16.77 0.02 2.7571 0.6073 -0.0371 -0.0528 -0.0303 0.4307 0.1253 0.3068 0.6111  13 16.77 0.02 2.7577 0.1165 -0.0531 -0.0538 -0.0746 0.4074 0.1253 0.3068 0.2690  14 19.01 0.02 7.7777 0.1165 -0.0531 -0.0538 -0.0746 0.4074 0.1251 0.4074 -0.1269  15 21.06 0.02 3.3756 -0.4011 -0.0532 -0.0101 -0.0235 0.3879 0.1205 0.2674 -0.1206  15 21.06 0.02 3.9226 -1.0735 -0.0447 -0.0733 -0.0277 0.3633 0.1173 0.2460 -0.2737  17 -0.14 0.01 -1.7465 7.4401 -0.0196 -0.0647 -0.0380 0.9850 0.1141 9.8709 -4.2551	-0.16 0.01 -1.75.7 7.667 -0.0195 -0.054 -0.0381 0.946 0.1125 0.8721 -4.2535 0.494 0.01 -1.5600 6.722 -0.0095 -0.0682 0.0339 0.9349 0.1141 0.8247 -4.5188 0.029 0.01 -1.3416 6.5099 -0.0161 -0.6573 -0.0336 0.8958 0.1173 0.7785 -4.8518 0.029 0.01 -0.9210 5.0716 -0.0127 -0.0576 -0.0370 0.6064 0.1205 0.6839 -6.0495 0.019 0.0127 -0.0247 -0.0247 -0.0348 0.1237 0.5901 -9.7774 0.01 -0.6727 4.6216 -0.0245 -0.0346 0.0190 0.1237 0.5901 -9.7774 0.02 0.01 0.6562 2.451 0.0245 -0.0346 0.0190 0.1237 0.4953 0.2003 0.332 0.01 0.6562 2.451 0.02465 -0.0346 0.0190 0.1237 0.4953 0.3508 0.0155 3.7262 0.1237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3590 0.2991 0.01237 0.4953 0.3050 0.2991 0.01237 0.4953 0.3050 0.2991 0.01237 0.4953 0.3050 0.2991 0.01237 0.4953 0.3050 0.2991 0.01237 0.4953 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.2993 0.3050 0.3050 0.2993 0.3050 0.3050 0.2993 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050 0.3050	2												<u> </u>	
5	1.92 0.01 -1.910 6.5099 -0.0101 -0.0573 -0.0336 0.9349 0.1173 0.7785 -0.8510  4.02 0.01 -1.9210 5.5710 -0.0127 -7.0576 -0.0370 0.6000 0.1237 0.6039 -0.0453  4.02 0.01 -0.9217 4.6210 -0.0265 -0.0275 -0.0360 0.7785 -0.839 -0.095  4.02 0.01 0.9277 4.6210 -0.0265 -0.0370 0.6000 0.1237 0.5901 -9.7774  8.22 0.01 0.9767 4.6210 -0.0265 -0.0364 0.6190 0.1237 0.4953 02.0203  10.33 0.01 0.6562 7.0451 -0.0265 -0.0365 -0.0384 0.6190 0.1237 0.4953 02.0203  10.33 0.01 0.6562 7.0451 -0.0265 -0.0365 -0.0383 0.5392 0.1237 0.4155 3.7262  12.46 0.01 1.7251 1.0066 -0.0265 -0.0556 -0.0383 0.5392 0.1237 0.4155 3.7262  12.46 0.01 1.7251 1.0060 -0.0376 -0.0213 -0.0276 0.6543 0.1253 0.3590 1.2991  14.61 0.02 1.766 1.0600 -0.0376 -0.0213 -0.0276 0.6543 0.1253 0.3054 0.6111  16.77 0.02 2.2571 0.6073 -0.0371 -0.0528 -0.0303 0.4307 0.1253 0.3054 0.2690  19.01 0.02 7.777 0.11c -0.0531 -0.0534 -0.0246 0.4074 0.1221 0.2853 0.0403  21.04 0.02 3.3256 -0.4011 -0.0532 -0.1011 -0.0235 0.3679 0.1205 0.2676 -0.1206  23.76 0.02 3.9220 -1.0736 -0.0447 -0.0733 -0.0249 0.3633 0.1173 0.2460 -0.2737  -0.14 0.01 -1.7465 7.4401 -0.0195 -0.0647 -0.0380 0.9650 0.1141 0.8709 -4.2551	3													
7	**************************************	5													
8	### ### ##############################	6		0.01	-1.3410				-0.0336	0.0958	0-1173	0.7785	-4.8510		
9	## 10   1   1   1   1   1   1   1   1   1	7													
10 10.33 C.01 0.6562 7.0051 -0.0270 -0.0285 -0.0383 0.5392 0.1237 0.0155 3.7262 11 12.06 0.01 1.7251 1.0006 -0.0267 -0.0550 -0.0331 0.0003 0.1253 0.3590 1.2991 12 14.61 C.02 1.7060 1.0000 -0.0370 -0.0213 -0.0276 0.0541 0.1253 0.3288 0.0111 13 16.77 0.02 2.7571 0.0073 -0.0731 -0.0520 -0.0303 0.4307 0.1253 0.3050 0.2690 14 19.01 0.02 2.7572 0.0170 -0.0531 -0.0530 -0.0240 0.4074 0.1251 0.2553 0.0003 15 21.06 0.02 3.3256 -0.0211 -0.0532 -0.101 -0.0235 0.3870 0.1205 0.2674 -0.1206 16 23.26 0.02 3.9220 -1.0736 -0.0007 -0.0733 -0.0249 0.3633 0.1173 0.2460 -0.2737 17 -0.14 0.01 -1.7465 7.0401 -0.0196 -0.0647 -0.0380 0.9850 0.1141 0.8709 -4.2551	10.33	<del>-</del>													
11 12.46	12.46	10													
13 16.77 0.02 2.7571 0.6073 -0.0771 -0.0528 -0.0303 0.4307 0.1253 0.3054 0.2690 14 19.01 0.02 7.7772 0.1120 -0.0531 -0.0534 -0.0746 0.4074 0.1221 0.2553 0.0003 15 21.04 0.02 3.3754 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206 16 23.78 0.02 3.9228 -1.0738 -0.0447 -0.0733 -0.0299 0.3633 0.1173 0.2460 -0.2737 17 -0.14 0.01 -1.7455 7.4401 -0.0195 -0.0647 -0.0380 0.9850 0.1141 0.8709 -4.2551	16.77 0.02 2.7571 0.6073 -u.0371 -u.0528 -0.0303 0.4307 0.1253 0.3054 0.2690 19.01 0.02 7.777 0.11cn -0.0531 -0.0534 -0.0246 0.4074 0.1221 0.2553 0.0403 21.04 0.02 3.3754 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206 23.76 0.02 3.9226 -1.0735 -0.0467 -0.0733 -0.0249 0.3633 0.1173 0.2460 -0.2737 -0.14 0.01 -1.7465 7.4401 -0.0195 -0.0647 -0.0380 0.9850 0.1141 0.8709 -4.2551		12.46				-6.026¢	-0.0454	-0.0331	0.4843		0.3590	1.2991		
14 19.01 0.02 7.7972 0.11cn -0.0531 -0.0534 -0.0746 0.4074 0.1221 0.2853 0.0403 15 21.04 0.02 3.3254 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206 16 23.26 0.02 3.9226 -1.0735 -0.0447 -0.0733 -0.0299 0.3633 0.1173 0.2460 -0.2737 17 -0.14 0.01 -1.7485 7.4401 -0.0195 -0.0647 -0.0380 0.9850 0.1141 8.8709 -4.2551	19.01 0.02 7.777 0.11cn -0.0531 -0.0534 -0.0246 0.4074 0.1271 0.2553 0.0403  21.06 0.02 3.3756 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206  23.76 0.02 3.9220 -1.0736 -0.0447 -0.0753 -0.0249 0.3633 0.1173 0.2460 -0.2737  -0.14 0.01 -1.7465 7.4401 -0.0196 -0.6647 -0.0380 0.9850 0.1141 0.8709 -4.2551														
15 21.06 0.02 3.3256 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206 16 23.26 0.02 3.9228 -1.0736 -0.0447 -0.0733 -0.0249 0.3633 0.1173 0.2460 -0.2737 17 -0.14 0.01 -1.7485 7.4401 -0.0196 -0.6647 -0.0380 0.9850 0.1141 0.8709 -4.2551	21.06 0.02 3.3256 -0.4011 -0.0352 -0.1051 -0.0235 0.3879 0.1205 0.2674 -0.1206 23.26 0.02 3.9220 -1.0735 -0.0447 -0.0753 -0.0299 0.3633 0.1173 0.2460 -0.2737 -0.14 0.01 -1.7485 7.4401 -0.0196 -0.6647 -0.0380 0.9850 0.1141 0.8709 -4.2551														
16 23.76 0.02 3.9278 -1.0736 -0.0047 -0.0733 -0.0244 0.3633 0.1173 0.2460 -0.2737 17 -0.14 0.01 -1.7485 7.4401 -0.0196 -0.6647 -0.0380 0.9850 0.1141 0.8709 -4.2551	23.76														
		17	-0.14	0.41	-1.7455	7.4401	-0.0196	-0.6647	-0.0380	0.9850	0-1141	0.8709	-4.2551		
		<del></del> _					<del></del>		· · · · · · · · · · · · · · · · · · ·					·	
										•				·	
						<del></del>									
									·		<del></del>				
							Ţ.								
						<del></del>									
										•					
				<u>_</u>		<del></del>	<del></del>			<del></del>			·		
									•						
				=											
													<del></del>		
							•	•							
					<del></del>	,					······	·			

	1 OF 1			ANGLEY R	ESEAHCH C	ENTERINAS MAPTIN M	AI . ISSILE TA	UNITAL IL EFFECTS	DATA .	1ND TUNN	EL (UP#T)		
	165T 3		/µCM #X]U=0		CUNF 1=0F30 0		1 DEL2.	0 -50					
DINT	ALPHA	eETA	CN	CLM	CY	CL*	CLL	CA	CAB	CAF	ACP		
1	-3.65	0.0	-1.4061	6.7044	0.0026	-G. U7-1	-0.0210	3.6857	0.0664	0.8193	-3.5706		
5	-2-13		-1.4307	4.2213	-^.01uh	-0.0579		0 - + 253	0.0664		-3.8151		
3	-1.11	0.0	-1-44-1	5-1495		-0.0-70		0.7535	0.0565		-4.0409 -4.3217		
5	0.97	11.0	-1.0546			-0.0462		0.7034	0.0685		-4.7270	· · ·	
6	1.9e	0.0	-0.9003	4.6309	0.0004	-0.0449	-0.024A	0.6657.	0.0465	0.5972	-5.1436		
7	4.07	0.0	-0-47-0	3.7734		-0.0399		0.5661	0.0706		-7.8941		
9	8.23	0.0	0.1302	2.3117		-0.030F	-0.02/3	0.4686	0.0727	0.4412	-51.6103 6.9264	<del> </del>	
10	10.27	0.01	6.7203			-0.0550		0.4479	0.0728	0.3751	2.6757		
11 .	12.34	6.01	1.2047			-0.0431		0.4411	0.0728	0.3663	1.6156		
12	14.44	0.01	1.4542			-0.034		0.4362	0.0778	0.3634	1.0224		
13	16.55	0.01	2.7839			-0.0508		0.4375	0.0706	0.3669	0.6821 0.4393		
15	16.71 26.71	0.01	2.7395				-0.0263	0.4394	0.0706	0.3714			
15	27.92	0.01	3 500				-0.6135	0.4385	0.0664	0.3721	0.0749	•	
17	-0.04	0.01	-1.2469	5.3701	-0.0144	-0.0307	-0.0253	0.7395	0.0685	0.6710	-4.3226		
									<del></del>			<u> </u>	
								•					
													•
			<del></del>		<del></del>			<del></del>	<del></del>				
												•	
											•		-
	<u></u>	<u></u>					<del></del>						
			• •										
·			·								<del></del>	· · · · · · · · · · · · · · · · · · ·	
			<u> </u>										
<u></u>	<u> </u>								<del></del>				
											-	•	
								- <del></del>	<del></del>		·	<del></del>	

	1 OF			ANGLET H	ESEAHCH C			UNITAG		INU TUNK	EL (UPIT)	
	725 3		-LCH HX1U-4		CONF 1 = UF 34 0		0 -50 1 DEFS	DEL3 DEL4 0 -20	TRANSIT			
PUINT	ALDHA	HETA	C۳	CL4	CY	CLY	CLL	CA	CAB	CAF	ACP	
1	-3.27	_	-1.6034	5.4206	-0-00#3	-6.0332	-0.0204	0.7954	0.0507		-3.5593	
_{-{1 \over 2}}_{-}	-1.75 -0.75		-1.2453	5.371h	0.0011	-0.0532	-0.0200	0.7364	0.0507	0.6457		
4	0.31		-1-0234	4.6928	-0.0105	-0.03/A	-0.0197	0.6592	0.0507	0.6085	-4.4953	
-5-	1.30		-0.4521	4.7577	-G.0061	-0.6317	-0.0190	0.6200	0.0507		-4.9970	
b	2.34	0.0	-0.5563	3.4417	-0.0004	-0.0443	-0.0107	0.5843	0.0507	0.5336	-5.9145	
	4.41		-0.2440	3.16-3	0.0114	-0.0540	-0.0180	0.5113	0.0534		-10.9491	
8	6.51		n-1000	7.5036	3.0177	=0.0645	-0.0239	0.4546	7.0534	0.4062		
10	10.54		0.4024	7.1412	C.0115	-0.0546	-0.0230	0.4359	0.0534 0.0534	0.3825	5.4399 2.6826	
11	12.58		1.07/2	1.029	0.0111		-0.9210	5654.0	v. 0534	0.3718	1.7552	
15	14.44		. 1.3646	1-cul-	-0.0067	-0.0696	-0.0199	0.+760	0.0534	0.3726	1.1722	
13	16.75	-	1.7641	1.3703	0.0444		-0.0255	0.4324	0.0534	0.3790	0.7957	
14	19.47		2.1175	1-1977	-0.0047	-C.07→7	-0.0176	0.4349	0.6507	0-38A2	0.5184	
15 16	20.44		2.5321	0.7787	-0.0402 -0.0533		-0.0163	0.4408	0.0507	0.3961	0.3076 0.1161	
<del>-1</del> y	0.32		-1.0251			-0.0327		0.6598	3.0440	0.6118		<del></del>
	_											
					<del></del>				<del></del>			
				-							-	
					- <del></del>						<del></del>	
				•			-					
			<del></del>					· · · · · · · · · · · · · · · · · · ·				

E T	1 OF 1			LANGLEY	ESEAHCH C	EATEH (485 M PTT48M	A) ISSILE TA	UNITAF IL EFFECTS	Y PLAN .	1 TUNN	EL (UP41)	
			200 129									
	1651		ach #x10-		1+5+33 0	-0	0 -50	0 +28	TRANSITI FIXEL			
			30 3.0		15 % 33 0	••		0 -20		<u> </u>		
INT	ALPHA	PETA	CN	CL=	CA	CLN	CLL	CA	CAR	CAF	ACP	<del>.</del>
1	-3.49	0.02	-2.4501		-0.0570	0.0938	0.0084	1.3652	0.1355	1.2297	-3.8103	
2	-2.1c	0.02	-5-41-4	16.45-2	-( -0671	0.1104	0.0101	1-28#2	0.1396	1.1406	-3,9926	
3	-1	0.02	-2-35-11	9.770.		0.1374	0.0000	1.23.0	U-1437	1.0903	-4.1273	
-	-0.01 0.93	0.01	-2.1483	9.2712	-0.0667	0.1752	0.0054	1.1797	0.1465	1.0332 0.9745	-4.2759 -4.4693	<del></del>
6	2.04	0.01	-1.7024		-0.0636	0.1352	0.0017	1.0705	0.1508	0.9197	-4.7413	
Ť	4.07	0.01	-1.2526		-9.0768	0.15	0.0004	0.9707	0.1564	0.51-3		
je .	4.24	0.01	-0.7517	5.7441	-4.0624	0.1002	-0.0003	0.8669	0.1407	0.7062	-7.6364	
9	5. TH	0.60	-0.2311	4.5777		C-2778	-0.0031	0.7601	0.1593		-19.8946	
9	10.51	0.02	0.3578	300,	-0.1644	J-24F8	-0.0055	0.0767	0.1593	0.5174	8.7828	
1	17.56	C. UZ	1.1166	2-113-		0.2273	-0.0041	0.5722	0.1594	0.4128	1.6693	
2	14.87	0.00	1.9307	0.7705	-0.0975	0.2379	0.0113	0.4591	0.1594	0.3297	0.5345	
3	17.07	0.00	7.4755	Colobo	-0.1.33	0.2477	0.0198	0 367	0.1608	0.2779	0.0673	
4	19.33	0.02	3.1141	-0.7617	-1 -1 104	0.2017	0.0259	0.3972	0-1421	0.2351	-0.1800	
15	21.43	6.03	3.7776	-1-221-		(-55/25	0.0397	0.3593	0.1508	0.1965	-0.3269	
7	23.72 -0.02	0.03	-2.15eu	7.2-67	-0.1325 -0.0528	0.2623	0.0054	1.1754	0.1591	1.0288	-0.4706 -4.2928	
	-0405	0.91	-501240	4.5-01	-0411350	0.10.0	0.0034	101134	0.1400	1.45.00	-4.2766	
				<del></del>							<del></del>	
											<del></del>	
					<del></del>							
											<del></del>	
										•		

GŁ.	1 OF 1			La~OLEY K	ESEAPCH CI	CAPINATION	ISSILE TAI	UNITA	HY PLAN .	TWD TOWN	CL (UP#1)	,	
	I OF I			·		TONIA H	TPPIFE IN	L CFFECIS	UNIA			····	
	·····												
	7651 3		86 3.0		CUNF 1 muf 33 0		0 -50 J DEFS (	0 -50					
	ALPHA	BETA	CN	CLH	CY	CLN	CLL	at CA	CAB	CAF	ACP		
<u> </u>	-3.77		-5-4456		-0.0274		-0.0034	1.1859	0.0961		-3.7146		
<del>-</del> -	-7.75	0.01	-2.2247		-0-0246		-0.0014	1-1144	0-1013		-3.9135		
3	-0.15	0.01	-1.7405		-0.0750	0-0396	-0.0056	1-0638	0.1045	0.9593	-4.0744		
5	0.91		-1.5707	7-1411	-6.035+	0.0563	-0.0030	.0.9658	0.1077	0.8591	-4.5458	<del></del>	<del></del>
6	1.92		-1.3-76		-0.0395		-0.0034	0.4194	0.1109	0.8045	-4.8653		
7	30.0	0.4	-0-6357		-v.0334	0.0674	-2.0043	0.3264	0.11-1		-6.0706 -		
A	6.19	0.01	-0.452-		-0.0443	0-1010	-0.0128	0.7369	0-11/3		-9.6830		
4	4.19	5.01	6.033>		-0.0405		-0.0120	0.6426	0.1173		104.3801	•	
11	10.31	0.01	1.2402	7.4427	-0.0560	0.1594	0.0030	0.5052	6-1189	0.4458	3.7806 1.2773		
5	14.59	0.01	1.7414		-0.0799	0.154	0.0023	0.5052	0.1189	0.3578	0.5927		
15	14.77	0.01	2.25.5		-0.0781	0.1744	0.0129	0.4509	0.1173	0.3336	0.2501		
14	18.94	0.02	2.7950		-0.0931	0.1966	0.0193	0.4319	0.1173	0.3146	0.0229		
5	21.03	0.02	3.3191	4004	-0.0299	6.1711	0.0305	0.4118	G-1157	0.29+1	-0.1407		<del></del>
16	23.26	0.42	3.4157	-1.1466	-0.1035	0.2106	0.0342	6.3874	0.1125	0.2749	-0.2926		
17	-0,13	0.01			-0.0322	0.0345	-0.0026	1.0174	0.1061	0.9063	-4.3088		
										·			
			<del></del>	<del></del>		<del> </del>	·		<del></del>				
		· · · · · ·	<del> </del>	<del></del>	<del></del>			<del> </del>	<del> </del>	<del></del>	<del></del>	<del> </del>	
				<del></del>		·				•	<u> </u>	<u>-</u> _	
				•									
							•	. •					

PAGE '1 OF 1 SHEET TOF T

TEST FEDT PACH DAIJ-6

45 3.45 3.6

POINT	ALPHA	HETA	CH	CLM	CY	CLY	CLL	CA	CAB	CAF	ACP			
	-3.6		-1.9399		-0.0243	0.0397	0.0053	0.9977	0.0598	0.6479				
	-2.11	6.01	-1 - 47 17	5.9831	-0.0300	0.0165	0.00/4	0.5472	0.0598	0.7440	-3.8691			
. 3	-1.13	10.01	-1.27+5	5.5062	-0-0420	0.0579	0.0114	0.7645	0.0620	0.7028	-4.3297			
	0.98	6.31	-1-00-5		-0.0331	0.0496	-0.0056	2.7236	0.0642	0.6594	-4.7149			
6	1.49	0.0	-0.91.4	4.7201	-0.0246	0.0418	0.00-9	0.6840	0.0663	0.6177	-5.1846			
7	4.07	0.0	-0.5500	3.6733	-0.0287	9.656	0.003A	0.0055	0.0503	0.5392	-7.6450			
6	2.12	0.0	-0.1-47	3.0024	+0.0342	0.0597	0.0059	6.53-0	0.0684		-35.6577			
9-	Ŭ5.€	0.0	(-3.45	1.9733	-0.0301	0.0541	0.00.37	0.4899	0.0644	0.4215	7.6585 2.8271			
10	17.32	9.91	1.0000	107175		0.1170	3.0111	0.4548	0.0705	0.3943	- 1.6136	<del></del>	<del></del>	
15	14.42	0.01	1.4403	1.4973	-u.0711	0.1413	0.0176	2.4508	0.0684	0.3924	1.0338			
13	16.54	0.01	I.MASO	1.2264	-0.0677	0.1371	0.0189	G. 4588	0.0663	0.3925	0.6571			
. 14	14.56	0.01	2.2460	0.4771	-0.0642	0.1355	0.0105	0.4592	0.0542	0.3950	0.4282			
15	27.71	0.01	2.7470.		-0.0031	0.1517	0.0303	0.4601	0.0620	0.3981	0.2260			
16	22.63	0.01	3.2.75		-0.0639	0.1683	0.0345	0.4596	0.0599	0.3997	0.0676			
17	-0.05	0.0	-1.2577	2.2020	-6.0204	0.0173	0.0061	0.7585	0.0620	0.6965	-4.3768		•	
			<del></del>											
				•										
			- <del> </del>											
										<del></del>		· · · · · · · · · · · · · · · · · · ·		
										•				
					<u> </u>							·		
									<del></del>		···			
		•		_										
					·									
									. <del></del>					
											<del></del>			
		_									······································			
						-								

MANTIN HISSILE TAIL EFFECTS DATA

0 -20

DELI DELZ DELA DELA TRANSITION

0 -20 FIXED

LANGLEY RESEARCH CENTER (NASA)

PHI CONF

C.0 61.0F33 0.0

UNITARY PLAN SIND TUNNEL (UPST)

.

TEST   3   26   1.75   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30   1.30	5ETA 0.0 0.0 0.0 0.0 0.0	-1.6970 -1.42nh -1.27ny -1.0500	0.0 H	CY -U.0161	.O CLN	0 -20	0 -\$8 0 -\$8					
3.26 1.75 0.30 1.34 2.33	0.0 0.0 0.0	-1.6970 -1.42nh -1.27n9 -1.0500	6.1050 5.5254	-0.0161		C1.1						
1.75 0.76 0.30 1.34 2.33	0.0 0.0 0.0	-1.42nh -1.27ny -1.05ou	5.5254		£ 034E	CLL	CA	CAR	CAF	XCP .		
1.34 2.33	0.0	-1.0500	5-1162			-0.0005	0.8157	0.0453		-3.5975		
1.34 2.33	0.0	-1.0500	3-1162	-0.0055	0.0256	0.0097	0.7569	0.0453		-3.8732	·	
1.34 2.33	0.0		4 PLAE	-0.0749	0.0464	0.0052	0.7162	0.0453		-4.1632	•	
2.33		-0.4595	<u> </u>	-0.0110	0.0336	0.0074	0.6779	-0.0453		-4.5024 -5.0575		
4.41		-0.073	4-0012	-0.0330	0.0275	0.0067	0.6406	0.0480 G.0480	0.5844 0.5844	-5.8218		
	0.U	-0.3615	3-2664	-0.0320 -0.0185	0.0575	0.0059	0.6046	0.0-80	0.4442	-10.1709		
	0.0	0.0575	2.4094	-0-0115	0.0433	-0.0038	0.4432	0.0507		30.7157		
4.51	0.0	0.1959	7.1219	-0.0115 -0.ulo1	0.0433	-0.0029	0.4606	U.0507	0.4101	5.6275		_
1.53	0.0	0.7147	1.7895	-0.0284	0.0905	0.0048	0.4554	0.0507	0.4047	2.7644		
2.60	6.0	1.0194	1.0284	-6.0431	0.1036	0.0058	0.4524	0.0507	0.4022	1.7940		
.67	0.0	1 - 3662	1.6113	-0.0311	G. 0847	0.0069	0.4509	0.0507	0.4002	1.1794		
4.73	0.0		1.3013	-0.0467	0-10-0	0.0080	0.4574	0.0480	0.4094	0.7633		
3.44			1.70-	-U.0634								
			0.7347	-6.0744			U.4719					
							0.4734	0.0426				
0.32	0.0	-1.0576	4./35/	-0.0177	0.0324	3.00/4	0.6794	0.0453	0.6341	4871		
_			·							<del></del>	<del> </del>	
		•						-				
						-						
		<del></del>			<del></del>	<del></del>						_
				<u></u>	•							
										· · · · · · · · · · · · · · · · · · ·		
							·	<del></del>			· <del></del>	
		<del></del>						<del></del>				
3	.67	.67 0.0 .73 0.0 4 0.01	.67 0.0 1.7662 .73 0.0 1.7379 4 0.01 2.1295 5 0.01 2.5395 6 0.01 3.0329	.67 0.0 1.3662 1.6113 .73 0.0 1.7379 1.3613 .44 0.01 2.1295 1.770- .55 0.01 2.5395 0.7347 .60 0.01 3.0329 0.7926	-67 0.0 1.3662 1.6113 -0.0311 -73 0.0 1.7377 1.3613 -0.0462 -44 0.01 2.1298 1.3700 -0.0034 -45 0.01 2.5368 0.7367 -0.0734 -60 0.01 3.0329 0.2926 -0.0073	-67 0.0 1.3662 1.6113 -0.0311 6.0847 -73 0.0 1.7379 1.3613 -0.0462 0.10-0 -44 0.01 2.1298 1.7700 -0.034 (.1272 -55 0.01 2.555 0.7367 -0.0764 0.15-3 -60 0.01 3.0329 0.2926 -0.0073 0.1611	-67 0.0 1.3662 1.6113 -0.0311 0.0867 0.0069 -73 0.0 1.7379 1.3613 -0.0467 0.10-0 0.0089 -44 0.01 2.1298 1.700.058 (.1272 0.0100 -55 0.01 2.559 0.7367 -0.073 0.1611 0.0128	-67     0.0     1.3662     1.6113     -0.0311     0.0867     0.0069     0.4509       -73     0.0     1.7379     1.3613     -0.0467     0.10-0     0.0080     0.4574       -4     0.01     2.1298     1.770	-67         0.0         1.3662         1.6113         -0.0311         6.0867         0.0069         0.4509         0.0507           -73         0.0         1.7379         1.3613         -0.0467         0.10-0         0.0080         0.4574         0.0860           -4         0.01         2.1293         1.770	-67 0.0 1.3662 1.6113 -0.0311 0.0877 0.0069 0.6509 0.0507 0.6002 -73 0.0 1.7379 1.3613 -0.0467 0.10-0 0.0080 0.4574 0.0860 0.40944 0.01 2.1293 1.700.0634 (-1272 0.0100 0.6652 0.0653 0.41995 0.01 2.5365 0.7347 -0.0744 0.15-3 0.0120 0.4719 0.0653 0.470860 0.01 3.0329 0.2926 -0.0873 0.411 0.0128 0.4734 0.0426 0.4308	-67 0.0 1.3662 1.6113 -0.0311 0.0867 0.0069 0.4509 0.0507 0.4002 1.1794 -73 0.0 1.7379 1.3613 -0.0467 0.10-0 0.0080 0.4574 0.0860 0.4094 0.78334 0.01 2.1295 1.7700.034 (-1272 0.0100 0.4652 0.0453 0.4199 0.50285 0.01 2.5365 0.7367 -0.0744 0.15-3 0.0212 0.4719 0.0453 0.4764 0.289900 0.01 3.0329 0.2926 -0.0073 0.1411 0.0128 0.4734 0.0426 0.4308 0.4965	-67 0.0 1.3662 1.6113 -0.0311 0.0867 0.0069 0.4509 0.0507 0.4002 1.1794 -73 0.0 1.7379 1.3613 -0.0462 0.10-0 0.0080 0.4574 0.0480 0.4094 0.78334 0.01 2.1293 1.7700.054 (-1272 0.0100 0.4652 0.0453 0.4199 0.56285 0.01 2.5365 0.7347 -0.0744 0.1563 0.012 0.4719 0.653 0.4766 0.289900 0.01 3.0329 0.2926 -0.073 0.1611 0.0128 0.4734 0.0426 0.4308 0.0965

	1 05			LANGLEY H	ESEAHCH C	ENTERIVAS	A)	UNITA	HY PLAN A	IND TUNK	EL (UPAT)	
	1 OF					764114 6	ISSILE TA	IL EFFECTS	UNIA	<del></del>		
157	- 1 m								·			
	TEST	EAST W	ALM PATE	6 PHI	CONF	1 (.61	1 DELZ	IFI 3 DEL A	TPANETT	044		
	3		30 2.5			.0 2	0 -20	20 -20				
	44 0/44			<b>5</b>	~-		<b>6</b> 1.1					
POINT	-3.00	BETA	-4-05-40	CL# 16.1274	-0-0013 CA	CL4	CLL -0-0211	2.7363	0.1505	CAF 2.045A	-3.9791	
ž ·	-2.07			14.4746				2.1098	0.1556		-4.1209	
3	-1.44			14.3215				5-1540	U-1573	1.0696	-4.2099	
•	0.02			13.4374				1.4484	0.1507		-4.3341	
5	2.07			13.0210		-0.04/3		1.6722	0.1641		-4.4584 -4.6227	
7	4.16			11-1967				1.6343	- <u>1.1656</u> 		-5.0675	
8	6.25		-1.6353	4.6211		-0-0766		1.4579	0.1692		-5.8834	
9	6.33		-100195			-6.0576		1.7054	0.1754		-7.6698	
10	10.43		-0.4634	7.6373		-0.05-6		1.1752	0.1510		-15.1732	
11	12.55	0.04	0.1416 0.7826	5.2614	-0.0366	-0.034Z	-0.0257	1.0732	0.1844	0.8068	42.9785 6.7485	
13	14.96			4.0776	-0.0434	-0.0534	-0.0270	0.9222	0.1844	0.7378	3.1722	
14	19.10		2: 1752	_3.66lo	-0.0550	-0.0419	-0.0213	0.575	0.1844	0.6731	1.7644	
15	21.17						-0.0450	0.7905	0.1827		1.0394	
16	23.40		-3-154-				-0.0393 -0.0333	1.9485	0.1624		0.5260 -4.3231	-· <u>·</u>
••	7945	0.40	-3.1540	1300341	0.0022	-6.10,7	-010333	103403	491354	1.001	-413531	
					<del> </del>					<del></del>	<del></del>	
					_							
			-									
						··· <u>-</u>	· · · · · · · · · · · · · · · · · · ·					
											·	
					<del></del>			<del></del>				<del></del>
									•			
		<del></del>				•						
							·					
												-

	1 OF 1			ANGLEY A	ESEANCH (	ZACIWITOS M HITHAM	A) ISSILE TA	UNITA	DATA .	IND TUNN	LL (UPST)			
ET	1 OF 1													
		<del></del>	•									·		
	TEST	PAPT FA	CH -X10-0	े हता	CUNF .	L CEL	1 DELZ	DEL3 DEL4	TRANSITI	ON				
	3	49 3.4	3.0	45.0 d	1=UF33	)•0 z	0 -20	20 -20	FIXE			<u> </u>	<u> </u>	
INT	ALPHA	SETA	C₩	CL#	CY	CLM	CLL	CA	CAR	CAF	XCP			
1	-3,43		-5.4471	9-480H		-0-1243		1.4342	0.0562		-3.0120			
2 .	-1.46		-2.1975 -2.0114	n-3/1-	0.0234	-0.1943	-0-0244	1.767	0.0562	1.2316	-4.0062			
3	0.16		-1.575	7.4313	0.0036	-0.0735	-0.05.0	1-2264	0.0543	1.2310	-4.3400			
<u> </u>	1.19		-1.5200	7.5001	0.0000		-0.0237	1.1704	0.0583	1.1121				
6	2.18		-1527	7-1043	-0.0125	-0-0490	-0.0235	1.1152	r.0605	1.0547	-4.8904			
7	4.30		-1 533	6-7444	0.0124		-0.0230	1.0070	0.0626	0.9444	-5.9197			
8	6.31			5.4466	-0.0165	-0.0417	-0.024	0.9230	0.0447	0.4583	-8.2136			
9	H-4-1	0.02	-0.2623	407237	0.0007	-0.06-1	-0.0216 -0.0207	0-6592	0.0669		-18-3908 42-4163			
10	10.47	0.02	0.10-0		-0.0169		-0.0204	0.7649	C-0669	0.7180	7.9547			
15	14.60	0.00	A AU3	3.7162	-0.0000		-0.0238	0.7726	0.0569	0.7057	4.2215			-
13	16.76	0.02	1.2923	3-4774	-6.0023		-0.0277	0.7777	0.0669	0.7108	2.6908			
14	14.95	0.02	1.7955		-0-0204		-0.0317	0.7760	0.0647	0.7113	1.9040		•	
15	50.00	0.02	5-14-1			-2-12-7		0.7633	0-9426	0.7007	1.3096		-	
16 17	23.04	0.02	7.755z -1.4143	7.9055		-0.1048		1.2249	0.0605	0.6753	-4.3573			
.,	1.010	0.03	-10-145	109055	0.0177	-041103	-0.0240	105544	444603	101000				
								<del></del>						
												··· <del>-</del>		
			<del></del>											
										•	,			
								-		<del></del>		•		·
														•
					<del></del>	<del> </del>			<del></del>					<u> </u>
							•							
										,			•	
	•													
				·				·						
												·····		
							•							
			<del></del>	<del>:-</del> -										

	1 OF				LANGLEY H	ESEAHCH C	ENTENCHAS MARTIN M	A) ISSILE TA	UNITAL LL EFFECTS	RY PLAN I	IND TUNH	EL (UPUT)	
. Y	1 0	1			<del></del>	<del> </del>					<del></del>		
				CH HATU-					DEL3 DEL+				
	3		50 4.0	64 3.0	45.0 8	1=0F33 0	.0 2	0 -50	20 -20	FIXE	)		
NT	ALP-		RETA	CN	CLM	CA	CLN	CLL	CA	CAB	CAF	XCP	
l	-3.0		0.02	-2.2033			-0-1001		1.2974	0.0433		-3.7989	
	-1.4		0.02	-1.4175	7-4462	3.0154	-0-1049 -C-0616	-0.0146	1.1006	0.0406	1.1660	-4.0137 -4.2201	
	0.5		0.60	-1-50-0			-0.0768		1-0931	0.0433	1-1007	-4.4662	
5	1.5		0.00	-1.3071	0.5097	-C. GOS	-0.0711	-0.0179	1.0421	0.0433	AHPPAO	-4.7548	<del></del>
6	2.6		4.00	-1.1450	A-1577	-0.6174		-0.0176	0.4913	0.0433		-5.1520	
,	4.1		0.02	-0.6129	5.4470	3.0014	-0.0014	-0.0237	0.8999	0.0433		-6.7007	
<b>B</b>	6.0	9	0.41	-0.4471	4./074	0.0025	-0.0714	-0.0230	0.4312	0.0460	0.7852	-10.6630	
9	4.7			-031152	4.5107		-0.0948		0.7819	G-0+60	0.7359	-37-4208	
D	10.7		0.01	2902.0	3.9826	0.0257	-0.1855	-0.0781	0.7534	0.0457		19.3143	
1	12.6		0.01	0.5309				-0.0271	0.7449	0.0467	0.6962	6.9379	
2	14.6		0.01	0.4352			-0.1092		0.7442	0.0467	0.6955	4.2784	
3	16.			1.2204			-0.13un		0.7343	0.0460		2.6751	
5	21.0		6.01	2-1959	2.4-11	-0.0104	-0.1219	-0.0535	0.7178	0.0460	0.6565	1.6978	
5 6	23.		0.01	7.6444		-6-0271	-0.1004	-0-1720	0.675B	0.0406	0.6352		
7		57	0.02		6.7807	-0-0010	-0.0758	-0.0181	1.0931	0.0406		-4.4668	<del></del>
												•	
					<del></del>			<del></del>					
												<del></del>	
_													
												•	
								<del> </del>					
										_			
										<u> </u>			<del></del>

_				LANGLEY H				UNITA		IND TUNK	EL (UPST)		
	1 OF 1		<del></del>		<del></del>	MARTIN M	ISSILE TA	IL EFFECTS	DATA				
									·	<del> </del>	<del></del>		
	3		36 2.9		1+0F33 0			DEL3 DEL4					
OINT	ALPHA	RETA	C4	CLM	CY	CLN	CLL	CA	CAH	CAF	KCP		
1	-3.5e	0.0	-0.7029	1.4784	-0.0357	0.1391	-0.0119	0.4478	0.1219	0.3259	-2.3078		_
3	-0.95	0.0	-0.393-		-0.0537	0-1720	-0.0150	0.4441	0.1103	0.3256	-2.4193 -2.4800	<del></del>	
٨	0.09	0.0	0.0176	-0.0157	-0.0665	0.2024	-0.0179	U-4-15	U.1163	0.3252	-1.0090		
6	2.15	0.01		-0-4642			-0.01.0 -0.0137	0.4450	0.1162		-2.1844 -2.2772		
7	4.26	0.0	0.4114	-1.0451	-0.0511	0.2153	-7.0044	0.4551	0.1265	0.3286	-2.3218	<del></del>	
9	6.33	0.01		-2.4324		0.2267	-0.0194	0.4746	0.1382		-2.3013 -2.2434		
10	10.59	0.61		-5.2091		0.2666	-0.0215	0.4975	0.1484		-2.1559		
11	12.77	0.01		-6. 7347		0.2901		0995	0-1481		-2.0489		
13	17.13	0.01		-7.4345 -n.6357		0-2550	-0.0135 -0.0115	0.4966. 0.5020	0.1451		-1.9636 -1.9085		
1.	14.36	0.02		-4.4542		6.2.39		0-5104	6.1349		-1.8661		
15	21.54	0.01		-11-1544		0.2940		0-5157	0.1276		-1.8422		
16	23.79	0.02	0.0100	-12.6467	-0.0535	0.3272	-0.0144	0.5347	0.1204		-1.8337 -1.0000		
					··········								_
			<del></del>				<del>_</del> _					<del></del>	
												•	
							· · · · · · · · · · · · · · · · · · ·						
							-		, ,		•		
					• • • • • • • • • • • • • • • • • • • •								
													_

-47

	1 OF 1			LAMOLEY N	ESEARCH C		A) )1551LE_TA	UMITA IL EFFECTS		IND TUNK	EL (UP+T)	
	1t 5 f		30 2.9 30 3.0	6 -41 45.0 b	CUNF 1+0F33 0		1 DEL2 1	EL3 DEL4				
INT	ALDHA	SFTA	CN	CLM	CY	CLN	CEL	CA	CAR	CAF	XCP	
_	-3.57	0.00	-0-690 4		-0.0764	0-0450		0.4440	0.1188		-2.2757	
ζ	-1.97 -u.9c	0.01	-0.1817		-6.0775	0.0344	-0.0149 -0.0142	0.4434	0.1175	0.3259	-2.2443 -2.1969	
<b>3</b>	0.10	0.01	0.0260		-0.0504	0.0957	-0.0216	0.4411	0-1160	0.3251	-3.1657	
5	1.14	0.01	0.2080	-0.5674	-0.0365	0.0753	-0.0178	0.4432	0.1160	0.3272	-2-5260	
6	2.14	0.0	0.3950	-6.0463	-0.0375	C-0835	-0-0140 -	0.4443	0.1174	0.3769	-2.4857	
7	4.23	-0.01	0.4634		-0.0251	0.0470	-0.0207	0515	0.1218	0.3797		
8	6.31	-0.01 -G.ul	1.2435	-3-100/	-0.024H	1140.0	-0.0236	0.4577	0.1335 0.1409	0.3342	-2.397 <u>1</u> -2.3259	
0	10.55	-0.01	204614		-0.0701	0.1555	-0.0181	0.4827	0.1379	0.3445	-2.21 <b>25</b>	
<del>i -</del>	12.76	-0.02	3.1275		-0.0E34	0.1767		0595	0.1409	0.34E9	-2-0698	
ž	14.96	-0.02	3.4054		-0.0670	0.1530		0-5005	0-1424	0.3581	-1.9639	
3	17.07	-0.02		-h.6778		0.2051	-0.0171	0.5064	0-1-40	0.3624	-1.9100	
•	10.50	-0.63	5.2453		-0.1116		-0.0192	0.5204	0.1-68		-1.8669	
5 6	23.72	-(1-,14		-11.4266		(-2531	-0,0284	0.5350 0.5462	0.143d 0.1351	0.3912	-1.8676 -1.8862	
7	6.09	0.01	0-0242	-0.0438	-2-0300	0.0510		0.4432	0.1175		-2.8692	
								•				
											,	•
											<del></del>	
		<del></del>		<del></del>		<del></del>					·····	
							<del></del>				<del></del>	
			•									
		<del></del>										<del></del>
		•									•	_

E	1 OF 1			LAMOLET H	ESEMBCH C	ENTER(NAS	A) ISSILE TAI	UNITA	HY PLAN I	IND TUNK	LL (UPST)		
	1 OF 1	~		<del></del> -		MAKITA P	.1221FE IN	F. ELLECIS	UATA				
•												,	
					•	•							
	TEST	PART W	ACH RAIO-	6 Pnl	CONF	L UEL	.1 UEL2 i	DEL3 DEL4	THANSIT	OM	<del></del>		
	. 3		66 3.2		1=0+33 4		0 0		, FIXE			•	
								_					-
	ALPHA	0.01	-0.6235	CLM	CY	CLM	-0.0161	<u>CA</u> 0.3907	CAR 0.0953	0.2954	1.917Z		
2	-2.01	0.0	-0.3535	0.6471	-0.0133	-0.0018	-0.0082	0.3945	0.0951	0.2994	-1.8306	•	
3	-1.00	0.01	-0-1759	0.3992	-0.010-	0.0037		0.3958	0.0969	0.2989	-1.7477		
•	0.06	0.01	0.0040	-0-0-64	-0.0292	_0.0337		0.3943	0.6964	0.3009	-5.2000		
5	1.11	0.0	6.1421		-0.0164	0.0150		0.4000	0.0969	0.3031	-2.1578		
6	2.13	0.0	0.3465	-0.7214	-0.0142	0.0716	-0.0107	0.4001	0.0969	0.3032	-2.0820	<del></del>	
<u>'</u> .	4.23	0.0	0.7144	-1.4733	-0.0293	0.0376		0.4036	0-0984	0.3052	-2.0622		
<del>- G</del>	5.43	-0.01	1.1470	-2-3255	-0-0777	0.0465	-0.0094	0.4238	0-1076		-7.0225	<del></del>	<u>·</u>
10	19.55	-0.01		-4.1474		0.0448	-0.0111	0.4238	0-1075		-1.8992		
<del>ii                                    </del>	12.50	-0.01	2.7854	-5.0714			-0.0136	0.4370	0.1075		-1.0200		
iż	14.54	-0.01	3.3972		-0.059	0.1276	-0.6122	0.4448	0-1060		-1.7601	_	
13	10.49	-0.42	4.0-14	-7.0124	-0.0935	0.1555		0.5733	0.1060		-1.7351		
1+	19.23	-0.6¢	4.7169		-0.0976	0-1515			0.1045		-1.7292		
15	71.7e	-0-03	5-4115		-0-0406	0.1652		0.4903	0-1015	0.3868	-1.7392		
16	7.09	-0.04	4.7556	-11.0330	-0.0924		-0.01-1	0.5113	0.0953		-1.7637		
1 /	W V V	0.01	6.0144	-0.0533	-0.0143	C-0137	-0.0113	0.4009	0.0984	0.3053	-2.7454		
— <del></del> -							<del></del>		•				
								•					
									<del> </del>				
								•					
													•
•							-	-					
									- <del></del>	<del></del>			
									<u> </u>				
	<u> </u>												
			<del></del>		<del></del>	<del></del>		<del></del>	<del></del>				
				·							<del></del> -		
		•											

7 1 7 7 7 1 7

	1 OF 1			LANGLEY H	ESEANCH C	ENTER(NAS	A) ISSILE TA	UNITA	HY PLAN .	IND TUNN	EL (UPaT)	
Ţ	1 OF 1										-	
			· · · · · · · · · · · · · · · · · · ·	<del></del>		·		1				
	TEST	PAPT P	ALE SAIGE	6 701	COUL	1 181	1 0612	UEL3 DEL4	TRANSIT	ON	<del></del>	
•	3	54 2	bo 3.2	0.0 +	1 × 0 F 33 0	• 0	0 0	0 _ 0	FIRE			
A) 7	ALPHA	HETA	CN	CLH	CA	CLN	CLL	CA	CAB	CAF	ACP	
701	-3.71		-0.6355				-0.0125	0.3966	0.0984		-1.9991	
<u> </u>	-7.16	0.01	-0.3454	C.7161	-0.0615	6-1158	-0.0091	0.3956	0.0959	1005.0	+7.0649	
,	-1-13	0.01	-0.15])	10-3453	-0.0503	r.1129	-0.007H	V.3976	0.0969	0.3007	-2.1039	
	-0.07 J.96	0.01	0-17-6	-0.3293	-6.0137	0-1436	-0.0075 -0.0071	0.4006	0.0984	0.3022	-6.5714 -1.8198	
	1.96	0.01		-0.6235		0.1297	-0.0068	0019	0.0984	0.3035	-1.9136	
	4.09	0.01	0.7100	-1.3440	-0.0714	6.1532	-0.0061	0.4072	0.0999	0.3073	-1.9493	
	4.16	0.01		-2.17n5			-0.0052	0.41##	0.1045	0.3143	-1.9450 -1.9260	
)	10.39	0.41 0.0<	2-17-5	-3.0450 -6.000	-0.0751		-0.0074	0.4292	0.1106 0.1136		-1.8735	
	12.53	0.02		-4.760+			-0.0051	0.4368	0.1106	0.3262	-1.8026	
2	14.70	0.02	3.364	-5 · n 755	-0.1151	0.2557	-0.0035	0.4435	0.1091	0.3347	-1.7544	
	16.87 19.96	0.05		-6.4154		0-2740	0.0019	0.4529	0.1060		-1.7247	
5	21.16	\$0.0	5.3710	-4.711c	=101317	6.2574	0.0111	0.455 0.4798	0.1030	0.3799	-1.7122 -1.7146	
<b>N</b>	23.44	U.03		-10.7552		0.2845	0.7147	0.4955	0.3923		-1.7422	
-	-0.00	0.01	-0.303>	0.6230	-0.0740		-0.0037	0.3994	0.0984	0.3010	-6.5714	
							<del></del>	<del></del>	<del></del>			
		1000										
					-							
												•
							<del> </del>					
			······	<del></del>			·					<del></del>
							_ · -					
					<del></del>							
						- <del></del>						

1	3	PART -						IL EFFECTS	DATA	··		
1	3	PART W			<del></del>							
1	3	-	CH PXIU-	6 PHI	CUNF	L GEL	1 DEFS	JELS DEL	THANSIT	04	<del></del>	
THE		55 3.9	65 3.0	45.0 H	1 + UF 33 0	. 0	0 0		FIXE			
1		BFTA	CN	CLM	C∢	CLY	CLL	CA	CAB	CAF	XCP	
	-3.42	0.01	-0.4614		-0.0191	0.01-6	0.0042	0.3115	0.0637	0.2.78	-1.3534	
<u>z.</u>	-1.49 -C.40	0.01	-0.23-7	0.2967	-0.0307	0.0252	-0.0003	0.3113	0.0616	0.2497	-1.2641 -0.9d23	<del>-                                    </del>
4	0.19	0.0	0.0453	-0.1095		2410.0	0.0001	0.3129	C.0616	0.2513	-2.4243	
5	1.21	0.0	0.1000	-0.51HH	-0.0235	0.6366	0.0057	0-3141	0.0016	0.2525	-1.7101	····
6	2.22	0.0	0.3275	-0.526+	-0.0292	0.0347	0.0007	0.3170	0.0616	0.2554	-1.6089	
-	4.29 6.34	0.0	0.9693	-0.7770		0.0354	0.0021	0.3234	0.0538	0-2546	-1.5730 -1.573A	
9	A 3	6.0	1.3651	-2.1233	-0.v3e5	0.0535	-0.0023	0.3389	0.0659	0.2730	-1.5734	
10	10.46	0.0	1.7952	-2.726.	-6.6455	0.0725	-0.0013	0.3514	0.0659	0.2855	-1.5107	
11	12.50	0.0	2.2535	-3.356-		0.0919	-0.0054	0.3531	0.0638	0.2993	-1,4903	
12	10.70	0.0	2.7676	-4.1273 -5.0350	-0.0706	0.1336	-0.0043	. 6-3212 0-4041	0.0595	-0-3196	-1.4902 -1.5088	
14		-0.01	3.9416	-6.7434	-0.0491		-0.0072	0.4254	0.0574	0.3540	-1.5334	
15	20.93	-0.01	4.5410	-7-171p	-6-0495	0.1572	-0.0059	0.4467	0.0531	0.3456	-1.5334 -1.5654	<del></del>
16		-0.01	5.3044	-8.4334	-0.1124	0.1650		0.4731	0.0489	5+5+0	-1.5897 -2.2756	<del> </del>
17	0.19	0.01	0.0603	-0.1372	-0.0300	0.0274	0.0001	0.3110	0.0595	0.2519	-2.2756	
			•									
				<del></del>					····			<del></del>
							•					
										· · ·		
										-		
							·	<del></del>			······································	
										<del></del>		

2 - 3 - 5 6 7 8 9 10 11 11 11 11 11 11 11	3		0.1477 0.2667 0.6000 0.9014	0.0 b	CY -0.6231 -0.0312 -0.0464 -0.0431 -0.0372	O CLN	-0.0012 -0.0006	CA 0.3080 0.3087 0.3084	TRANSITI FIXEG CAM 0.0616 0.0616 0.0616	CAF 0.2464 0.2471	-1.4011 -1.4171 -1.4434	
3 - 5 6 7 8 9 10 11 11 12	ALPHA -3.61 -2.36 -1.06 0.01 1.00 2.61 4.69 6.16 d.24	DETA 0.0 0.0 0.0 0.0 0.0 0.0 0.0	CN -0.4704 -0.2702 -0.1352 -0.1457 0.2167 0.2167 0.4002 0.9014	CL# 0.0000 0.3415 0.1907 -0.0235 -0.2181 -0.0208	-0.0372 -0.0312 -0.0431 -0.0372	CLN 0.0560 0.0407 (.04-3 0.0964	-0.0012 -0.0003	CA 0.3080 0.3087 0.3084	CA9 0.0616 0.0616	CAF 0.2464 0.2471	-1.4411 ·	
3 - 5 6 7 8 9 10 11 11 12	-3.61 -2.36 -1.06 0.01 1.00 2.01 4.09 6.16 d.70	0.0 0.0 0.0 0.0 0.0 0.0	-0.4704 -0.2092 -0.1359 0.0149 0.1477 0.2607 0.4000 0.9414	G.0006 0.3415 0.1467 2650-0- 2650-0-	-0.6231 -0.0312 -0.0164 -0.0431	0.0560 0.0907 0.096	-0.0012 -0.0006 -0.0003	0.30#0 0.30#7 0.30#4	0.0616 0.0616	0.2464	-1.4411 ·	
2 - 3 - 5 6 7 8 9 10 11 11 11 11 11 11 11	-2.06 -1.0d 0.01 1.0u 2.01 4.09 6.16	0.0 0.0 0.0 0.0 0.0	-0.7h92 -0.1359 0.0149 0.1477 0.2h07 0.4000 0.4000	0.1767 -0.1767 -0.253-0- 1815-3-	-0.0312 -0.0164 -0.0372	0.09b4	-0.0003	0.30#7 0.35#4	0.0616	0.2471	-1-4171	
3 - 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	1.00 1.00 2.01 4.09 6.16 3.74	0.0 0.0 0.0 0.0 0.6 0.0	0.1359 0.0149 0.1477 0.2667 0.4000 0.4000	-0.1462 -0.2181 -0.2181 -0.248	-0.0164 -0.0431 -0.0372	0.0954	-0.0003	0.3684				
5 6 7 8 10 1	0.01 0.01 0.01 6.09 6.16 6.24	0.6 0.0 0.6 0.6	0-0149 0-1477 0-2667 0-6000 0-9-14	-0.0235 1015.0- 6454.0-	-0.0431	0.0964			V = U = I I			
5 6 7 8 9 10 1	1.00 7.01 4.09 6.16 3.74	0.0 0.0 0.6 0.0	0.1477 0.2667 0.6000 0.9014	-0.4248	-0.03+Z		~~~~~	D - ROMP	0.0615		-1.5745	•
6 7 8 10 1	7.01 4.09 6.16 3.74	0. U 0. G 0. U	0.2667 0.4000 0.9414	-0-4246			0.0004	0.3105	0.0616		-1.4765	
8 9 10 1 11 1	6.16 6.26 10.29	0.G 0.v	0.400e n.9414	-0.5465		6.0263	0.0007	0.3133	0.0616	0.2517	-1.5133	
8 10 1 11 1	6.16 3.74 10.29	0.0	0.9414		-u-0-60	6.0849		0.31-3		0.2555	-1.4917	
10 1 11 1 12 1	9.50 10.29	0. 4		-1.4107			-0.6029	0.3252	0.0638		-1.5070	•
10 1	10.29		1 。 345と	-20-341		0.1139	-0.0019	0.3377	0.0559	0.2718	-1.5156	
12 1	12-36		1.7471	-2.6350	-0.0715	0.1644	-0.0008	0.3510	0.0459	0.2051	-1.4912	
12 - 1		0.01	2.7775	-3.2831	-0.0787	0.1660	0.0004	0.3655	0.0659		-1.4726	
	14.47	0.01	2-7142	-3.9924	-0.0776	0.1735	0.0056	0.3825	0.0638		-1.4709	
	15.57	0.01				0.1951	Se00.0	0.0012	0.0616		-1.4911	
	19.74	0.71		-5.9421		C.174A	0.004	955000	0.0595		-1.5240	
	20.75	3.01		-1-4545		0.1790	9.0111	0.4444	0.0552		-1.5616	
	25.43	0.01	5.2750	-6.453	-0.0723	0.1732	0.0233	0.4700	0.0510		-1.6004	
17	-0-05	0.0	0-01-5	-0.0255	-0.0434	0.0826	9.0001	0.3100	0.0595	0.5203	-1.5726	
						<del></del> -		<del></del>			<del></del>	
								•				
										-	•	
					<u> </u>							
			·									
			<del></del>			<del> </del>						
									-			
											<del></del>	
								<del></del>				
										•		
								<del></del>	<del></del>			
				•								
		·						<del></del>				

-----

٠. .

											#		
PAGE	1 OF			LANGLEY H	ESEARCH CE		A) 1551LE TAI			IND TUNN	EL (UPWT)		
SHEET			<del></del>				1331FF 144	L EFFECTS				<del></del>	<del></del>
ę	-		·				<u> </u>	<del></del>			<del> </del>	· · · · · · · · · · · · · · · · · · ·	
				•				•	•				
	165	Y PART .	ALP KAID-	6 PHI	CUNF	L UEL	I OELZ	DELS DELA	TRANSIT	OM			<del></del>
	3	57 4	64 3.0	0.0	1.0F33 0		0 0		FIXE				
POINT	ALPHA	9FTa	CN	CLH	CY	CLN	CLL	CA	CAR	CAF	ACP		•
1	-3.25		-0.4107	0.4774	0.0087	0.0243	-0.0012	0.2887	0.0447		-1.1636	<del></del> :	<del></del>
ż	-1.49		-0.1946	0-7262	45E0.U-	0.0771	-0.0006	0.2464	0.0447	0.2421	-1.1673		
3	-0-15		-0.0735	6-66-4	-0-0-20	0.0044	-0-0005	0.2686	0.0447	0.2439	-1-1551		
•	0.30		0.0400		-0.0515	0.1010	0.0061	0.2862	0.0447	0.2415	-1.2034		
5	7.35		0-1404	-0-2257 -0-3640		0.0976	0.0005	0.2890	0.0447	0.2443	-1.1631 -1.1712		
<del></del>	4,42			-0.7196		0.0530	0.0016	0.2937	0.0447		-1.1992		
8	6.45			-1.2259		0.0409	5+00-0-	0-3018	0.0447	0.2571	-1.2796		
9	4.55			-1.690-		0.6752	-0.0033	0.3142	6.0447		-1.2967		
16	10.57			-2-2031		0-1256	-0.0023	0.3277	0.0474		-1.3157		
11	12.61			-3.6136		0-1320	-0-0013 -0-0001	0.3416	0.0474		-1.3485 -1.4025		
13	16.70			-4.5522		0.1.64	0.0010	0.3764	0.0447		-1.4764	·	
14	16.42		3.7110	-5.7503	-0.1014	0.1912	0.0023	0.3990	0-0470		-1.5492	_	
15	50.AF			-7.0073		0-1520	0.0103	0.4240	0.0392		-1.6149		
16	23.96			-8.4810		0.1549	-0.0016	0.4509	0.0365		-1.6752		
17	0.32	0.0	0-0-53	-0.0556	-0.0245	U-0665	0-0001	0.2869	0.0420	0.2469	-1.2013		
	<del></del>		····				<del></del>				<del></del>		
						<del> </del>	<del></del>						
					•						•	-	
												<del></del>	
				·									
							<del></del>					<del></del>	
						-					•		•
			<del></del>	·	*					<del></del>			
<del></del>						<del></del>		<del></del>	<del> </del>	<del> </del>			
		······································											
								•		_			
					<del></del>								
		-											

.

THE PROPERTY.

6E	1 OF 1	·		LANGLEY HI	SEAHCH C	ENTERL-AS MARTIN M	A) 1551LE TA	UNITA	ARY PLAN M	IND TUNN	EL (UPWT)		
					<del></del>	··· · · · · · · · · · · · · · · · · ·		· · · · ·				· · · · · · · · · · · · · · · · · · ·	
	TEST		ALH PAIU-		-		0 0		TRANSITI	UN			
OTAT	ALPHA	BETA	CN	CLM	· C4	CLN	CLL	CA	CAR	CAF	xce		
	-5.95	4.0	-0.7495			-9.0026	-0-0010	0.2908	0.0447	0.2451	-1.0674		
ž	-1.44	0.0	-0.1571	0.1045	-0.0072	-0.0143	-0.0005	0.2903	0.0446		-0.9865		
3	0-47	0.0	-0.1570	0.3334	-0.0135	0114	-0.0002	0.2410	0.0446		-0.5979		
•	0.59	0.0	0.0724	-0-1096			-0.0046	0.7914	0.0446		-1.5050		
5	1.56	0.0		-1.2050		0.0196	0.0005	0.2922	0.0446		-1.3070 -1.2669		
-6	2.60	0.0	0.6250	-0.74by		6-0135	-0.0052	0.2948	0.0446		-1.2750		
8	6.71	0.0		-1-2712		0.0362	-0.004	0.3053	0.0473		-1.3397		
<del>Q</del>	A.78	.0.4		-1./6/4			-0.0104	0.3158	U.0473	0.2645	-1.3592		
10	10.42	0.0		-7.308.		6.0358	-0.0094	0.3270	0.0473		-1.3529		
11	12.46	0.0		-2. ¥306		6.0775	-0.0065	0.3408	0.0473		-1.3764		
12	10.94	0.0	2-6011	-3.7192	-0.0624		-0.0075	0.3598	0.0474	0.3124	-1.4299		
13	17.01	-0.01		-4-6127			-0.0065	0.3794	0.0446		-1.4749		
15	21.12	-0.01	3-555	-5-5746	-0.0613	0-12-6	-0.0054	0.4225	0.0392	7.3563	-1.5144 -1.5481		
16	23.27	-0.41	4.2010	-7.7675	-0-0672	6-1358	-6.0097	0.4450	0.0337	0.3033	-1.5606		
17	0.58	0.0	0.0720	=0-1092	=0-0017	-0.0206	0-0001	0.2930	6.0392	0.2538	-1.5003	<del></del>	
				<del></del>							-		
	<u>,</u>	•	<del>.</del>			<del></del>	•	J.					
				•									
											· · · · · · · · · · · · · · · · · · ·		
	,	<u> </u>											
											·		
										•			
				<del></del>			-					<del></del>	
							·			<del></del>			

LANGLEY RESEARCH CENTER (-ASA) UNITARY PLAN WIND TUNNEL (UPOT)

MANTIN MISSILE TAIL EFFECTS DATA

PAGE 1 OF 1

SHEET TOF I

A GA	1 OF 1			LAHGLEY H	ESEAHUH C	ENTENINAS	A)	UNITA IL EFFECTS	RY PLAN	IND TUNN	EL (UPAT)	<del>,,                                    </del>
EET	i of i			•				E LIVEUIS	,		,	
	•	<del></del>						<del></del>		·····		
	VEEV	DADY W	4 C S	<b>ह</b> हना	COLE	1 664	1 0613	DEL3 DEL4	73 A N P 7 P 7	(O)		·
	3		36 3.0		1×0F34 0	L DEL	0 0	0 0				
AO I N. T	ALPHA	6FT4	C4	CLM	CY	CLN	<b>C</b> 1		CAR	5.5		
1	-3.56		-0.736H		-0.0097		CLL 0.0356	0.4249	0.1239	0.3010	-2.4030	
2	-2.01	0.01	-0.4760	1.0475	-0.0172	-0-0344	-0.031A	0.4212	0.1274	0.2988	-2.4589	
3	-0-98	0.01	-6-55%	0.56m4	-0.0191	-0.0342	-0.0384	0.4190	0.1775		-2.5556	
	1.15	0.01	0.0003	-0-1645	-0.0314		-0.0382	0.4170	0.1210	0.2960	219.2664 -2.0100	<del></del>
6	2.15	0.0	0.3720	-0.6149	-0.0281		-0.0330	0.4150	0.1197		-2.1906	•
7	4.25	0.0	0.7950	-1.0711	-0.0152	-0.01:15	-0.0312	0.4728	0.1268	0.2950	-2.2455	
8	6.33	-0.ul	1.2752	-2.901c	-0.0737	0.0124	-0.0331	. 0.4349	0.1352	0.2997	-2.2702	
10	10.59	-0.02		-3.9667 -5.6144		0.0758	-0.0405	0.4427	0.1423		-2.2129 -2.0964	
-11	12.75	-0.01	3.0120	-5.7930	-0.0701	0.0962	-0.0434	0.4501	G. 1451	0.3050	-1.9546	
12	14.94	-0.02	3.6713	-6.017v	-0.0734	0.0957	-0.0456	0.4605	0.1489	0.3116	-1.8571	
13	17.13		4.3517	-7.7405	-0.097K			0.4603	0.1452	0.3151	-1.7806	
15	21.55	-c.03	F. CH29	-R-Fays	-0.0763	0.0019	-0.0576	0.4742	G.1479 G.1465	0.3199	-1.7419 -1.7261	
16	23.78		£ .7155	-11.6509	-0.1160	0.1460		0.4884	0.1440	0.3404	-1.7340	
17	0.06	0.01	-0.00me	7500.0	-0.0315		-0.0302	0.4169	0.1211	0.2458	-9.6405	
					<del></del>							·
											· · · · · · · · · · · · · · · · · · ·	
				<del></del>	<del></del>							
	•											
			·	<del></del>		<del></del>	<u> </u>				·	
								-				•
											<del></del>	
					-							

			, , , , , , , , , , , , , , , , , , ,									
				LANGLEY H	ESEARCH C				AHY PLAN A	IND TUNA	EL (UPWT)	
	1 OF 1					M MITHAM	ISSILE TA	IL EFFECTS	5 DATA	•	<del></del>	
ET	1 OF 1											
								<del></del>	<del></del>		<del></del>	
										•		
	TEST	PART -	ACH HATU-	6 PHI	CONF	L ULL	I UELS	DEL3 DEL	THANSIT	ON		
	3	61 ć.	80 3.0	45.0 B	1 = 0 F 3 4 0	• 0	0 0	0 (	0 FIXE	<u> </u>		
0 T A. T	ALPHA	BETA	CN	CL-	CY	CLN	e.	CA	CAR	CAF	xcp	
10101	-3.55	- 6. 1	-0.65-4	1.3395	0.0036		-0.07d7	J. 37 44	-0.1011		-2.0329	
è	-7.00	0.01	-0.3572	11.753-	-4.0041	-0.0503	-0.0242	0.3764	0.0979		-2-1091	
3	-0.40	0.01	-0.1703	(.3444	-0.0155	-0.03ah	-0.0278	U.3764	0.0979	0.2765	-7.2890	
•	0.96	0.01	-0.0147	C. UHU 4	-0.0155	-0-0374	-0.9236	0.3756	0.0995	0.2761	-5.4612	
5	7.13	0.41	6.1443	-0.7645	-0.0722	1650-0-	-0.0256	0.3761	0.0445	0.2766	-1.6014	
6	2.13	0.0	0.3345	-0.5107	-0.0176	-0.0207	-0.0256	0.3768	0.0979	0.2789		
7	4.25	6.0	0.7001	-1.3455		-9.0400	-0.0276	0.3818	0-1311		-1.9219	
8	6.31	-0.61	1-1155	-2.4710	-0.015*	-0.0146 -0.0145	-0.0254	0.3900	0.1075	0.2625	-1.9159 -1.8696	
10	10.53	-0.01			-0.0375	0.01-1	-0-030-	0.0900	G-1123	0.2851 0.2877	-1.7892	
11	12.46	-0. vI		-4.520+		0.0325	-0.7340	0.4004	0.1123		-1.7034	
is	14.40			-5254		C. 04d4	-0-0366	0.4139	0-1091		-1.6487	
13	10.45	-0. Ui	3.9000	-r. 3274	-0.0660	0.0716	-0.0342	0.4226	0.1091	0.3135	-1.6192	
1.	19.17	-0. ui		-7.3627		0.0440	-0.0457	0.4332	0.1091		-1.6159	
15	51.50	-4) · uc	4.5000			0.0576	-0.04m3	0-4472	0-1075		-1.6243	
16	23.46	-0.03		-9.4678		0.0A31	-0.0506	0.4655	0.1059		-1.6530	
17	0.05	0.01	-0.0027	0.0724	-0.0524	-0.0255	-0-0276	0.3770	0.0995	0.2775	-26.8074	
•	<u> </u>					····						
								<del></del>		·		
											<del></del>	
								<del></del>			<del></del>	
							•		·			
			•				-					
						<del> </del>	··-		· · · · · · · · · · · · · · · · · · ·			

1 -3.71	## CR   CLM   CT   CLM   CLL   CA   CAB   CAF   XCP      0		1 OF			LANGLEY N	ESEARCH (		(1551LE TA)			IND TUNK	EL (UPaT)	
1 -3.71	0.01 -0.3-a7 (.76cv -2.01) -0.06/5 -0.0209 0.37/6 0.0095 0.2771 -7.0454 0.01 -0.3-a7 (.76cv -2.01) -0.0167 0.0167 0.3766 0.0095 0.2771 -7.0454 0.01 -0.21 0.465 0.0077; -2.0167 0.01 0.3765 0.0095 0.2771 -2.0167 0.01 -0.0763 0.077; -2.0167 -0.0168 0.3772 0.0995 0.2777 -3.1541 0.01 -0.0763 -0.077; -2.0167 -0.0168 0.3772 0.0995 0.2777 -3.1541 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.													
7 -7.19	U.U1 -0.3-a7	INT								. CA				
3 -1.16	0.01 -0.0700 0.077: -0.0167 -0.0271 -0.0133 0.3795 0.0995 0.2777 -3.1541 0.01 -0.0700 0.077: -0.0167 -0.0270 -0.0116 0.3772 0.0995 0.2771 -3.1541 0.01 -0.0100 -0.0273 -0.0270 -0.0100 0.0995 0.2771 -1.7671 0.0 0.03200 -0.0100 -0.0073 -0.0300 -0.0125 0.3780 0.0995 0.2771 -1.7671 0.0 0.03200 -0.0115 -0.0073 -0.0125 0.3780 0.0995 0.2775 -1.8746 0.01 0.0700 -1.3050 -0.0115 -0.0262 -0.0131 0.3843 0.1027 0.2816 -1.9329 0.01 1.1120 -7.1173 -0.0311 0.0110 -0.0170 0.3967 0.1091 0.2876 -1.9027 0.01 1.5514 -2.0070 -0.0200 0.0100 0.3967 0.1091 0.2876 -1.9027 0.01 2.5774 -4.7263 -0.0263 0.0100 -0.0228 0.0115 0.1155 0.2960 -1.8159 0.02 3.3304 -5.5596 -0.0573 0.0498 -0.0252 0.0150 0.1139 0.3007 -1.7329 0.02 3.3304 -5.5596 -0.0573 0.0498 -0.0237 0.0200 0.1107 0.3093 -1.6815 0.02 3.3004 -5.0596 0.0573 0.0498 -0.0237 0.0200 0.1107 0.3093 -1.6815 0.02 3.3004 -5.0596 0.0573 0.0498 -0.0237 0.0200 0.1107 0.3093 -1.6815 0.02 3.5310 -0.0467 -0.0511 0.0234 -0.0264 0.075 0.3199 -1.6446 0.02 3.5310 -0.0467 -0.0511 0.0234 -0.0264 0.0577 0.3523 -1.6819 0.02 5.2310 -0.0655 -0.0162 -0.0268 -0.0110 0.3760 0.0935 0.2765 -5.7333	Ĭ								3.37/6			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
+ -0.96	0.01 -0.07ee 0.077: -2.0187 -0.07em -0.0118 0.3772 0.0995 0.2777 -3.1541 0.01 0.1ev -0.2633 -0.07em -0.01em -0.0121 0.37em 0.0995 0.27em -1.7671 0.0 0.37ev -0.01e -0.073 -0.03em -0.0125 0.37em 0.0995 0.27em -1.8746 0.0 0.37ev -0.01e -0.073 -0.03em -0.0125 0.37em 0.0995 0.27em -1.8746 0.01 0.09em -1.34e -0.0073 -0.03em -0.0125 0.37em 0.0995 0.27em -1.8746 0.01 1.1122 -7.1173 -0.0311 0.0118 -0.017e 0.39e7 0.1091 0.287e -1.8929 0.01 1.1122 -7.1173 -0.0311 0.0118 -0.017e 0.39e7 0.1091 0.287e -1.8055 0.01 7.1ev2 -3.eme2 -0.02em 0.0002 -0.0202 0.emi1 0.1139 0.29e2 -1.8655 0.01 7.1ev2 -3.eme2 -0.0283 0.0139 -0.022e 0.emi1 0.1139 0.29e0 -1.8119 0.02 3.30e4 -5.559e -0.0573 0.04em -0.0252 0.emi6 0.1139 0.3007 -1.7329 0.02 3.30e4 -5.559e -0.0573 0.04em -0.0237 0.ex00 0.1107 0.3093 -1.6815 0.02 3.910 -0.0131 -0.0569 0.07em -0.0222 0.ex7e 0.1075 0.3199 -1.64em 0.02 4.5ecc -7.ex4f -0.0511 0.023e -0.022e 0.ex7e 0.1075 0.3199 -1.64em 0.02 5.731 -0.ex6f -0.0572 0.0000 0.002em 0.ex7f 0.1077 0.3344 -1.6306 0.01 -0.0122 0.0585 -0.0162 -0.0258 -0.0116 0.37em 0.0995 0.27e5 -5.7333	<del>{     </del>												
5	0.61	•												
7	0.01 0.7455 -1.3467 -0.0115 -0.0742 -0.0131 0.3843 0.1027 0.2816 -1.9329 0.01 1.1125 -7.1173 -0.0311 0.0118 -0.0174 0.3967 0.1091 0.2876 -1.9027 0.01 1.5514 -7.0767 -0.0207 0.0002 -0.0202 0.4071 0.1134 0.2942 -1.8655 0.01 7.1442 -3.8442 -0.0283 0.0134 -0.0228 0.415 0.1155 0.2460 -1.8119 0.01 2.7774 -4.7263 -0.0461 0.0363 -0.0252 0.415 0.1139 0.3007 -7.7329 0.02 3.3344 -5.5592 -0.0573 0.0448 -0.0237 0.4200 0.1107 0.3043 -1.6815 0.02 3.3344 -5.5592 -0.0573 0.0448 -0.0237 0.4200 0.1107 0.3043 -1.6815 0.02 3.4910 -0.0131 -0.0564 0.0744 -0.0222 0.4274 0.1075 0.3199 -1.6449 0.02 3.5757 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306 0.02 5.2314 -3.4055 0.00725 0.0070 -0.0228 0.4274 0.1075 0.3344 -1.6306 0.02 5.2314 -3.4055 0.00725 0.0070 -0.0228 0.426 0.0915 0.3713 -1.6351 0.02 5.7715 -9.7642 -0.0572 0.0514 -0.0130 0.4626 0.0915 0.3713 -1.6351 0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	5												
6 6.15 0.01 1.1120 -7.1173 -0.0311 0.0113 -0.0174 0.3967 0.1091 0.2876 -1.9027  9 8.24 0.01 1.5514 -2.4507 -0.0207 0.0002 -0.0202 0.4071 0.1134 0.2942 -1.8655  10 10.34 0.01 7.1492 -3.4742 -0.0263 0.0134 -0.0226 0.4115 0.1155 0.2940 -1.8119  11 17.55 0.01 2.7774 -4.7263 -0.0461 0.0363 -0.0252 0.415 0.1139 0.3007 -1.7329  12 14.69 0.02 3.3364 -5.5594 -0.0573 0.0498 -0.0237 0.4200 0.1107 0.3093 -1.6615  13 16.82 0.02 3.010 -6.131 -0.0564 0.0744 -0.0222 0.4274 0.1075 0.3199 -1.6448  14 19.62 0.02 4.5655 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306  15 21.16 0.02 5.2314 -2.4656 0.0070 -0.0228 0.4572 0.0974 0.3523 -1.6219  16 23.37 0.02 5.4715 -9.7642 -0.0572 0.0751 -0.0130 0.4666 0.0915 0.3713 -1.6351  17 -0.07 0.01 -0.0122 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0995 0.2765 -5.7333	0.01 1.1129 -7.1173 -0.0311 0.0113 -0.0174 0.3967 0.1091 0.2876 -1.9027  0.01 1.5914 -7.907 -0.0207 0.0002 -0.0202 0.4071 0.1134 0.2942 -1.8655  0.01 7.1442 -3.4442 -0.0263 0.0134 -0.0226 0.415 0.1155 0.2440 -1.8119  0.01 2.7774 -4.7263 -0.0461 0.0343 -0.0252 0.4140 0.1139 0.3077 -1.7329  0.02 3.3444 -5.5596 -0.0573 0.4440 -0.0237 0.4200 0.1107 0.3043 -1.6815  0.02 3.9110 -0.4131 -0.0564 0.0744 -0.0222 0.4274 0.1075 0.3149 -1.6440  0.02 4.5557 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6440  0.02 5.2314 -3.4555 0.0765 0.0050 -0.0228 0.4274 0.1075 0.3344 -1.6306  0.02 5.2314 -3.4555 0.0052 0.0050 -0.0228 0.4565 0.0974 0.3523 -1.6214  0.02 5.7715 -9.7642 -0.0572 0.051 -0.0130 0.4626 0.0915 0.3713 -1.6351  0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0995 0.2765 -5.7333	6												
\$\frac{4}{0.70} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.01 1.5514 -2.4707 -0.0207 0.0002 -0.0202 0.4071 0.1134 0.2942 -1.8655 0.01 2.1442 -3.4442 -0.0263 0.0134 -0.0226 0.415 0.1155 0.2440 -1.8119 0.01 2.7774 -4.7263 -0.0461 0.0343 -0.0252 0.4146 0.1139 0.3007 -1.7329 0.02 3.344 -5.5596 -0.0573 0.0448 -0.0237 0.4200 0.1107 0.3043 -1.6615 0.02 3.944 -0.0131 -0.0564 0.0744 -0.0222 0.4274 0.1075 0.3199 -1.6448 0.02 3.9410 -6.4131 -0.0564 0.0744 -0.0222 0.4274 0.1075 0.3199 -1.6448 0.02 4.5607 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306 0.02 5.2314 -2.4650 0.0745 0.0040 -0.0228 0.4274 0.1075 0.3344 -1.6306 0.02 5.2314 -2.4650 0.0745 0.0040 -0.0228 0.4274 0.1075 0.3523 -1.6214 0.02 5.2314 -2.4650 -0.0572 0.0572 0.0051 0.3760 0.0915 0.3713 -1.6351 0.01 -0.0122 0.0585 -0.0162 -0.0258 -0.0118 0.3760 0.0935 0.2765 -5.7333	7					_				-			
10 10-38 0.01 7.1842 -3.8742 +0.0283 0.0134 -0.0226 0.0115 0.1155 0.2460 -1.8119 11 17.35 0.01 2.7774 -4.7263 -0.0461 0.0363 -0.0262 0.0164 0.1139 0.3007 -1.7329 12 14.69 0.02 3.3364 -5.5592 -0.0573 0.0448 -0.0237 0.0200 0.1107 0.3093 -1.6815 13 10.82 0.02 3.910 -0.0131 -0.0569 0.0744 -0.0222 0.0274 0.1075 0.3199 -1.6646 14 19.62 0.02 4.5632 -7.0464 -0.0511 0.0234 -0.0200 0.0371 0.1027 0.3346 -1.6306 15 21.18 0.02 5.2317 -4.0656 0.0010 -0.0228 0.0507 0.0977 0.3523 -1.6219 16 23.37 0.02 5.715 -9.7662 -0.0572 0.0512 0.0130 0.0626 0.0915 0.3713 -1.6351 17 -0.07 0.01 -0.012 0.0585 -0.0162 -0.0258 -0.0118 0.3760 0.0935 0.2765 -5.7333	0.01 7.1072 -3.8702 -0.0263 0.0137 -0.0226 0.0115 0.1155 0.2760 -1.8119  0.01 2.7774 -4.7253 -0.0461 0.0363 -0.0252 0.0106 0.1139 0.3007 -1.7329  0.02 3.3344 -5.5592 -0.0573 0.0470 -0.0237 0.0200 0.1107 0.3093 -1.6815  0.02 3.910 -6.0131 -0.0569 0.0740 -0.0222 0.4270 0.1075 0.3199 -1.6408  0.02 4.5502 -7.4447 -0.0511 0.0234 -0.0224 0.4270 0.1075 0.3344 -1.6306  0.02 5.2317 -8.0550 -0.0725 0.0000 -0.0228 0.4270 0.0977 0.3523 -1.6219  0.02 5.7317 -8.0550 -0.0725 0.0000 -0.0228 0.4270 0.0977 0.3523 -1.6219  0.02 5.7715 -9.7642 -0.0572 0.0511 -0.0130 0.4626 0.0915 0.3713 -1.6351  0.01 -0.0102 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	<u></u>												
11 17.75 U.UI 2.7774 -4.7263 -0.0461 0.0363 -0.0252 U.4146 0.1139 0.3007 -1.7329 12 14.69 0.UZ 3.3044 -5.559c -0.0573 0.0496 -0.0237 0.4200 0.1107 0.3093 -1.6815 13 16.82 U.UZ 3.911U -6.131 -0.0569 0.0794 -0.0222 0.4274 0.1075 0.3199 -1.6446 14 19.82 U.UZ 4.5675 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306 15 21.16 U.UZ 5.2317 -8.4656 0.0705 0.0070 -0.0228 0.4666 0.0974 0.3523 -1.6219 16 23.37 0.0Z 5.4715 -9.7642 -0.0572 0.0751 -0.0130 0.4626 0.0915 0.3713 -1.6351 17 -0.07 0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0114 0.3760 0.0935 0.2765 -5.7333	U.U. 2.7774 -4.7263 -0.0461 0.0363 -0.0252 0.4166 0.1139 0.3007 -1.7329 0.U. 3.3044 -5.559c -0.0573 0.0498 -0.0237 0.4200 0.1107 0.3093 -1.6815 0.U. 3.911U -0.4131 -0.0569 0.0794 -0.0222 0.4274 0.1075 0.3199 -1.6448 U.U. 4.5655 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306 0.U. 5.7317 -0.4656 0.0572 0.0074 0.0228 0.4274 0.0977 0.3523 -1.6219 0.02 5.7317 -0.4656 0.0572 0.0751 -0.0130 0.4626 0.0915 0.3713 -1.6351 0.01 -0.0102 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	•												
12 14.69 0.02 3.3046 -5.559c -0.0573 0.0498 -0.0237 0.8200 0.1107 0.3093 -1.6815 13 10.82 0.02 3.910 -0.131 -0.0569 0.0794 -0.0222 0.4274 0.1075 0.3199 -1.6440 14 19.82 0.02 4.5555 -7.4447 -0.0511 0.0234 -0.0244 0.371 0.1027 0.3344 -1.6306 15 21.16 0.02 5.2317 -8.6655 0.0000 -0.0228 0.4502 0.0977 0.3523 -1.6219 16 23.37 0.02 5.715 -9.7642 -0.0572 0.0751 -0.0130 0.4626 0.0915 0.3713 -1.6351 17 -0.07 0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	0.02 3.3044 -5.559c -0.0573 0.0498 -0.0237 0.4200 0.1107 0.3093 -1.6815  0.02 3.910 -0.4131 -0.0569 0.0794 -0.0222 0.4274 0.1075 0.3199 -1.6448  0.02 4.5000 -7.4447 -0.0511 0.0234 -0.0244 0.4371 0.1027 0.3344 -1.6306  0.02 5.2319 -3.4050 -0.0050 0.0000 -0.0228 0.4502 0.0977 0.3523 -1.6219  0.02 5.4715 -9.7642 -0.0572 0.0751 -0.0130 0.4626 0.0915 0.3713 -1.6351  0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333													
19 19.02	0.02     0.023     0.023     0.024     0.0371     0.1027     0.3344     -1.6306       0.02     5.231     -0.072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0.0072     0													
15 21.16 6.32 5.2312 -4.4555 -0.0765 0.0050 -0.0228 0.4562 0.0972 0.3523 -1.6219 16 23.37 0.02 5.2715 -9.7642 -0.0572 0.0512 -0.0130 0.4626 0.0915 0.3713 -1.6351 17 -0.07 0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	0.02 5.2317 -3.8050 -0.0725 0.0000 -0.0228 0.8507 0.0974 0.3523 -1.6219 0.02 5.2317 -9.7642 -0.0572 0.051 -0.0130 0.4626 0.0915 0.3713 -1.6351 0.01 -0.0102 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	3	10.AS	0.VC	3.9110	-6.+131	-0.0569	0.0294	-0.0222	0.4274	0.1075	0.3199	-1.6440	
16 23,37 0.0c 5.4715 -9.7642 -0.0572 (.0751 -0.0130 3.4626 0.0915 0.3713 -1.6351 17 -0.07 0.41 -0.0132 0.4585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	0.0c 5.4715 -9.7642 -0.0572 (.0751 -0.0130 3.4626 0.0915 0.3713 -1.6351 0.01 -0.0132 0.085 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333													
17 -0.07 0.01 -0.0132 0.0585 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333	0.01 -0.0112 0.085 -0.0162 -0.0258 -0.0116 0.3760 0.0935 0.2765 -5.7333													
		•	-0.07	0.01	2.0138	0+0363	-0.0195	-0.0230	-040110	023/60	0.0993	0.2703	-3,1333	
					<del></del>									
												_		
										•	•			
				<del></del>							· <del></del>			
									-					
					<del> </del>									
													·	
		-												
					<del></del>				·	<del></del>			<del></del>	
											·			

e E				LAHGLEY H	ESEAHCH, C	ENTER LAS	4)		HY PLAN .	INU TUNK	L(UP#1)	<del></del>
	1 OF 1	<del></del> -				MARTIN M	ISSILE TAT	L EFFECTS	UNTA			
					•					•		
	TEST	FEFT P	LCH EXTU-	F PHI	CUNF	L UEL	I DEFS (	EL3 DEL4	THANSITI	DN		
	3	63 3.	45 3.0	45.0 8	1 - OF 34 0	•0	0 0		FIXED		<del></del>	
INT	ALPHA	BETA	C∿	CL#	CY	CLN	CLL	Ca	CAR	CAF	ACP	
7	-3.42	0.01	-0.4953		-0.0014	-0.0424	-0.0168	0.2967	20000	0.2325	-1.5523	
5	-1.45	0.01	-0.2659	0201	-0.0161	-0.0265	-0.0163	0.2955	0.0543	0.2312	-1.5798	
3	6.15	0.01	0-00-1	0.5054	0.0u24	-0.0370	-0.01eu -0.0156	0.2949	0.0643	0.2299	-1.7017 0.7343	
5	1.22	V. U	Delano	-0-1927		U-004#	-0.0144	0.2955	0.0543	0.2312	-1.3034	
6	15.5	0.0	7.7997	-0224	-0.0204	-0.0050	-0.0132	0.2977	0.0643	0.2334	-1.4117	
7_	4.10	0.0	0.5876	-C+356v		-0.61-3	-0.0160	0.3050	0.0564	0.2386	-1.4519	
8	A.37	0.0	1.37-3	-1.5220		-0.0005	-0.0190 -u.0199	0.3110	0.0685		-1.4564	
10	10.+6	0.0		-2.4744	-0.0342	0.01-1	-0.0259	0.3242	0.0605		-1.4467 -1.4135	
ii ···	12.55	3.0		-3.6315	-0.0463	0.2350	-0.0315	0.3394	0.0685	0.2709	-1.3909	
12	14.00	0.0		-3./457		0.0355		0.3577	0.6564		-1.4021	
13	14.76	-0.01		-4.5715	-0.0515	(.0336	-0.0450	0.3779	0.6543		-1.4217	
15	24.95	-0.01		-4.6462		3-0754	-0.0478	0.3984	0.0579		-1.4506 -1.4630	
16	23.15	-0.01	5.2051		-0.1051		-0.0516	0.4407	0.0556		-1.5079	
17	0.14	0.01		-0.0082		0.0064	-0.0156	0-2941	0.0621		-0.3280	
				- Inter							LOCAL DEPT. CONCE	
												•
								<del> '</del>	<del></del>	•		
										<u>.                                    </u>		•
			7 7 7 7 7 7					<del> :</del>				
				···								
					•	<del></del>						
											• /	
											•	
							- :			· · · · · · · · · · · · · · · · · · ·		
								-	-	•		
		<del></del>										

	LANGLEY HESEARCH CENTER (VASA)	UNITARY PLAN KIND TUNNEL (UPAT)	
PAGE 1 OF 1	MAHTIN MISSILE TA	IL EFFECTS DATA	
SHEET 1 OF 1			

			ALH HATE-		CUNF	L VEL			THANSITE				
	3	64 3.	95 3.0	0.0 4	1.0F34 0	.0	0 0	0 0	FIXED				
OINT	ALPHA	HETA	CN	CLM	CY	CLN	CLL	CA	CAR	CAF	XCP .	27	
1	-3.62	0.0	-0.4916	0.75.0	0.0157	-0.6624	-0.0116	0.2921	0.0643		-1.5332		
è	-7.05	0.0	-0.2019	0.4106	0.0105	-4.0630	-0.0098	0.2425	0.0643		-1.5535		
3	-l.ve	0.0	-0.1306	0.5151	-0-00-3	-0.0.305	-0.0076	0.2438	0.0543		-1.6289		
-	0.0	0.0	0.0025	0.0163	-0.0041	-0.0 lb6	-0.0052	0.2941	0.0643	0.2298	7.4162		
<b>5</b>	2.03	0.0	0-15-1	-0.2107	-0.0035	-0.0373	-0.0057	0.2955	0.0643	0.2312	-1.3948 -1.4272		
<del></del>		0.0	0.5400	-c.6452	-0.0015	-0.03/5	-0.0125	0.3031	0.0543	0.2378	-1.4360		
	4.15	0.0	0.94+6	-1.3610	-0.0013	-0.6253	-0.0173	0.3123	0.0664	0.2459	-1.4559		
<del>-</del>	F.25	0.01	1.3003	-1.45GU	-0.0201	0.0011	-0.0176		0.0664	0.2526	-1.4549		
10	10.20	0.01	1.7603	-2.5304	-0.621#	0.0040	-0.0164	0.3316	0.0605	0.2631	-1.4309		
ii	12.36	0.01	2.2109	-3.1256	-0.0243	-0.0050	-0.0205		0.0464	0.2787	-1.4099	<del></del>	
iż	14.47	0.01	7.7024	-3.6044	-0.6210	-V-00-V-	-0.0245	0.3503	0.0554	0.2939	-1.4078		
13	16.51	0.01	3.2462	-4.5067	-0.0462	0.0516	-0.0231	0.3785	0.0643	0.3142		<del></del>	<del></del>
1.	16.70	0.01	3.87mu	-5.5212	-0.0367	0.01-3	-0.0270	0.3952	0.0600	0.3362	-1.4440		
15	20.75	0.41	4.4516	-5.5701	-v.6531	6.0077	-0.0150		0.0579	0.3592			
16	27.95	6.01	5.1920	-7.4205	-0.0512	0.0422	-0.0135	0.4404	0.0536	0.3A6H	-1.5097		
17	-0.02	0.0	0.0022	0.0162	-0.0C41	-0.0367	-0.0052	0.2942	0.0621	0.2321	7.3727		
			<del> </del>		·			· 					_
				<del></del> -									
			··,		·			<del></del>					
		···						<del></del> -	<del></del>	<del></del>		<del></del>	
	··· <u>·</u> ·····												
	· · · · · · · · · · · · · · · · · · ·												
		<del></del> .	<del></del>										

	1 OF 1			LANGLEY H	istakin C		A) ISSILE TAI			INU TUNN	EL (UPHT)	
	7E.S1		ALM #210-		CUNF. 1-0F34 Q	L UEL	1 0862 0	DEL3 DEL4	TRANSIII FIXED			
DINT	ALPHA	HFTA	C»	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	
1	-3.26	0.0	-0,4045	0.5000		-0.0434		0.2727	0.0492		-1.2359	
3	-1.75	0.0	-0,2124	0.0051	0.0019	-9.0403	-0.00m9	0.2717	0.0442	0.2717	-1.2489 -1.3619	
•	0.34	0.0	0.0513	-0-0321	-G.03un		-0.0065	0.2715	0.0492		-0.6261	
5	1.35	0.0	C.1435	-0.19-1	-0.0021		-0.0073	0.2726	0.0482		-1.0269	
<del>-</del>	2.35	0.4	0.3134	-126.0-	-0.0039	-0.0126	-0.0001	0.2736	0.0481	0.2755	-1.0765 -1.1555	
å	6.47	0.0	1459.7	-1.1394			-0.0175	0.2456	0.0462	0.2374		
4	8.74	0.4	1.4103	-1.631-	-0.0075		-0.0732	0.2464	0.0509		-1.2394	
16	10.56	0.0	1.4453	-5-15+5	-0.0130		-0.0772	0.3165	0.0509	0.2596	-1.2530	
11	17.53	0.U	2.5510	-2.4741	-0.0135 -0.0361	0.0150	-0.0278	0.3217	0.0509	0.2708	-1.2766 -1.3344	
13	16.76	9-91		. =4.3027	-0.0500		-0.0256	0.3534	0.0481	0.3053	-1.3977	
14	IH. HE	0.01			-0.0413		-0.02+3	0.37-0	0.0454		-1-4690	
15	20.00	G. u		-6.470	-0.0253	0.0757		. 9.3961	0.0427	0.3534	-1.5257	
$-\frac{16}{17}$	23.07	0.01		-7.9454			-0.0065	0.2737	0.0373	0.2263	-1.5769 -0.8416	
11	V2.34	U . W	0.0134	-6.0033	-0.9010	-4.4334	-0.0003	002/3/	040434	0.5563	-419478	
					-				•			
		<del> </del>									<del></del>	
								<del></del>			<del></del>	
				•								
		•			-							
							•					•
		·										
•												•
						<del></del>					•	
							<del></del>					
				<del></del>	<del></del>						<del></del>	

	-			<del> </del>
AGE.	_	0F	LANGLEY MESEARCH CENTEM (NASA) UNITARY PLAN MIND TUNNEL (UPWT)  MARTIN MISSILE TAIL EFFECTS DATA	

3			63 3.0		CU4F 1=0F34 0	-O	0 0	O O	THANSITI FIREC			
T ALP	HA.	HETA	CH	CLM	CA	CLN	CLL	CA	CAB	CAF	ACP	
•? <b>.</b>	46	0.0	-0.4190	0.5361	0.0065	-0.05-1	-0.0211	0.2767	0.0509	0.2758	-1.2795	
-1.	50	0.4	-5.2274	0.3114	-0.0113	-4.0170	-0.0207	0-2744	0.0481	9962.0	-1.3710	
-0.	+6	0.0	-0.07-0	0-1517	-0.0655	-0.0159	-0.0203	0.2753	0-04-1	2755.0	-1.6051	
. 0.	59	0.0	0.05+0	-0.0324	-6.0170	-0.0166	-7.0199	0.2736	0.0481	0.2255	-0.5559	
1.	43	0.0	0-1660	-0.1576	-0.0200	-0.0020	-0.0185	0.2749	0.0451	0.2268.	-0.9494	
>.	<b>←</b> 0	0.0	0.3113	-0.3191	-0.0741	0.0005	-3.0170	0.2757	0.0461	0.2276	-1.0251	
4.	58	0.0	C.610¢	-0.7746	-0.0154	-0.0012	-0.0206	0.2808	0.0401	0.2327	-1.1302	
	71	0.0	0.9354	-1.1271	-0.0255	0.0115	-0.0179	0.2873	6.6509	0.2361	-1.2043	
А,	77	0.0	107914	-1.5470	-0.0132	6.0050	-0-0260	0.2454	0.0509	0.2.47	-1.2366	
10.	79	0.0	1.6641	-2.0911	-0.0105	0.0033	-0.0341	0.3054	0.0509		-1.2476	
12.		-0.01	2.0752	-2.6/41	-4.6751	7-0105	-0.0351	0.3166	0.0509	0.2657	-1.2586	
14.		0.0	2.52.3	-3.3435	-0.0451	0.0774	-0.0409	0.3346	0.0509	0.2837	-1.3383	
17.	112	-C.Ul	3.0444	-4.2822	-0.0521	0.0447	-9.0465	0.3574	0.0481	0.3043	-1.3974	
19.	10	-0.01	3.5476	-5.2003	-0.0544	U-0519	-0.0455	0.3746	0.0454	0.3292	-1.4476	
21.	13	-0.01	4. 544	-0.1585	-0.0562	6.0547	-0.044	0.3943	0.0427	0.3516	-1.4812	
23.	24	-0.01	4.8334	-7.3294	-0.0786	2.0775	-0.0448		6.0373	0.3001	-1.5164	
0.	60	0.0	0.05+0	-0.0320	-0.0170	-0.0165	-0.0199	0.2734	0.0427	0.2307	-0.5559	
		<del></del>										···
			<del></del>								···	•
			•	•	<del></del>				<del></del>	<del></del>		
				<del> </del>		·						
····			<del>- · · · · _ · · · · ·</del>		·- <u></u>		<del></del>	<del> </del>			· · · · · · · · · · · · · · · · · · ·	<del></del>
			<del></del>	<del></del>		<del></del>	<del></del> -		<del></del>			

										<del></del>		×. <u>**,</u>
				LANGLEY H	ESEAHUM C	ENTERCIAS	4)	UNIT	KY PLAN E	IND TUNN	EL (UPUT)	
GE	1 OF 1							IL EFFECTS				
	1 OF 1								· · · · · · · · · · · · · · · · · · ·			
							•	•			•	
	1851	FART -	LL4 HXIU-	ואץ פ	LU-eF	L UEL	1 DFL2	DEL3 DEL	TRANSITI	ON		
	3		36 3.0		1+1+3+ 15		5 0		FIXE			
BOILT	ALFHA	SETA		<u> </u>				· ·	640	Ć.E		
	-3.43		-1.1727	CL4 1.6645	CY	-0.0772	-0.0377	0.4764	U-1270	CAF	-1.4236	
ż	-7.14	0.01	-2-6716	0.4546	-0.0139	-0.06.0	-0.0399	0.4715	0.1228	0.3487		
3	-1.12	0.01	-1. 1400	405321	-0.0025		-0.0320	0.4664	6-1554	0.3459	-1.5356	
•	0.01	0.01	-0.0212		-0.61m4		-0.0312	9.4672	0.1227		-4.7821	·
5	1.10	0.05	3+44.0		-0.0351		-0.0303	0.4676	6-1554	0.3447	-0.9895	
6	2.17	0.61	0.5945	-4.7213		-0-0354	-0.0331	0.4701	0.1241		-1.2032	·
	4,36	0.01	1.7077	-1.4633		-0.0352	-0.0279	0.4757	0.1284	0.3503	-1.3354 -1.4022	
	8.77	0.02			-0.0397	0.0016	-0.02+3	0.4955	0.1397		-1.4403	
10	10.44	0.02		-5.1020		0.0134	-0.0259	0.5246	0.1552		-1.4676	
11	13.15	0.02		-t-1072		0.0353	-0.0273	0.5320	0.1495	0.3725	-1.4766	
12	152	0.03	5.1910	-7.5430	-0.0739	0.0403	-0.0215	V.5335	0.1580	0.3755	-1.4607	
13	17.71	4.42		-4.7395		-0.0736	-0.0150	9-5312	6.1454		-1.4443	
. 14	19.99	0.02		->-4491	-0.0454	-0.0572	-0.0135	0.5387	0.1364		-1.4226	<del></del>
15	55.50	r.u3		-11-2102	-0.0590	-0.0350	4500.0	0.5496	0-13-0		-1.4271	
16	24.54 U.01	0.03				-0.0567		0.4668	0.1284		-1.4396 -4.8927	
4.	0.01		-0,0602	011003	-0.0100	-0.0351	-010301	0.4000	0.155.	0.3439	-410151	
_						_						
	_											
								•				
				<del></del>				<del></del>				
			-									
										•		
				<del> </del>				<del></del>				
											<del></del>	
				<del></del>	<del></del>							

)

G.	1 OF 1			LANGLEY H	ESEAHCH C		A) 15SILE TAI			INU TUNN	EL (UPat)
	1 0 1		·			100	- 331CC 1A	E CITEGIS			
	TEST	FADT .	ALH PATO-	PHI PHI	CONF	6 UEL	1 DELS I	EL3 DEL4	TRANSITI	ON	
	3.	69 60	30 3.0	45.0 5	1-1F34 15	.420	0 0	0 (	FIRE		
POINT	AL PHA	RETA	CN	CLH	CY	CLN	CLL	CA	CAH	CAF	XCP
1	-3,41		-1.1550	1.0200	-0.0105	-0.0715	-0.0305	0.4826	0.1268		-1.4024
2	-5.55	U. 0 ć				-r.0479		0.4755	0.1239		-1.4555
3	-1-12	0.02	-0-3-1-		-9-0152	-0.04-1	-0-0351	V-4705	0.1723		-1.5453
- 5	1.05	0.05	-0.050V	-0-217-	-0.0144	-0.0505	-0.0305	0.4676	0.1578		-3.5729 -0.836 <b>3</b>
6	2.16	0.02	0.5606	-0.6302		-0.0203	-0.0298	0.4723	0.1239		-1.0958
Ť	4, 78	0.01	1.2925	-1.5805		6.0050	-0.0352	0.4436	0.1295		-1.2519
	4.54	0.0	1.8457	-2.4733	-0.0509	0.0155	-0.0372	0.4925	0.1351	0.3574	-1.3052
9	H.74	6.01		-3.4755		0.0.26	-0.0426	0.5005	0.1344		-1.3232
10	10.90	6.0	3.7611			0.0509	-0.0480	0.5073	0.1450		-1.3140
11	13.10 15.35	0.0	3.9471	-5.7314 -6.1501		0.0906	-0.0497	0.5117	0.1479 0.1450		-1.3122 -1.2987
13	17.58	-0.01		-6.4737			-0.0600	0.509	0.1393		-1.2732
1-	19.85	-0.01		-7-4304			-0.0615	2.5177	0.1394		-1.2486
15	22.05	-0.vi		-4.7944			-0.0700	0.5301	0.1464	0.3637	-1.2375
16		-0.02		-10-0466			-0.0607	0.5364	0.1479		-1.2433
17	0.01	0.02	-0.0314	0.1635	-0.0188	-0-0567	-0.0347	0.4712	0-1539	0.3473	-5.2057
					··						
							-				
								•			
								-			<del></del>
	·		<del></del>	<del></del>							<del></del>
									·-·-		

AGE	I OF 1			LANGLEY RI	LDEAMEN C	CA+) NJIVA M Plivam	A) ISSILE TA	UNITA IL EFFECTS	RKY PLAN W 5 data	IND TUNN	LC(UP41)	
EET	1 OF 1										•	
				<u>-</u>								
	1651	PART -	ACH HXIU-	6 Fal	CUNF	L ULL	1 OELZ	DEL 3 DEL	TRANSITI	OM		·····
	3		66 3.C		1-1F34 15		0 0		FIXE			
THIOP	ALPHA	BFTA		CLM	CY	CL*	CLL	CA	CAB	CAF	KCP	
1	-3.75	0.01	-0.94>0	1.7610	0.0075	-0.0670	-2.0255	0.4319	0.1044	0.3275	-1.2479	
_2_	-2.22	Ú.01	-0.5141	0-1717	0-0390	-0.0462	-0.0212	0.4241	0-1012	0.3279	-1.2557	
3	-1.11	(.01	=^-31=n	0-4203	-0.0022	-6.0745	-0-0204	0-4259	0.1012	2.32.7	-1.3352	
<del>-</del>	1.07	0.01	-0.03-7 -0.2125	-0-1517	0.00el	0 <u>-0911</u> -0-0729	-0.01+7 -0.0230	0.4216	0.1012 0.1012	0.3264	-3.5066 -0.7053	
6	2.12	¢.61	0.4127	-0-4695		-0.0450	-0.0263	0.4292	0-1011	0.3281	-0.9721	
<del>-</del> -	4.24	0.01	1.0371	-1.1624	-0.0304	-0.0313	-0.0259	0.4371	0.1028	0,3343	-1.1401	
•	6.41	0.0	1.5771	-1.9965	-0.0204	-0.0361	-0.0275	0.4436	0.1044		-1.2271	
4	9.50	0.6	5-5045	-2507	+3.6344	-0.0254	-9.0340	G.44HM	4.1076	0.3412	-1.2702	
10	10.72	0.6	2.4542	-3.4625	-4.0443	P.0130	-0.0354	0.4564	0.1108	0.3456	-1.2767	
11	12.40	0.0	3.5335	-4.4845	-0.0705	0.0463	-0.0388	0.4613	0.1076	0.3537	-1.2691	
12	17.23	-0.01	4.9157	-5.3249 -6.0970	-C.0825	0.0670	-0.0450	0.4750	0.1060	0.3615	-1.5058	
13	17.67	-0.vl	5.6723	-5.775	-0.0594	r.0475	-0.0492	0.4495	0.1060		-1.2403 -1.2282	
15	21.63	-0.01	4.4473	-7.H919	-0.1654	0.0977	-0.0553	0.5030	0.1076	0.3954	-1.2241	
16	23.96	-0.01		-6-7700	-0.1023	0.0355		0.5205	0.1075		-1.2239	
17	0.0		-0.0446	0.1340		-0.0781		0.4240	0.1020		-3.0094	
			· · · · · · · · · · · · · · · · · · ·							· · · · ·		
										•		
		•										
								<del></del>			<del></del>	·····
										•		
					•							
								<del></del>	<del></del>		<del></del>	
									•			
	·									<del></del>	<del></del>	<del></del>
												<del></del>
							_					
							•					
											·	
						<del></del>						
											•	
								<del> </del>				

	1 OF 1							UNITAL LL EFFECTS		227 1207		
	<del></del>											
			-LH ##1 v-	6 241					TRANSIT		•	<u></u> -
	3	70 20	to 3.0		1-1534 15	.420	0 6	0 0	FINE	<u> </u>	<del></del>	
DINT	-3.92	HETA	CN	1.3170	CY	CLN	-0.0264	CA	CAR	0.3224	XCP	. <del></del>
Ş	-2.32	0.0 0.01	-1.07ev	1.3176	0.0084	-0.0946	-0.0264	0.4255	0-1031 0-1031	0.3220	-1.2558	
3	-7.30	0.01	-0.6615	1.7554	-0.0049	-0.01.6	-0-0252	0261	0.1031	0.3230	-1.2559	W 1
•	-1.21	0.01	-0-3324	0.4233	-0.0124	-0.0673	-0.0245	0.6274	_0.1031_		-1.2733	
6	-9.16	0.01	-0.05vr	0.110: -0.1614	-0.017¢	-0.0006 -0.0337	-0.0237	0.4232	0.1031 0.1031		-2.1900 -0.6436	
Ť	1.97	0.01	0.6514	-0.5007			-0.0222	0.4287	0.1631	0.3256	-1.0400	
8	ie	6.05	1.0244	-1.2302	-0.0457	-0.0131	-0-0707	0.4334	6-1347		-1.1958	
9	6.27	0.05	1-43-1 2-25-1		-0.0420	0-0014	-0.0172	0.440	0-1111		-1.2613 -1.3142	
10	10.57	0.04	7.4456	=3.4000	-0.0475	0.0074	-0.0216	0.4554	-0.1191-	0.3475	-1.3462	<del></del>
12	12.77	0.02		-5-6237	-0.0633	0.01-9	-0.0160	0.4703	0-1191		-1.36R3	
13	14.44	U. U.	4.4.100	-n.v03/			-0-0151	0.4811	0.11+3	0.3668	-1.3630	
15	17.14	0.02	5.1743	-7.055u		0.07-2	-0.0141	0.4947	0-1111		-1.3622	
15	21.55	0.03	-		-0.0055		-0.0000	0-5011	0-1031		-1.3613	
17	23.43	0.03		-10.6052	-0.0721		-0.0076	0.5344	0.0951		-1.3946	
16	-0.10	0.01	-0.05-0	0-1264	-0.0335	-0-0404	-0.0237	55500	0-1631	0.3191	-5.0000	
											•	
			<del></del>		<del></del>						<del></del>	
								•				
			<del></del>						·			
				-								
						•						
											······································	
											-0.77	
							•	- · · · _ · _ · - · · · · · · ·	<del>- · · · - ·</del>			
			•									

.GE	1 OF 1		i	ANGLEY HI	SEAHCH C	ENTEH (MAS	A) ISSILE TAI	UNITA	PY PLAN S	IND TUNN	EL (UP#T)	
EET	1 OF 1								•			
					——————————————————————————————————————		<del> </del>					
	TEST		ACH HATU-		CUIAF		1 DELZ		THANSIT			<del></del>
		71 3.	45 3.U	45.0 H	1-163- 15	.470	00_	<u>0</u> 0	FIXE	·		
THIO	ALPHA	8FTA	CN	CLM	CA	CLN	CLL	CA	CAB	CAF	ACP	
	-3.53	0.0	-0.6475	2.7725	0.0094			0.3358	0.0683	0.2575		<del></del>
<u>5.</u>	-2.01	0.0	-0.4055	0.4454	0.0284	=0.07~U	-0.0062	0.3347	0.0653	0.2654	-1.1414	
3	-0.96 0.13	0.0	-G-20mm	0.0554	0.0247	-0.0740	-0.0103.	0.3799	0.0563	0.2416	-1.2202 3.3500	
	1.15	0.0	0.20*5	-n.1430	. <u>0.01</u> -1-	-0.01ab	-0.0098	0.3329	0.0663	0.2646	-0.8724	
,	5.15	0.0	0.4257	-0.4247	-0.0063	-0.0397	-0.0093	0.3327	0.0583	0.2707	-9.9953	
·- <del></del>	4.28	0.0	C 415	-4.6751	-0.0205	-0.0103	-0.0134	0.3450	0.0693	0.2767	-1.0429	
	6.35	0.0	1.2850	-1-1601	-0-0444	-0-0340	-0.0122	0.3527	0.0643	0.2R44	-1.0631	
9	7.47	0.0	1.75,4	-1-4107	-0.0134	-0.0175	-0.0163	0.3609	0.0663	0.2926	-1-0916	·
10	10.53	-0.61	2.3113	-2.0324	-0-015d	-0-0071	-0.0202	0.3725	U.C704	0.3021	-1.1391	
11	12.63	-0-01	7401	-3.3914	-0.0257		-0.0241	0.3915	0.0704	0.3211	-1-1746	
15	14.79	-0-01	3.5?>3	-4-1519		. 0.0169	-0.0278	0.4145	0.0583	0.3462	-1.1777	
13	16.91	- 6-0	• 1506		-0.0639		-0.0367	0.4342	0.0683	0.3659	-1.1798	
14	19.48	-0.01	4.5614	-5.7564	-0.0605	9.94.7	-0.0454	U - 574	0.0652	0.3912		·
15	21.16	-0.01	6.4415 6.4035	-r.7527 -7.519*	-0.0/15	0.0022	-	0.5108	0.0640	0.4215	-1.1903	
16	0.12	0.0	0.0232	0.0118		-0.0561		0.3227	0.0619	0.2545	-1-1742 0-5095	· · · · · · · · · · · · · · · · · · ·
• •	00.2	***	080232		00013	-000302	-000,03	003221	000002	086343	******	
					<del></del> -					· · · · · · · · · · · · · · · · · · ·	····	
								•				
												<u> </u>
										-		
											<del></del>	<del></del>
												<del></del>
										,		
											<u> </u>	
					···							
	_	-								-		

EET	1 OF 1			LANGLEY H	ESEAHCH C	ENTER( . AS	A) ISSILE TA	UNITA IL EFFECTS	HY PLAN W	IND TUNN	EL (UPYT)	
		<del></del>			- <del></del>							
	TEST		45 3.0		CONF 1-1-34 15		DEL2 I	DEL3 DEL4				
OINT	ALPHA	EETA	CN	CL7	CÝ	CL~	CLL -	CA	ÇAB	CAF	ACP	
1	-3.73	0.0	-0.7122	0.=022	0.0094	-0.05-1	-v.0125	0.3260	0.0587		-1.1263	
2	-2.21	0.0	-0.2045	0.4711	0.074h	-0.0416	-0.0064 -0.011v	0.3254	0.0688		-1.2166	
-	-0.00	0.0	C. (013	2.6543	0.0169	-0.0429	-0.010-	0.3207	0.0444		22.5231	
5	9.96	0.0	11.20.7		-0.00e3		-0.0038	0.3275	U.U688 ~	0.25A7	-0.9169	
6	1.96	0.0	C.4634	-r.4017		-0.0391	-0.0145	0.3315	0.0688	0.2627	-0.9896	
7	6. AK	0.0	0134	-11-14-03		-0.0427		0.3354	0.0666		-1.0429	
- 4	4.1¢	6.0	1.73+1	-1.754-	-0.0003	-0.0207 -0.0120	-0.0121	0.3469	0.0709		-1.0858 -1.1155	
10	15.34	0.01	2.2145	-2.7969	-0.0167		-0.0147	0.3690	0.0709		-1.1366	
11	12.46	0.01	2.41-3	-3.2240	-0.0240		-0.0103	0.3899	0.0709	0.3190	-1.1457	
12	14.56	0.01	3.4147	-7.4065	-6.0505	0.0276	-0-0510	0.4123	0.0688	0.3435	-1-1622	
13	16.73	0-07	4.0545	-4.F310		-0.0062		0-4350	0.0667		-1.1873	
15	10.87	10.0	4.75.7		-0.035#		-0.0185	0.454H	0.0624		-1.2135	
10	23.1e	0.01	5.5137	-6-29#4	-0.0343		-0.0045	0.5011	0.0561		+1.2492 -1.2952	
17	-0.11	0.0	0.0016			-0.0301		0.3214	0.0667	0.2547	15.8776	
					•							
					-							
			-						··		· <del></del>	
						<del></del>		<del></del>				
			<u>-</u>									
												•

GF	1 OF 1			LANGLEY P	ESEAHCH C	ENTER INAS	A) ISSTIA TA	UNITAL IL EFFECTS	RY PLAN	HIND TUNN	EL (UP=T)			
	1 0# 1					HEAT &	ASSIGE IA	ic errects						
					a.com/per_									
	7EST		63 3.0		CUMF 1+1+34 15			DEL3 DEL4						
DINT	ALPHA	FF TA	C+	CL#_	CA	CLN	CLL	CA	CA9	CAF	KCP		•	
J.	-3.35	-2.0.	-0.5705	n.5+80		-1-0565		0.2498	0.0538		-0.9606			
5	-1.×3	1 . U	-0.3:173	116003		-0.0477		0.2976	0.0538		-0.9669			
3	-0.79	0.0	=4.1103			-6.0447		0.5456	0.0534		-1.0724			
<u> </u>	1.27	0.0		-0-1826	-0-0615			0.2920	0.0538		-0.7696			
2	7.31	0.0	6.62.0		-0.0120	-0.0509		0.2976	0.0538		-0.8646			
<del></del>	4.40	0.0		-0.714A		-9.0411		0.3056	0.0530		-0.6949		<del></del> -	
à	6.44	0.0			-0-0027			0.3171	0.0536		-0.9406			
<u> </u>	7.59	0.0		-101207		-0.0270		0.3259	0.0538		-0.9983			<del></del>
10	10.57	0.0			-0.0167			0.3463	0.0538		-1.0273			
-11	12.40	0.0			-0.0217			6.3679	0.0538		-1.0659	<del></del>		
iż	14.73	0.01			-0.0259			0.3856	0.0538		-1.1065			
13	16.82	0.01		-4.4015		-0.01:1		0.4072	0.0511		-1.1696			
1.	14.97	0.0	_		-c.0145			0.4292	0-0484		-1.2240			
15	21.00	0.61			-0.0301			0.4547	0.0456		-1.2076			
16	23.20	0.01				0.0359		0870	0.0402		-1.3526			
17	0.25	0.0					-0.0132		0.0464		-0.6309			
-		•												
				-										
				•										
								-						
								-	•					
							, <u></u>							
				<del></del>			<del> </del>							
				<del> </del>										
										<del></del>				
				•										
													<u> </u>	
													•	
									<del></del> _		<del> </del>			
								·						

				LANGLEY H	ESEARCH C	ENTERI-AS	À	UNIT	ARY PLAN .	INU TUNN	EL (UPUT)	
	1 OF 1					MARTIN M	ISSILE TA	L EFFECT	S VATA			
MEET	1 0 1								-			
								· <b></b>				
	TEST	PART M	ALM FX10-	6 PnI	CUNF	L VEL	1 DELZ	DEL3 DEL	4 TRANSITI	ON		
	3	74 4.	63 3.6	45.0 B	1.1F34 15	-420	0 0	0	O FIXE			·
THIOS	ALPHA	HETA	CN	CLM	CA	CLN	CLL	CA	CAR	CAF	XCP	•
1	-3.11	0.0	-0.5A05	U-5563	0.0334	-0.1004	-0.0083	0.3091	0.0505	0.2546	-0.9925	
_ Z	-1.50	0.0	-0.304c	0.3314	0.0277	-0.0444	-0-0142	0.306+	0.0533		-1.0886	
3	-7-57	0.0	-0-1559	0.1557	0.0141		-0.0137	0.2999	0.0532		-1.2666	
<del>-</del> :-	1.53	0.0	0.244	-0.0103	0-0141	-0.0539 -0.0411	-0.0132	0.2910	0.0532	0.2435 0.2521	-0.1727 -0.6630	
6	7.56	0.0		-0-1555		-0.0433		0.3103	0.0533	0.2570	-0.8327	
Ť	4.64	0.5		-0.6930		-0.6458		0.3148	J-0533	0.2615	-0.8689	
8	e.70	0.0	1.2142	-1-1199	-0.0055	-0-0263	-0.0234	0.3225	0.0533	0.2592	-0,9165	
9	e.7e	0.0		-1.6175	-0.0105		-0-0555	0.3302	G-6532	0.2770		
10	10.81	0.0		-2.7355	-0-0155		-0.0277	0.3471	0.0560		-1.0396	
11	15.01	0.0		-2.4635 -3.7211	-0.0060		-0.0331 -0.0364	0.3e75 0.3901	0.0560		-1.0876 -1.1302	
15	17.10	-0.01	3.431-	-4.6360	-6.0314		-0.0370	0.4131	0.0533		-1.1715	
14	19.23	-0.61		-5.5356				0.4384	0.0532		-1.2115	
15	21.27	-0.ul	5.3351	-6-5065	-0.0374	0.0235	-0.0473	0.4675	0.6505		-1.2312	
16	23.45	-0.01	6.0742	-7182	-0.0551	C-0170	-0.0589	0.4961	0.0478	9.4493	-1.2213	
17	0.52	0.0	0.3648	Ŭ•¥005	0.0109	-0.0775	-0.0132	0.2979	0.0505	0.2474	0.0079	
					<del></del>		· · · · · · · · · · · · · · · · · · ·					<del></del>
				<del></del>								
						•					•	
				·								
												•
											·· <del>·····</del>	•
						•						
	<del>,</del>											
					•							
			<u> </u>									

 1210
 Æ
 D
 <u> </u>
R-7
 AEDC-TR-75-125
125
-

	1 OF 1			LANGLEY H	ESLANCH C	ENTERINAS MARTIN M	A) ISSILE TA	UNITAR	DATA	IND TUNN	EL (UP=T)	
	TEST	PART -	ACH RETU-	6 PnI	CONF	L VEL	1 0EL2	UEL3 DEL4	THANSITI	DN	•	
	3	75 2.	30 3.0	0.0 н	141/34 15		0 -50	05-0	FIRE			
DINT		EETA	C4	CL=	۲۷	CLN	CLL	CA	CAH	CAF	XCP	
1	-1.44	0.02	-3.15+1	10-1241		-0.1191	-0.0420	1.2470	0.1445	1.1425	-3.2098	
- <u>\$</u>	-2.26	0.05	-2.4415	9-5477	-0.0344	-0.115h	-0-0321	1.2366	0-1-31 0-1-45	1.0045	-3.5456 -3.6351	
3	-0.10		-2.7643	9-1715	-0.0314	-0.1091	-0.0327	1-1779	0.1488	1.0043	-3.8351 -4.2371	
<del>-</del> -	1.72		-1.7321	4.7981		-0.0547		1.1391	0.1514	0.9877	-4.7650	<del></del> -
6	2.06	0.00	-1.4311	7.773.				1.6947	0.1517	0.9430	-5.5478	
7	4.31	4.66	-0.65+7	6.76UY	-0.0001		0.0312	. 0.4456	0.1544		-9.7967	<del></del>
8	5.47	0.02	0.04-4		-0.0515		-0.0356	0.9036	0.1601		111-1165	
3	4.46	0.03	0.4575	4.7735	-0.06-1	-0.0716	-0-(3:9	0.6049	0.1572	0.6376	4.9204	
10	10.40	0.02	1.6673				-0.0293	0.7014	0.1700	0.5314	1.5720	
11	13.05	0.03	3.4552	-4.157n	-0.0667 -0.0716	-0.0247 -0.0271	-0.0276	0.5946	0.1714	0.4234	0.4321	
13	17.61	0.03	4.2569		-0.0500	-G.0m+3	-0.0738	-0.4713	0.1672	0-3041	-0.2594	<del></del>
14	19.73	0.03	5.6273	-1.1790	-0.0517		-0.0150	0.4331	0.1601		-0.3540	
15	22.13	دد.ن	5-1305		-0.05-8		-0.0076	0.3993	0.1616		-D.4486	
10	24.45	0.04		-3.6175			-0.0076	0.3579	0.1602		-0.5379	
17	-0.10	0.43	-2.0533	0.7517	-0-0-65	-0.0904	-0.0361	1.1774	G-1489	1.0205	-4.2623	
							<del></del>					
		<del></del>						<del></del>				····
		•										
						····			•		····	
	<del></del>				· · ·						<u> </u>	
	<del></del>											
					•							
				<del></del>							·	
				-	-							
										•		
								<del></del>				
								-				
					····							
										<del></del>		

· ·	1 OF 1			THEFF H	ESEAHCH C		A) ISSILE TAI			IND TUNN	EL (UPUT)	
	OF 1					784114 5	1331LE TAI	C CFFECIS	UPIA			
	YESY	DACY P	ALP RXIU-	6 271	CUNF	L JEL	) DELS (	EL3 DELA	THANSITI	Δ <b>u</b>	<del></del>	
	3		66 3.Q		1=1F34 15		0 -20	0 -20				
						-						
1-1	ALPHA	HETA	CN	CLM	CY	CLM	CLL	CA	CAR	CAF	XCP	
1	-2.41	0.01	-2.7147	6-6661	-0.0252	-0.1114		1.1203	0.1086		-3.1578 -3.4939	
3	-1.15	U.JI	-2.1447	7.7715	-0.021	-0.10-0		1.0547	0.1086	0.9461	-3.7037	
	-0.23		-1.7407			-0.1216		1.0227	0.1102	0.9125	-4.2061	
5	0.45	0.01	-1.4427	6.090.1		-0.10/4	-0.0328	0.9948	0.1119	0.0749		
6	1.49	0.01	-1.1-32	A.+257	-0.01-7	-0.1053	-0.0315	0.4475	0.1134	0,8341	-5.6208	
7	4.09		-0.0852	5.3351	-0-0504	-0.0954		0.9550	0.1150		-10.9969	
۲	4.75	0.02	0-1-13	4.3116	-0.0246	-1.04-5	-0.0254	0.7709	0.1199		30.5137	
9	3.38	0.02	C.4238			-0.0561		0.6623	U-121-	0.5609		
U	10.55	0.02	1.0009	1.0167		-0.0545		0.5234	0.1247	0.4609	1.1320	
1	12.68	0.02	3.0075		-0.0423		-0.0242	0.4924	0.1247	0.3987	-0.0100	
3-	17.00	0.05	3,4344	-0.5344	-0.0494		-0.0224	U. +d03	0.1230		-0.1386	
•	19.36	0.03	4,3109	-1-3079	-0.0590		-0.0167	0.4693	0.1199		-0.2337	
5	21.50	0.03	4 - 4 - 4 - 1)	-105721	-0.0463		-0.0150	0.4532	0.1166	0.3366		
16	23.76	0.63				-0.U49A		0.4375	G-1134	0.3241	-0.3997	
17	-0.23	0.04	-1.7344	7-3320	-0-0166	-0.1705	-0.0379	1-62-1	0.1103	0.9138	-4.2157	
											<del> </del>	
				-								<del></del>
	<del></del>			·		·		<del>-,</del>		<del></del>		
									2000			
											· · · · · · · · · · · · · · · · · · ·	
			<del></del>								· · · · · · · · · · · · · · · · · ·	<del></del>
-												
						-,,	•					
								<u> </u>				
											· · · · · · · · · · · · · · · · · · ·	
							•					
					<del></del>				- ···			
					_							

	1 of 1		1	ANGLEY M	ESEAHCH (	ENTER(NAS) M FITRAM	A) . ISSILE TA	UNITA	DATA	IND TUNN	EL (UPaT)			
•	TEST	PADT M	ALM RELU-	PAL	CUNF	L OEL	1 OFLE	JEL3 UEL4	TRANSITI	On				·
-	3		45 3.0		1-1F34 19		0 -20	0 -20						
POINT	ALPHA	META	CN.	CL"	CY	CLN	CLL	CA.	CAB	CAF	XCP			
2 .	-3-+6	G. 3	-2-0453	6.4937		-0.0607		3.8765	0.0675		-3.1749	-		
<del>- 5</del> -	-2.24	0.0	-1.70-7	5-6421	0.0014		-0.0245	0.F316 0.503h	0.0554 U.3554	0.7384	-3.5316 -3.4533	-		
•	-0.13	0.0	-1.7362	5.3147	0.0099	-0.0873	-0.0306	0.7716	0.0654	0.7062	-4.3203			
5	1.93	0.0	-0.7324	4.457		-0.0975	-0.0292 -0.0278	6.7355 0.6480	0.0675	0.6305	-4.9369 -6.0995			
7	4.05	0.0	-0.2176	3.9151	0.0940	-0.0797	-0.0248	0.6242	0.0675	0.5567	-16.6137			
<u>e</u>	6.19	0.01	0.6411	2.6947	-0.0704	-0.0755	-0.0169	0.5479	0.0696	0.4783	2.0103			<del></del>
10	10.33	0.47	1.3520	1.2025		-0.0444	-0.0157	0.4584	0.0718	0.3866	0.8696		-	
11	122	0.0	1.63-9	0.4431	-0.0073	-0.0466	-0.0161	9.46JR	0.0597	0.3941	0.5140			
13	14.55	0.01	2.7016	0.7647		-0.0555 -0.0596	-0.0208		0.0597	0.4267	0.3322	- <del></del>		
1.	16.43	0.41	3.4057	0.3750	-0.0314	-9.0514	-0.0239	0.5066	0.0654	0.4412	0.1146			
15	20.47	0.01	3.0709	0.042a		-0.0545 -0.0720			0.0533	0.4531	0.0230			
16 17	-0.13	0.02	4.5447	5.3057		-0.1030			0.0612	0.4599	-0,0761			
														·
	,													
			<del></del>											
·			<del></del>								<del></del>			
								•						•
							7.7							
			<del></del> -									<u>-</u>	<del></del>	
									<u> </u>				•	
													<del></del>	
			<u> </u>									· · · · · · · · · · · · · · · · · · ·	· ·	
		·· · · · ·				•				<del></del>				
				<del></del>	-··· <del>-</del>								<del></del>	
						<del></del>			<del></del>					
												·	· · · · · · · · · · · · · · · · · · ·	

	1 OF 1			LANGLEY H	ESEANCH C	ENTER(NAS MARTIN M	A) 1551LE TAI	UNITA IL EFFECTS	HY PLAN W	IND TUNN	EL (UPUT)		
	YEST 3		63 3.0			L UEL	0 -50	DEL3 DEL4					
OINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP		
1	-3.40	0.0	-1.7950			-0.0454	-0.0212	0.7843	0.0496		-3.1649		
-3-	-1.62	0.0	-1.6326	5-1556		-0.0608	-0.0232	0.7350	0.0496		-3.5988 -3.9244		
4	0.24	0.0	-0.946H	4.4911		-U.OA91		0.6761	0.0496	0.6265	-4.5055		
5	1.26	0.0	-0.7530			-0.0536		0.5400	0.0496	0.5904	-5.4190		
6	7.27	0.0	-0.5337		-0.0001		-0.022A	0.6051	0.0496		-6.9359		
7	4.38	0.0	-0.0506			-0.0442		0.5353	0.0496		-50.5363		
8	A.42	0.0	0.4594	2-1118		-0.0525		0.4663	0.0523	0.4140	4.5976		
10	8,53	0.4	1.3036	1-30/5		-0.0476		0.4401	0.0523	0.3878	0.9994		
11	12.65	0.0	1.6932			-C.0491		0.4572	0.6523	0.4049	0.6057		
12	14.71	0.0	2.0763	1	-0.0643	-0.0678	-0.0243	0.4743	0.0496	0.4247	0.5242		
13	16.80	0.01	2.5061			-0.0353		0.4946	0.0496	0.4450	0.3011		
14	19.96	. 0.01	3.0032			-0.0700		0.5133	U.0469	9.4664	0-2403		
15 16	20.96	0.01	3.5024 4.1176			-0.0096		0.5290	0.0441	0.4649	0.1163 -0.0067		
-iř	0.23	6.5	-0.9969	4.4913	0.0190	-0.0832	-0.0200	0.6764	0.0469	0.6295		<del></del>	
	555					118 2		1.115 1.15			11111		
					•				-				
							<del></del>	<del> </del>				<del></del>	
		•											
								•		<del></del>	<del></del>		
							<del></del>						
-							<del>-</del> -					•	
	<del></del>						<del>.</del>				<del></del>		
			<del></del>									<del></del>	
										<u> </u>			
			<del></del> -			<del>-</del>						<del></del>	
		_											
										•			
			-					•					

				TANGE SHE	Chau(# F	Service Contract	A1:	LIN TTA	RY PLAN HI	with Trible	EL CHOUTS	
Ē.	1 OF 1		•	LAMOLET N	L3EARCH C		ISSILE TAI				ELIOPATI	
ET	OF											
							<del></del>			•	<del></del>	
					-	•						•
			ALM FATO-						TRANSITIO	H	•	
	3	79 2.	30 2.5	45.0 5	1-11-34 15	.420 . 5	0 -50	50 -50	FIXED			
INT	ALFMA	SFTA	CN	CL4	CY	CLY	CLL	CA	CAB	CAF	XCP	
	-3-A1		-4.0705	14.2059		-0.0949	-0.0321	2.0553			-3.4849	
2	-2-51	0.07		13.0074				5.0020	6.1652	1.8368		
	-1.17	0.07	-1.2~12 -2.9#75	13.1631	-0-0223	-0.0F27	-0.0346	1.4576	G-1667 U-1684		-4.0117 -4.2707	
	1.03		-7.5063		-0.0206	-0.0A7	-0.0333	1.4608	0.1707		-4.6183	<del></del> -
	. 2.15	0.05	-7.3564	11-6193	-0.0275	-C.0774	-0.0327	1.8029	0.1720	1.6309	-5.0158	
	4.24			17.7551			-0.0355	1.6471	6.1719		-6.5177	
3	5.75	7.05	-0.23+1		-0.0749	-0.017B	-0.03d8	1.5253	0.1719 0.1770		-10.2098 -35.7013	<del></del>
,	10.70	0.00	0.0006		-0.9499		-0.0349	1.2610	U.1622		15.2347	
-	12.43	0.05		6.4632			-0.0-10	1.1393	0.1957	2,9536		
2	15.02	0.00	1.2558		-0.0730		-0.03-5	1.0399	3.1874	0.8525		
3	17.74	0.00	2. A 154		-0.0586		-0.0479	0.9495	0.1874	0.7621		
<u>•</u>	21.50	0.04	3.7512		-0.0924		-0.048	0.7964	0.1857	0.6842		
6	23.49	0.05	4.9273		-0.1264		-0.0550	0.7341	0.1857	0.5484		
7	-0.00	0.07	-7.9h20			-0.10+0	-0.0338	1.9072	0.1689		-4.2732	
												<del></del>
								•				•
			<del></del>	<del></del>							<del></del>	
							· · · · · · · · · · · · · · · · · · ·					
			<del></del>					<del></del>				
									-			•
	<del></del>						<del></del>		<del></del>		<del></del>	
								•				
					•		-					<del></del>

T	1 OF 1			LANGLEY H	ESLARCH C	ENTENT AND ME	A) 1551LE TA	UIITAI IL EFFECTS	DATA	IND TUN	EL (UPST)	
		· •••								<del></del>		
	7ES1 3		*C* PY10-			L DEL		50 -50 DET3 DET4				•
		W 200										
NT	-3.21 -	PFTA	C^	11.9492	CY	CLN	CLL	CA 1.7872	CAH	CAF	-3.4375	<del></del>
2	-5.50	0.00	-3.0717	11.3635	0.0015		-0.0298	1.7200	0.1159		-3.6995	
<del>-</del>	-1.17	0.05	-2.7774	10.4340	0.0159			1.5714	0.1160		-3.9370	
<u> </u>	-0.37	0.06	-2.4443	1000407	0.0013			1.6216	0.1160		-4.2244	
5	1.02	0.45	-2.1741	10.0000		-0.1127		1.5655	0.1176		-4-6120	
<u> </u>	2.05		-1.4972		-0.3113	-0.0938	-0.0314	1.5171 _	0.1207	1.3964		
9	4.23	0.05	-0.6147	8.5514 7.5551	-0.0305	-0.0534	-0.0341	1.3699	0.1224		-6.8636 -12.1915	
•	7.54	0.04	0.0004	5.0359			-0.0294	1.1489	0.1287		962-1653	
D	10.45	0.04	0.6294	5.4064	-0.0592		-0.0333	1.0446	0.1320	0.4126		
i	12.40	0.04	1.261.	5.0301	-0.0564	-0.0073		0.9502	0.1336	0.8166		
5	14.99	0.04	1.4206		-4.0703		-0.0371	0.6572	0.1335	0.7337		
3	17.16	0.04	2.5544		-0.6735		-0.0300	0.8145	0.1336	0.6809		
5	21.63	0.04	3.2752		-0.0597	-C.0057	-0.0364	0.7599	0.1320	0.6279		<del></del>
6	23.96	0.0-	4.6624		-0.0948		-0.5452	0.6994	0.1319	0.5675		
7	-0.00	U.06	-2.4731			-0-1174		1.4212	0.1175	1.5037		<del></del>
									<del></del>			
							<del></del>				· · · · · · · · · · · · · · · · · · ·	······································
			-									
	•											
					<del></del>	<del></del> -						
	<b>:</b>				·							
												· · · · · · · · · · · · · · · · · · ·
							•					
			<del></del>								<del></del>	
							****					· · · · · · · · · · · · · · · · · · ·

66	1 0F 1			ANGLEY M	ESEAHCH C	ENTERIORS	A)	UNITA	HY PLAN W	IND TUNK	EL (UPaT)	<del></del>	
	0/ 1				•		133166 14	IL CIPCUIS	<u> </u>	-			
					, , <u>, , , , , , , , , , , , , , , , , </u>								
	3	81 3.	95 3.0	45.0 B	1=1534 15	7 020°°	0 -50	DEL3 DEL4 20 -20					
DINT	ALPHA	BFTA		CLH	СŸ	CLH	CLL	CA	CAR	CAF			
5	-3.50		-2.5939	#.3763		-0.1062		1.3018	0.0645		-3.4625 -3.7515		
3	-1.00		-5.9515	6.1362		-v.1725		1.2697	0.0645		-3.9772	·····	<del>-:</del>
4	0.00	60.03	-1.7691	7.5944	4560.0	-0.0635	-0.0294	1.2225	0.0566	1.1559	-4.3177		
5	1.13	0.03	-1.5123	7-171-		-0.1001		1.1717	0.0566		-4.7421	•	•
<del></del>	7.16		-1.2612			-0.0626		1.1151	0.0667 0.0688		-5.3294 -7.9331	<del></del>	<del></del>
B	6.31		-0.2453			-6.03-9		0.9325	0.0709		-19-5506		
9	4.45		. 4.5510	4.5504		-0.0264		U. +561	0.0709	0.7852	20.6353		
16	10.53	0.02				-0.0191		0.7923	0.0730	0.7193			
11 12	17.61	0.02	1.2439			-0.0133 -0.0407		0.7506 0.7370	0.0730	0.6640	2.7621 1.0316		
13	16,87	0.02	2.24.4			-C.0437		0.7357	0.0730	7590.0			
14	19.07	0.00		7.1275	-0.0794	-C.C4	-0.0146	9.7339	0.0730	0.6609	0.9551		
15	21.15	1.02	3.4214			-0.0711		0.7335	0.5730	0.6605			
17	23.37 0.08	0.02	-1.7536			-0.0497	-0.0246	0.7311 1.2157	0.0730	0.6581	%-5710 -4-3152		
• •										1. 1. 1.		<u> </u>	
	•						·	•	· · · · · · · · · · · · · · · · · · ·				
_								·					
			•										
										•			
		·									······································		
-			<del></del>			,	· · · · · · · · · · · · · · · · · · ·	-	•				
											<del></del>	<del></del>	<del></del>

			· · · · · · · · · · · · · · · · · · ·	ANGLET H	ESEARCH C	ENTERTUAS	4)	UNITA	TY PLAN .	IND TUNN	LL (UPST)	
	1 OF 1			·		784114 7	TASTEE IN	IL EFFECIS	UNIA			<del></del>
			<u> </u>	<del></del>						<del></del>		
	•											
	TEST		ACH HXIU-6						TRANSITI			
	3	82	63 7.0	45.0 8	1×1F34 15	-420 Z	05- 0	20 -20	FIXED			
INT	ALPHA	BETA	c∾ .	CLH	CY	CLN	CLL	CA	CAB	CAF	ACP	
1	-3.13		-2.2533	7.0265	0.0142	-0.1053	-0.0198	1.7320	0.0484	1.1836	-3.4735	
2	-1.56		-1-7063	7-7411	0.0056	-0.0P-6	-0.0191	1-1615	0.484		-3.7985	<del></del>
.3 4	-0.57		-1.6400	6.4741	0.0305	-0.11-1 -0.1125	-0.0254	1-1161	0.0484		-4.0874 -4.4421	
5	1.54	0.02	-1.22.5	CENTRO		-C.1181	-0.0245	1.0180	0.0484		-4.9569	<del></del>
6	2.53		-0.9961	5.0966	-0.0016	-0.0696	-0.0241	0.9691	0.0484		-5.7205	
7	4,54	0.00	-0.5043	4.7687	-0.0189		-0.0231	0.0617	0.0511	0.8306	-9.7564	
8	6.59	0.05		4.35ln	-0.0334		-0.0589	0.6061.	0.0511		-76.7474	······································
J	7.75 10.79	0.01	0.3691 0.4352	3.7vij 3.7843	-0.0+27 -0.0185		-0.0313 -0.0313	0.7433 0.7030	0.0511	0.6492	10.3050 3.9324	
Ť	12.86	0.01	1.2326	3.0996	-0.0131	-C.0554	-0.0247	0.6384	0.0538		. 2,5142	<del> </del>
Ş	14.97	0.01	1.6957	2.4044	-0.0086	-0.0441	-0.0208	0.7022	0.0538	0.6484	1.7169	
3	17.05	0.01	2-1740	2.7174				0.7106	0.0536	0.6568	1.2447	
•	19.55	0.01	7.4933		-0.0361	-0.05h2		0.7205	0.0538	0.6667	0.9406	
6	23.39	0.00	3.1754	2.303/	-0.0453 -0.0391		-0-0297 -0-0381	0.7229 0.7185	0.0538 0.0536	0.6647	0.7419 0.5634	
7	3.49		-1.4508	6.4867		-0.1347		1.0683	0.0511		-4.4541	
											•	
									<u>.</u>	<del></del>	· ·	
					•				_			
								•		<del></del>		
								<del></del>			<del></del>	
											•	
												•
						<del></del>				· · · · · · · · · · · · · · · · · · ·		<del></del>
							<u> </u>					
							·····			<u> </u>		
-												•
			<del></del>			·····				<del></del>	<del> </del>	<del></del>
									•			
					-							· · · · · · · · · · · · · · · · · · ·

	1 OF · 1			LANGLEY R	SEARCH C	ENTEH (VAS	A) ISSILE TA	UNITA IL EFFECTS	DATA	INO TUNN	LL (UPUT)	
	TEST 3	PART -	ALM R#10-	6 PnI 0.0 a	CUNF 1=1F0 15	L ∪€L	1 OEL2 F OFF	DEL3 DEL4 OFF OFF	TRANSITI FIXED			
DINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAS	CAF	ACP	
Ĭ.	-3.91	0.0	-0.6961	-0.2485	-0.0142	-6.0245	-0.0101	0.3636	0.1310	0.2326	0.4271	
<u></u>	-2.26	0.0	-0.3462	-6-1723	-0.0165		+0.0052	0.3561	0.1255	0.2306	0.4349	
3	-1.13 -0.01	0.01	-0.2020	-0.039	-0.0446		-0.0043	V.3537 0.3526	0.1235	0.2302	0.4707	
~રં	1.07	0.01	7.2151		-0.0240	- 4-0019	-0.0025	0.3531	0.1533	0.2798	0.4391	
6	7.1.	0.01	0.3944		-0.0-37	-0.0005	-0.0051	0.3547	0.1246	0.2299	0.4879	
7	4.13	0.01	6.2004		-0.0412	0.0050	-0.0034	0.3625	0.1332	0.2294	0.4018	
8	4.50	0.00	1.2754		-0.0532	0.0037	-0.0016	U-3714	0.1388	0.2326	0.3895	
9	R. 72	0.02	1.6540	いんななのの	-0.0534	0.0005	0.0001	0.3567	0.1530	0.2357	0.3540	
10	10.46	0.01	2.1515		-0.0371	-0.6115	0.0018	0.4121	0.1700	0.2421	0.2686	
11	13.08	0.05	2.7039	0.4630	-0.0561	-0.0031	0.0001	0.4722	0.1770	0.2452	0.1709	
12	15.30	0.02	3.3005	r-1701	-0.0653	-0.0033	0.0021	0.4253	0.1798	0.2455	0.0505	
13	17.57	0.02	4.02.16	-0-031/	-0.0031	-0.0063	0.0040	033	0.1798	0.2536	-0.0079	
14	14.46	0.03	4.4572	-0.1484	-0.0651	-0.0224	0.0093	2.4445	0.1412	0.2633	-0.0310	
15	55.114	0.02	5.30.4	-0.3725	-0.0479	-0.0050	0.0076	0.4462	0.1769	0.2643	-0.0703	•
16	-0.02	0.03	4.0421 0.0133		-0.0839	-0.0064	-0.0033	0.4534	$-\frac{0.1727}{0.1233}$	0.2807	-0.1208	
		<del></del>										,
				<u> </u>			<u> </u>			•		
	- <del></del>										<del></del>	•
<del> :</del>					<del></del>						<del></del>	·
-												
	<del></del>				· · · · · · · · · · · · · · · · · · ·						<del></del>	

EET	1 OF 1			CT.IOCLI K	LJEANON C	M WITHAM	ISSILE TA	UNITAL IL EFFECTS	UATA .	TIND TUNN	(L (UPAT)	
	1 OF 1				-							
	TEST	PART	ACH RAIJ-	6 Pril	LUNF	L uth	1 DEL2	DEL3 DEL4	TRANSIT	ON .		
	3	H4 2.	30 3.9	45.0 d	1-1F0 15	.420 UF	F OFF	OFF OFF				
OINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	ACP	
1	-3.43	6.01	-0.7255	-0.2540	-0.0260	-v.03+1	-7.0069	0.3613		9.2352	0.3499	
2	-7.74	0.92	-9-4174	-i. 1540	-0.0307	-7.0494	-0.0005	0.3545	0.1235	0.2310	0.4006	
3	-1.1-	0.01	-0.2722		-0.0305		0.0014	U.352h	0.1221	0.2307	0.4048	
4	0.0	0.05	0.0064	-0.0031	-0-0-67	-0.0737	0.0	0.3514	0-1222		-10.0667	
5	1.00	0.00	0.2652	0.0030	-0.6433	-0.0268	0.0009	0.3511	0.1208	0.2303	0.3100	
6	? <u>.13</u>	0.02	0.3417	r-1547	-0.0452	-0.0187	2.0052	0.3518	0.1235	0.27A3	0.3950	
-	3.	0-05	1 2147		5540.0-		0.0035		0.1292	0.2300	0.4405	
6	4.70	0.05	1.2397	0.0001	-0.0459 -C.U437	-0.0306	0.0071	0.3794	0.1377	0.2313	0.4553	
10	10.46	0.02	7.0127		-0.0605	0.0291	0.0049	0.3935	0.1545	0.2390	0.5271	
11	13.06	0.04	2.4950		-0.0767		0.0109	0.4075	0.1645	0.2433	0.4929	
12	15.26	0.04	2.4751		-0.0984	0.0229	0.0128	0.4159	0.1729	0.2430	0.4755	
13	17.53	0.00	3.4213		-0.1050	0.0168	0.0113	0.+245	0.1614	0.2471	0.4241	<del></del>
1.	19.43	0.05	4.1105		-0-1394		0.0119	4.4294	0.1514	0.2484	0.3901	
15	21.47	0.45	4.7000	1.0014	-0.1151	0.0060	0.0046	0.4358	0.1757	0.2601	0.3403	
16	24.29	0.05	5.3976	1.4606	-0.1356	0.04#5 -0.0328	0.0123	0.4450	0.1757	0.2693	0.2717	
17	0.0	0.05	0.0033	0.0239	-0.0406	-0.0328	0.0035	9.3528	0.1234	0.2294	7.2364	
					_						•	
					<del></del>	<del></del>		<del></del>				
								-				
												·
						· .						
												•
						. <u> </u>						
				·							<del> </del>	
												<del></del>
											•	
								<del></del>			· · · · · · · · · · · · · · · · · · ·	····
			-	<del></del>		<del></del>		<del></del>	<del></del>			

TEST PAST SALE NATURE OF THE COURT LOCAL OFF OFF OFF OFF OFF OFF OFF PIRED    1	TEST PART FACH RATURE PHI COMF L OELI DELS DELS DELS TRANSITION  3 65 2+06 3+0 45.0 minifo 15.470 OFF OFF OFF OFF FIXED  DINT ALPHA META C4 CLM CV CLM CV CLM CLL CA CAB CAF XCP  1 -3.77 0.01 -0.551 -0.7747 -0.0200 -0.0349 0.000m 0.3248 0.1072 0.2176 0.4231 2 -7.27 0.0 -0.4071 -0.1635 -0.0103 -0.0171 0.0036 0.3717 0.1056 0.2161 0.4004 3 -1.17 (-0.1 -0.71/3 -0.037 -0.01)m -0.0271 0.0036 0.3717 0.1056 0.2161 0.4004 4 -0.07 0.01 -0.0077 -0.0156 -0.0270 -0.0172 0.0038 0.3229 0.1056 0.2173 2.0545 5 1.00 0.01 0.1556 0.0074 -0.0253 -0.0203 0.0046 0.3233 0.1056 0.2173 2.0545 5 1.00 0.01 0.1556 0.0074 -0.0263 -0.0203 0.0046 0.3233 0.1056 0.2173 2.0545 6 7.10 0.01 0.3391 0.1570 -0.0277 -0.0135 0.0054 0.3233 0.1056 0.2177 0.5627 7 0.76 0.01 0.0678 0.3887 -0.0765 -0.0110 0.0070 0.3298 0.1072 0.2726 0.5062 8 6.36 0.02 1.0344 0.5702 +0.0466 -0.0600 0.0066 0.3346 0.1120 0.2746 0.5598 10 10.66 0.02 1.7390 1.0017 -0.0507 0.0073 0.0006 0.3366 0.120 0.2746 0.5598 10 10.66 0.02 1.7390 1.0017 -0.0507 0.0073 0.0000 0.3566 0.1231 0.2355 0.5577 11 12.85 0.02 7.2265 1.1509 -0.0541 0.0067 0.3690 0.1255 0.2301 0.2556 0.5597 12 1.00 0.03 3.7104 1.2263 -0.0777 0.0223 0.0136 0.3169 0.1257 0.2708 0.4541 0.4546 0.000 0.0000 0.3566 0.1231 0.2355 0.5577 13 17.26 0.03 3.7104 1.3263 -0.0777 0.0223 0.0136 0.3169 0.1257 0.2708 0.4541 0.4546 0.000 0.0000 0.3660 0.1237 0.2708 0.4541 0.4546 0.000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4546 0.0000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.4000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.40000 0.0000 0.3000 0.1359 0.2506 0.4007 0.4541 0.40000 0.4000 0.40000 0.4000 0.40000 0.40000 0.40000 0.40000 0.40000 0.40000 0	E	1 OF	1		LAHGLEY H	ESEAHCH C	ENTER (NASA MARTIN MI	SSILE TA	UNITA	NY FLAN N	IND TUNN	EL (UPaT)	
3 85 2.66 3.0 45.0 Blaif 0 15.470 UFF OFF OFF OFF FIXED  UINT ALPHA HETA CN CLM CV CLN CLL CA CAB CAF NCP  1 -3.77	3 65 2.66 3.0 45.0 81-160 15.470 OFF OFF OFF OFF FIRED    INT ALPHA   HETA   CN   CLM   CV   CLN   CLL   CA   CAB   CAF   RCP     1	EY	1 0#	<del>i                                    </del>					77.6	THE CLIFTON			<del></del>	
3 85 2.66 3.0 45.0 Blaif 0 15.470 UFF OFF OFF OFF FIXED  UINT ALPHA HETA CN CLM CV CLN CLL CA CAB CAF NCP  1 -3.77	3 65 2.66 3.0 45.0 81-160 15.470 OFF OFF OFF OFF FIRED    INT ALPHA   HETA   CN   CLM   CV   CLN   CLL   CA   CAB   CAF   RCP     1			·							<del></del>			
UINT ALPHA HETA CN CLM CY CLN CLL CA CAB CAF NCP  1 -3.77	3 65 2.66 3.0 45.0 81-160 15.470 OFF OFF OFF OFF FIRED    INT ALPHA   HETA   CN   CLM   CV   CLN   CLL   CA   CAB   CAF   RCP     1					<del>,</del>			1.635	,	88	<u> 120   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110   110 </u>		
CUINT ALPHA   6FTA   CN   CLM   CV   CLN   CLL   CA   CAB   CAF   RCP						45.0 H	1 = 1 F O 1 5	.420 UFF	OFF	OFF OFF				
1 -3.77	1 -3.77	••••		^										
2 -7.22 0.0 -0.4070.1635 -0.0103 -0.0371 0.0036 0.3717 0.1056 0.2161 0.4004 3 -1.12 0.01 -0.2703 -0.037 -0.0100 -0.0271 0.0057 0.3223 0.1040 0.2163 0.4037 4 -0.02 0.01 -0.0077 -0.0156 -0.0270 -0.0172 0.0038 0.3229 0.1056 0.2173 2.0565 5 1.04 0.01 0.1554 0.0074 -0.0263 -0.0203 0.0046 0.3233 0.1056 0.2173 2.0565 6 2.10 0.01 0.3291 0.1570 -0.0277 -0.0135 0.0054 0.3251 0.1072 0.2179 0.4629 7 4.26 0.01 0.0077 0.3402 -0.0270 -0.0135 0.0054 0.3251 0.1072 0.2179 0.4629 8 6.32 0.02 1.3374 0.5707 -0.0466 -0.0070 0.3299 0.1072 0.2226 0.5062 9 9.55 0.02 1.3374 0.5707 -0.0366 -0.0070 0.0086 0.3366 0.1120 0.2246 0.5489 10 10.66 0.02 1.7760 1.0017 -0.0502 0.0073 0.0080 0.3566 0.1231 0.2355 0.5577 11 12.83 0.02 2.2265 1.1589 -0.0541 0.0067 0.0080 0.3566 0.1231 0.2355 0.5577 12 15.02 0.03 2.7044 1.2263 -0.0743 0.0136 0.0116 0.3797 0.1327 0.2470 0.4561 13 17.20 0.03 3.7701 1.3055 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2508 0.4067 15 21.61 0.03 4.3342 1.2431 -0.0874 0.0220 0.0141 0.3959 0.1327 0.2532 0.3462	2 -7.2? 0.0 -0.40n -0.1635 -0.0103 -0.0371 0.0036 0.3717 0.1056 0.2161 0.4004 3 -1.12 0.01 -0.7073 -0.037 -0.010n -0.0741 0.0057 0.3223 0.1040 0.2133 0.4037 4 -0.02 0.01 -0.0077 -0.0156 -0.0270 -0.01n2 0.0038 0.3229 0.1056 0.2173 2.0545 5 1.04 0.01 0.1554 0.0074 -0.0263 -0.0703 0.0046 0.3223 0.1056 0.2177 0.5627 6 7.10 0.01 0.3391 0.1570 -0.0270 -0.0135 0.0054 0.3251 0.1072 0.2179 0.4629 7 4.76 0.01 0.6678 0.3487 -0.0765 -0.0101 0.0070 0.3299 0.1072 0.2266 0.5062 8 6.32 0.02 1.0398 0.5705 -0.0101 0.0070 0.3299 0.1072 0.2266 0.5062 9 9.55 0.02 1.0398 0.5705 -0.0134 0.0066 0.3368 0.1120 0.2246 0.5489 10 10.66 0.02 1.7980 1.0017 -0.05507 0.0073 0.0080 0.3366 0.1231 0.2355 0.5577 11 12.83 0.02 2.2265 1.1589 -0.0541 0.0067 0.0080 0.3690 0.1295 0.2393 0.5298 12 15.02 0.03 2.7044 1.2263 -0.0743 0.0136 0.0116 0.3797 0.1327 0.2470 0.4561 13 17.25 0.03 3.7104 1.3055 -0.0777 0.0223 0.0136 0.3363 0.1359 0.2504 0.4067 15 71.61 0.03 4.3342 1.2431 -0.0874 0.0020 0.0140 0.4079 0.1327 0.2632 0.3462	TNT-		47 34	<u> </u>	CLM	CY	-0-0349						<del></del>
3 -1.12	3 -1.1	Ş												
5 1.00 0.01 0.1550 0.0074 -0.0263 -0.0703 0.0046 0.3233 0.1056 0.2177 0.5627 6 2.10 0.01 0.4391 0.1570 -0.0279 -0.0135 0.0054 0.3251 0.1072 0.2170 0.4620 7 0.266 0.01 0.6678 0.3482 -0.0765 0.0101 0.0070 0.3299 0.1072 0.2246 0.5062 6 0.3062 6 0.3062 0.0060 0.3486 0.1120 0.2246 0.5062 6 0.5062 6 0.3060 0.3486 0.1120 0.2246 0.5062 6 0.5062 6 0.3060 0.3486 0.1120 0.2246 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5062 6 0.5	5 1.00 0.01 0.1554 0.0074 -0.0263 -0.0703 0.0046 0.3233 0.1056 0.2177 0.5627 6 2.10 0.01 0.3391 0.1570 -0.0270 -0.0135 0.0054 0.3251 0.1072 0.2179 0.4629 7 0.766 0.01 0.477 0.3487 -0.0765 -0.0101 0.0070 0.3299 0.1072 0.2226 0.5062 6 0.32 0.02 1.0399 0.5705 -0.0060 0.0086 0.3366 0.1120 0.2246 0.5489 0 0.5598 0.10 0.02 1.4166 0.7939 -0.0378 -0.0134 0.0064 0.3469 0.1160 0.2301 0.5598 0.10 0.02 0.02 0.02 0.0079 0.0073 0.0080 0.3586 0.1231 0.2355 0.5577 0.10 0.02 0.02 0.0348 0.0064 0.3690 0.1295 0.2395 0.5597 0.10 0.03 0.03 0.03 0.03 0.03 0.03 0.13 0.23 0.39 0.52 0.5598 0.23 0.03 0.03 0.03 0.03 0.03 0.03 0.3590 0.12 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.2	3	-1.14		-0.2013	-0.Ca37	-0.0]na	-0-0241	0.0057	0.3223	0.1040	0.2143	0.4037	
6	6	•												
7	7	_												
6 6.3c 0.02 1.0374 0.5704 40.066 -0.0000 0.0066 0.3366 0.1120 0.2246 0.5489 9 9.55 0.02 1.4166 0.7937 -0.0378 -0.0134 0.0066 0.3669 0.1160 0.2301 0.5598 10 10.66 0.02 1.7360 1.0017 -0.0502 0.0073 0.0080 0.3546 0.1231 0.2355 0.5577 11 12.85 0.02 2.2265 1.1587 -0.0541 0.0067 0.0098 0.3690 0.1295 0.2395 0.5206 12 15.02 0.03 2.7048 1.2263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.561 13 17.20 0.03 3.7120 1.3052 -0.0771 0.0223 0.0136 0.3863 0.1359 0.2506 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0671 0.0220 0.0141 0.3959 0.1327 0.2632 0.3662	8 6.3c 0.02 1.03+h 0.570- +0.0466 -0.00n0 0.0086 0.3366 0.1120 0.2246 0.5489 9 9.5h 0.02 1.4156 0.7939 -0.0378 -0.0134 0.0060 0.3469 0.1160 0.2301 0.5598 10 10.66 0.02 1.79h0 1.0017 -0.0507 0.0073 0.0080 0.3586 0.1231 0.2355 0.5577 11 12.83 0.02 2.2265 1.1589 -0.0541 0.0067 0.0088 0.3690 0.1295 0.2395 0.5208 12 15.02 0.03 2.7044 1.2263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.4541 13 17.26 0.03 3.712h 1.3052 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2506 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0071 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462	7												
9	9 9.56 0.02 1.4166 (.793) -(.0378 -0.6134 0.0066 0.3469 0.1160 0.2301 0.5598 10 10.66 0.02 1.7960 1.0017 -0.0507 0.0073 0.0080 0.3586 0.1231 0.2355 0.5577 11 12.85 0.02 2.2265 1.1589 -0.0541 0.0067 0.0098 0.3690 0.1295 0.2395 0.5200 12 15.02 0.03 2.7044 1.2263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.4541 13 17.20 0.03 3.7126 1.3055 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2506 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0071 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 21.61 0.03 4.33-2 1.2431 -0.0744 0.0304 0.0140 0.4079 0.1327 0.2752 0.2868	8				0.570-	-0.0466	-0.0000						
10 10.66 0.0c 1.7960 1.0017 -0.0507 0.0073 0.0080 0.3586 0.1231 0.2355 0.5577 11 12.65 0.0c 2.2235 1.1589 -0.0561 0.0067 0.0098 0.3690 0.1295 0.2395 0.5206 12 15.02 0.03 2.7044 1.2263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.4541 13 17.02 0.03 3.7120 1.3055 -0.0771 0.0223 0.0136 0.3863 0.1359 0.2506 0.2607 14 19.46 0.03 3.7701 1.3052 -0.0071 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 21.61 0.03 4.33-2 1.2431 -0.0874 0.0160 0.4079 0.1327 0.2752 0.2868	10 10.66 0.02 1.7960 1.0017 -0.0507 0.0073 0.0080 0.3586 0.1231 0.2355 0.5577 11 12.83 6.02 2.2265 1.1589 -0.0541 0.0067 0.0098 0.3690 0.1295 0.2395 0.5200 12 15.02 0.03 2.7044 1.2263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.4541 13 17.26 0.03 3.7126 1.3055 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2504 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0071 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 21.61 0.03 4.33-2 1.2431 -0.0744 0.0304 0.0140 0.4079 0.1327 0.2752 0.2868	4			1.4156	0.7935	-0.0376	-0.0134	0.0064	0.3469	0.1100	1065.0	0.5590	<del></del>
12 15.02 0.03 7.7044 1.7263 -0.0793 0.0136 0.0116 0.3797 0.1327 0.2470 0.4541 13 17.26 0.03 3.7126 1.3055 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2504 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0871 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 71.61 0.03 4.3342 1.2431 -0.0874 0.0304 0.0140 0.4079 0.1327 0.2752 0.2866	12					1.0017	-0.0507	0.0073		0.3546	0.1231			
13 17.20 0.03 3.712n 1.305 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2504 0.4067 14 19.46 0.03 3.7701 1.3052 -0.0871 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 21.61 0.03 4.33-2 1.2431 -0.0274 0.0304 0.0140 0.4079 0.1327 0.2752 0.2866	13 17.20 0.03 3.712n 1.3055 -0.0777 0.0223 0.0136 0.3863 0.1359 0.2504 0.4067 14 19.46 0.03 3.77u1 1.3052 -0.0m71 0.0220 0.0141 0.3959 0.1327 0.2632 0.3462 15 21.61 0.03 4.33-2 1.2431 -0.0874 0.0304 0.0140 0.4079 0.1327 0.2752 0.2868													•
10 19.46 0.03 3.7701 1.3052 -0.0871 0.0220 0.0101 0.3959 0.1327 0.2632 0.3062 15 21.61 0.03 4.3342 1.2431 -0.0274 0.0304 0.0100 0.0379 0.1327 0.2752 0.2868	10 19.46 0.03 3.77u1 1.3052 -0.0n71 0.0220 0.0101 0.3959 0.1327 0.2632 <b>0.3662</b> 15 21.61 0.03 4.33-2 1.2031 -0.0074 0.0300 0.0100 0.0079 0.1327 0.2752 <b>0.2060</b>													
15 71.61 0.03 4.33-2 1.2431 -0.0774 0.0304 0.0140 0.4079 0.1327 0.2752 6.2866	15 71.61 0.03 4.33-2 1.2431 -0.0774 0.0304 0.0140 0.4079 0.1327 0.2752 0.2668					1-3052	=0-0771	0.0223						•
17 -0.03 0.01 -0.01d= 0.010= -0.0173 -0.0140 0.0078 0.3255 0.1119 0.2136 -0.5739	17 -0.03 0.01 -0.01d* 0.010b -0.0173 -0.0180 0.0076 0.3255 0.1119 0.2136 -0.5739		23.A5	0.04	4.9698	1.1472	-0.1097	0.0339	0.0100	0.4208	0.1327	0.2481	0.2300	
		17	-0.03	0.01	-0.01de	0.0106	-0.0173	-0.0140	0.0076	0.3255	0-1119	0.2136	-0.5739	
					-									<del></del>
										•				
										·	<del></del>		····	
							······································							
									<u> </u>					
						<del></del>								<del></del>
												· · ·		

11 12.59 0.02 2.4493 0.760 -0.004 0.0250 0.0057 0.3732 0.1341 0.2391 0.1127 12 14.86 0.02 2.9454 0.0041 -0.0647 0.0176 0.0113 0.3813 0.1341 0.2472 0.0281 13 17.06 0.02 3.5450 -0.0471 -0.0744 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 4.140 -0.2234 -0.0453 0.0482 0.0110 0.3993 0.1309 0.2664 -0.0540 15 23.73 G.ua 5.3226 -0.7052 -0.1200 0.0075 0.0155 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.7277 -0.4623 -0.1631 0.0607 0.0126 0.4101 0.1261 0.2642 -0.0977 17 21.46 0.04 4.7325 -0.4565 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2642 -0.0966	
1 -3.92	FMALH RAID-B PHI CUMF L DELI DELI DELI DELI DELI TRANSITION 2.66 3.0 U.O 8121FO 15.420 UFF OFF OFF OFF FIXEO
1 -3.92	TA CH CLM CY CLN CLL CA CAB CAF ACP
3 -1.2h	01 -0.50-0 -0.2951 -0.0036 0.0763 -0.0029 0.3274 0.1117 0.2157 0.4568
4 0.96 0.61 0.1654 0.0693 -0.0509 0.0115 0.0008 0.3266 0.1070 0.2196 0.5401 5 -0.16 0.01 -0.0715 0.0116 -0.0473 9.0075 0.0039 0.3268 0.1086 0.2162 -0.056 6 1.91 0.01 0.3250 0.1862 -0.051 0.0134 0.0016 0.3276 0.1085 0.2191 0.5729 7 4.11 0.02 0.6854 0.4839 -0.0580 0.0134 0.0031 0.3366 0.1085 0.221 0.5605 8 6.24 0.02 1.0481 0.4777 -9.0435 0.0138 0.0047 0.3387 0.1117 0.2270 0.4576 9 8.37 0.02 1.0530 0.5220 -0.0665 0.011 0.0002 0.3540 0.1161 0.2399 0.3396 10 10.53 0.02 1.0296 0.0622 -0.0665 0.0121 0.0002 0.3540 0.1161 0.2399 0.3396 11 12.57 0.02 2.0093 0.7760 -0.0605 0.0121 0.0002 0.3711 0.1325 0.2366 0.2395 12 14.86 0.02 2.0093 0.7760 -0.06047 0.0176 0.0013 0.3813 0.1301 0.2391 0.1127 13 17.06 0.02 3.5450 -0.0471 -0.0704 0.0019 0.0091 0.3915 0.1301 0.2574 -0.0133 14 19.28 0.03 0.1406 -0.2234 -0.0953 0.0047 0.0126 0.0103 0.3993 0.1309 0.2664 -0.0540 15 23.73 0.00 5.3266 -0.7052 -0.1200 0.0077 0.0126 0.0101 0.2993 0.1261 0.2802 -0.0130 16 21.46 0.03 0.7077 -0.0623 -0.0120 0.0077 0.0126 0.0101 0.1261 0.2602 -0.0977 17 21.46 0.09 4.7375 -0.0553 -0.0167 0.0126 0.0103 0.1261 0.2802 -0.09977	
5 -U.16 0.V1 -0.0715 0.U16 -0.0073 0.0075 0.0039 0.3246 0.1086 0.2162 -0.0750 6 1.01 0.01 0.3250 0.1862 -0.0531 0.0134 0.0016 0.3276 0.1085 0.2191 0.5729 7 4.11 0.U2 0.6854 0.4584 0.0133 0.0031 0.3306 0.1085 0.2221 0.5055 8 6.24 0.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	
6 1.91 0.01 0.3250 0.1862 -0.0531 0.0134 0.0016 0.3276 0.1085 0.2191 0.5729 7 4.11 0.02 0.6854 0.3650 0.0193 0.0031 0.3306 0.1085 0.2221 0.5005 8 6.24 0.02 1.0441 0.4777 -0.0436 0.0136 0.0047 0.3387 0.1117 0.2270 0.4576 9 8.37 0.02 1.9296 0.6622 -0.0665 0.0126 0.0047 0.3711 0.1325 0.2366 0.2395 10 10.53 0.02 1.9296 0.6622 -0.0665 0.0267 0.0079 0.3711 0.1325 0.2366 0.2395 11 12.57 0.02 2.4493 0.6760 -0.0844 0.0268 0.0057 0.3732 0.1341 0.2391 0.1127 12 14.86 0.02 2.9464 0.0841 -0.0847 0.0176 0.0113 0.3813 0.1341 0.2391 0.1127 13 17.06 0.02 3.5450 -0.0471 -0.0744 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 0.1406 -0.2234 -0.0453 0.0842 0.0110 0.3993 0.1309 0.2678 -0.0133 15 23.73 0.00 5.3268 -0.7052 -0.1200 0.0075 0.0126 0.4101 0.1261 0.2842 -0.0967 16 21.46 0.03 0.7247 -0.4623 -0.1631 0.0657 0.0126 0.4101 0.1261 0.2842 -0.0967	
7 4.11 C.U2 C.6H76 C.3+30 -0.05H0 0.0143 U.0031 0.3306 0.1985 0.2721 0.5005 R 6.24 0.U2 1.5441 0.4747 -0.0636 C.0138 0.0047 0.3387 0.1117 0.2770 0.4576 9 8.34 0.U2 1.4530 (.5220 -5.0665 U.0151 0.0052 0.3540 U.1161 0.2359 0.3596 10 10.53 U.02 1.4246 0.4627 -0.0856 U.027 0.0079 0.3711 0.1325 0.2386 0.2395 11 12.55 U.02 2.4443 0.766 -0.0846 0.0268 0.0057 U.3732 0.1341 0.2391 0.1127 12 14.86 U.02 2.4443 0.766 -0.0847 0.0176 0.0113 0.3813 0.1341 0.2391 0.1127 13 17.06 0.U2 3.5450 -0.0471 -0.0647 0.0176 0.0113 0.3813 0.1341 0.2574 -0.0133 14 19.28 0.03 4.1406 -0.2234 -0.0753 0.0467 0.0110 0.3943 0.1309 0.2664 -0.0540 15 23.73 0.U0 5.3826 -0.7052 -0.1200 0.0075 0.0126 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.7277 -0.4623 -0.1203 0.0667 0.0126 0.4103 0.1261 0.2842 -0.0966	
9 8.3v 0.v2 1.*530 (.5220 -3.0665 0.0121 0.0052 0.3540 0.1161 0.2359 0.3396 10 10.53 (.02 1.9296 0.4622 -0.0856 0.0267 0.0079 0.3711 0.1325 0.2366 0.2395 11 12.59 (.02 2.4493 0.760 -0.084 0.0268 0.0057 0.3732 0.1341 0.2391 0.1127 12 14.46 (.02 2.4493 0.0841 -0.0847 0.0176 0.0113 0.3813 0.1341 0.2472 0.0281 13 17.06 0.02 3.5450 -0.0841 -0.0647 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 4.1406 -0.2234 -0.0453 0.0842 0.0110 0.3993 0.1309 0.2684 -0.0540 15 23.73 0.0 5.3226 -0.7522 -0.1200 0.0675 0.0145 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.7247 -0.4623 -0.1631 0.0607 0.0126 0.4101 0.1261 0.2640 -0.0977 17 21.46 0.09 4.7325 -0.4555 -0.1167 0.0529 0.0166 0.4101 0.1261 0.2642 -0.0966	U2
10 10.53	
11 12.57 0.02 2.4493 0.7760 -0.0844 0.0258 0.0057 0.3732 0.1341 0.2391 0.1127 12 14.86 0.02 2.4954 0.0841 -0.0647 0.0176 0.0113 0.3813 0.1341 0.2472 0.0281 13 17.06 0.02 3.5450 -0.0471 -0.0744 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 4.1400 -0.2234 -0.0453 0.042 0.0110 0.3993 0.1309 0.2684 -0.0540 15 23.73 0.00 5.3826 -0.7052 -0.1200 0.0075 0.0165 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.727 -0.4623 -0.1631 0.0607 0.0126 0.4101 0.1261 0.2642 -0.0977 17 21.46 0.04 4.7325 -0.4565 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2642 -0.0966	
12 14.86 0.02 2.9454 0.0841 -0.0847 0.0176 0.0113 0.3813 0.1341 0.2472 0.0281 13 17.06 0.02 3.5450 -0.0471 -0.0744 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 4.1406 -0.234 -0.0453 0.0482 0.0110 0.3993 0.1309 0.2684 -0.0540 15 23.73 0.00 5.3828 -0.752 -0.1200 0.0875 0.0155 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.7277 -0.4623 -0.1031 0.0867 0.0126 0.4101 0.1261 0.2842 -0.0977 17 21.46 0.04 4.7325 -0.4555 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2842 -0.0960	
13 17.06 0.02 3.5650 -0.0471 -0.0744 0.0019 0.0091 0.3915 0.1341 0.2574 -0.0133 14 19.28 0.03 4.1406 -0.2234 -0.0953 0.042 0.0110 0.3993 0.1309 0.2664 -0.0540 15 23.73 0.04 5.3226 -0.7052 -0.1200 0.0675 0.0145 0.4266 0.1277 0.2991 -0.1310 16 21.46 0.03 4.7247 -0.4623 -0.1031 0.0607 0.0126 0.4101 0.1261 0.2848 -0.0977 17 21.46 0.04 4.7375 -0.4565 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2842 -0.0960	the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
15	
16 21.46 0.03 4.72+7 -0.4623 -0.1631 0.0607 0.0126 0.4101 0.1261 0.2840 -0.0977 17 21.46 0.04 4.7325 -0.4545 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2842 -0.0960	
17 21.46 0.04 4.7325 -0.4545 -0.1167 0.0529 0.0166 0.4103 0.1261 0.2842 -0.0966	
	·
•	

. . . .

			- (	44ULEY +	LSEAPCH C	ENTERIVASA	}	LATINU	RY PLAN I	IND TUNN	L(UPat)		
GE	1 OF 1					MANTIN MI	SSILE TA	ALL EFFECTS	DATA				
ELT .	I OF I												
		<del></del>	<del> </del>				•						
	TEST		ACH -X10-		COMP	L DELI		DEL3 DEL4					
	3	H9 3.	45 3.0	45.0 t	1=1f0 15	.420 UFF	OFF	OFF OFF	FIXE	)			
61. 7	ALPHA	BETA	CN	C. 10		<b>C4</b> 41	<b>5. 1</b>	•	C+B	5.5	<b>7-0</b>		
OINT	-3.5¢	0.0	-0.4574	CLM	( A) 10	-0.0276	CLL 0.0032	<u>CA</u> 0.2543	0.0678	0.1865	3CP 0.6194		<del></del>
;	-1.94	0.0		-0.1733		-0.0276 -0.0132	0.0064		0.0678	0.1512	0.6845		
3	-1,05	Ú.Ú	-0-115-	-11-04-0		-1.6101	0.0004		0.670	0.1416	0.8561		
•	0.04	0.0	0-6/15	-0.0327	-0.01-7	0.0036	0.0106		0.0678	0.1802	-1.5009		
5	1.16	0.0	0.1075	0.0315	-0.0091	-0.0046	0.0113		0.0656	0.1848	0.1454		
6	7.13	0.0	7.27.17	3-1341		-0.00-0	0.0056		0.0656	0.1660	0.4900	·	
7	4.25	0.0	0.5721	0.2421		-0.0116	0.0132		0.0578	0.1921	0.5157		
8	6.33 8.44	0.01	1.1-42	0.5450		6-00-9	0.0106		0.0678	0.2012	0.4977		
10	10.54	0.01	1.5374		-0.0328	0.0671	0.0121		0.0720	0.2196	0.4665		
<del>ii -</del>	12.42	0.01	1.9441	0.7701	-0.267	-4-6148	0.0138		0.0742	0.2317	0.3992	<del></del>	
15	14.75	0.01	3000		-0.0370	-C.0014	0.0154		0.0742	0.2451	0.3473		
13	10.59	0.01	2.407		-0.0491	C-G070	0.0119		0.0742	0.2614	0.2875	<del> </del>	
14	19.04	0.02	3.3576		-0.0532	0.0165	0.0126		0.0742	0.2779	0.2470		
15	21.14	0.01	3.6443		-0.0510	0.0072	0.0119		0.0763	0.2958	0.2353		
16	23.39	0.05	4.4740	C-926+	-0.0697	0.0172	0.0112		0.0763	0.3180	0.2075		
17	0.10	0.0	0.0210	-6-0327	-0-01-7	0.0036	0.0106	0.2445	0.0678	0.1767	-1.5009		
					•								· · · · · ·
	•												
				· · · · · · · · · · · · · · · · · · ·									
	-	•											
										· · · · · · · · · · · · · · · · · · ·			
		•											
				<del></del>			<del></del>					<del></del>	
				<del> </del>							···	<del></del>	
	_				_								
				. <u>.                                   </u>	·····	<del></del>					·	······································	~-
				<del></del>						<del></del>			
										<del></del>			

	1 OF 1			LANGLEY A	ESEAHCH (	EHTER( VAS.	issile ta	UNITAI IL EFFECTS	DATA	INO TUNN	EL (UP #T)	
				6 PHI	CUNF	L JEL			TRANSIT			
OINT	ALPHA	BETA	53 3.0 CN	0.0 B	14160 15			OFF OFF	FIXE	CAF	ACP	····
1	-3.75	0.0	-0.45v1	-0.2556	-0.0156	0.0213	0.0032	0.2444	0.0678	0.1806	-0.5904	···
è	-7.19	0.0	-0.744-	-0.1516	-0.0171	0.0453	5+00.0	0.2460	0.0678	0.1742	0.6205	
3	-1.1-	6.0	-r-113-	-0.0835		0.01.1	0.0045	U-2444	U-478	0-1766	0.7367	
4	-9-10	0-0	0.0366	-0.3201	-0.0247	0.0312	0.0002	0.2447	6.0678	0.1769	-0.7689	
5	0.95	0.0	0.1700	0.0.45	-0.0145	0.0161	9.0006	C.7454	G. 0676	0-1791	0.2769	
6	1.95	0.0	0.3012	n.12m6	-0.0124	0.0007	2-0014	0.2504	0.0678	0.1826	0.4270	
-	4.77	0.0	0.5632		-0.0220	0.011	0.0027	0-2580	0.0678	0.1902	0.4711	
-3-	4.23	0.0	1.2256		-0.0295	0.01-9	0.0039	1465°0	0.0699	0.1949	0.4050	
10	10.30	0.01	1.6245	6.2633	-0.0417	0.0200	0.0015	0.2903	0.0720	0.2163	0.1744	
ii	12.34	0.01	2.01-7	0.2434	-0.0441	0.0427	0.0029	0.3019	0.0720	0.2299	0.1205	
15	14,54	0.01	2.4732	7-1660	-0.0663	0.0418	0.0045	0.3163	0.0720	0.2443	0.0674	
13	14.55	0.01	2.9003		-0.0710	0.6544	0.0061	0.3325	0.0720	0.2605	0.0227	
14	10.30	0.01	3.4472	-0-7540	-J.0e33	0.0300	0.0026	0.3443	0.0720	0.2763	-0.0084	
15	Su-Wh	0.01	3.4414		-3-0754	0.0451	0.0043	0.3685	C.0720	0.2965	-0-0393	
16	23.10	0.01	4.5678	-r.3533	-0.0708	0.0377	0.0061	0.3896	0.0699	0.3197	-0.0773	
17	-0.10	0.0	0.0371	-0.0107	-0.0041	-0-0086	-0.0051	0.2429	0.0699	0.1730	-0.4500	
						<del></del>				<del></del>		<del></del>
								•		į		
									1,000	,		
									·*	•		
•				•							-	•
								•				
									<del></del>			
					•							
			· · · · · · · · · · · · · · · · · · ·					······································			· · · · · · · · · · · · · · · · · ·	
					·							
			-								, ,	
											· · · · · · · · · · · · · · · · · · ·	
				<del></del>	<del></del>			· · · · · · · · · · · · · · · · · · ·	<del></del>			
	·										•	
											<del> </del>	<del></del>

PAGE 1 OF 1 SHEET 1 OF 1

	TEST 3		AL- PX10- 64 3.0		CONF 1-1+0 1	L DEL		UEL3 DEL4 UFF OFF	THANSITI	N			
INT	ALPHA	HETA	CN	CLM	CY	CLN	CLL	CA	CAR	CAF	ACP		
1	-3.36	(· • U	-0.3649	-0.2515	-0.0095	0.0129	-0.0016	1225.0	0.0499	0.1728	0.6894		
2	-1.53	(-6	-0-1717	-0.1537	-6.0075	0.0040	-0.0076	0.2192	0.0499	0.1693	0.8924		
3	-1)-44	(1 . 0	-0.0500	-0.0827	-0.0165	0.0210	-0.0003		U-0499	0.1699	1-6540		
4	0.76	0.0	0.0463	-0.ulle	-0.4043	0.0057	-0.0064	0.2202_	0.0499	0.1703	-0-1232		
5	1.28	0.0	1635.0	0-6730	-0.0196	0.0744	-0.0057	0-22-0	0.0499	0.1741	0.3199		•
6	2.27	0.0	0.3342	0.1260	-0.0061	0.0008	-0.9052		0.0449	0.1771	0.4672	· · · · · · · · · · · · · · · · · · ·	<u>,                                      </u>
7	4.36	0.0	7.6056	6.315.	~0.0062	0.0047	-0.00+0		0.0499	0.1815	0.5156		
8	6.42	0.0	200347	0.3563	-0.0071	0.0054	-7.0095		0.0499	0.1940	0.3962		
9	#.50	0.0	1.19-5		-0.0046		-0.0003		0.0576	0.1990	0.3266		
0	10.55	V. U	1.5030	C-3213	-0.0273	0.0184	-0.0049		0.0526	0.2120	<u>0-2055</u>		
1	17.60	0.0	1.9060	0.2005		-0.0023	-0.0057		0.0526	1.2247	0.1470		
2	14.71	6.01	2.1724	0.1466	-0.05+4	0.0376	-0.0041		0-0526	0.2369	0.0355		<del></del>
3	16.91	0.01	2.7355	0.1021	-0.0547		-0.0094		0.0526	0.2553	0.0373		
4	18.92	0.01	3.21+3	-ú-00+0	-9.0540		-0-0078		0.0526	0.2715	-0.0263		
5	20.45	0.01	3.7132	-0.5647	-0.0557		-0-0062		0.0526	0.2434	-0.0751 -0.1313		
6	23.17	0.01	4.2407				-0.0063		0.0526	0.1692		·	<del></del>
7	0.26	0.0	0.1179	-0.0272	-0.0051	0.000	-0.0063	0.2210	0.0354	0.1035	-0.2304		
												·	
								<u> </u>		-,	·	<del></del> ,	
									· · · · · · · · · · · · · · · · · · ·			<del></del> _	
			···	<u> </u>			_				· · · · · · · · · · · · · · · · · · ·		
					<del></del>		•						
		•											•
				-								"	

LANGLEY RESEMPCH CENTER (MASA) UNITARY PLAN WIND TUNNEL (UPWT)
MARTIN MISSILE TAIL EFFECTS DATA

		·	
	LANGLEY HESEARCH CENTER (NASA)	UNITARY PLAN WIND TUNNEL (UPST)	
.PAGE 1 OF 1	MARTIN MISSILL TA	AIL EFFECTS DATA	
SHEET 1 GF 1			

	1 -3.12 -0.31 -0.255 -0.2133	1 -3.12 -0.81 -0.425 -0.2133	-3.12 -0.81 -0.255 -0.2133		TEST		64 3.0		CUMF 1-1F0 15	. +20 OF		OFF OFF				•
7 -1.5\(\text{P}\) 0.0\(\text{C}\) -1.2\(\text{Ps}\) \(\text{Ps}\) -0.0\(\text{Ps}\) \(\text{Ps}\) \	7 -1.5\( 0.0 \) -0.7\( 0.0 \) -0.7\( 0.0 \) -0.7\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \) -0.0\( 0.0 \)	7 -1.5# 0.0 -1.276.9	-1.5P	]×T		6ET4	CN			CLY	CLL	CA	CAB	CAF		
3 -0.58 -0.01 -0.042 -0.023	3 -0.58 -0.01 -0.042 -0.023	3 -0.58 -0.01 -0.042 -0.023	-0.5h -0.0l -0.42v -0.0239 v.0340 -0.4573 -0.0023 u.7218 u.024v 0.1719 0.2587 0.500 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0			-0.01										
4	4	4	1.53 0.0 0.0 9.041% 0.044 0.0335 -0.0515 0.0003 0.2227 0.0499 0.1723 1.0726 1.53 0.6 7.1933 7.1045 0.0072 -0.0162 -0.0058 0.2247 0.0499 0.1728 0.5753 2.54 0.0 7.2775 0.1910 0.0109 -0.0141 0.0014 0.2275 0.0499 0.1776 0.6428 4.61 0.0 0.5731 0.3466 0.0133 -0.0143 -0.0004 0.2275 0.0499 0.1776 0.6428 4.61 0.0 0.5731 0.3466 0.0133 -0.0143 -0.0004 0.2336 0.0499 0.1777 0.6051 4.67 0.0 0.07399 0.5255 0.0335 0.0022 -0.0028 0.2236 0.0499 0.1837 0.6051 4.67 0.0 0.07399 0.5255 0.0141 -0.0045 -0.0001 0.2664 0.0526 0.1949 0.5671 10.41 0.0 1.4646 0.0045 0.0045 0.0017 -0.0045 0.2794 0.0553 0.2241 0.3665 12.57 0.0 1.6550 0.0680 -0.0184 -0.0077 -0.0064 0.2794 0.0553 0.2241 0.3665 14.97 0.0 2.2471 0.0950 -0.0015 -0.0444 -0.0038 0.2942 0.0553 0.2349 0.3093 17.06 0.0 2.5540 0.700 -0.0071 -0.0345 -0.0022 0.3093 0.0553 0.2339 0.3093 17.14 0.0 3.1677 0.6557 -0.0024 -0.0546 -0.0022 0.3093 0.0553 0.2339 0.3093 27.40 0.01 4.1778 0.6557 -0.0054 -0.0064 0.3717 0.0553 0.2724 0.2070 27.40 0.0 4.1778 0.6557 0.00557 0.0064 0.0071 0.0553 0.0553 0.2340 0.0553 27.40 0.01 4.1778 0.6657 -0.0064 -0.0064 0.0071 0.0553 0.0553 0.2346 0.1541 0.49 0.0 0.0017 0.0557 0.0059 -0.0070 -0.0064 0.0071 0.0066 0.0071 0.0066 0.0071 0.0065 0.0071 0.0065 0.0071 0.00553 0.2547 0.00553 0.2547 0.2655	<u> </u>												
5 1.53 0.6 7.1933 7.1045 0.0072 -0.0162 -0.0058 0.7247 0.0699 0.1746 0.5753 7.56 0.6072 0.1910 0.0104 -0.0161 0.0014 0.275 0.0699 0.1776 0.6626 7.6075 0.1910 0.0104 0.6026 7.6075 0.0049 0.1375 0.6082 7.6080 0.7336 0.0499 0.1877 0.6082 7.6080 0.7336 0.0499 0.1877 0.6081 8 6.67 0.0 0.7309 0.7257 5.0335 0.0022 -0.0028 0.2233 0.0499 0.1924 0.6330 7.77 0.0 1.140 0.0062 0.0062 0.0062 0.2255 0.0526 0.1949 0.5671 0.410 0.0 1.4846 0.0065 0.0141 0.0045 0.0062 0.2255 0.0526 0.1949 0.5671 0.411 0.0 1.4846 0.0065 0.0141 0.0045 0.0062 0.2555 0.0526 0.2138 0.4018 12.67 0.0 1.6556 0.0065 0.0018 0.0065 0.2759 0.0553 0.2261 0.3065 1.2677 0.0065 0.0076 0.0077 0.0065 0.2794 0.0553 0.2261 0.3065 0.1949 0.3065 0.2241 0.0055 0.0065 0.2082 0.0055 0.2261 0.3065 0.2082 0.0055 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0082 0.3080 0.0082 0.00	5 1.53 0.6 7.1933 7.1095 0.0072 -0.0162 -0.0058 0.7247 0.0699 0.1746 0.5753 6 7.54 0.0 7.2775 0.1910 0.0109 -0.0161 0.0014 0.2275 0.0699 0.1776 0.6628 7 4.61 0.0 0.5731 0.3665 0.0133 -0.0133 -0.0040 0.2336 0.0499 0.1877 0.6051 0 6.67 0.0 0.0739 0.0735 0.0013 0.0022 -0.0028 0.223 0.0499 0.1924 0.6330 0 7.77 0.0 1.140 0.00626 0.0055 0.0022 -0.0028 0.2235 0.0526 0.1999 0.5671 0 10.41 0.0 1.4866 0.0005 0.0111 -0.0465 -0.0001 0.2666 0.0256 0.2138 0.6018 1 12.67 0.0 1.6556 0.0005 0.0005 0.2245 0.0552 0.2241 0.0651 0.1999 0.5671 0.0005 0.2241 0.0055 0.2241 0.0055 0.2241 0.0055 0.2241 0.0055 0.2041 -0.0045 -0.0056 0.2794 0.0553 0.2241 0.3665 0.1999 0.0553 0.2241 0.3665 0.1999 0.0553 0.2241 0.3665 0.1999 0.0553 0.2241 0.3665 0.1999 0.0553 0.2241 0.3653 0.2341 0.0055 0.2041 0.0055 0.2042 0.0553 0.2241 0.3665 0.1999 0.0553 0.2241 0.3655 0.2041 0.0055 0.2042 0.0553 0.2241 0.3665 0.2042 0.0553 0.2341 0.0055 0.2042 0.0553 0.2341 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.2042 0.0055 0.20	5 1.53 0.6 7.1933 7.1045 0.0072 -0.0162 -0.0058 0.7247 0.0699 0.1746 0.5753 7.56 0.6072 0.1910 0.0104 -0.0161 0.0014 0.275 0.0699 0.1776 0.6626 7.6075 0.1910 0.0104 0.6026 7.6075 0.0049 0.1375 0.6082 7.6080 0.7336 0.0499 0.1877 0.6082 7.6080 0.7336 0.0499 0.1877 0.6081 8 6.67 0.0 0.7309 0.7257 5.0335 0.0022 -0.0028 0.2233 0.0499 0.1924 0.6330 7.77 0.0 1.140 0.0062 0.0062 0.0062 0.2255 0.0526 0.1949 0.5671 0.410 0.0 1.4846 0.0065 0.0141 0.0045 0.0062 0.2255 0.0526 0.1949 0.5671 0.411 0.0 1.4846 0.0065 0.0141 0.0045 0.0062 0.2555 0.0526 0.2138 0.4018 12.67 0.0 1.6556 0.0065 0.0018 0.0065 0.2759 0.0553 0.2261 0.3065 1.2677 0.0065 0.0076 0.0077 0.0065 0.2794 0.0553 0.2261 0.3065 0.1949 0.3065 0.2241 0.0055 0.0065 0.2082 0.0055 0.2261 0.3065 0.2082 0.0055 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2261 0.3065 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0553 0.2082 0.3080 0.0082 0.3080 0.0082 0.00	1.53 0.6	3												
6 7.54 0.0	6 7.54 0.0	6 7.54 0.0	7.54 0.0	<u> </u>												
7 4.61 0.6 0.5731 0.3465 0.0193 -0.0193 -0.0193 0.2336 0.0499 0.1937 0.6051 0.677 0.0 0.0739 0.0555 0.0355 0.0355 0.0499 0.1937 0.6051 0.0177 0.0081 0.2823 0.0499 0.1937 0.6338 0.0499 0.1937 0.6338 0.0499 0.1938 0.0555 0.1949 0.5671 0.0177 0.0082 0.2525 0.0526 0.1949 0.5671 0.0410 0.0 1.4040 0.0441 0.0 1.4040 0.0445 0.00845 0.0001 0.2664 0.0526 0.2138 0.4410 0.0 1.4050 0.0401 0.0410 0.0085 0.0081 0.2664 0.0553 0.2241 0.3665 0.1941 0.0085 0.0081 0.2664 0.0553 0.2241 0.3665 0.3083 0.3790 0.2794 0.0553 0.2241 0.3665 0.3083 0.3790 0.0553 0.2349 0.3083 0.3083 0.3790 0.0553 0.2349 0.3083 0.3083 0.3083 0.3083 0.3083 0.3083 0.3083 0.3083 0.3517 0.0557 0.4055 0.4026 0.0553 0.2517 0.2655 0.4026 0.0553 0.2517 0.2655 0.4026 0.0553 0.2517 0.2655 0.4026 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2724 0.2770 0.0553 0.2792 0.1832 0.0553 0.2792 0.1832 0.0553 0.2792 0.1832 0.0553 0.2792 0.1832 0.0553 0.0553 0.2792 0.1832 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0.0553 0	7	7 4.61 0.0 0.5731 0.34ec 0.0193 -0.0193 -0.0000 0.2536 0.0499 0.1837 0.6051 0.6070 0.0 0.2535 0.0526 0.0299 0.1837 0.6051 0.0027 -0.0028 0.2823 0.0499 0.1924 0.6338 0.777 0.0 1.140 0.6400 0.0000 -0.0177 -0.0002 0.2525 0.0526 0.1999 0.5671 0.4140 0.0 1.4040 0.0445 0.0445 -0.0001 0.2664 0.0526 0.2138 0.4418 0.0 1.4040 0.0445 0.0445 -0.0001 0.2664 0.0526 0.2138 0.4618 0.2541 0.0400 0.2541 0.0400 0.02794 0.0553 0.2241 0.3665 0.3090 0.0553 0.2241 0.3665 0.3090 0.0553 0.2241 0.3665 0.3090 0.0553 0.2349 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.3093 0.30	4.61 0.0 0.5731 0.3600 0.0133 -0.0143 -0.0040 0.2336 0.0499 0.1837 0.6051 0.0477 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-												
8	8	8 6.67 0.0 0.2309 0.525y 5.9335 0.0027 -0.0028 0.2423 0.0499 0.1924 0.6330  9 10.77 0.6 1.1 40 0.6 0.0 0.0000 0.0000 0.2000 0.2525 0.0526 0.1949 0.5671  10 10.41 0.0 1.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	6.67 0.0 0.0-309 0.525y 5.0035 0.0027 -0.0028 0.2023 0.0049 0.1924 0.6330  1.77 0.0 1.140 0.0 0.000 -0.0107 -0.0002 0.2525 0.0526 0.1949 0.5671  10.41 0.0 1.600 0.0045 0.0045 -0.0001 0.2664 0.0526 0.2138 0.4018  12.67 0.0 1.605 0.0600 -0.0016 -0.0077 -0.0054 0.2794 0.0553 0.2241 0.3665  14.97 0.0 2.201 0.0690 -0.0015 -0.0044 -0.0038 0.2942 0.0553 0.2349 0.3093  17.00 0.0 2.5040 0.7050 -0.0071 -0.0355 -0.0022 0.3040 0.0553 0.2339 0.3093  14.14 0.0 3.1677 0.6557 -0.0026 -0.0565 -0.0027 0.0553 0.2724 0.2070  21.23 0.0 3.6331 0.6537 0.0055 -0.0040 -0.0031 0.3955 0.0553 0.2724 0.2070  23.40 0.01 4.1778 0.6437 -0.0740 -0.0740 -0.0110 0.3717 0.0553 0.3164 0.1541  0.44 0.0 0.0017 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.3164 0.1541	<u>-</u>												<del></del>
7	7	7	10.41 0.0 1.440 0.650 0.0141 -0.0045 -0.0001 0.2664 0.0526 0.2136 0.4610  12.57 0.0 1.655 0.6000 -0.0184 -0.0074 0.2794 0.0553 0.2241 0.3665  14.97 0.0 2.241 0.6950 -0.0015 -0.0044 -0.0038 0.2942 0.0553 0.2369 0.3093  17.06 0.0 2.654 0.705 -0.0074 -0.0345 -0.0022 0.3093 0.0553 0.2517 0.2655  14.14 0.0 3.1477 0.6557 -0.0024 -0.0555 0.2021 0.3093 0.0553 0.2517 0.2655  14.15 0.0 3.6331 0.657 0.0059 -0.0059 0.0051 0.3277 0.0553 0.2724 0.2704  21.23 0.0 3.6331 0.657 0.0059 -0.0060 0.0011 0.3095 0.0553 0.2942 0.1832  27.40 0.01 4.1778 0.6637 -0.0745 -0.0280 -0.0114 0.3717 0.0553 0.3164 0.1541  0.49 0.0 0.0417 0.0557 5.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362			_		-								
10.41 0.0 1.484e	10.41 0.0 1.484e	10.41 0.0 1.484e	10.41 0.0 1.eAab G.bas5 G.Ulyl -0.0455 -0.0001 0.2664 0.0526 0.2138 0.4618 12.57 0.0 1.e554 0.bd0C -0.018A -0.0077 -0.0054 0.2794 0.0553 0.2241 0.3665 14.97 0.0 2.241 0.6950 -0.0015 -0.0046 -0.0038 0.2942 0.0553 0.2349 0.3093 17.06 0.0 2.6545 0.7050 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 14.17 0.0 3.1677 G.6557 -0.0026 -0.0565 -0.0022 0.3090 0.0553 0.2537 0.2655 21.23 0.0 3.631 0.6657 0.0050 -0.0060 0.3277 0.0553 0.2942 0.2070 21.23 0.0 3.631 0.6657 0.0050 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 23.40 0.01 4.1770 0.6437 -0.0246 -0.0246 -0.0114 0.3717 0.0553 0.3164 0.1541 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362													
1 12.57 0.0 1.c756	1 12.57 0.0 1.e756 0.000 -0:0188 -0.0077 -0.0054 0.2796 0.0553 0.2241 0.3665 2 14.97 0.0 2.241 0.6456 -0:0015 -0.0046 -0.0038 0.2942 0.0553 0.2349 0.3093 3 17.06 0.0 2.6461 0.7056 -0.0071 -0.0345 -0.0022 0.3093 0.0553 0.2537 0.2655 4 14.14 0.0 3.1677 0.6557 -0.0026 -0.0565 -0.0022 0.3093 0.0553 0.2724 0.2076 5 21.23 0.0 3.6341 0.6657 0.0054 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1032 6 27.40 0.01 4.1778 0.6437 -0.0246 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.44 0.0 0.0417 0.0557 0.0333 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	1 12.57 0.0 1.e756	12.57 0.0 1.c55								_					-
14-97 0.0 2.24/1 0.6950 -0.0015 -0.0044 -0.0038 0.2942 0.0553 0.2349 0.3043 3 17.06 0.0 2.6549 0.7056 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 6 14-14 0.0 3.1677 0.6557 -0.0026 -0.0555 -0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6341 0.6657 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0745 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	14-97 0.0 2.24/1 0.6950 -0.0015 -0.0044 -0.0038 0.2942 0.0553 0.2349 0.3043 3 17.06 0.0 2.6549 0.7056 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 6 14-14 0.0 3.1677 0.6557 -0.0026 -0.0555 -0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6341 0.6657 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0745 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	14-97 0.0 2.24/1 0.6950 -0.0015 -0.0044 -0.0038 0.2942 0.0553 0.2349 0.3043 3 17.06 0.0 2.6549 0.7056 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 6 14-14 0.0 3.1677 0.6557 -0.0026 -0.0555 -0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6341 0.6657 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0745 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	14.97 0.0 2.241 0.6950 -0.0015 -6.0646 -0.0038 0.2942 0.0553 0.2389 6.3093 17.06 0.6 2.6586 0.7056 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 14.15 0.0 3.1677 0.6557 -0.0026 -0.0565 -0.0277 0.0553 0.2724 0.2070 21.23 0.0 3.6331 0.6657 0.0059 -0.0046 -0.0031 0.3277 0.0553 0.2942 0.1832 23.40 0.01 4.1778 0.6637 -0.0746 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362		12.57											
3 17.06 0.6 2.6585 0.7050 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 4 14.19 0.0 3.1677 0.6557 -0.0026 -0.0545 -0.0015 0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6531 0.6557 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1032 6 23.40 0.01 4.1778 0.6437 -0.0740 -0.0280 -0.0319 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	3 17.06 0.6 2.6585 0.7050 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 4 14.19 0.0 3.1677 0.6557 -0.0026 -0.0545 -0.0015 0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6531 0.6557 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1032 6 23.40 0.01 4.1778 0.6437 -0.0740 -0.0280 -0.0319 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	3 17.06 0.6 2.6585 0.7050 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 4 14.19 0.0 3.1677 0.6557 -0.0026 -0.0545 -0.0015 0.3277 0.0553 0.2724 0.2070 5 21.23 0.0 3.6531 0.6557 0.0059 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1032 6 23.40 0.01 4.1778 0.6437 -0.0740 -0.0280 -0.0319 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	17.06 0.6 2.654 0.7056 -0.0071 -0.0345 -0.0022 0.3090 0.0553 0.2537 0.2655 14.19 0.0 3.1677 0.6557 -0.0026 -0.0565 -0.0015 0.3277 0.0553 0.2724 0.2070 21.23 0.0 3.6331 0.6657 0.0059 -0.0060 -0.0031 0.3495 0.0553 0.2942 0.1832 23.40 0.01 4.1778 0.6637 -0.0260 -0.0216 0.3717 0.0553 0.3164 0.1541 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	_												
4 14.19 7.0 3.1677 G.6557 -4.0026 -C.05-5 -7.0015 0.3277 0.0553 7.2724 0.2070 5 21.23 0.0 3.6331 7.6657 7.0059 -0.0640 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 C.6437 -0.0265 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	4 14.19 7.0 3.1677 G.6557 -4.0026 -C.05-5 -7.0015 0.3277 0.0553 7.2724 0.2070 5 21.23 0.0 3.6331 7.6657 7.0059 -0.0640 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 C.6437 -0.0265 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	4 14.19 7.0 3.1677 G.6557 -4.0026 -C.05-5 -7.0015 0.3277 0.0553 7.2724 0.2070 5 21.23 0.0 3.6331 7.6657 7.0059 -0.0640 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 C.6437 -0.0265 -0.0260 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	19.19													
5 21.23 0.0 3.6351 7.6657 7.0054 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0240 -0.0240 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.44 0.0 0.0417 0.0557 0.0330 -0.0349 -0.0064 0.2244 0.0553 0.1691 1.3362	5 21.23 0.0 3.6351 7.6657 7.0054 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0240 -0.0240 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.44 0.0 0.0417 0.0557 0.0330 -0.0349 -0.0064 0.2244 0.0553 0.1691 1.3362	5 21.23 0.0 3.6351 7.6657 7.0054 -0.0040 -0.0031 0.3495 0.0553 0.2942 0.1832 6 23.40 0.01 4.1778 0.6437 -0.0240 -0.0240 -0.0114 0.3717 0.0553 0.3164 0.1541 7 0.44 0.0 0.0417 0.0557 0.0330 -0.0349 -0.0064 0.2244 0.0553 0.1691 1.3362	21.23 0.0 3.6351 0.0657 0.0059 -0.0060 -0.0031 0.3695 0.0553 0.2942 0.1832 23.40 0.01 4.1778 0.6437 -0.0746 -0.0240 -0.0114 0.3717 0.0553 0.3164 0.1541 0.49 0.0 0.0417 0.0557 0.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	4	19.19	9.0	3.1477	0.6557	-4.0026	-0.05-5	-7.0015	0.3277				
7 0.49 0.0 0.0417 0.0557 2.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	7 0.49 0.0 0.0417 0.0557 2.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	7 0.49 0.0 0.0417 0.0557 2.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	0.49 0.0 0.0417 0.0557 2.0330 -0.0399 -0.0064 0.2244 0.0553 0.1691 1.3362	5		0.0	3.6331	3.6657	6.0074	-0.0040	-0.0031	U.3495	0.05>3		6.1835	
					0.49	0.0	0.0417	0.0557	5.0330	-0.0399	-0.0064	0.2244	0.0553	0.1691	1.3362	
				_												

-------

. . . . .

				LANGLEY H	ESEAHCH C	ENTENTHASA				IND TUNN	L (UPWT)		<del></del>
	1 OF 1					ARKITA MI	SSILE TA	IL EFFECTS	DATA				
			<del></del>						<del></del>				
	1651		AL- FRIU-	Ind d	CUNF	L DELI			THANSIT!			· · · · · ·	
	3	93 5.	36 3.0	0.0 A	146+0 0	o Off	OFF	off off	FIXE	<u> </u>			
INT		META	CN	CLM	CY	CLN	CLL	CA	CAR	CAF	ACP		
1	-3.41		-0-1445		-0.0135		2400-0	0.2955	0.1230	0.1725	2.6767		
2	-7.13	0.01	-0.1715	-0.2805	-0.01++	-0-0211	0.0075	0.2479	0.1187	0.1692	. 2.3095		
3	-1.11 -0.01	0-07	-0.0552	-4-1316	-0.0042	-0-0316	0.0031	0.2850	0.1185	0.1675	1.9882		
5	1.49	0.01	0.0372	0.1835	-0.01/0 -0.0303	-0.0274	0.0004	0.2055	0.1187	0.1653	-1.6976 4.9333		
9 6	5.05	0.01	0.10.1	0.3334	-0.0157	-0.0279	0.0043	0.2870	0.1200	0.1670	3.2071	•	
Ÿ	4.16	6 <del>. 31</del>	0.7276	0-551-	-0.0297		-0.005i	- 0.2942	U.1258	0.1684	2.8369		<del></del>
ė	5.19	0.91	UUHF.O	0-690 4	-0.0261	-0.0254	0.0075	0.3077	0.1356	0.1721	2.3429		
9	5.32	0.01	0.5875	100942	-0.0269	-6.0303	0.0015	0.3717	0.1409	0.1746	1.8625		
0	10.00	0.01	0.4317	1-1352	-0.0164	-0.0700	0.0013	0.3358	0.1596	0.1762	1.2182		
11	12.57	0.01	1.3407	1.1527	=0.020d	-0.01.5	0.0029	0.3442	0.1709	0.1783	0.8542		
2	14.40	0.02	1.5074	1.1057	-0.0454	-0.0144	0.0045	0.3544	0.1737	0.1807	0.6118		
3	16.90	0.02	5.2617		-0.0576	0.0103	9200.0	0.3627	v.1766	0.1841	0.4772		
4	19.19	0.03	2.7524		-0.0570	0.0036	5-00-C	0.36A0	0.1765	0.1915	0.3756		
15	51.32	0.03	3-2350	0.7470			0.0057	0.3069	0.1551	0.1947	0.2927		
6	23.+3	0.04	3.7713		-0.0959	0.0176	0.0038	0.3805	0.1495	0.2110	0.2151		<u></u>
17	-0.61	0.41	-0.0041	0.0244	-0-6178	-0.0331	0.0001	0.2827	6.1147	0.1640	-3.6346	•	
									<del>-</del>			<del></del>	
			<del></del>						-	•	·		
		• • • • • • • • • • • • • • • • • • • •			• • • • • • • • • • • • • • • • • • • •			•	<del></del>		<del></del>		
									•				
					······································						<del></del>		
									•				
											· · · · · · · · · · · · · · · · · · ·		
											_		
			<del></del>					<del></del>			<del> </del>		
			<del></del>										<del></del>
					·····		· <del></del> -		<del></del>				

				LANGLEY 4	ESEARCH (	ENTER LASA		UNITAL	Y PLAN	IND TUNN	L (UP4T)	
	1 OF 1 1 OF 1				<del></del>	MARTIN MI	SSILE TA	IL EFFECTS	DATA			
EET,												
	<del></del>		<del></del>			<del></del>		<del></del>		***************************************	<del></del>	
									1011			
			ACH HAID-			L LELI			THANSIT			
	3	<u> </u>	bb 3.0	V.U B	1=6F0 (	0.0 UFF	DFF	OFF OFF	FIXE	<del>'</del>		
OINT	ALPHA	PFTA	CN	CLM	CY	CLN	CLL	CA	CAH	CAF	ACP	
	-3,77	0.0	-7.2150	-0.5604	-0.0001	-4.05.45	0.0025	0.7604	0.1032	0.1572	2.6065	
2	-2.7-	0.0	-^-1247	-0.43/v	-0.0034	-0.0754	9.0031	0.7592	0-1000	0.1592	2.7057	
3	-1.20	0.01	-0.0744	-10-151n	-v-C175	-1.00.00	0-0035	0-2517	0-1901	0.1616	2.1753	
•	-0.17	0.01	-7-0095	0.0341	-0-0161	-6-0215	0.0	0-26-5	0.1037_	0.1613	-0.4211	
6	0.43	0.01 0.01	0.0411			-0.0295	0.0004	0.2673	0.1033	0.1640	3.9333 3.0340	
<u> </u>			3.73				0.0010	-0634	- 1017		-3.4401	
6	3.46	0.44	-2356	0.6134	-6.0233	-0.0254	G.Ouln	0.2677	0.1017	0.1660	2.6931	
9	6.43	0	200155	C-0583	-0-0173		0.0025	0.2746	0.1049	0.1717	2.1413	
10	A.15	0.01	0.6602	0.7481	-0.0211	-6.0367	6.0036	0.2885	0.1145	0.1740	1.4361	
11	10.25	0.01	1.0104			-6.0179	0.0009	0.3005	0.1757	0.1748	0.9116	
12	12.36	0.01	1.3729		-0.020A	-0.0122	0.0023	0.3067	<u>0.1273</u>	0-1814	0.6914	
14	10.00	0.05	2.2015	0.0561	-0.0613	-0-99E	0.0038	0.3162	0.1305	0.1857	0.4985 0.3888	
15	16.65	0.36	2.5335	(.7947		-0.01.6	12000	0.3240	0.1239	0.2001	0.3010	
16	20.44	0.03	3.0629	0.7239	-0.0780	4450.0	5.0042	0.3405	0.1272	0.2133	0.2364	
17	23.17		3.5244	0.5768		0.0123	V.0056	0.3544	0.1257	0.2287	0.1640	
18	-0.17	0.01	-0.0097	0.0133	-0.0166	-0.0209	0.0	0.2669	0.1064	0.1605	-1.3691	
<del></del>											<del> </del>	
								•				
		_										
							•					
_												<del>:</del>
												<del></del>

-	
<del></del>	
•	
	<b>&gt;</b>
· ·	EDC
	AEDC-TR-75-125
<del></del>	75-12
	σì

				L ANULEY H	tatamin (	ENTERINASA	)	UNITAL	T PLAN .	IND TUNN	EL (UP# 1)	
	1 OF 1					MARTIN MI	SSILE TA	ALL EFFECTS	DATA			
E E. Y	1 OF 1											
,								· ,				
	77.57	FAUL -	ACH HATU-	6 PH1	CONF	L DELI	DELZ	DEL3 DEL4	TheMSIT	ON		
	3		Y5 3.0	C.0 b		.0 OFF	OFF	OFF OFF	FIXE		•	
										-		
Olwt	ALPHA	SETA	C-a	CLH	CY	CL4 ·	CLL	CA	CAH	CAF	ACP	
1	-1.60	0.0	-0.2050	-6.4277		-0.0194	0.0040	0.2063	0.0568	0.1395	2.0762	
<u>. 5</u>	-2.21	6.6	-0.1144	-4.5.54	-0.0224	0.0016	0.00-6	0.2055	0.0669	0.1346	2.0334	<del></del>
3	-0.13	0.0	0.000	0.0300	-0.01-1 -0.0053	-0.0100 -0.0217	0.0050	0-2343	0.0668	0.1375 0.1300	2.3791 33.3778	
<del>-</del>	20.13	0.0	0.0520	- 0.1/81	-6.0176	-0.0067	0.0057	0.2071	0.0668	0.1403	3,4250	<del></del>
•	1.42	0.01	0.1723	0.2692	-0.0294	0.0078	0.0061	0.2085	0.0468	0.1417	2.3645	-
ż	4.00	0.01	2.2014		-0.0331	0.0112	0.0069		0.0566	0.1444	2.0500	
8	6.03	0.0	0.45-10	0.6502	-0.0123	-0.0156	0.0078	0.2145	0.0689	0.1496	1.4177	
4	9.12	0.01	0.727	U+9400	-0.0273	47)C.U-	0.0069	0.2266	0.6710	C.1556	0.8894	
10	10.10	0.01	1.0101	0.6717	-0.020A	0.0036	0.0047	0.2336	0.0753	0.1583	0,6651	
11	17.25	C. V1	1.3140	0.7044	-0.0213	-0.0075	0.0059		Q.0753	0.1693	0.5365	
12	14.33	0.01	1.0353	0.7226	-0.0342	5500.0	0.0071	6.2552	_6.0753	0.1799	0.4416	
13	15.44	0.01	1.5765	0-1-03	-0.0467	0.0158	0.0084	2892.0	0.0753	0.1929	0.3745	
15	16.50	0.04	2.3522	0.7020	-0.0604	0.6131	0.0095	0.2527	0.0753	0.2074	0.2985	
16	20.52	0.02	2.7356 3.2116	4500.U	-0.0665	0.0450	3.0074		0.0732	0.2497	0.1630	
17	-0.12	0.01	0.0013	0.0295	-0.0765		0.0054		0.0710	0.1319	22.6769	
••		••••	***************************************	*******				***************************************				-
						-						
					-							
										<u> </u>		<u> </u>
								•				
							<del></del>				<del></del>	
									<del></del>		· · · · · · · · · · · · · · · · · · ·	
											••••	
												<del></del>
								-				

.. ....

		war . Er w	
PAGE 1 OF 1	LANGLEY MESEANCH CENTEM (1854) MARTIN MISSILE T	U-TTARY PLAN WIND TUNNEL (UPWT) TAIL EFFECTS DATA	
SHEET 1 OF 1			

3 -	3 1,32 1,43	.0.0	63 3.0 Ch		1-0F0 (	0-0 UFF	OF F	OFF OF	F FIXE	v	
3 -	3.32 1.43	.0.0		<b>~</b> 1						<del></del>	<del></del>
3 -	1.43			CLM	CA	CC~	CLL	CA	CAB	CAF	xce
3 -			-0.1950	-0.380H	-0.0170	+0.0127	0.0055	0.1845	0.0513	0.1332	1.9528
•	1 - 7 3	0.01	-0-1365	-C-1+10	-0.0345	0.00PA	6.0051	0.1836	6.0513	0.1373	1.8009
		C.U	-0-0-05	-0-0451	-0.0159	-1.01.13	U-0U65	0-143-	0.0513	0-1351	1.6199
5	0.23	0.0	0-0250	0.07/5	-0.0061	-0.0255	_0 <u>•0069</u>	0.1657	0.0513	0.1344	3.0258
	1.76	0.6	0-025	0-203/	-0-0104	-0.0134	0.0073	0.1870	0.0513	0.1357	2.2095
	5.26	0.01	7-1540	0.3296	-0.6301	0-0011	0.0010	0.1690	0-0513	0.1377	2.0730
	4.32	0.0	0.3155	0-5353	-0.0275	-0.0042	0.0018	0.1919	0.0513	0.1406	1.6913
	h. 16	0.61	n.4255	0.4137	-0.0460	0.0046	<u>4507.0</u>	0.1455	0.0513	0.1443	1.1669
	93	0.01	0.7719	V+0466	-C-0327	-0-0043	C.C037	0.232+	0.6513	0.1511	0.8325
	03	0.41	1.0161	0.7354	-0.0109	-0.0038	0-0047	0.2129	0.0540	0.1569	0.6942
	2.50	0.01	1.2477	3.7315	-0.0087	-0.0369	0.0058	0.2197	0.0540	0.1657	0.5662
	4.58	0.01	1.58-4	3.0405	-3.0368	0.0008	0.0002	0.55H4	0.0540	0.1744	0.4356
	6.06	0.01	1.9050	0-61/-	-0-0433		0-0091	0.2-10	0.0540	0.1870	0.3244
	· . 74	0.01	5.244	0-4647	-0.0448	-(.0175	0.0026	0.2549	0.0540	0.2058	0.2158
	0.77	0.01	5-6517	G-3965	-0.00/5	0.0747	0-0034		0.0540	0.2249	0.1513
	5.95	0.01	3.0430	6.5222	-0.0665	0.0227	0.0053		6.0540	0.2427	0.0853
17	0.24	0.0	6.0254	0.0776	-0.0055	-L.078B	0.0005	0.1874	0.0540	0.1334	3.0567
							•				
				7			-				
							···-·			·	
		<del> </del>					1				
						<del></del>				<del>, ,,, ,,, ,,, ,,, ,,, ,, ,, ,, ,, ,, ,,</del>	
					•					· · · · · · · · · · · · · · · · · · ·	

## APPENDIX D TEST 4

GE EET	1 OF 1			LANGLEY R	ESLARCH C	ENTEH (NAS MARTIN M	A) ISSILE TAI	UNITA L EFFECTS	DATA	140 TUNN	EL (UPUT)	
				<u></u>	·	·						
	†EST	PART H	ACH PX10-		CONF 20534 0		0 0 1 DEFS (	DEL3 DEL4	TRANSIT!	ION )		
DINT	ALPHA	BETA	CN	CLM	_CY	CL#	CLL	CA .	CAB	CAF	XCP	<del></del>
1	-4.07	0.01	-0.9036				-0.0737	0-4771	0.1361		-5.2637	
ζ_	-2.00	0.01	-0.4927		-0.0292		-0.0694	0.4696	0.1320		-2.3686	<del> </del>
5	-0.97	0.0	-0.2872 -0.0818	0.7112	-0.0184		-0.0675 -0.0674	0.4678	0.1316 0.1305		-2.4763 -3.2552	
<del></del>	1.07	0.01		-0.1707	-0.0232		-0.0678	0.4649	0.1313		-1 .5850	
-	2.12	0.0	0.3114	-0.6110	-0.0223	0.0425	-0.0684	0.4658	0.1325		-1.9629	
7	4.16	0.0		-1.5022	-0.0270		-0.0756	0.4687	0.1351		-2.0914	
8	6.23	0.0			-0.0261		-0.0739	0.4823	0,1455		-2.0954	
9	8.32	0.0	1.6438				-0.0720	0.4925	0.1555		-2.0598	
10	10.45	0.0		-4.4133	-0.0308		-0.0741	_0.4976_	_ 0.1608_		-1.9661	
11	12.59	0.0		-5.3806	-0.0159		-0.0746	0.4960	0.1616		-1.8676	
15	14,74	0.0		-6.2539	-0-0269		0.0745	0.4878_	0.1616		-1.7820	· · · · · · · · · · · · · · · · · · ·
13	16.91	0.0	4.1920		-0.0069		-0.0726	0.4854	0.1611		-1.7269	
14	19.06	0.0	4.8631		-0.0131		-0.0689	0.4816	0.1593		-1.6775	
15 16	21.21	0.0	-0.0946	-9.1065	-0.0233		-0.0606	0.4784	0.1571 0.1310		-1-6405	
10	0.00	0.41	-0.0746	0.2172	-0.0233	~ 0.0591	-0.0/1/	U . 4040	0.1310	<u>0</u>	<u>-5.95[\$</u>	
												_
					•							
												_
												· · · · · · · · · · · · · · · · · · ·
			<del></del>									
							<del></del>					······································
					· · · · · · · · · · · · · · · · · · ·			···		<del></del>	·····	
									•			
	_											
					•							
											·	

GE.	1 OF 1			LANGLEY RE	SEARCH C	ENTER (NAS	A)	UNIT	ARY PLAN W	IND TUNN	EL (UPWT)	
	i of i						TABLE IN	E EFFECT	, vara			
		PART M	ACH RAID-		CONF	L OEL			TRANSITI			
		3 2.	36_3.0	-90.0 B	240134 0	•0	0 0	0	O FIXED	<u> </u>		
POINT	ALPHA	RETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	
1	-4.05	0.0	-0.8642	1.9662	0.0133	-0.0329	-0.0692	0.4765	0.1362	0.3403	-2.2751	
- 2	-1.98	0.0	-D.4578	1.0755	0.0185	-0.0467	-0.0683	0.4696	0.1334	0.3362	-2,3493	
3	-0.97 0.06	0.0	-0.2577	0.6244	0.0213	-0.0483	-0.0681 -0.0677	0.4677	0.1329	0.3348	-2.4230 -3.0921	
<u> </u>	1.08	- 0.0-	0.1303	-0.2412			-0.0650	0.4670	0.1318	0.3352		
6	2.11	0.0	0.3335	-0.6860		-0.0461		0.4670	0.1325	0.3345		
Ť		0.0	0.7340	-1.5737	0.0331	-0.0659	-0.0722	0.4724	0.1368	0.3356	-2.1439	
8	6.24	-0.01	1.1.008	-2.5182	0.0364		-0.0695	0.4880	0-1491	0.3369	-2.1326	
9	8.31	-0.01	1.6561	-3.4653	0.0326	-0.0618	-0.0707	0.5006	0.1585	1546.0	-2.0899	
10	10.44	0.0	2.2510	-4.4719	0.0119	-0.0400	-0.0737	0.5058	0.1635	0.3423	-1,9066	
11	12.60	0.0	2.4914	-5.4626	0.0206	-0.0486	-0.071B	0.5047	0.1637		-1.8892	
12	14.74_	0.0	3.5728	-6.3390		-0.0697	_	0.4974	0.1637_	0.3337	-1,7994	
13	16.88	0.0	4.1799	-7.2694	_	-0.0755	-0.0722	0.4971	0.1653	0.331	-1.7439	
14	19.05	0-0	4.8639	-8-2401	0.0310		-0.0734	0.4920	0.1625	0.3795	-1,6872	
15	21.22	0.0	5.5616	-9.2127 0.2083	0.0366	-0.1006	-0.0728 -0.0696	0.4903	0.1611 0.1320	0.3292	-1.6505 -2.0537	
17	0.05	-0.01	-0.0730	0.2085		-0.0509		0.4661	0.1314	0.3347		
••	0,03		-500.00	***************************************	******	-000300	-0,00.5	01002	******	***************************************	-200000	
								•		-		
									•			
								<del> </del>	<del></del>	<u> </u>		
				<del></del>						<del></del>	<del></del>	
												····
							•					
				· ·		•						
	_									-		-
						<u>-</u>			·		<del></del>	
								-		•		
								<del></del>			<del></del>	<del></del>
									•			
								<del></del>				

····· .

					<u> </u>								
	•												
					, , , , , , , , , , , , , , , , , , ,		<del></del>						
				LANGLEY RE	SEARCH C	ENTERINAS	A) ISSILE TAI	UNITA	RY PLAN E	IND TUNN	EL (UPUT)		
	1 OF 1					MANTIN M	ISSILE TAI	L EFFECTS	DATA				
LI	1 0 1												
			·····			<del></del>			<del></del>				
	TEST	PART H	ACH RX10-	6 PHI	CONF	L OEL	1 DEL2 C	EL3 DEL4	TRANSITI	ON			
		4 2.	86 3.0	-90.0 d	240F34 0	•0	1 DEL2 C	• •	FIXE	)			
INT	ALPHA	BETA	CN	CLM	CY	CLM_	CLL	ÇA	CAB	CAF	XCP	•	
			-0.7631	1.4355	0.0477	-0.0913	-0.0585	0.4249	0.1114		-1.0012		
_		-0.01	-0.3997	0.7495	0.0355	-0.086R	-0.0542	0.4176	0.1090		-1.8751 -1.9013	· · · · · · · · · · · · · · · · · · ·	
<u>.</u>	-0.11	-0.01	-0.0485	0-0617	0.0422	-0.0829	-0.0547	0-4154	0.1044	0.3070_	-1.6854		
5		-0.01		-0.2618	0.0358	-0.0757	-0.0574	0.4166	0.1085		-1.9198	•	
		-0.01 -0.01		-0.5933	0-0631	-0.0849	-0.0557	0.4161	0.1089 0.1113		-1.91 <u>57</u> -1.9073		
B	6.09	-0.01	1.0730	-2.0029		-0-1074		0.4327	0.1172		-1.8667	9	
9		-0.01		-2.7863			-0.0549	0.4409	0.1238	0.3171	-1.8136		
<u> </u>		-0.01 -0.01		-3.64 <u>67</u> -4.4546	0.0413	-0.1049	-0.0535	0.4435	0.1242_ 0.1238	_0.3535	-1 <u>.7486</u> -1.6798	<u>-</u>	
2	14.50	0.0		-5.2420	0.0457	-0.1200	-0.0607	0.4501	0.1255		-1.6273		
3	16.61	0.0		-6.0641	0.0470	-0.1344	-0.0632	0.4522	0.1200		-1.5921		
5	20.85	0.0		-6.9649	0.0466	-0-1343	-0.0687	0.4560	0.1164		-1.5599 -1.5586		
6		0.0		0.0916			-0.0521	0.4129	0-1085		-2-1693		
								<del></del>		<del></del>	<del></del>	<del></del>	
			·-··		···- ···					<del></del>			
			<del></del>										
						<del></del>						•	
						<del></del>					<del></del>		
_													
									· · · · · · · · · · · · · · · · · · ·				
											-		
										<del></del>			
		<del> </del>			<del></del>								
					· · · · · · · · · · · · · · · · · · ·						· · · · · · · · · · · · · · · · · · ·		

	1 OF			LANGLEY R	ESEARCH C	ENTER (NAS	A) ISSILE TA	UNIT IL EFFEÇT	ARY PLAN I S Data	IND TUNN	EL (UPST)	
:61		•										
			•						,			
	TES	T PART P	ACH RXIO-	6 PHI	CONF	L DEL	1 DELZ	DEL3 DEL	4 TRANSIT	ON		
	•	5 2	86 3.0	O.O B	2+0F34 (	0.0	00	. 0	O FIXE	)		
DINT	ALPHA	BETA	CN	CLM	CY	CLM	CLL	CA -	CAB	CAF	XCP	
1	-4.24		-0.4060	1.5331	0.0032	-0.0154	-0.0599	0.4241	0-1121	0.3120	-1.9022	· · · · · · · · · · · · · · · · · · ·
2	-2.16	0.0	+554.0-	0.8239	0.0035	-0.0152	-0.0577	0.4150	0.1084		-1,9505	
3	-1.13		-0.2302	0.4751	0.0037		-0.0577	0.4129	0.1073		-2.0637	
-	0.92		-0,0682 0.1217	-0.1573 -0.1865	0.0038	-0.0098		0.4112. 0.4128	0-1073 0-1069		-2.3069 -1.5322	
i	1.96		0.2459	-0.5267	-0.0016			0.4126	0.1074	0.3052	-1.7801	
7	4.01	0.0	0.6612	-1.1993	0.0045	-0.0041	-0.0575	0.4162	0.1093	0.3069	-1.8139	·····
	6.09			-1.9289	-0.0010	0.0128		0.4250	0.1169	0.3081	-1.4083	
. <b>9</b> :	10.29		1.5298	-2.7190 -3.5906	0.0047		-0.0581 -0.0583	0.4320	0.1227	0.3093	-1.7773 -1.7230	
10 11	12.41			-4.3932		-0.0094		0.4369	-0.1541		-1.6537	
iż	14.51			-5-1672	0.0150			0.4398	0.1218		-1.6075	
13	16.65	0.0	3.8278	-6.0197	0.0201	-0.0208	-0.0611	0.4423	0.1189	0.3234	-1.5726	
14	18.76	0.0	4.4255	-6.8813	0.0251	-0.0461	-0.0616	0.4455	0.1156	0.3299	-1,5549	
15) 16	20.86		5.0526	-7.8370 0.1539	0.0304			0.4485	0.1145		-1.5511 -2.7259	
10	-0.01	<u> </u>	-010358	U11337	0.0076	-010160	-000333	4.4122	0.1070	0.3035	-604634	<del></del>
			•									
											_	
								<del></del>				
		-										
									<del></del>			
							-				_	
								· · · · · · · · · · · · · · · · · · ·		<del></del>		•
						- <u>-</u>		- <u></u> -				
_												
			<del></del>									•
								•				
						-						
							=					

E 1 OF 1  EY 1 OF 1  TEST PART HACH PX10-6 PH1 CONF L OEL1 DEL2 DEL3 DEL4 TRANSITION 4 6 3.95 3.0 -90.8 82m0734 0.0 0 0 0 8 FIXED  INT ALPMA BETA CN CLM CY CLM CLL CA CAB CAF RCP 1 -6.13 0.0 -0.6141 0.9213 0.0055 -0.0579 -0.0351 0.3356 0.0753 0.2603 -1.500 2 -2.00 0.0 -0.3149 0.5030 0.0119 -0.0477 -0.0325 0.3337 0.0753 0.2566 -1.579 3 -1.07 0.0 -0.1731 0.2902 0.0052 -0.0007 -0.0325 0.3337 0.0753 0.2566 -1.570 5 0.077 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
A 6 3.95 3.0
A
1
1 -4.13
3 -1.07 0.0 -0.1731 0.2982 0.0052 -0.0407 -0.0325 0.3337 0.0753 0.2584 -1.72 4 -0.04 0.0 -0.0314 0.1006 -0.0019 -0.0334 -0.0368 0.3349 0.0753 0.2596 -3.20 5 0.97 0.0 0.1150 -0.1015 0.0154 -0.0512 -0.0348 0.3350 0.0753 0.2597 -0.88 6 2.00 0.0 0.2535 -0.2955 0.0128 -0.0486 -0.0300 0.3368 0.0753 0.2597 -0.88 7 4.06 0.0 0.5617 -0.7089 0.0062 -0.0486 -0.0300 0.3368 0.0753 0.2615 -1.166 8 6.12 0.0 0.9087 -1.1984 0.0785 -0.0649 -0.0413 0.3461 0.0753 0.2650 -1.266 9 9.18 0.0 1.3180 -1.7670 0.0205 -0.0568 -0.0447 0.3566 0.0759 0.2807 -1.34 10 10.25 0.0 1.7425 -2.3005 0.0125 -0.0660 -0.0475 0.3645 0.0767 0.2878 -1.32 11 12.34 0.0 2.2004 -2.8802 0.0108 -0.0648 -0.0506 0.3754 0.0767 0.2878 -1.32 12 14.41 0.0 2.6655 -3.5181 0.0276 -0.0942 -0.0575 0.3891 0.0761 0.3130 -1.31 13 16.48 0.0 3.1765 -4.2601 0.0276 -0.0942 -0.0575 0.3891 0.0761 0.3130 -1.31 14 18.56 0.0 3.7353 -5.1286 0.0327 -0.0942 -0.0669 0.4343 0.0694 0.3288 -1.34 15 20.64 0.0 4.3678 -6.1714 0.0236 -0.1107 -0.0689 0.4343 0.0694 0.3649 -1.41 16 -0.04 0.0 -0.0392 0.1015 0.0181 -0.0706 -0.0336 0.3346 0.0731 0.2615 -2.58
6         -0.04         0.0         -0.0314         0.1000         -0.0019         -0.0334         -0.0368         0.3349         0.0753         0.2596         -3.20           5         0.97         0.0         0.1150         -0.1015         0.0154         -0.0512         -0.0348         0.3350         0.0753         0.2597         -0.86           6         2.08         0.0         0.2535         -0.2955         0.0128         -0.0486         -0.0360         0.3368         0.0753         0.2615         -1.16           7         4.06         0.0         0.5617         -0.7089         0.0062         -0.0486         -0.0360         0.3368         0.0753         0.2615         -1.16           8         6.12         0.0         0.9087         -1.1984         0.0762         -0.0420         -0.0430         0.3461         0.0753         0.2708         -1.31           9         3.18         0.0         1.3180         -1.7670         0.0205         -0.0568         -0.0447         0.3566         0.0759         0.2807         -1.34           10         10.25         0.0         1.7425         -2.3005         0.0125         -0.0660         -0.0475         0.3645         0.0767
5
6         2.08         0.0         0.2535         -0.2955         0.0128         -0.0486         -0.0360         0.3368         0.0753         0.2615         -1.16           7         4.06         0.0         0.5617         -0.7689         0.0062         -0.0420         -0.0384         0.3403         0.0753         0.2650         -1.26           8         6.12         0.0         0.9087         -1.1984         0.0785         -0.0649         -0.0413         0.3461         0.0753         0.2708         -1.31           9         8.18         0.0         1.3180         -1.7670         0.0205         -0.0508         -0.0447         0.3566         0.0759         0.2807         -1.34           10         10.25         0.0         1.7425         -2.3005         0.0125         -0.0640         -0.0475         0.3645         0.0767         0.2807         -1.32           11         12.34         0.0         2.2004         -2.8802         0.0108         -0.0648         -0.0506         0.3754         0.0767         0.2987         -1.32           12         14.41         0.0         2.6655         -3.5181         0.0276         -0.0992         -0.0575         0.3891         0.0761
8       6.12       0.0       0.9087       -1.1984       0.0785       -0.0649       -0.0413       0.3461       0.0753       0.2708       -1.31         9       8.18       0.0       1.3180       -1.7670       0.0205       -0.0508       -0.0447       0.3566       0.0759       0.2807       -1.34         10       10.25       0.0       1.7425       -2.3005       0.0125       -0.0660       -0.0475       0.3645       0.0767       0.2878       -1.32         11       12.34       0.0       2.2004       -2.8802       0.0108       -0.0648       -0.0506       0.3754       0.0767       0.2878       -1.30         12       14.41       0.0       2.6655       -3.5181       0.0276       -0.092       -0.0575       0.3891       0.0761       0.3130       -1.31         13       16.48       0.0       3.1765       -4.2601       0.0227       -0.0942       -0.0575       0.3891       0.0742       0.3288       -1.34         14       18.56       0.0       3.7353       -5.1286       0.0325       -0.1226       -0.0647       0.4164       0.0725       0.3439       -1.37         15       20.64       0.0       4.3678       -
9
10 10.25 0.0 1.7425 -2.3005 0.0125 -0.0660 -0.0475 0.3645 0.0767 0.2878 -1.32 11 12.34 0.0 2.2004 -2.8802 0.0108 -0.0648 -0.0506 0.3754 0.0767 0.2987 -1.30 12 14.41 0.0 2.6655 -3.5181 0.0276 -0.0992 -0.0575 0.3891 0.0761 0.3130 -1.31 13 16.48 0.0 3.1765 -4.2601 0.0227 -0.0942 -0.0621 0.4030 0.0742 0.3288 -1.34 14 18.56 0.0 3.7353 -5.1286 0.0327 -0.1226 -0.0647 0.4164 0.0725 0.3438 -1.34 15 20.64 0.0 4.3678 -6.1714 0.0236 -0.1107 -0.0649 0.4343 0.0694 0.3649 -1.41 16 -0.04 0.0 -0.0392 0.1015 0.0181 -0.0706 -0.0336 0.3346 0.0731 0.2615 -2.58
$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
14 18.56 0.0 3.7353 -5.1286 0.0345 -0.1226 -0.0647 0.4164 0.0725 0.3439 -1.37 15 20.64 0.0 4.3678 -6.1714 0.0236 -0.1107 -0.0689 0.4343 0.0694 0.3649 -1.41 16 -0.04 0.0 -0.0392 0.1015 0.0181 -0.0706 -0.0336 0.3346 0.0731 0.2615 -2.58
15
16 -0.04 0.0 -0.0392 0.1015 0.0181 -0.0706 -0.0336 0.3346 0.0731 0.2615 -2.58
<del></del>

_				LANGLEY R	ESEARCH C	ENTERINAS	A)	UNITA	RY PLAN H	IND TUNN	EL (UPUT)		
EY	1 OF 1				***************************************	MAKILM	ISȘILE TA	IL EPPECTS	VATA				
		·-·		-									<del></del>
	6728	0.00 4		4 5						-	· <u>-</u>		
	4		'ACH RX10-		CONF 1240F34 0	L DEL	DELS	DEL3 DEL4	FIZE	OH			
INT	ALPHA	BETA	CN				C. I		CAB	CAF	T-00		
12	-4.15	0.0	-0.6576	CLM 0.9720	CY 	0.0009	-0.0385	CA 0.3353	0.0734	0.2619	-1.4781	<del></del>	
5	-2.08	0.0	-0.3352	0.5403	-0.0011	0.0080	-0.0350	0.3309	0.0739	0.2570	-1.6119		
3	-1.06	0.0	-0.1946	0.3289	-0.0015	0.0051	-0.0350	0.3315	0.0739	0.2576	-1.6900		
<u>*</u>	-0.04 0.97	0.0	-0.0534	0.1335 0.0556	0.0013 -0.0015	2800.0	0.035 <u>1</u> -0.0357	0.3344	0.0739	0.2605	-2,5007 -0.6534		
6	2.00	0.0	0.7438	-0.2653	-0.0015	0.0084		0.3352	0.0739	0.2613	-1.0860		
Ť	-4.04	0.0	0.5408	-0.6639	-0.0021			0.3409	0.0739		-1.2277		•
8	6.11	0.0	0.8921	-1.1390	-0.0023	0.0157		0.3441	0.0739		-1.2767		
9	8.17	0.0	1.3013	-1.7105	-0.0028		-0.0418	0.3510	0.0745	0.2765	-1.3145		
0	10.23 12.31	0.0		-2.232 <u>1</u> -2.6307	0 <u>.0043</u> 0.0035		-0.0484	0.3594 0.3719	0.0763_ 0.0763	0.2831	-1.3042 -1.29 <b>8</b> 4	<del></del>	
2	14.39	0.0		-3.4622	0.0105		-0.0553	0.3847	0.0763		-1.3075		
3	16,48	0.0	3.1500	-4.1751	0.0100		-0.0555	0.3977	0.0753	0.3224	-1.3254		
4	18.55	0.0	3.7213	-5.0734	0.0173		-0.0569	0.4097	0.0748	0,3349	-1,3634		
5	20.64	0.0	4.3342		0.0094	-0.0271		0.4252	0.0732	0.3520	-1.4035		
6	-0.05	0.0	-0.0734	0.1540	-0.0013	0.0010	-0.035Z	0.3321	0.0734	0,2587	-2.8986	<del></del>	
													-
			<del></del>										
								•					
													•
			<u> </u>						·				
				<del></del>		<del></del>		<del></del>	<del></del>				<del></del>
			-										
		•			· <del></del>						· • · · · · · · · · · · · · · · · · · ·	<del></del>	
							·						
			•									<del></del>	

2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 16 - 16 - 16 - 16 - 16 - 16	TEST PAI 4 ALPMA B -3.79 0 -1.73 0 -0.70 0 0.30 0 1.32 0 4.38 0 6.43 0 8.46 0 10.52 0 10.55 0 14.63 0 16.68 0 18.74 0 20.81 0	FTA	CN -0.5766 -0.7897 -0.1970 -0.0256 0.2566 0.5378 0.9634 1.2090 1.6049 2.0256 2.46632 2.9546 3.5116	0.0 8 CLM 0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.8567 -1.8668 -2.3857 -3.0331 -3.8281	CY -0.0198 -0.0202 -0.0205 -0.0208 -0.0215 -0.0215 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	CLN 0.0124 0.0123 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 -0.0063	CLL -0.0326 -0.0286 -0.0286 -0.0286 -0.0286 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	CA 0.3097 0.3089 0.3086 0.3086 0.3112 0.312 0.3142 0.3238 0.3337 0.3459 0.3586		CAF 0.2513 0.2505 0.2505 0.2502 0.2482 0.2510 0.2502 0.2534 0.2534 0.2729 0.2861	-1.5033 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507		
DINT 4  2	TEST PAGE 4 ALPMA BG -3.79	FTA	CN -0.5766 -0.7897 -0.1970 -0.0256 0.2566 0.5378 0.9634 1.2090 1.6049 2.0256 2.46632 2.9546 3.5116	0.0 8 CLM 0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.8567 -1.8668 -2.3857 -3.0331 -3.8281	CY -0.0198 -0.0202 -0.0205 -0.0208 -0.0215 -0.0215 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	CLM 0.0124 0.0123 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 0.0063	CLL -0.0326 -0.0286 -0.0286 -0.0286 -0.0286 -0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	CA 0.3097 0.3089 0.3086 0.3086 0.3112 0.3112 0.3142 0.3238 0.3337 0.3489 0.3586	CAB 0.0584 0.0584 0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608	CAF 0.2513 0.2505 0.2505 0.2502 0.2482 0.2510 0.2502 0.2534 0.2534 0.2729 0.2861	-1.0888 -1.0750 -1.1164 -1.5833 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
1	ALPMA B -3,79 0 -1,73 0 -0,70 0 0,30 0 1,32 0 2,34 0 4,38 0 6,43 0 8,46 0 10,52 0 12,56 0 14,63 0 16,68 0 18,74 0 18,74 0	FTA	CN -0.5766 -0.7897 -0.1970 -0.0256 0.2566 0.5378 0.9634 1.2090 1.6049 2.0256 2.46632 2.9546 3.5116	0.0 8 CLM 0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.8567 -1.8668 -2.3857 -3.0331 -3.8281	CY -0.0198 -0.0202 -0.0205 -0.0208 -0.0215 -0.0215 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	CLM 0.0124 0.0123 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 0.0063	CLL -0.0326 -0.0286 -0.0286 -0.0286 -0.0286 -0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	CA 0.3097 0.3089 0.3086 0.3086 0.3112 0.3112 0.3142 0.3238 0.3337 0.3489 0.3586	CAB 0.0584 0.0584 0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608	CAF 0.2513 0.2505 0.2505 0.2502 0.2482 0.2510 0.2502 0.2534 0.2534 0.2729 0.2861	-1.0888 -1.0750 -1.1164 -1.5833 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 16 - 16 - 16 - 16 - 16 - 16	ALPMA B -3,79 0 -1,73 0 -0,70 0 0,30 0 1,32 0 2,34 0 4,38 0 6,43 0 8,46 0 10,52 0 12,56 0 14,63 0 16,68 0 18,74 0 18,74 0	FTA	CN -0.5766 -0.7897 -0.1970 -0.0256 0.2566 0.5378 0.9634 1.2090 1.6049 2.0256 2.46632 2.9546 3.5116	0.0 8 CLM 0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.8567 -1.8668 -2.3857 -3.0331 -3.8281	CY -0.0198 -0.0202 -0.0205 -0.0208 -0.0215 -0.0215 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	CLM 0.0124 0.0123 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 0.0063	CLL -0.0326 -0.0286 -0.0286 -0.0286 -0.0286 -0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	CA 0.3097 0.3089 0.3086 0.3086 0.3112 0.3112 0.3142 0.3238 0.3337 0.3489 0.3586	CAB 0.0584 0.0584 0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608	CAF 0.2513 0.2505 0.2505 0.2502 0.2482 0.2510 0.2502 0.2534 0.2534 0.2729 0.2861	-1.0888 -1.0750 -1.1164 -1.5833 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
1 2 3 4 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	ALPMA 64 -3.79 0 -1.73 0 -0.70 0 0.30 0 1.32 0 2.34 0 4.38 0 6.43 0 6.43 0 10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	FTA	CN -0.5766 -0.2847 -0.0254 -0.1028 -0.7566 -0.5378 -0.8634 -1.2090 -1.6049 -2.0256 -2.4642 -2.9546 -3.5116	CLM 0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.3547 -1.8468 -2.3857 -3.0331 -3.8281	CY	CLN 0.0124 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 -0.0063 -0.0152	CLL -0.0326 -0.0286 -0.0286 -0.0286 -0.0304 -0.0321 -0.0412 -0.0415 -0.0458	CA 0.3097 0.3089 0.3086 0.3086 0.3112 0.312 0.3142 0.3238 0.3337 0.3459 0.3586	CAB 0.0584 0.0584 0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608	CAF 0.2513 0.2505 0.2502 0.2502 0.2510 0.2502 0.2502 0.2503 0.2729 0.2861	-1.0888 -1.0750 -1.1164 -1.5833 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
2	-3.79	.0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .	0.5766 8.7897 0.1570 0.0254 0.1028 0.2566 0.56378 0.9634 1.2090 1.6049 2.0256 2.4692 2.9546	0.6274 0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.3547 -1.8468 -2.3857 -3.0331	-0.0198 -0.0202 -0.0205 -0.0208 -0.0211 -0.0215 -0.0222 -0.0134 -0.0141 -0.0149 -0.0152	0.0124 0.0123 0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 -0.0063	-0.0326 -0.0286 -0.0286 -0.0286 -0.0295 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	0.3097 0.3089 0.3085 0.3086 0.3084 0.3112 0.3104 0.3142 0.3238 0.3238 0.3337 0.3489 0.3586	0.0584 0.0584 0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608	0.2513 0.2505 0.2505 0.2502 0.2482 0.2510 0.2502 0.2534 0.2634 0.2729	-1.0888 -1.0750 -1.1164 -1.5833 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
2	-1.73	.0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0	-0.78 by 7 -0.1570 -0.0254 -0.1028 0.2566 0.5378 0.9634 1.2090 1.6049 2.0256 2.4632 2.9546 3.5116	0.3103 0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.3547 -1.8668 -2.3857 -3.0331 -3.8281	-0.0202 -0.0205 -0.0208 -0.0211 -0.0215 -0.0222 -0.0129 -0.0134 -0.0141 -0.0152 -0.0155	0.0123 0.0123 0.0123 0.0125 0.0126 0.0026 0.0026 0.0063 -0.0152	-0.0286 -0.0286 -0.0286 -0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0458 -0.0458	0.3089 0.3085 0.3086 0.3112 0.3112 0.3142 0.3238 0.3337 0.3489 0.3586	0.0584 0.0584 0.0584 0.0602 0.0602 0.0608 0.0608 0.0608	0.2505 0.2501 0.2502 0.2482 0.2510 0.2502 0.2534 0.2630 0.2729 0.2861	-1.0750 -1.1164 -1.5033 -0.8454 -0.9363 -0.9667 -1.0637 -1.1205 -1.1507 -1.1776		
3 6 7 8 9 10 11 12 13 14 15	0.70 0.30 1.32 2.34 6.43 6.43 0.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.55 0.10.5	0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0	0.1570 0.0254 0.1028 0.2566 0.5378 0.5434 1.2090 1.6049 2.0256 2.46632 2.9546	0.1753 0.0402 -0.0869 -0.2403 -0.5199 -0.9356 -1.3547 -1.8468 -2.3857 -3.0331	-0.0205 -0.0208 -0.0211 -0.0215 -0.0222 -0.0129 -0.0134 -0.0141 -0.0149 -0.0152	0.0123 0.0124 0.0125 0.0126 0.0026 0.0026 0.0063 -0.0152	-0.0286 -0.0286 -0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0458 -0.0460	0.3085 0.3086 0.3084 0.3112 0.3104 0.3142 0.3238 0.3238 0.3337 0.3459 0.3586	0.0584 0.0584 0.0602 0.0602 0.0602 0.0608 0.0608 0.0608	0.2501 0.2502 0.2482 0.2510 0.2502 0.2534 0.2630 0.2729	-1.1164 -1.5633 -0.8454 -0.9363 -0.9667 -1.0837 -1.1205 -1.1507 -1.1778		
5 6 7 8 9 10 11 12 13 14 15 16	1.32 0 2.34 0 4.38 0 6.43 0 8.46 0 10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	• 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0	0.1028 0.2566 0.5378 0.3634 1.2090 1.6049 2.0256 2.4632 2.9546	-0.0869 -0.2403 -0.5199 -0.9356 -1.3547 -1.8468 -2.3657 -3.0331	-0.0211 -0.0215 -0.0222 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	0.0124 0.0125 0.0126 0.0026 0.0026 -0.0063 -0.0152	-0.0295 -0.0304 -0.0321 -0.0412 -0.0413 -0.0415 -0.0458	0.3084 0.3112 0.3104 0.3142 0.3238 0.3337 0.3489 0.3586	0.0602 0.0602 0.0608 0.0608 0.0608	0.2482 0.2518 0.2502 0.2534 0.2630 0.2729 0.2861	-0.8454 -0.9363 -0.9467 -1.0837 -1.1205 -1.1507 -1.1778		
6 7 8 9 10 11 12 13 14 15 16	2.34 0 4.38 0 6.43 0 8.46 0 10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0 0.30 0	. 0 . 0 . 0 . 0 . 0 . 0	0.2566 0.5378 0.8634 1.2090 1.6049 2.0256 2.4632 2.9546 3.5116	-0.2403 -0.5199 -0.9356 -1.3547 -1.8468 -2.3857 -3.0331 -3.8281	-0.0215 -0.0228 -0.0129 -0.0134 -0.0141 -0.0152 -0.0054	0.0125 0.0126 0.0026 0.0063 -0.0152	-0.0304 -0.0321 -0.0412 -0.0413 -0.0415 -0.0458	0.3112 0.3104 0.3142 0.3238 0.3337 0.3489 0.3586	0.0602 0.0602 0.0608 0.0608 0.0608	0.2510 0.2502 0.2534 0.2630 0.2729 0.2861	-0.9363 -0.9667 -1.0637 -1.1205 -1.1507 -1.1778		
11 12 13 14 15	4.38 0 6.43 0 8.46 0 10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	• 0 • 0 • 0 • 0 • 0 • 0 • 0	0.5378 0.5634 1.2090 1.6049 2.0256 2.4632 2.9546 3.5116	-0.5199 -0.9356 -1.3547 -1.8468 -2.3857 -3.0331	-0.0222 -0.0129 -0.0134 -0.0141 -0.0149 -0.0152	0.0126 0.0026 0.0026 -0.0063 -0.0152	-0.0321 -0.0412 -0.0413 -0.0415 -0.0458 -0.0460	0.3104 0.3142 0.3238 0.3337 0.3489 0.3586	0.0602 0.0608 0.0608 0.0608	0.2502 0.2534 0.2630 0.2729 0.2861	-0.9467 -1.0837 -1.1205 -1.1507 -1.1776		
11 12 13 14 15	6.43 0 8.46 0 10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	• 0 • 0 • 0 • 0 • 0	0.8634 1.2090 1.6049 2.0256 2.4632 2.9546 3.5116	-0.9356 -1.3547 -1.8468 -2.3657 -3.0331 -3.8281	-0.0129 -0.0134 -0.0141 -0.0149 -0.0152 -0.0054	0.0026 0.0026 -0.0063 -0.0152 -0.0150	-0.0412 -0.0413 -0.0415 -0.0458 -0.0460	0.3142 0.3238 0.3337 0.3489 0.3586	0.0608 0.0608 0.0608 0.0608	0.2534 0.2630 0.2729 0.2861	-1.0837 -1.1205 -1.1507 -1.1776		
11 12 13 14 15	10.52 0 12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	• 0	1.6049 2.0256 2.4632 2.9546 3.5116	-1.8468 -2.3857 -3.0331 -3.8281	-0.0141 -0.0149 -0.0152 -0.0054	-0.0063 -0.0152 -0.0150	-0.0415 -0.0458 -0.0460	0.3337 0.3489 0.3586	0.0608	0.2729	-1.1507 -1.1770		
11 12 13 14 15	12.56 0 14.63 0 16.68 0 18.74 0 20.81 0	• 0	2.0256 2.4682 2.9546 3.5116	-2.3657 -3.0331 -3.8281	-0.0149 -0.0152 -0.0054	-0.0152 -0.0150	-0.0458	0.3489 0.3586	0.0608	0.2861	-1.1776	<del></del>	-
12 13 14 15 16	14.63 0 16.68 0 18.74 0 20.81 0	• 0 • 0 • 0	2.4642 2.9546 3.5116	-3.0331 -3.8281	-0.0152	0.0150	-0.0460	0.3586					
13 14 15 16	18.74 0 20.81 0 0.30 0	-0	2.9546 3.5116	-3.8281	-0.0054								
15 16	20.81 0 0.30 0	.0		-4 8005				0.3727	0.0602	0.3125	-1.2956		
16	0.30 0					-0.0339		0.3818	0.0596		-1.3670		
		_0 •	4.1160 -0.02>4	-5.9077 0.0402		-0.0428 0.0123	-0.0467 -0.0286	0.3977	0.0582	0.3395 0.2498	-1.4353 -1.5833		:
	0.29		-0.0250		-0.0307		-0.0206	0.3084	0.0588		-1.5749		
						10000	H W	A.V.V.Z.	3232	124			
								<del></del>					
			<del></del>										
											•		
			•								<del></del>	<del></del>	
								•	•				
									*		<del></del>		
													•
					<del></del>								

ε :	1 OF 1			LANGLEY RI	ESEARCH C	ENTERINAS Martin M	A) ISSILE TA	UNITA IL EFFECTS	RY PLAN S	IND TUNN	EL (UPWT)	
ET	1 OF 1											
					•		<del></del>					
	TEST	PART	ACH RX10-	6 PHI	CONF	L OEL	1 DEL2	DEL3 DEL4				
			.6 <u>3 3.0 </u>	<u>-90.0 8</u>	5å0t 3 <u>4                                    </u>	.0	0 0	0 0	FIXE	)	<del></del>	
INT	ALPHA	BETA	CN	CLM	CY_	CLN	ÇLĻ	CA	CAB	CAF	xcp	
1			-0.5278		0.0725	-0.0955	-0.0306				-1.1196	
<del>2</del> —		-0.01 -0.01	-0.2544	0.2802		-0.0674		0.3093	0.0620		-1.1013 -1.1712	<del></del>
٠.		-0.01	0.0091	0.0163	0.0486	-0.0506	-0.0287	0.3108	0.0620	0.2488	1,7952 -0.7798	
5		-0.01	0.1368	-0-1067		-0.0766		0.3100	0.0620			
<del>-</del> }		-0.01 -0.01		-0.5626 -0.5626		-0.0758		0.3097 0.3113	- 0.0650 - - 0.0650 -		-0.9081 -1.0062	
è	-	-0.01	5564.0	-0.9813		-0.0876		0.3156	0.0620	0.2536	-1.0999	
9		-0.01		-1.4333		-0.0808		0.3267	0.0626		-1.1401	
1		-0.01 -0.01		-1.8933 -2.4397		-0.1005		<u>0.</u> 3371 0.3521	_ 0.0626 _ 0.0626		-1.1614 -1.1927	
2		-0.01		-3.0809		-0.1313		0.3635	0.0626		-1.2374	
3	16.70	-0.01	3.0024	-3.9109	0.0824	-0.1310	-0.0545	0.3752	0.0612	0.3140	-1.3026	
5		-0.01		-4.8807 -5.9947		-0.1280	-0.0578 -0.0582	0.4069	0.0599		-1.3773 -1.4467	
15 16		-0.01		0.0268		-0.0977		0.3074	0.0599		-26.8400	
				<del> –</del>					·			
·					<del></del>			<del></del>	<del></del>			
										<u>-</u>		
								*				
											<del></del>	
											•	
								<del></del>				

				ANGLEY RI	ESEARCH C	ENTER (NAS	<b>A</b> )	UNITA	RY PLAN I	INO TUNN	EL (UPWT)			
ET	1 OF 1					MARTIN M	ISSILE TAI	L EFFECTS	DATA	~- <del></del>				
		PAPT 1	ACH RALO-	6 PHI	CONF	L DEL	1 DELS C	EL3 DEL4	TRANSITI		· · · ·			
	ALPHA	BETA	63 3.0 CN	0.0 B	2#0F35 0 CY		6 0	CA C	CAB	CAF	ACP			
1	-3.76	0.0		0.7050			-0.0326			0.2355		·····		
2	-1.72	0.0	-0.2107	0.3165	0.0045	-0.0095	-0.0326	0.2816	0.0537	0.2279	-1.5023			
3	-0.71	0.0	-0.0780	0.1589	0.0090		-0.0327	0.2808	0.0537	0.2271	-2.0374			
5	1.32	0.0	0.0542	0.0017_ -0.1918	0.0089	-0.0095 -0.0093	-0.0328	0.2801 0.2807	0.0537	0.2264	-0-9540			
6	2.35	0.0		-0.3645	0.0084	-0.0093		0.2837	0.0537	0.2300	-1.0460			
7	4.39	0.0		-0.7301		0.0011	-0.0328	0.2876	0.0537	0.2339	-1.1372			
8	8.49	0.0		-1.1227 -1.4998		-0.0091		0.2965	0.0537	0.2478	-1.1670			
	10.53	0.0		-1.9231	0.0058		-0.0371	0.3044	0.0561	0.2570	-1.1444			
1	12.58	0.0		-2.3648		-0.0360		0.3258	0.0547		-1.1302			
2	14.64	0.0		-2.9362		-0.0449		0.3366	0.0549_		-1.1759_			
3	16.71	0.0		-3.6343		-0.0643		0.3487 0.3601	0.0541		-1.2148		•	
15	20.82	0.0		-5.3888		-0.0732		0.3779	0.0535		-1.3665	<del></del>	<del> </del>	
16	0.30	0.0				0.0023		0.2778	0.0535		-0.4848			
17	0.29	0.0	0.0268	-0.0130	-0.0112	0.0023	-0.0366	0.2779	0.0541	0.2236	-0.4840			
		<del></del>		- <del></del>	<del></del>	<del></del>			·	<del></del>			<del></del>	
												·		
					<del></del>	<del></del>		<del></del>				<del> </del>		
								<del></del>						
_														
									-		7,			
												. <u> </u>		
													•	
		~												
				<del></del>				<u> </u>	<del></del>					
	<del></del>													
		·						-		•				
								<del></del>						

LANGLEY RESEARCH CENTER (NASA) UNITARY PLAN WIND TUNNEL (UPWT)

MARTIN MISSILE TAIL EFFECTS DATA

DELI DELZ DELS DELA THANSITION

O O FIXED

PAGE 1 OF 1

SHEET 1 OF 1

TEST PART MACH RX10-6 PHI CONF L

11 2.60 3.0 0.0 82m0F35 0.0 8

	- AF +			LANGLEY R	ESEARCH C	ENTERINAS	A)	UNITA	RY PLAN .	IND TUNN	EL (UPHT)
ET	l OF r					HARILIN H	1221FE IN	IL EFFECTS	DATA		
	TEST		ACH RX10-			L DEL	1 DEFS	DEL3 DEL4			
		12 20	36 3.0	U.U B	200733 0		.0	<u> </u>	FIRE	<u>'</u>	
INT	ALPHA	BETA	CN	CL*	CA	CLN	CLL	<u>C</u> A	CAB	_ CAF	ICP_
1	-4.06	0.0	-0.8941		-0.0193	0.0315	-0.0608	0.4310	0.1275		-2.2751
-	-2.00 -0.97	0.0	-0.4677		-0.0185 -0.0079	0.0164	-0.0587 -0.0611	0.4272	0.1248	0.3024	-2.5721
	0.05	0.0	-0.0431		-0.0075		-0.0614	0.4305	0.1251	0.3054	-4.4855
	1.08	0.0		-0.2436			-0.0592	0.4285	0.1245	0.3040	-1-6967
	2.12	0.0		-0-7078		0.0377		0.4280	0.1246	_0,3034	-1.9820
Ţ	4.18	0.0		-1.6271		0.0425	-0.0551	0.4295	0.1274	0.3021	-2.0717
2	6.25	0.0	1.6722	-7.500Z -3.3155	-0.0102	0.0230	-0.0510	0.4415	0.1394	0.3021	-2.0596 -1.9827
Ö	10.46	0.0	2.2008		-0.0206	0.0390	-0.0448	0.4574	0.1536	0.3038	-1.0506
1	12.59	0.01	2.7741	-4.7962			-0.0452	0.4554	0.1507	0.3047	
2	14.76	0.01		-5.5398	-0.0177		0.0435	0.4478	0.1456		-1.6330
3	16.92	0.01		-6.3355		-0.0052		0.4482	0.1489		-1.5724
5	21.25	0.01	5.3780	-6.0216	-0.0045	-0.0250	-0.0397 -0.0356	0.4509	0.1516	0.2993	-1.5257 -1.4916
•	0.05	0.01	-0.0579		-0.0281		-0.0613	0.4298	0.1249		-3.4131
7	0.05	0.01	-0.0578		-0.0281		-0.0612		0.1256		-3.4137
<u> </u>	0.05	0.01	-0.0578	0.1973	-0-0585	0.0381	-0.0613	0.4308	0.1256	0,3052	-3,4137
_											
										-	
					-						
-							<del></del>				
										•	
		•									
		_									<del></del>
_											

	<u> </u>			LANGLEY RI	ESEARCH C	ENTER (HAS	A)	UNITA	RY PLAN	IND TUNN	EL (UPWT)	
	1 OF 1					MARTIN M	ISSILE TA	L EFFECTS	DATA		<del></del>	
									·			
	TEST	PART	ACH PALO-	6 PHI	CONF	L DEL	1 DEL2	DEL3 DEL		TOM .		
	•		95 3.0	0.0 8	240F35 0	.0	00	•	FIXE	0		
	41 544					•						
OTHI	ALPHA	BETA 0.0	-0.6587	CLM	CY	-0.0152	CLL CLL	CA 0.3100	CAB	CAF	XCP -1.6044	
ż	-2.08	0.0	-0.3147	0.5696	0.0140	-0.0151	-0.0415	0.3049	0.0697	0.2352	-1.6099	
3	-1.06	0.0	-0.1534	0.3201		-0.0150	-0.0415	0.3028	0.0691	0.2337	-2.0869	
. 4	-0.04	0.0	0.0078	0.0708		-0.0150		_0.3030	_0.0691_	0.2339	9.0754	
5	0.97	0.01			-0.0641	0.0660		0.3068	0.0697		-1.1808	
_6	2.01	0.0		-0.4102		0.0004	-0.0416_	0.3095	0.0697		-1.3106	
7	4.05	0.0		-0.8963		-0.0077		0.3162	0.0697		-1.4017	
-	6.11 8.17	0.0	1.3551	-1.8162	0.0129	-0.0077 -0.0075	-0.0387	0.3237	0.0697		-1.3707 -1.3393	<del></del>
10	10.25	0.0		-2.2538		-0.0073		_0.3350	0.0729		<u>-1,2753</u>	
ii	12.32	0.0		-2.7227		-0.0224		0.3427	0.0723	0-2704	-1.2385	
12	14.41	0.0	2.6478	-3.2607	0.0256	-0.0445	-0.0426	0.3535	0.0711	0.2824	-1.2315	
13	16.49	0.0	3.1547	-3.9301	0.0248	-0.0586	-0.0429	0.3658	0.0706	0.2952	-1,2458	
14	18.57	0.0		-4.6548		-0.0879		0.3792	0.0690	0.3102	-1,2646	
15	20.66	0.0		-5.5090	0.0234		-0.0434	0.3933	0.0669		-1.2050	
16	-0.04	0.0	<u>-0.013</u> 2	0.0755	2000.0	-0.0069	-0.0415	0.3032	0.0692	0.2340	-5.7218	
						<del></del>		····			<del></del>	
T.												<del></del>
								•				
			<u> </u>			<u> </u>			·			
												•
			<del></del>							•		
						·						<del></del>
											•	
									·		· — — — — — — — — — — — — — — — — — — —	
						·-						
												<del></del>
					<del></del>					<del></del>		
<del></del>					<del></del>					<del></del>		<del></del>

AGE	1 OF 1			LANGLEY R	ESEARCH C	ENTER (NAS	A)	UNITA IL EFFECTS	RY PLAN H	IND TUNN	EL (UPST)		
EET	1 OF 1			<del>-</del>			1331LL IN	AL EFFECIS	<u> </u>				
			<del></del>		<del></del> .		•					<del></del>	
								AP. B. AS		A			
	1651		ACH RX10-	6 PHI 0.0 B	CONF Sv0F33 a	L DEL	0 0	DEL3 DEL4	FIXE	)			
OTHT.	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP		
i		0.0	0.56#8	0.6299		-0.0222	-0.0160	0.3473	0.0681		-1.4590		
2	-2.08	0.0	-0.2916	0-4443	0.0072	-0.0221	-0.0161	0.3451	0.0682	0.2769	-1.5235		
3	1.06	0.0	-0.1335	0-2316	0.0070	-0.0250	-0.0161	0.3454	0.0676	0.2778	-1.7351		
	-0.05 0.97	0.0	0.1419	0.0439	0.0010	-0.0720 -0.0066	-0.0162	0.3484_ 0.3508	0.0676	0.2808	-2.7462 -1.1859	<del></del>	
3	2.00	0.0	0.2600	-0.3399	-0.0011	-0.0066	-0.0193	0.3531	0.0671	0.2860			
7	4.05	0.0	0.5769	-0.7490	-0.0015	-0.0064	-0.0194	0.3555	0.0682		-1.2903		
8	6.11	0.0	0.9464	-1.2920	-0.0017	0.0009	-0.0226	0.3618	9,0677	0.2941	-1.3651		
	8.16	0.0	1.3522	-1.6693	~0.0021	0.0011	-0.0227	0.3733	0.0688	0.3045	-1.3824		
10	10.24	0.0	2.2458	-2.4186 -3.0573	-0.0023 0.0004	0.000 <u>9</u> -0.0095	-0.0261 -0.0263	0.3819	0.0696_	_0.3123	<u>-1,3506</u>	<del></del>	
11	12.32	0.0	2.7113	-3.7292	0.0108		-0.0329	0.3967 0.4101	0.0696 0.0694	0.3271	-1.3614 -1.3754		
13	16.47	0.0	3.2489	-4.5309	0.0091			0.4263	0.0677		-1,3944		
14	18.55	0.0	3.8195	-5.5020	0.0062	-0.0300	-0.0301	0.4398	0.0467		-1,4407		
15	20.63	0.0	4.4475	-6.6003	-0.0044	-0.0146	-0.0303	0-4569	0.0657	0.3912	-1.4840		
16	-0.05	0.0	-0.0364 -0.0371	0.0488	-0.00A7		-0.0193	0.3455	_0.0672	0,2783	-1.7790	<del></del>	
4.	-0.06	0.0	-4.6211	0.0400	-0.0086	-0.0057	-0.0193	0.3482	0.0671	0.2011	-1.3149		
					<del></del>						<del></del>		
											- · · · · · · · · · · · · · · · · · · ·	<u> </u>	
						•					_		
					<del></del>				<del></del>		<del></del>	<del></del>	
				-									
											<del></del>		
									•				
				<del></del>			<del></del>	·				<del></del>	
							•						
									-				
										<del></del>	<del></del>		
				<del></del>							<del></del>		
ne													

E	1 OF 1			LANGLEY R	ESEARCH C	ENTER(NAS MARTIN M	A) ISSILE TA	UNITA	RY PLAN I	IND TUNN	EL (UPMT)	
ET	1 07 1											
	4		ACH RX10- 63 3.0	P PMI	CONF 2w0F33 0	L DEL	0 0	DEL3 DEL4	FIXE			
												· · · · · · · · · · · · · · · · · · ·
INT	ALPHA	BETA	<u> </u>	CLM	CY	-0.0062	CLL	CA	CAB	_CAF	XCP	<del></del>
1	-3.78 -1.72	0.0	-0.5371 -0.2571		-0.0200	-0-0062	-0.0205	0.3272	0.0535	0.2737	-1.0119 -0.9132	•
3	-0.71	0.0	-0.1244	0.1036	-0.0203	-0.0062	-0.0206	0.3262	0.0535		-0.8020	
<u> </u>	1.33	0.0_	0.1259	-0.1582	-0.0208	-0.0062	0.0207	_ 0.3282	0.0535		-1.2568	•
5	2.32 4.38	0.0	0.2535	1682-0-	-0.0211	-0-0062	-0-0207	0.3281	0.0535	0.2746	-1.1406 -1.1162	
<del></del>	6,42	0.0	0.8453	-1.0366	-0.0221	-0.0060 -0.0059	-0-0208	0.3360	0.0535		-1.1749	
8	8.47	0.01	1.2513	-1.5134	-0.0328	0.0047	-0.0291	0.3462	0.0535	0,2927	-1-2094	
9	10.52	0.01	1.6462	-2.0168	-0.0230		-0.0293	0.3596	0.0543		-1.2252	
10	12.56	0.0 <u>1</u>	2.0365	-2.5820 -3.2872	-0.0193	-0.0190	-0.0295	0.3752_ 0.3877	0.054 <u>3</u> 0.0543		-1.266 <u>0</u>	
įż	16.67	0.01	3.0114	-4.1688	-0-0163	-0.0233	-0.0256	0.4030	0.0543		-1.3643	
13	18.73	0.01	3.5878	-5.2318	-0.0196	-0.0086	-0.0258	0.4160	0.0528		-1.4502	<del></del>
4	20.80	0.01				-0.0043	-0.0300	0.4332	0.0533		-1.5316	
15	0.29	0.01	-0.0277	-0.0006	-0.0305	-0.0050	-0.0207	0.3258	0.0529	0.2729	0.4214	
											· · · · · · · · · · · · · · · · · · ·	
								<del> </del>				
				•			<del></del>		·			
		•				,						
											· · · · · · · · · · · · · · · · · · ·	
				•								
				•								
											·····	
	···											
				-					<u> </u>			
			<del></del>	<del></del>			<del></del>	<del></del>			<del></del>	<del></del>
						•					•	
						<del></del>						

							'		•			• • • • • • • •	
								•			-	<del>,</del>	<del></del>
		<del></del>	<del></del>	· · · · · · · · · · · · · · · · · · ·		<del></del>					<del></del>		
				LANGLEY R	ESEARCH C	INTER INAS	A)	UNITA	RY PLAN	IND TUNN	EL (UPHT)	· · · · · · · · · · · · · · · · · · ·	
30	1 OF 1					MARTIN M	ISSILE TA	L'EFFECTS	DATA				
ÆET	1 0 1	-		•					•	: •		-	
							<del></del>	<del></del>	•				
	TEST	PART H	ACH RX10-	6 PHI	CONF	L DEL	1 DELZ	DEL3 DEL	TRANSITI	ON			
	•	16 2.	36 3.0	O.O_B	2w0f33_0	. 0	00	0	FIXE		<u></u>		
POINT	ALPHA	BETA	CN	CLH	· CY	CLN	CLL	Ca	CAB	CAF	XCP		
1	-4.05	0.01	-0.8609	1.9334	-0.0290	0.0179	-0.0378	0.4931	0.1277	0.3654	-2.2450		
- {	-1.99 -0.97		-0.4669	0-6214	-0.0179		-0.0363	0.4845	0.1231		-2.2737 -2.3501		
•	0.05		-0.0726	0.2001	-0.0274	0.0183	-0.0359	0.4824		0.3606	-2.7488 .		
5	1.00	0.01		-0.2423	-0.0166	0.0077	-0.0340	1584.0	0.1203	0.3618	-1.8527		
<del></del>	2.09	0.01	0.7217		-0.0216	0.0133_	-0.03831 -0.0404	0.4820			-2.0 <u>546</u> -2.1379	•	<del></del>
8	6.25	0.01		-2.5111			-0.0446	0.5022	0.1240		-2,1435		
9	8.31	0.0	1.6652	-3.5139	-0.0246	0.0441	-0.0446	0.5132	0.1478	0.3654	-2.1102		
10	10.42	0.0		-4-6033			-0.0445	0.5178_	_ 0.1527_		-2.0324		
15	12.55	0.0		-5.6684 -6.6993			-0.0470 -0.0450	0.5168 0.5091	0.1543	0.3625	-1.9378 -1.8685		
-i3	16.85	0.01		-7.6429		0.0463	-0.0453	0.5067	0.1498	0.3569	-1.8234	<del></del>	
14	19.01	0.0	5.0224	-8.9513	-0.0090	0.0082	-0.0414	0.5061	0.1468	.0.3593	-1.7023		<u> </u>
15	21.16	0.0		-1n.1354 0.1967			-0.0305	0.5080	0.1463	0.3617	-1.7546 -3.3688		
16			-0.0365	0.1401	-0.0121	-0.0024	-0.0308	0.0010		0.3341	-3-3000	·	
			<del></del>						<u> </u>				
·				-							•		
				<del></del>			· <del></del>		<del></del>				
										<u> </u>			
				<del></del>									
				-									
					<del></del>		<del> </del>		<del></del>			<del></del>	
												****	
						<del></del>		<del></del>					
				•									
									<del></del>			<del></del>	
			<del></del>						<del></del>				
			-										
			<u></u> -										•

PAGE 1 OF 1 SHEET 1 OF 1

POINT ALPHA BETA CN CLM CY CLM CLL CA CAS CAF ICP  1 -3-80 0,001 -2-8-554 10-0325 -0-0018 -0-1103 -0-0411 1-3460 0.1456 1.2704 -3.7225 2 -1-82 0,001 -2-8-554 0.7554 0.0093 -0-1158 -0-0.0392 1.2562 0.1478 1.1104 -3.9743 3 -0-77 0.01 -2-2-2467 9.3033 0.0147 -0-0.255 -0-0437 1.2151 0.1688 1.0603 -4.1409 4 0.22 0.01 -2-2-554 8.8550 0.0094 -0-1051 -0-0.0415 1.1725 0.1504 1.0221 -4.3112 5 1.25 0.01 -1.6357 8.3713 0.0155 -0-1177 -0-0.0415 1.1725 0.1504 1.0221 -4.3112 6 2.20 0.01 -1.6270 7.6771 0.0006 -0.0403 0.0438 1.0211 0.1510 0.9755 -4.5526 7 4.35 0.01 -1.0230 5.4100 0.0005 -0.0403 0.0438 1.0700 0.1334 0.9255 0.1366 0.3588 -4.8135 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.0014 0.00		FET	PART W	ACH RX10-	6 PHI	CONF	L DEL	1 DELE	DEL3 DE	4 TRANSET	T CHI				<u> </u>
1 -3,89 0.01 -2,6563 10.0325 -0.0018 -0.1103 -0.0411 1.3640 0.1455 1.2004 -3,7225 2 -1.82 0.01 -2,6564 9.7546 0.0093 -0.158 -0.0392 1.2582 0.1478 1.2104 -3,7223 3 -0.77 0.01 -2,2667 9.3033 0.0147 -0.1255 -0.0437 1.2151 0.1408 1.0063 -4.1409 4 0.22 0.01 -2.0548 8.3569 0.0003 -0.1051 -0.0415 1.1725 0.1506 1.0021 -4.3112 5 1.22 0.01 -1.6387 8.3713 0.0105 -0.1197 -0.0418 1.1271 0.1515 0.9756 -4.5526 6 2.22 0.01 -1.6220 7.8791 0.0006 -0.0493 0.0438 1.1271 0.1515 0.9756 -4.5526 7 -4.35 0.01 -1.16393 6.9160 0.0005 -0.0990 -0.0403 0.9936 0.1508 0.9251 -4.8576 7 -4.35 0.01 -0.7108 5.8586 0.0074 -0.0995 -0.0990 0.0403 0.1619 0.7317 -2.2446 9 8.49 0.01 -0.7108 5.8586 0.0074 -0.0995 -0.0047 0.9936 0.1619 0.7317 -2.2445 0.1000 0.0000 0.0000 0.0000 0.0000 0.7949 0.1616 0.0378 -2.317596 10 10 0.00 0.01 0.3979 3.8092 -0.0200 -0.0200 0.0407 0.9939 0.1010 0.0534 0.5534 0.5732 11 12.75 0.01 1.1044 2.6140 0.0005 -0.0000 -0.0047 0.9110 0.1570 0.5554 0.5532 1.3069 12 14.91 0.0 1.1044 2.6140 0.0005 -0.0007 -0.0007 0.0007 0.0007 0.0007 0.1033 0.0007 0.4000 0.1037 0.1373 0.1524 0.4505 2.3069 13 17.00 0.0 2.4557 0.0031 0.0007 -0.0005 -0.0007 0.0047 0.1313 0.132 0.2703 11 12.75 0.01 1.1044 2.6140 0.0005 -0.0007 -0.0007 0.0007 0.1047 0.133 0.134 0.0007 0.4505 0.1047 0.0008 0.0007 0.0007 0.0007 0.1047 0.133 0.134 0.132 0.2703 11 12.75 0.01 1.1044 2.0140 0.0005 -0.0007 0.0007 0.0007 0.1047 0.133 0.134 0.2222 -0.1040 13 17.00 0.0 2.4557 0.0031 0.0007 0.0007 0.0007 0.0007 0.1047 0.133 0.2703 0.134 0.2222 0.1040 13 17.00 0.0 2.4557 0.0031 0.0007 0.0007 0.0007 0.0007 0.1047 0.1037 0.154 0.2222 0.1040 15 0.2222 0.1040 15 0.0007 0.0007 0.0007 0.0007 0.1057 0.154 0.2222 0.1040 15 0.2222 0.1040 15 0.0007 0.0007 0.0007 0.0007 0.1057 0.154 0.2222 0.1040 15 0.2222 0.1040 15 0.0007 0.0007 0.0007 0.0007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.1007 0.	•														
1 -3;89 0.01 -2;6563 10:0325 -0.0018 -0.1103 -0.0411 1:3600 0.1456 1:2004 -3,7225 2 -1,82 0.01 -2;6564 9.7546 0.0093 -0.1158 -0.0392 1:2592 0.1478 1:1104 -3;7473 3 -0.77 0.01 -2;2407 9.3033 0.0147 -0.1255 -0.0437 1:2151 0.1408 1:0663 -4:1409 4 0.22 0.01 -2;0554 8.85569 0.0004 -0.1051 -0.0415 1:172 0.1508 1.0221 -4:3112 5 1:25 0.01 -1,6387 8.3713 0.0105 -0.1197 -0.0418 1:271 0.1515 0.9756 -4:5526 6 2;29 0.01 -1,6220 7:8791 0.0006 -0.0943 1.0709 0.1539 0.9751 -4:8576 7 4.35 0.01 -1:1893 6.9140 0.0006 -0.0943 0.9856 0.1506 0.0228 -5:8135 8.6+1 0.01 -0.7106 5.8586 0.0074 -0.0995 -0.0995 0.0487 0.9856 0.1506 0.0228 -5:8135 0.01 10:00 0.01 0.3979 3.8092 -0.0005 -0.0995 -0.0407 0.9994 0.1616 0.6378 -23.7596 10:00 0.0393 0.0006 -0.0006 -0.0007 0.0007 0.0007 0.0531 0.5317 -23.7596 10:00 0.0393 0.0006 -0.0007 0.0007 0.0007 0.0007 0.0551 0.5318 -23.7596 10:00 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.	INT ALP	PHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	٠.		
3 -0.77 0.01 -2.2047 9.3033 0.0147 -0.1255 -0.0447 1.2151 0.1468 1.0643 -4.1009 4 0.222 -0.01 -2.0544 6.8559 0.0049 -0.0151 1.7725 0.1504 1.0221 -4.3112 5 1.25 0.01 -1.6387 8.3713 0.0105 -0.1197 -0.0418 1.277 0.1515 0.9736 -4.5529 6 2.20 0.01 -1.6220 7.8791 0.0006 -0.0943 -0.0438 1.0271 0.1515 0.9736 -4.5529 7 4.35 0.01 -1.1093 6.9140 0.0005 -0.0943 0.0438 0.1519 0.9251 -4.5529 7 4.35 0.01 -1.1093 6.9140 0.0005 -0.0909 -0.0448 0.0515 0.1568 0.0288 -5.8138 8 6.41 0.01 -0.7116 5.8586 0.0074 -0.0905 -0.0807 0.0838 0.1510 0.7317 -8.2046 9 5.49 0.01 -0.2040 4.6470 0.0029 -0.0832 -0.0846 0.7994 0.1616 0.6378 -23.5798 10 10 10.00 0.01 0.3979 3.8092 -0.0080 -0.0847 0.0447 0.7111 0.1570 0.5551 9.5732 11 12.75 0.01 1.1044 2.6140 0.0085 -0.0687 -0.0848 0.6057 0.1472 0.4585 2.3668 12 14.91 0.0 1.8012 1.5106 0.0085 -0.0633 -0.0842 0.5198 0.1472 0.4585 2.3668 13 17.00 0.0 2.4557 0.6431 0.0075 -0.0535 0.0971 0.4632 0.1497 0.3706 0.8386 13 17.00 0.0 2.4557 0.6431 0.0075 -0.0535 0.0971 0.4632 0.1497 0.1315 0.2793 14 19.23 0.0 3.6589 0.0286 0.0060 -0.0555 0.0971 0.4632 0.1497 0.1315 0.2793 15 21.41 0.0 3.6859 0.0286 0.0060 -0.0555 0.0971 0.4632 0.1497 0.1315 0.2793 16 0.2100 0.2282 -0.1641 0.0062 -0.0555 0.0061 0.0555 0.0971 0.4632 0.1497 0.1315 0.2292 -0.1641 16 0.21 0.0062 -0.0638 0.0068 0.0055 0.0055 0.0055 0.0057 0.0555 0.0871 0.4032 0.1501 0.2222 -0.1641 16 0.21 0.0062 0.0068 0.0068 0.0055 0.0055 0.0057 0.0057 0.1492 0.1492 1.0232 -4.2887 17 0.21 0.01 -2.0645 0.0068 0.0055 0.0055 0.0057 1.1724 0.1492 1.0232 -4.2887 17 0.21 0.01 -2.0645 0.0068 0.0055 0.0055 0.0057 1.1724 0.1492 1.0232 -4.2887 17 0.21 0.001 -2.0645 0.0068 0.0055 0.0055 0.0057 1.1724 0.1492 1.0232 -4.2887 17 0.21 0.001 -2.0645 0.0068 0.0055 0.0055 0.0057 1.1724 0.1492 1.0232 -4.2887 17 0.0057 0.0055 0.0055 0.0055 0.0057 1.1724 0.1492 1.0232 -4.2887 17 0.0057 0.0057 0.0055 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.0057 0.	1 -3.	.89	0.01	-2.8563	10.6325	-0.0018		-0.0411		-0.1456	1.2004				
4 0.22 0.01 -2.0544 8.3569 0.0049 -0.1051 -0.0418 1.1725 0.1504 1.0221 -4.3112 5 1.25 0.01 -1.6327 8.3713 0.0105 -0.1197 -0.0418 1.1271 0.1515 0.09756 -4.5529 6 2.29 0.01 -1.6220 7.8791 0.0006 -0.0033 -0.0438 1.0790 0.1539 0.9251 -4.8576 7 4.35 0.01 -1.1033 6.9140 0.0005 -0.0090 -0.0483 0.9055 0.1568 0.05288 5.8135 8 6.41 0.01 -0.7106 5.8586 0.0074 -0.0995 -0.0487 0.8636 0.1619 0.7317 -822448 9 8.69 0.01 -0.2040 4.8570 0.0025 -0.0032 -0.0466 0.7994 0.1616 0.62737 -8237596 10 10.60 0.01 0.3979 3.8092 -0.0020 -0.0080 -0.0487 0.7111 0.1570 0.5551 0.5573 11 12.75 0.01 1.1044 2.6140 0.0085 -0.0087 -0.0448 0.6057 0.1472 0.4585 2.3669 12 14.91 0.0 1.8012 1.5194 0.0082 -0.0033 -0.0464 0.6577 0.1472 0.4585 2.3669 13 17.06 0.0 2.4657 0.4631 0.0074 -0.0535 -0.0471 0.0535 0.4913 0.1355 0.2793 14 19.23 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4913 0.1528 0.2665 0.0878 15 21.41 0.3 3.6889 -0.6124 0.0164 -0.0535 0.4913 0.1528 0.2665 0.0687 15 21.41 0.0 3.6889 -0.6124 0.0164 -0.0535 0.4913 0.1528 0.2665 0.0687 16 0.21 0.01 -2.0662 8.8568 0.0069 -0.1095 -0.0458 1.1799 0.1487 1.0222 -0.0641 16 0.21 0.01 -2.0662 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1487 1.0222 -0.0661			0.01								1.1104	-3.9743			
5 1.25 0.01 -1.6387 8.3713 0.0105 -0.1197 -0.0018 1.1271 0.1515 0.9756 6. \$5229 6 2.290 0.01 -1.6222 7.8791 0.0006 -0.0003 -0.0048 1.1079 0.1515 0.9755 -4.8576 7 4.35 0.01 -1.1893 8.0100 0.0055 -0.0090 -0.00483 0.9856 0.1508 0.0248 -5.8133 8 6.41 0.01 -0.7106 5.8586 0.0074 -0.0095 -0.00487 0.9856 0.1508 0.0248 -5.8133 9 6 6.41 0.01 -0.2005 -0.00487 0.00487 0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048 -0.0048															
6 2,29 0.01 -1.6220 7.8791 0.0006 -0.0043 -0.0431 1.0790 0.1539 0.9251 -4.8576 7 4.35 0.01 -1.1893 6.9140 0.0005 -0.0990 -0.0483 0.9956 0.1568 0.8288 5.8135 8 6.41 0.01 -0.7106 5.8586 0.0074 -0.0985 -0.0487 0.8936 0.1619 0.7317 -8.2446 9 8.49 0.01 -0.2204 4.8470 0.0029 -0.0024 -0.0794 0.1616 0.8378 -23.7598 10 10.60 0.01 0.3979 3.8092 -0.0020 -0.0600 -0.0465 0.7994 0.1616 0.8378 -23.7598 11 12.75 0.01 1.104 2.6140 0.0005 -0.0067 -0.0480 0.6057 0.1472 0.4583 2.3464 12 14.91 0.0 1.8012 1.5104 0.0005 -0.0067 -0.0480 0.6057 0.1472 0.4583 2.3464 13 17.06 0.0 2.4057 0.8431 0.0074 -0.0335 -0.0492 0.5198 0.1492 0.3706 0.8386 13 17.06 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4193 0.1528 0.2655 0.8087 14 19.23 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4193 0.1528 0.2265 0.8087 15 21.41 0.0 3.5689 -0.012 0.016 -0.0050 -0.0555 0.4193 0.1528 0.222 -0.1661 10 0.21 0.01 -2.0642 8.8568 0.0068 -0.0955 -0.0457 1.1724 0.1492 1.0222 -0.2697 17 0.21 0.01 -2.0648 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0222 -0.2698															
7															
8 6.41 0.01 -0.7106 5.8586 0.0074 -0.0985 -0.0487 0.8936 0.1619 0.7317 -8.2446 9 8.49 0.01 -0.2200 4.6870 0.0029 -0.0832 -0.0486 0.7994 0.1616 0.6378 -23.7596 10 10.60 0.01 0.3979 3.8092 -0.0020 -0.0680 -0.0487 0.7111 0.1570 0.5551 9.5732 11 12.75 0.01 1.1046 2.6140 0.00085 -0.0687 -0.0487 0.7111 0.1570 0.5551 9.5732 12 14.91 0.0 1.8012 1.5106 0.0082 -0.0633 -0.0472 0.5198 0.1492 0.3706 6.3386 13 17.06 0.0 2.4657 0.6831 0.0076 -0.0535 -0.0871 0.4832 0.1497 0.3135 0.2898 14 19.23 0.0 3.0593 0.0286 0.0006 -0.0386 -0.0555 0.1497 0.3135 0.2885 0.8887 15 21.41 0.0 3.6889 -0.6124 0.0166 -0.0630 -0.0601 0.3763 0.1528 0.2865 0.8887 16 0.21 0.01 -2.0646 8.8556 0.0084 0.0165 -0.0635 1.1709 0.1887 1.222 -0.1861 17 0.21 0.01 -2.0646 8.8556 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2898														<del></del>	
9 8,49 0,01 -0,2040 4.0470 0.0029 -0.0082 -0.0466 0.7994 0.1616 0.0578 -23,7596 10 10 10.00 0.01 0.3979 3.8092 -0.0020 -0.0668 00087 0.7111 0.1570 0.5551 9.8732 11 12,75 0.01 1.1046 2.6140 0.0085 -0.0687 -0.0488 0.6057 0.1472 0.4585 2.3669 12 14.91 0.0 1.8012 1.5106 0.0082 -0.0633 -0.0472 0.1518 0.1492 0.3706 0.3386 13 17.06 0.0 2.4557 0.8631 0.0074 -0.0535 -0.0471 0.4632 0.1492 0.3706 0.3385 13 17.06 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4193 0.1528 0.2665 0.8087 15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0630 -0.0555 0.4193 0.3528 0.2665 0.8087 15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0630 -0.0555 0.4193 0.3528 0.2665 0.8087 17 0.222 -0.1661 16 0.21 0.01 -2.0642 8.6568 0.0088 -0.1095 -0.0555 1.1799 0.1487 1.0222 -4.2897 17 0.21 0.01 -2.0646 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2898						_									
10 10.60 0.01 0.3979 3.8092 -0.0020 -0.0607 -0.0467 0.7111 0.1570 0.5561 9.5732 11 12.75 0.01 1.104 2.6140 0.0005 -0.0607 -0.0448 0.6057 0.1472 0.4585 2.3669 12 14.91 0.0 1.8012 1.5100 0.0062 -0.0633 -0.0492 0.5190 0.1492 0.3706 0.8386 13 17.06 0.0 2.4457 0.4631 0.0074 -0.0535 -0.0471 0.4632 0.1997 0.3135 0.2793 14 19.23 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0575 0.4632 0.1997 0.3135 0.2793 15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0630 -0.0601 0.3763 0.1554 0.2222 -0.1661 16 0.21 0.01 -2.0642 8.8560 0.0046 -0.0195 -0.0651 1.1724 0.1492 1.0222 -4.2897 17 0.21 0.01 -2.0646 8.8568 -0.0055 -0.0757 1.1724 0.1492 1.0232 -4.2898															
11 12,75 0,01 1,104 2,6140 0,0085 -0,0687 -0,0688 0,0687 0,1472 0,4585 2,3669 12 14,91 0,0 1,8012 1,5106 0,0082 -0,0633 -0,0492 0,5198 0,1492 0,3736 0,8386 13 17,06 0,0 2,4457 0,6431 0,0074 -0,0535 -0,0471 0,4632 0,1497 0,3135 0,2743 14 19,23 0,0 3,0593 0,0266 0,0000 -0,0366 -0,0555 0,4193 0,1528 0,2665 0,8087 15 21,41 0,0 3,6869 -0,6124 0,0146 -0,0630 -0,0601 0,3763 0,1541 0,2222 -0,1641 16 0,21 0,01 -2,0642 8,8556 0,0048 -0,1095 -0,0458 1,1709 0,1467 1,0222 -4,2007 17 0,21 0,01 -2,0646 8,8568 -0,0055 -0,0989 -0,0457 1,1724 0,1492 1,0232 -4,2898		7	-												
12 14.91 0.0 1.8012 1.5108 0.0062 -0.0633 -0.0492 0.5198 0.1492 0.3706 0.6386 13 17.06 0.0 2.4557 0.6631 0.0076 -0.0535 -0.0471 0.6632 0.1497 0.3135 0.2793 14 19.23 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4193 0.1528 0.2665 0.0087 15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0030 -0.0001 0.3763 0.1541 0.2222 -0.1661 16 0.21 0.01 -2.0642 8.8568 0.0048 -0.1095 -0.0458 1.1709 0.1487 1.0222 -4.2007 17 0.21 0.01 -2.0646 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2098															
14 19.23 0.0 3.0593 0.0266 0.0060 -0.0366 -0.0555 0.4193 0.1528 0.2665 0.0087 15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0630 -0.0601 0.3763 0.1541 0.2222 -0.1661 16 0.21 0.01 -2.0642 8.8568 0.0088 -0.1095 -0.0458 1.1709 0.1487 1.0222 -4.2697 17 0.21 0.01 -2.0646 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2898					1.5106										
15 21.41 0.0 3.6869 -0.6124 0.0146 -0.0030 -0.0001 0.3763 0.1541 0.2222 -0.1461 16 0.21 0.01 -2.0642 8.8568 0.0048 -0.1095 -0.0458 1.1709 0.1487 1.0222 -6.2887 17 0.21 0.01 -2.0646 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2898	3 17	.06	0.0	2.4457	0.6831	0.0074	-0.0535	-0.0471	0.4632	0.1497	0.3135	0.2793			
16 0.21 0.01 -2.0642 8.8558 0.0048 -0.1095 -0.0458 1.1709 0.1487 1.0222 -4.2007 17 0.21 0.01 -2.0645 8.8568 -0.0055 -0.0989 -0.0457 1.1724 0.1492 1.0232 -4.2008			0.0	3.0593	0.0266			-0.0555	0.4193	0.1528		0.0087			
17 0.21 0.01 -2.0646 8.8566 -0.0055 -0.0069 -0.0457 1.1724 6.1492 1.0232 -4.2698															
	7 0.	-21	0.01	-2.0646	8.8568	-0.0055	-0.0989	-0.0457	1.1724	0.1492	1.0535	-4.2898			
						•									
				<del></del>											
												•			
							<del></del>								
												<del></del> -			
				•											
					·										
										•					
					<del></del>			<del></del>	<del></del>			<del></del>			
										•					
								<del></del>						<del> </del>	
							-								
						·		<del></del>						<del></del>	-

LANGLEY RESEARCH CENTER(NASA) UNITARY PLAN WIND TUNNEL (UPWT)
MARTIN MISSILE TAIL EFFECTS DATA

TO ATTEMPT AND A STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE S

GE E	0° 1			ANGLEY	RESEARCH (	ENTER(NAS MARTIN M	ia) Hissile Ta	UNITAL ALL EFFECTS	RY PLAN I	IND TUNN	EL (UPST)	
	TEST		ACH #X10-6		CONF BZ#0F34	L DEL	0 -50	DEL3 DEL4	TRANSIT			
OINT	ALPHA	BETA	CN	CLM	CY	CLN '	CLL	CA	CAB	CAF	KCP	
1	-4.09	-0.0	-2.0078	7.0645	0.0314	-0.1212	-0.0477	0.9518	0.0688	0.6830	-3.5165	
<del>-</del> 5	-2.04	0.0	-1.6326	<u> </u>	0.0321		-0.0446	0.6723	0.0685	0.8043	-3.8601 -4.0765	
•	0.0	0.0	-1.2593	5.5086	0.0250	-0.0983	-0.0447	0.7912	0.0640	0.7232	-4.3743	
5	1.02	0.0	-1.0658	5.1285		-0.0910	-0.0447	0.7511	0.0681	0.6830	-4.8110	
<u> </u>	2 <u>.05</u>	0.0	0. <u>8</u> 725_ -0.4867	3.9561	0.0256	0,0910 -0,0#35	-0.0416	0.7108	0.0684 _ 0.0685	0.6424	-5.4425 -6.1283	· · · · · · · · · · · · · · · · · · ·
Á	6.13	0.0	-0.0459	3.1196		-0.0752		0.5561	0.0695		-67.9659	
9	8.20	0.0	0.3797	2.4982			-0.0418		0.0687	0.4422	6.5794	
10	10.26	0.0	0.7535	2-1485			-0-0420	0.4890	0.0653	0.4237	S*0213	
11	12.35	0.0	1.1322	1.7454		-0.0683 -0.0681	-0.0483 -0.0484	0.4822 0.4755	0.0641	0.4181	1.7033	
3	16.54	0.0	1.8856	1.5310			-0.0549		0.0630	-0.4119 -0.4127	0.6119	
14	18.63	0.0	2.2777	1.303-	0.0191	-0.0748	150		0.0653	0,4091	0,5722	
15	20.74	0.0	2.7503	0.993			-0.0583		0.0661	0.4068	0.3612	
16 17	-0.02	0.0	-1.3001 -1.3195	5.5504 5.5871		-0.0821	-0.0446		0.0694		-4,2692	<del> :</del>
.,	-0.05	0.0	-103173	363011	0.0074	-0.0051	-0.0440	0.7936	9.0609	0.12-1	-405346	
						-						
											•	
												<del>-</del>
												•
		<del></del> .		<del></del>		<del></del>						<del></del>
												•
								<del></del>				
						<del></del>						
								<del></del>				

		<del></del>		ANGLEY R	ESEARCH C			UNITA		IND TUNK	EL (UPHT)	
1	OF 1	•				MARTIN M	ISSILE T	AIL EFFECTS	DATA			· · · · · · · · · · · · · · · · · · ·
						<del></del>			<del></del>			<del></del>
	7557	DADY A	ACH RX10-		CONE	L DEL	· DEL 3	OEL3 DEL4	TD-METT!	I OM	<u> </u>	<del></del>
	4		63 3.0					0 -50				
INT	ALPHA	BETA	CM	CLM	CY	CLN_	CLĻ	CA	CAB	CAF	XCP	
	-3.75	0.01	-1.8331	6.1250	-0.0129	-0.0646	-0.0446	0.8465	0.0528	0.7937	-3.3413	•
	-1.70	0.01	-1.4762		-0.0123 -0.0121	-0.0553	-0.0406		0.0534		-3,6763 -3,9620	<del></del>
	0.31		-1.0939			0.0551_	-0.0408		0.0534		-4.2998	
5	1.32	0.01	-0.9202				-0.0408		0.0541		-4.7591	
	2,34	0.01	-0.7473 -0.3491				-0.0409 -0.0370		_0.0535 0.0546		-5,378 <u>6</u> -9,54 <b>96</b>	
ų.	6,41	0.01	0.0204	2.7222	-0.0114	-0.0544	-0.0412	0.4930	0.0547		133,4404	
) _	8.46	0.01	0.3680			-0.0543			0.0541	0.4170	6.4285	
	10.53	0.01	0.6948			-0.0543	-0.0413 -0.0414		0.0516	0.4115	3.1080 2.0638	<del></del>
2	14.66	0.01	1.3267	1.9177	-0.0164	-0.0631	-0.0456	0.4620	0.0447	0.4173	1.4433	
3	16.70	0.01	1.6768			-0.0733	-0.0458		0.0466	0.4181	1.0238	
<u> </u>	18.76	0.01	-1.1194			-0.0639 -0.0551			0.0503	0.4168	-4.2252	
							,					
	<del></del>										<del></del>	<del> </del>
				<u> </u>							•	<del></del>
				<del></del>								
												•
										<del></del>		
	<del> </del>											
			···								·	
						<del></del>			<del></del>		<del></del>	<del></del>

<del></del>					<del></del>						<del></del>		
y E	165			ANGLEY RE	SEARCH C	ENTERINAS	A)	UNITA	RY PLAN .	IND TUNN	EL (UPST)	····	
39	1 OF 1	<del></del> .				MARTIN M	ISSILE TA	IL EFFECTS	DATA				
EET :	1 00 1									· 			
	TEST	PART =	ACH RX10-	b PHI	CONF	L DEL	1 DELE	DEL3 DEL4	TRANSIT	ON			
	4		36 3.0	O.O_B2	WOF35 0	. 0	0 -20	0 -50			<u> </u>		
OINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF_	XCP		
1	-3.97		-5.6195	9.2953		-0-1014		1.1887	0.1493		-3.5489		
2	-1.87		-2.2311	8-5578		-0.0953		1-1093	0.1498		-3.4357		
3	0.16		-2.0503 -1.8587	6.1890 . 7.7915	0.0071	-0.0900	-0.0459 -0.0459	1.0720	0.1518		-3.9941 -4.1919		
	1.51	0.01	-1.6675	$-\frac{70.7913}{70.3719}$		-0.1046	-0.0483	0.9921	0.1549	0.8372		<del></del>	
1	2.23	0.01	-1.4626	6.9474			-0.0504	0.9556	_0.1573		-4.7500		
7	4.28	0.01	-1.0666	6.1266			-0.0527	0.8782	0.1599		-5.7440	<del></del>	<del></del>
	6.39	0.01	-0.5965	5.2136	0.0090		-0,0529	0.7967	0.1606	0.6361			
9	8.47		-0.1250	4.3693	0.0039		-0.0531	0.7161	0.1573		-34.9544		
10	10,60	0.01	0.4667	3.4417	0.0037		0.0553	0.6392	0.1519		7,3746		
11	12.75	0.01	1.1371	2.4005		-0.1071		0.5585	0.1459		2.1111		
12	14.89	0.01	1.8087	1.4167	0.0128		-0.0666	0.4916	0.1510		0.7832		
13	17.05	0.01	2.4562	0.5336		-0.0914		0-4328	0.1510	0.2818	0.2171		
14	19.22	0.01		-0.1552			-0.0692	0.3878	0.1531		-0.0501		
15	21.40	0.01	3.7178	-0.7628	0.0296	-0.1451	-0.0674	0.3483	0.1522	0.1961	-0.2052		
													. <del></del> -
					<del></del>			<del></del>			·		
			<del></del>								<del></del>		
							•					•	
									<del></del>		<u></u>		
									<del></del>		<del></del>		
	•												
													<del>- ^</del>
								· - · - · · · ·					
								<del></del>		<del></del>	<del></del>		
													•
							_		<del> </del>				

				1	ANGLEY RE	SEARCH C	ENTERINAS	(A)	UNITA	RY PLAN	IND TUNK	EL (UPut)	
	1 OF						MARTIN P	ISSILE TA	IL EFFECTS	DATA			···
E I	1 OF												
				CH RX10-4	PHI	CONF	L DEL	1 DEFS		TRANSITI	DNE		
		24	3.9	5 3.0	0.0 8	20F35 0	-0	0 -50	<u> </u>	FIXE			<del> </del>
OINT	ALPH			CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP	
<u>1</u> –	-4-0			-1.8140 -1.4824	6.2483	0.0571	-0.1240	-0.0362	0.8584	0.0639		-3,4445	
3	-1.0			-1.3077	5.3417			-0.0384	0.7612	0.0636		-3.826 <del>5</del> -4.0848	
•	-0.0	1 .0.	0	-1.1324	5.0273	0.0496	-0.1155	-0.0385	0.7249	0.0645	0.6604	-4.4395	
5	1.0			-0.9576	4.6965		-0-1154	-0.0385	0.6911	0.0646	0.6265	-4.9045	_
<b>-</b> ;	2.0		0	-0.7835 -0.3921	3.6735	0.0502	-0.1081 -0.1006	-0.0385 -0.0385	0.6547 0.5828	0•0641 0•0651	0.5177	-5.5515 -9.3667	<u>-</u> -
	6.1	4 -0.	01 <u> </u>	9.0106	2.4543	0.0505	-0.1003	-0.0387	0.5128	0.0646		275.8750	
9	8.2			0.4352	2.2072		-0-1000	-0.0420	0.4694	0.0637	0.4057	5,2558	
10 11	10.2			1.1847	1.7128	0.0090	-0.1070 -0.1067	-0.0487 -0.0551	0.4474	0.0602_	_0,3872_ 0.382 <b>6</b>	2.39 <u>76</u> 1.4409	<del></del>
iż	14.4			1.5449	1.5354		-0.1360	-0.0587	0.4389	0.0583	0.3806	0.9913	
13	16.	3 0.	0	1.9498	1.3159	0.0595	-0.1583	-0.0622	0.4364	0.0583	0.3781	0.6749	
14	16.0			2.3704	1.0591		-0.1476	-0.0658	0.4364	0.0601	0,3763	0,4468	
15 16	20.7 -0.0			2.0110 -1.1734	0.7819		-0.2098 -0.1075	-0.0693	0.4337	0.0640	0.3730 0.6613	0.2761 -4,3058	
-			-			<u> </u>							
									<del></del> -			<del></del>	
								•					
									. —				
								,**				,	
										<del></del>			
			:								<del> </del>	·	
								-					
													<del></del>
													_

			· ·	ANGLEY RE	SEARCH C	ENTERINAS	A)	ATINU	RY PLAN N	IND TUNN	EL (UPUT)	
	1 OF 1					MARTIN M	ISSILE TA	IL EFFECTS	DATA			
LET	1 OF 1											•
										,		
	· TEST	PART	ACH RXIO-	PHY	CONF	L DEL	1 DELS	DEL3 DEL4	TRANSIT	ON	•	
	<u> • .</u>	<u>25 _                                </u>	63 3.0	0.0 8	240F35 0	.0	0 -20	0 -20				<del>,, </del>
DINT	ALPHA	BETA	CN	CLH	CY	CLN	CLL	CA	CAB	CAF	ACP	
	-3.76	0.0	-1.6220	5.4142	0.0266	-0.0967	-0.0367	0.7663	0.0466	0.7197	-3.3300	
3	-1.71 -0.71	0.0	-1.7961 -1.1482	4.6274	0.0168	-0.0772	-0.0325	0.7066	0.0466		-3,7649 -4,0302	
4	0.32	0.0	-0.9718	4.3353	0.0187	-0.0768	-0.0367	0.6425	0.0466	0.5959	-4.4611	
5	1.33	0.0	-0.7990	4.0331	0.0190	-0.0770	-0.0328	0.6082	0.0466	0.5616	-5.0476	
9	2,35 4,39	0.0	-0.623 <u>8</u> -0.2507	3.7461	0.0188	-0.0768 -0.0766	-0.0369	0.572 <b>5</b>	_0.0459_ 0.0459		-6.80 <u>52</u> -12.3025	·
Ġ	6.43	0.0	0.1187	2.4875	0.0189	-0.0855	-0.0373	0.4515	0.0453		20.9550	
9	8.48	0.0	0.4666	2.1337	0.0179	-0.09+4	-0.0416	0.4292	0.0454	0.3838	4.5729	
10 11	10.53 12.59	<u> </u>	1.0722	1.8234	0.0205	-0.1136 -0.1421	0.0500_	0.4236 0.4247	_0.0441 0.0398	0.3795	2.5174 1.7006	<del></del>
iż	14.65	0.0	1.4264_	1-6801	0.0331	-0.1509	-0.0545	0.4249	0.0373	0.3876	1.1779	
13	16.71	0.0	1.7583	1.5235	0.0415	-0.1704	-0.0589	0.4264	0.0398	0.3866	0.8664	
15	20.84	0.0	2.1391	1.0123	0.0499	-0.1896	-0.0632	0.4276	0.0434	0.3842		<del></del>
16	8,30	0.0	-1.0000	4.3465		-0.0759		0.6438	0.0459		-4,3465	
			<del></del>									
			- <del></del>	<del></del>	· ·	<del></del>		<del></del>		· ·· · · · · · · · · · · · · · · · · ·		
	<u> </u>	_										
	<del></del>				<del></del>			<del></del>		<del></del>		
							<u>.</u>					
												•
												<del></del>
						·						
					`							
			<del></del>									
		<del></del>		<del></del> .				<del></del>				

### ARTIN MISSILE TAIL EFFECTS DATA    TEST PART MACH RAID=6	TEST PAPT WACH RAID-6 PMI CONF L DELI DEL2 DEL3 DEL4 TRANSITION  4 26 2.86 3.0 0.0 92 0 733 0.0 0 -20 0 -20 FIRED  OINT ALPHA BETA CN CLM CY CLM CLL CA CAB CAF RCP  1 -4.09 0.01 -2.5968 9.5170 0.0207 -0.1363 -0.0427 1.2399 0.1069 1.1330 -3.6448 2 -2.03 0.01 -2.1068 8.5349 0.0217 -0.1251 -0.0428 1.1365 0.1068 1.0297 -3.9389 3 -0.99 0.01 -1.9512 8.0191 0.0224 -0.1250 -0.0361 1.0869 0.1061 0.9808 -4.1099 4 0.01 0.01 -1.9512 7.5501 0.0170 -0.1133 -0.0405 1.0400 0.1063 0.9337 -4.3114 5 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9987 6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9913 0.1068 0.8345 -4.9788 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2641 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0359 0.8511 0.1097 0.7414 -6.2641 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3441 10 10.35 0.0 0.0953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1046 0.4812 3.7238 11 12.47 0.0 1.2665 1.8019 0.0141 -0.727 -0.0386 0.5521 0.1042 0.4979 1.4221 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0727 -0.0360 0.5521 0.1042 0.4979 1.4221 13 16.74 0.0 2.2806 0.3578 0.0330 -0.0164 -0.0516 0.4509 0.1080 0.3429 0.3121 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0471 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0471	
A 26 2.86 3.0	A 26 2.86 3.0 0.0 82m0F33 0.0 0 -20 0 -20 FIRED  DINT ALPHA BETA CN CLM CY CLM CLL CA CAB CAF RCP  2 -2.03 0.01 -2.5968 9.5170 0.0207 -0.1363 -0.0427 1.2399 0.1069 1.1330 -3.6449  2 -2.03 0.01 -2.61668 8.5349 0.0217 -0.1251 -0.0428 1.1365 0.1068 1.0297 -3.9389  3 -0.99 0.01 -1.9512 8.0191 0.0224 -0.1250 -0.0381 1.0869 0.1061 0.9808 -4.1099  4 0.01 0.01 -1.7512 7.5501 0.0170 -0.1133 -0.0405 1.0400 0.1063 0.9337 -4.3114  5 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9987  6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9764  7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2647  8 6.18 0.0 -0.4552 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.417  9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443  10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1066 0.4012 3.7259  11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0386 0.5321 0.1042 0.4279 1.4228  12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7186  13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0409 0.4746 0.1057 0.3689 0.3591  14 18.87 0.0 2.8066 0.3578 0.0337 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.047	
** 26 2.86 3.0	POINT ALPHA BETA CN CLM CY CLN CLL CA CAB CAF RCP  1 -4.09 0.01 -2.5968 9.5170 0.0207 -0.1363 -0.0427 1.2399 0.1069 1.1330 -3.6649 2 -2.03 0.01 -2.1668 8.5349 0.0217 -0.1251 -0.0428 1.1365 0.1068 1.0297 -3.9389 3 -0.99 0.01 -1.9512 8.0191 0.0224 -0.1250 -0.0381 1.0869 0.1061 0.9808 -4.1999 4 0.01 0.01 -1.7512 7.5501 0.0170 -0.1133 -0.0405 1.0400 0.1063 0.9337 -4.3114 5 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9987 6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9706 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2647 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0359 0.8511 0.1097 0.7414 -6.2647 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4612 3.7256 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2710 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7186 13 16.74 0.0 2.8806 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.3271 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.476	
1 -4.09	1 -4.09	
2 -2.03	2 -2.03	
3 -0.99 0.01 -1.9512 8.0191 0.0224 -0.1250 -0.0381 1.0869 0.1061 0.9808 -4.1099 4 0.01 0.01 -1.7512 7.5501 0.0170 -0.1133 -0.0405 1.0400 0.1063 0.9337 -4.3114 5 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9987 6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9704 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2641 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4171 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 4.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7259 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 13 16.74 0.0 2.2897 0.0833 0.0347 -0.0961 -0.0441 0.4998 0.1061 0.3937 0.7180 13 16.74 0.0 2.2897 0.083 0.0347 -0.0961 -0.0499 0.4746 0.1057 0.3699 0.3539 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1089 0.3190 -0.476	3 -0.99 0.01 -1.9512 8.0191 0.0224 -0.1250 -0.0381 1.0869 0.1061 0.9808 -4.1099 4 0.01 0.01 -1.7512 7.5501 0.0170 -0.1133 -0.0405 1.0400 0.1063 0.9337 -4.3114 5 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9987 6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9764 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2647 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.417 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7259 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4221 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7186 13 16.74 0.0 2.2897 0.6083 0.0347 -0.0961 -0.0409 0.4746 0.1057 0.3689 0.3578 14 18.87 0.0 2.8806 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1089 0.3190 -0.4727 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.4727	
\$ 1.03 0.01 -1.5363 7.0527 0.0175 -0.1130 -0.0407 0.9895 0.1059 0.8836 -4.9907 6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9706 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2641 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4171 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 4.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1066 0.4812 3.7250 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7180 13 16.74 0.0 2.2897 0.6083 0.0347 -0.0964 -0.0489 0.4061 0.3937 0.7180 14 18.87 0.0 2.8056 0.3576 0.0330 -0.1064 -0.0516 0.4509 0.1089 0.3190 -0.0476 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	\$\begin{array}{cccccccccccccccccccccccccccccccccccc	
6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9766 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2641 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4171 9 6.27 0.0 0.0830 3.4806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7256 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.479 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7180 13 16.74 0.0 2.2807 0.6083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.4476	6 2.07 0.01 -1.3204 6.5632 0.0122 -0.1014 -0.0383 0.9413 0.1068 0.8345 -4.9766 7 4.11 0.01 -0.9027 5.6546 0.0131 -0.0903 -0.0359 0.8511 0.1097 0.7414 -6.2641 8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4179 9 8.27 0.0 0.0830 3.0806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3403 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0363 0.6687 0.1116 0.5571 44.3403 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0386 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 9.7186 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3531 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0542 0.4279 0.1089 0.3190 -0.0478 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0478	
7	7	
8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4171 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7250 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0346 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1081 0.3937 0.7180 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0481 0.4998 0.1081 0.3937 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1084 -0.0516 0.4509 0.4080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	8 6.18 0.0 -0.4542 4.7315 0.0196 -0.0906 -0.0361 0.7617 0.1120 0.6497 -10.4177 9 8.27 0.0 0.0830 3.6806 0.0202 -0.0902 -0.0363 0.6687 0.1116 0.5571 44.3443 10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7259 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7188 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3538 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1279 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.047	
10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7250 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7180 13 16.74 0.0 2.2897 0.6083 0.0347 -0.0961 -0.0469 0.4746 0.1057 0.3689 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.4476	10 10.35 0.0 0.6953 2.5900 0.0263 -0.0959 -0.0342 0.5898 0.1086 0.4812 3.7259 11 12.47 0.0 1.2665 1.8019 0.0141 -0.0727 -0.0386 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1081 0.3937 0.7188 13 16.74 0.0 2.2897 0.6083 0.0347 -0.0961 -0.0499 0.4746 0.1057 0.3689 0.3538 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1279 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.474	
11 12.47 0.0 1.2665 1.4019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4228 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0,7180 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	11 12.47 0.0 1.2665 1.6019 0.0141 -0.0727 -0.0366 0.5321 0.1042 0.4279 1.4220 12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7180 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1271 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	
12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0,7180 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3530 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	12 14.60 0.0 1.7702 1.2716 0.0244 -0.0950 -0.0441 0.4998 0.1061 0.3937 0.7186 13 16.74 0.0 2.2897 0.8083 0.0347 -0.0961 -0.0489 0.4746 0.1057 0.3689 0.3536 14 18.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1271 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	
16 18.87 0.0 2.8066 0.3578 0.0330 -0.1066 -0.0516 0.4509 0.1080 0.3429 0.1275 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	16 16.87 0.0 2.8066 0.3578 0.0330 -0.1064 -0.0516 0.4509 0.1080 0.3429 0.1271 15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	
15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.4476	15 21.01 0.0 3.3523 -0.1596 0.0373 -0.1174 -0.0542 0.4279 0.1089 0.3190 -0.0476	
		<del></del>
		•
		<del></del>
	,	
		<del></del>

7 ALI -3. -1 -0. 0 1 2 4 6 8 10	PHA	27 2. 8ETA 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	CM RX10-130 2.0 CM -3.0451 -2.6701 -2.3706 -7.1716 -1.7191 -1.2690 -0.7901 -0.2741	CLM 11.3390 10.3846 9.6329 9.3145 A.7525 8.1964 7.1196 6.6473	CONF 2 J OF 33 0 CY 0 . 0958 0 . 0847 0 . 0877 0 . 0723 0 . 0813 0 . 0892	CLM -0.1364 -0.1204 -0.1168 -0.0917	1 DEL2 0 0 0 CLL -0.0367 -0.0395 -0.0408 -0.0402	CA 1.4306 1.3429 1.2891 1.2368 1.1829	CAB 0.1451 0.1462 0.1473 0.1490	ION	XCP -3.7237 -3.9634 -4.1166 -4.2892	
7 ALI -3. 0 0 1 2 4 6 10 12	EST F	27 2. 8ETA 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	CN -3.0451 -2.6701 -2.3866 -2.1716 -1.9464 -1.7191 -1.2690 -0.7901	-90.0 %; CLM 11.3390 10.3846 9.6329 9.3145 A.7525 8.1964 7.1196 6.6473	CY 0.0958 0.0847 0.0847 0.0817 0.0813 0.0892 0.0641	CLM -0.1364 -0.1204 -0.1206 -0.1188 -0.0917	CLL -0.0367 -0.0395 -0.0408 -0.0408	CA 1.4386 1.3429 1.2368 1.1829	CAB 0.1451 0.1462 0.1473 0.1490	CAF 1.2735 1.1967 1.1418	-3,7237 -3,9634 -4,1166	
7 ALI -3. -1 -0. 0 1 2 4 6 8 10	0HA 192 87 85 17 17 19 24 27 33	27 2. 8ETA 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	CN -3.0451 -2.6701 -2.3866 -2.1716 -1.9464 -1.7191 -1.2690 -0.7901	-90.0 %; CLM 11.3390 10.3846 9.6329 9.3145 A.7525 8.1964 7.1196 6.6473	CY 0.0958 0.0847 0.0847 0.0817 0.0813 0.0892 0.0641	CLM -0.1364 -0.1204 -0.1206 -0.1168 -0.0917	CLL -0.0367 -0.0395 -0.0448 -0.0402	CA 1.4306 1.3429 1.2891 1.2368 1.1829	CAB 0-1451 0-1462 0-1473 0-1490	CAF 1.2735 1.1967 1.1418	-3,7237 -3,9634 -4,1166	
7 ALI -3. -1 -0. 0 1 2 4 6 8 10	0HA 192 87 85 17 17 19 24 27 33	27 2. 8ETA 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	CN -3.0451 -2.6701 -2.3866 -2.1716 -1.9464 -1.7191 -1.2690 -0.7901	-90.0 %; CLM 11.3390 10.3846 9.6329 9.3145 A.7525 8.1964 7.1196 6.6473	CY 0.0958 0.0847 0.0847 0.0817 0.0813 0.0892 0.0641	CLM -0.1364 -0.1204 -0.1206 -0.1168 -0.0917	CLL -0.0367 -0.0395 -0.0448 -0.0402	CA 1.4306 1.3429 1.2891 1.2368 1.1829	CAB 0-1451 0-1462 0-1473 0-1490	CAF 1.2735 1.1967 1.1418	-3,7237 -3,9634 -4,1166	
-3: -1: -0: 0: 1: 2: 6: 8: 10: 12:	92 87 85 17 17 19 24 27 33	0.01 -0.02 -0.02 -0.02 -0.02 -0.02	-3.0451 -2.6701 -2.3666 -2.1716 -1.7191 -1.2690 -0.7901 -0.2741	11.3390 10.3846 9.6329 9.3145 A.7525 8.1964 7.1196 6.6473	0.0958 0.0847 0.0877 0.0723 0.0813 0.0892	-0.1364 -0.1204 -0.1206 -0.1188 -0.0917	-0.0367 -0.0395 -0.0448 -0.0402 -0.0428	1.4306 1.3429 1.2891 1.2368 1.1829	0-1451 0-1462 0-1473 0-1490	1.2935 1.1967 1.1418	-3,7237 -3,9634 -4,1166	
-1, -0, 0 1, 2, 6, 8, 10, 12,	87 85 17 17 19 24 27 33	0.02 -0.02 -0.02 -0.02 -0.02	-2.6701 -2.3866 -2.1716 -1.9464 -1.7191 -1.2690 -0.7901 -0.2741	10.3846 9.0329 9.3145 A.7525 8.1964 7.1196 6.6473	0.0847 0.0877 0.0723 0.0813 0.0892 0.0641	-0.1204 -0.1206 -0.1188 -0.0917	-0.0395 -0.0448 -0.0402 -0.0428	1.2891 1.2891 1.2368 1.1829	0.146Z 0.1473 0.1490	1.1967	-3,9634 -4,1166	<del></del>
-0, 0 1 2 4 6 8 10	17 17 19 24 27 33	0.02 -0.02 -0.02 -0.02 -0.02	-2.3066 -2.1716 -1.9464 -1.7191 -1.2690 -0.7901 -0.2741	9.8329 9.3145 A.7525 8.1964 7.1196 6.6473	0.0877 0.0723 0.0813 0.0892	-0.1206 -0.1188 -0.0917	-0.0448 -0.0402 -0.0428	1.2891 1.2368 1.1829	0.1473 0.1490	1.1418	-4.1166	
1 2 6 8 10 12	17 19 .24 .27 .33 .41	0.02 -0.02 -0.02 -0.02	-1.9464 -1.7191 -1.2690 -0.7901	A.7525 8.1964 7.1196 6.6473	0.0813 0.0892 0.0641	-0.1188	0.0402 -0.0428	1.1829		1.0878		
2 6 8 10 12	24 27 33 41	-0.02 -0.02 -0.02	-1.7191 -1.2690 -0.7901 -0.2741	8.1964 7.1196 6.6473	0.0892 1440.0	-0.0917 -0.0969	-0.0428					
10 12	33 41 48	-0.02 -0.02	-0.7901	7.1196 6.6473	0.0641	-0.0764	-0.0420		0.1488	1.0341		
10 12	33 41 48	-0.02 -0.02	-0.7901	6.6473	0 6055		-0-0456	1.0280	0.1507 0.1526	0.8754	-4,7 <u>478</u> -5.61 <b>9</b> 4	
10 12	41	-0.02	-0.2741		U. 0853	-0.0831	-0.0462	0.9306	0.1573		-7.6538	
12	48			4.9920	0.1056	-0.1335	-0.0490	0.6360	0.1581	0.6779	-18.2122	
14			0.3281	3.9000	0.1017	-0.0932	-0.0482	0.7454	0-1547	0.5907	11.0065	<del></del>
16			1.0007	2.7804		-0.0893		0.6417	0.1483	0.4934	2.7784	
	44	0.02	2.3063	1.6680		-0.0814		0.5542	0.1486	0.4056	1.0009	
		-0.02	2.9072	0.1641		-0.0945		0.4527	0.1521	0.3006	8.0565	
20	90	-0.02		-0.5248	0.0907	-0.0301	-0.0562	0.4137	0.1542	0.2595	-0.1482	
0	14	-0.02	-2.1739	9.3094	0.0924	-0.1227	-0.0468	1.2365	0.1487	1.8878	-4.2823	
							<del></del>		<del></del>			
		-									· <del></del>	
				<del></del>						<del></del>		
			· ·					· · · · · · · · · · · · · · · · · · ·	- <del></del>			<del></del>
-				<del>-</del>		· · · · · · · · · · · · · · · · · · ·					<del></del>	<del></del>
							· ·					
		•										
		·			<del></del>	<del></del>						<del></del>
					-							
											•	
									<del> </del>			

11 12.46 -0.01 1.2516 1.6537 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4248 1.4813 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7483 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 8.3931 14 18.87 -0.01 2.7736 0.4475 0.0490 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3187 -0.0142 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3655	JE ET	1 OF 1			ANGLEY RI	SEARCH C	ENTER (NAS MARTIN M	A) ISSILE TA	UNITA 1L EFFECTS	RY PLAN (	11ND TUNN	EL (UPUT)		
1 -4.10 -0.01 -2.6137 9.5822 0.0080 -0.1516 -0.0432 1.2480 0.1048 1.1440 -3.6662 2 -2.04 -0.02 -2.1809 8.5885 0.0742 -0.1197 -0.0456 1.1471 0.1053 1.0418 -3.9361 3 -0.99 -0.01 -1.9603 8.6779 0.0592 -0.1016 -0.0458 1.0954 0.1068 0.9806 -4.1208 4 0.03 -0.01 -1.7507 7.5813 0.0605 -0.1003 -0.0458 1.0454 0.1084 0.9370 -4.3365 5 1.04 -0.01 -1.5437 7.1072 0.0499 -0.0670 -0.0432 0.9959 0.1093 0.8066 -4.6040 6 2.07 -0.01 -1.3296 6.6212 0.0537 -0.0886 -0.0453 0.9488 0.1104 0.0384 -4.9766 7 4.12 -0.01 -0.9039 5.6981 0.0470 -0.0901 -0.0395 0.8567 0.1123 0.7444 -8.2492 8 6.19 -0.01 -0.4594 4.7630 0.0580 -0.0977 -0.0406 0.7657 0.1158 0.6499 -10.3678 9 8.26 -0.01 0.0705 3.7165 0.0675 -0.1038 -0.0423 0.6739 0.1169 0.5570 52.7160 10 10.35 -0.01 0.6715 2.6455 0.0559 -0.0890 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.46 -0.01 1.7512 1.3455 0.0577 -0.0846 -0.0451 0.5382 0.1134 0.4248 1.4613 12 14.61 -0.01 1.7512 1.3455 0.0377 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7683 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 0.3931 14 10.87 -0.01 2.7736 0.4475 0.0490 -0.1055 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0070 0.0402 -0.0807 -0.0824 0.4315 0.1128 0.3187 -0.0122 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3455			PART H ZR 2.	ACH RX10-6	-90.0 S	CONF	L DEL	1 DEL2	DEL3 DEL4	TRANSIT	ION (	-		
1	DINT	ALPHA	BETA	CN	CLM	CY	. CLN	CLL				XCP -		
3 -0.99 -0.01 -1.9603 8.6779 0.0592 -0.1016 -0.0458 1.0954 0.1068 0.9886 -4.1208 4 0.03 -0.01 -1.7507 7.5813 0.0605 -0.1003 -0.0458 1.0454 0.1084 0.9370 -4.3365 5 1.04 -0.01 -1.5437 7.1072 0.0499 -0.0670 -0.0432 0.9959 0.1093 0.8866 -4.6040 6 2.07 -0.01 -1.3296 6.6212 0.0537 -0.0886 -0.0453 0.9488 0.1104 0.8384 -4.9790 7 4.12 -0.01 -0.9039 5.6981 0.0470 -0.0901 -0.0395 0.8567 0.1123 0.7444 -6.2092 8 6.19 -0.01 -0.4594 4.7630 0.0580 -0.0977 -0.0406 9.7657 0.1158 0.6499 -10.3678 9 8.26 -0.01 0.0705 3.7165 0.0675 -0.1038 -0.0423 0.6739 0.1169 0.5570 52.7160 10 10.35 -0.01 0.6715 2.6455 0.0559 -0.0890 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.40 -0.01 1.2516 1.6539 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4248 1.4813 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7683 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 0.3931 14 18.87 -0.01 2.7736 0.4475 0.0409 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3405 0.162 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3455	1				9.5822	0.0880	-0.1516	-0.0432	1.2480	0.1040	1.1440	-3.6662		
4 0.03 -0.01 -1.7507 7.5813 0.0605 -0.1003 -0.0458 1.0454 0.1084 0.9370 -4.3305 5 1.04 -0.01 -1.5437 7.1072 0.0499 -0.0670 -0.0432 0.9959 0.1093 0.8866 -4.6040 6 2.07 -0.01 -1.3296 6.6212 0.0537 -0.0886 -0.0453 0.9488 0.1104 0.8384 -4.9790 7 4.12 -0.01 -0.9039 5.0981 0.0470 -0.0901 -0.0395 0.8567 0.1123 0.7444 -6.2492 8 6.19 -0.01 -0.4594 4.7630 0.0580 -0.0977 -0.0406 9.7657 0.1158 0.6499 -10.3678 9 6.26 -0.01 0.0705 3.7165 0.0675 -0.1038 -0.0423 0.6739 0.1169 0.5570 52.7160 10 10.35 -0.01 0.6715 2.6455 0.0559 -0.0890 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.40 -0.01 1.2516 1.6539 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4240 1.4813 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7683 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 0.3931 14 18.87 -0.01 2.7736 0.4475 0.0490 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3187 -0.0142 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3455	<del>-</del> -				8-6779	0.0742	-0.1197	-0.0456						
5	4	0-03	-0-01	-1-7507	7.5613	0.0605	-0-1003	-0.0458	1.0454					
7	5	1.04	-0.01	-1.5437		0.0499	-0.0070	-0.0432	0.9959	0.1093	0.8866	-4.6040		
8 6.19 -0.01 -0.4594 4.7630 0.0580 -0.0977 -0.0406 0.7657 0.1158 0.6499 -10.3678 9 8.26 -0.01 0.0705 3.7165 0.0675 -0.1038 -0.0423 0.6739 0.1169 0.5570 52.7160 10 10.35 -0.01 0.6715 2.6655 0.0559 -0.0890 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.40 -0.01 1.2516 1.6539 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4248 1.4813 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7683 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 8.3931 14 18.87 -0.01 2.7736 0.4475 0.0490 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0524 0.4315 0.1128 0.3187 -0.0142 16 0.02 0.0 -1.7374 7.5840 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3655	_6	2.07_	-0.01	-1.3296		0.0537	-0.0886	0.0453_						
9 8.26 -0.01 0.0705 3.7165 0.0675 -0.1038 -0.0423 0.6739 0.1169 0.5570 52.7160 10 10.35 -0.01 0.6715 2.6655 0.0559 -0.0890 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.40 -0.01 1.2516 1.6539 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4248 1.4013 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7683 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 8.3931 14 18.87 -0.01 2.7736 0.4475 0.0490 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3187 -0.0142 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3455	á	6-19	-0-01			0.0580	-0.0901	-0-0406						
10 10,35 -0.01 0.0715 2.6455 0.0559 -0.0840 -0.0412 0.5928 0.1146 0.4782 3.9397 11 12.40 -0.01 1.2516 1.6539 0.0517 -0.0846 -0.0461 0.5382 0.1134 0.4248 1.4813 12 14.61 -0.01 1.7512 1.3455 0.0372 -0.0712 -0.0477 0.5047 0.1138 0.3909 0.7483 13 16.75 -0.01 2.2660 0.8909 0.0575 -0.1068 -0.0533 0.4787 0.1125 0.3662 0.3931 14 18.87 -0.01 2.7736 0.4475 0.0490 -0.1005 -0.0612 0.4533 0.1128 0.3405 0.1613 15 21.01 -0.01 3.3063 -0.0470 0.0402 -0.0807 -0.0624 0.4315 0.1128 0.3187 -0.0142 16 0.02 0.0 -1.7374 7.5846 0.0294 -0.0938 -0.0407 1.0427 0.1090 0.9337 -4.3455	9	8.26	-0.01	0.0705						0.1169				
12		10.35	-0.01			0,0559	-0.0890	-0.0412	0.5928	0.1146	0.4782	3,9397	<del>-,</del>	
13		12.48	-0.01			0.0517	-0.0846	-0.0461						
14	15	16.75												
15	14	18.87	-0.01	2.7736										
	15	21.01	-0.01	3.3063										
	• •	0.02	0.0	-101500	103333	4.0584	-0.0721	-0.0434	1.0430	0.100	V.7340			
												<del> </del>		
			•											
					· · · · · · · · · · · · · · · · · · ·					·				
									<u></u>				<u> </u>	·
												<del></del>		
								<u> </u>						
									<del></del>					
			-			· · · · · · · · · · · · · · · · · · ·			<del></del>					
							<del>-,</del> -							
			•	•										
<del></del>						<del></del>		·				· · · · · · · · · · · · · · · · · · ·	<del></del>	<del></del>
•														
												•		

AGE	1 OF 1		· L	ANGLEY R	ESEARCH C	ENTERINAS	A) ISSILE TA	UNITA	RY PLAN	IND TUNN	EL (UPHT)	
HEET	1 OF 1		·		· · · · · · · · · · · · · · · · · · ·	MAN CAN	1331FF IW	C EFFEC.3	VAIR			
											<del></del>	
	TEST	PART H	ACH RX10-6	PHI -40-0 A	CONF	L DEL	1 DELZ	PEL3 DEL4	TRANSITI	ON		•
DOTAT	ALPHA	BETA	CN		CY	CLN		CA	CAB			•
1	-4.08	-5.6	-2.0450	7.2795	0.0145	-0.0563	-0.0274	0.9809		CAF 0.9157	-3.5597	
5	-5.03	0.0	-1-6624	6-4668	0.0060	-0-0444	-0.0282	0.8977	0.0657	0.6320	-3,8900	
3	-1.02	0.0	-1.4726 -1.2879		-0.0081		-0.0286	0.8550	0.0663		-4.1090	_
<del>-4.</del> 5	0.0 1.01	0.0	-1.0959	5.2392		-0.0423		_ 0.8150 0.7732	0.0669		-4.7608	
6	2.05	0.0	-0.9117	4.6526	-0.0009	-0.0312	-0.0266	0.7314	0.0689	0.6625	-5.3228	
7			-0.5042	4.0127	0.0190	-0.0320	-0.0274	0.6493	0.0689	0.5804	-7.9684	
9	8.20	-0.01	-0.0905 0.3310	3-1924 2-5584	0.0230	-0.0335	-0.0280	0.5748	0.0712		-35,2753	
10		-0.01	0.7170	2.2031	0.0505	-0.0408 -0.0707	-0-0351	0.5290 0.5108	0.0708	0.4582	7.7292 3.0727	
11		-0.01	1.0861	1.9666	0.0535	-0.0661	-0.0354	0.5029	0.0695	0.4334	1.8107	
12	14.45	-0.01	1.4643	1.7618	0.0486	-0.0491	-0.0438	0.4975	0.0690_	0.4285	1.2032	<u> </u>
13		-0.01		1-5724	0.0505	-0.0540	-0.0457	0.4955	0.0665	0.4290	0.8551	
15		-0.01	2.7261	0.9986	0.0518	-0.0582 -0.0765	+0.0450 -0.0473	0.4934	0.0665 0.0664	0,4269		
16			-1.3246	5.6939		-0.0436		0.8165	0.0673	0.4243	-4.2986	
17	-0.01	-0.01	-1.3247	5.6867			-0.0321	0.8164	0.0677		-4.2920	<del></del>
			· <del>- ·</del> · · · · · · · ·	<del> </del>		- <u></u>					<del></del>	
								•		•		
							· · · · · · · · · · · · · · · · · · ·		······································			
			<del></del>	<del></del>			<del></del>		<del> </del>			
										<del></del>		
						<del></del>		<del></del>				
									<del> </del>		<del></del>	
						-		-				
······································		<del></del>	<del></del>			<del></del>	*	<del></del>			······································	<del></del>

E .	1 0#	1		LANGLEY RE	SEARCH C		A) 1551LE TAI		AY PLAN I	IND TUNN	EL (UPHT)		
	) of												
	186	T DADY	MACH RX10-	6 PHI	CONF	L DEL	1 DEL2 (	DEL 3 DEL	TRANSIT	1004			
			.63 3.0		-0F33 0		00		FIXE				
INT	ALPHA		CN	CLM	CY	CLN	<u>cut</u>	CA	CAB	CAF	xce		
ļ	-3.75 -1.72			6.2398 5.5370	0.0754	-0.0668	-0.0250	0.8734	0.0516 0.0518	0.8216	-3.4450 -3.6108		-
3	-0.70			5.1653	0.0814	-0.0700	-0.0298	.0.7584	0.0521	0.7063	-4.0953		
<u>•</u>	0,31			4.8110	0.0671_	-0.0542	-0.0287	_ 0.7215	0.0532	0.6683	-4,4484		
•	2.36			4.4680	0.0581	-0.0440 -0.0132	-0.0316 -0.0305	0.6817	0.0532	0.6285	-4.9272 -5.637 <b>8</b>		•
7	4,3	-0.01	-0.3486	3.3907	0.0563	-0.0179	-0.0323	0.5690	0.0550	0.5140	-9.7267		
<u> </u>	6,43			2.7582	0.0691	-0.0299	-0.0328	0,5151	0.0557	0.4594	85.9257		·
0	10.52			2.4167	0.0891	-0.0729 -0.0939	-0.0340 -0.0374	0.4916	0.0557 0.0545	0.4359	6,653 <b>8</b> 3,231 <b>8</b>		
ì	12.59	-0.01	0.9996	2.0952	0.0836	-0.0719	-0.0399	0.4839	0.0557	0.4282	2.0961		
Ž	14.65			1.9584	0.0584	-0.0488	-0.0423	0.4838	0.0520	_ 0.4318_	1.4710		
3 4	16.71			1.7500	0.0647	-0.0579 -0.0691	-0.0454 -0.0450	0.4826	0.0514 0.0520	0.4312 0.4323	1.0285		
<u>Š</u>	20.8	-0.01	2.4939	1.1671	0.0405	-0.0783	-0.0450	0.4882	0.0520	0.4362	0.4680		<del></del>
6	0.32	-0.01	-1.0928	4.8364	0.0427	-0.0079	-0.0327	0.7196	0.0536	0.6660	-4.4257		
		-				······································		•				<del></del>	
								<del> </del>					<del></del>
													•
				<del></del>							<del></del>		
													•
										<del></del>			
	·												
					·								

	OF 1	• 							· 			
	TEST	PART H	ACH RX10-	6 PHI	CONF	L DEL	1 DELS	DEL3 DEL4	TRANSITI	ON	<del></del>	
TAIT	ALPHA	BETA	36 3.0 CN	_90.0 B.	<u>2#0F31 0</u> CY			20 <u>0</u>	CAB	CAF	XCP	
<u></u>	-4.03	0.01	-1.8479	5.6893	-0.0169	-0.0113	-0.0136	0.8721	0.1390		-3,0700	·
2	-1.96	0.01	-1.5297	5.2422	-0.0187	-0.0092	-0.0122	0.8053	0.1355	0.6698		
<b>5</b>	-0.92 0.11	0.01	-1.3734 -1.2000	5.0120 4.7544	-0.0129 -0.0078	-0.014B -0.0197		0.7777	0.1302	0.6395	-3.6494 -3,945]	
5	1.15	0.0	-1.2064 -1.0370	4.4990	-0.0027	-0.0246	-0.0130	0.7205	0.1432	0.5773	-4.3365	<del></del>
6	2.19	0.01	-0.8830	4.2595	-0.0102	-0.0165	-0.0126	0.6932	_0.1461_	0.5471	-4.8239	
7	4.25	0.01	+0.5530		-0.0124	-0.0026	-0.0115	0.6397	0.1503	0.4894	-6.8348	
€—	8.45	0.0	0.2202	3.2650	-0.0039 -0.0088	4400-0	-0.0128	0.5896	0.1576	0.4320	-17.7663 12.6721	<del></del>
0	10.59	0.0	0.7274	2.2678	-0.0060	-0.0108	-0.0124	0.5028	0.1635	0.3393	3.1177	
1	12.76	0.0	1.2911	1.7774	-0.0047	-0.0034	-0.0124 -0.0132	0.4645	0.1616	0.3029	1.3766	
<u> </u>	14.93	0.01	T-8303	1.3803	<u>-0.0156</u>	-0.0047	-0.0151	0.4390	0.1617	0.2773	0.7541	<del></del>
3	17.09	0.0	2.3668 2.9416	0-6408	0.0003	-0.0090	-0.0205	0.4205	0.1623	0.2582	0.43 <b>84</b> 0.2179	
5	21.46	0.0	3.5103	0.2977	0.0036	-0.0037	-0.0228	0.3775	0.1613	0.2162	0.0848	
6	0.11	0.01	-1.2256	4.7948	-0.0069	-0.0207	-0.0111	0.7503	0.1397	0.6106	-3.9122	
7	0.10	0.01	-1.2151	4.7785	-0.0075	-0.0201	-0.0133	0.7502	0.1397	0.6105	-3,9326	
						<del></del>	<del></del>	<del></del>				
	<del></del>											
						<u> </u>						, , , , , , , , , , , , , , , , , , ,
	<del></del>											
											•	

Æ	1 OF 1		L	ANGLEY	RESEARCH	CENTER (NA!	ISSILE T	UNITAL AIL EFFECTS	DATA	IND TUNK	EL (UPAT)	 
E7 ——	1 07 1					<del></del>						· • · · · · · · · · · · · · · · · · · ·
	TEST		ACH RX10-6			L DEI	1 OELZ	DEL3 DEL4	TRANSITI	.DN		 
		35 2.	66 3.0	40.0_	BZWOF 31	0.0	2 <u>0                                    </u>	50 0	FIXEO	)		 
TMT	ALPHA	BETA	CN	CLM	CY	CLM	CLL	CA	CAB	CAF	XCP	
i	-4,20	0.0	-1.6753	4.9445	0.0165			0.7952	0.1153	0.6799	-2.9514	 · · · · · · · · · · · · · · · · · · ·
Ž	-2,13	0.0	-1.3621	4.5432	0.0167	-0.0401	-0.0154	0.7314	0-1120	0.6194	-3.3354	
3	-1.09	0.0	-1.2083	4.3280	0.0093		-0.0167	0.7020	0-1120	0.5900	-3,5019	
4	-0.07	0.0	-1,0498	4-1058		0.040 <u>0</u>	<u>-0</u> .0157	0.6751	0.1131_		-3,9110	 •
5	0.96	0.0	-0.8921	3.8775		-0.0321	-0.0148		0.1151	0.5326	-4.3465	
_ , -	<u>2.00</u> _	0.0	-0.7344 -0.4006	3.6545 3.2037		0.0395 -0.0386	-0.0162	0.6218	_0.1161	0.5057	-4.9761	 
	6.15	0.0	-0.0409	2.7442		-0.0358			0.1196	0.4501	-7 <b>.9973</b> -67.0962	
-	8.25	0.0	0.3759	7.2627	0.0095				0.1256	0.3487	6.0193	 W
10	10.36	0.0	0.8632	1.7535		-0.0144			0.1250	0.3136	2.0314	
<del>ii</del>	12.49	0.0	1.3490	1.3230	0.0103	-0.0243			0.1221	0.2847	0.9008	 
12	14.63	0.0	1.8251	1.0286	0.0046	0.0091	-0.0204	0.3930	0.1226	0.2704	0.5636	 
13	16.76	0.0	2.2937	0.7676		-0.0555			0.1234	0.2575	0.3346	
14	18,91	0.0	2,7628	0.5390		-0.0477			0.1222	0.2498	0.1951	 
15	21.05	0.0	3.2616	0.2585		-0.0444			0.1555	0.2449	0.0793	
16	-0.06	0.0	-1,0488	4.1068	0.0013	-0.0368	-0.0156	0.6743	0-1145	0.5601	-3,9158	 
								<del></del>		· · · · · · ·		 
		•										
				_								 
			_									 
					***				·			
				•						-	<del>-</del>	 
			<del> </del>					<del></del>	·			 
•												
										<del></del>		 
												•
									<del></del>			 <del></del>
	•	•										•

AGE WET	1 OF 1			ANGLEY R	ESEARCH C	ENTER (NAS	A) ISSILE TA	UNITA IL EFFECTS	RY PLAN &	IND TUNN	EL (UPST)	
											<del> </del>	<del></del>
	YEST	DADY :	ACH RETO-	- PwY	COME	) OF	1 0612	OF T OF	TOANETT	64		
		36 3	95 3.0	-90.0 8	20F31 0	.0 2	0 0	50 (				
POINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAD	CAF	XCP	
1	-4.13	0.0	-1.3776	3.8738	-0.0065	-0.0260	-0.0164	0.6418	0.0720	0.5698	-2.6120	<del></del>
<del></del> _	-2.08	0.0	-1.0830	3.5067		-0.0173		0.5904	0.0712		-3.2380	- <del></del>
3	-1.05 -0.03	0.0	-0.9330 -0.7910	3.1245		-0.0100 -0.0033		0.5663 0.5400	0.0712 0.0723	0.4951		
<u> </u>	0.99	0.01	-0.6346	2.9266	-0.0207	0.0041		0.5178	0.0731	0.4447	-4.6103	
6	2.02	0.0	-0.4865			-0.0093		0.4933	0.0733	0.4200	-5.6254	<del></del>
7.	4.07 6.13	0.0	-0-1742 0-1811	2.3481		-0.0151 -0.0186		0.4418	0.0739	0.3679	-13.4791	
	8.20	0.0	0.5501	1.5038		-0.0063		0.3647	0.0742	0.2905	10.4536 2.7337	
10	10.27	0.0	0.9178	1.7516	-0.0123		-0.0216	0.3510	0.0738	0.2772	1.3607	
11	12.36	0.0	1.2724	1.1210		-0.0198		0.3478	0.0719	0.2759	0,8810	
<u> 15</u>	14.45	_0.0	1.6174	1-0273	0.0179		-0.0238	0.3493_	0.0694	0.2799	9.6358	
13	16.53 18.63	0.0	1.9923 2.3980	0.9024			-0.0259	0.3559	0.0702 0.0717	0.2857	0.4529 0.3109	
15	20.73	0.0	2.0350	0.5417	0.0254			0.3667	0.0719	0.2948	0.1911	
16	-0.03	0.0	0.7909	3.1245	0.0066	-0.0738	-0.0172	0.5398	0.0730	0.4668	-3,9506	
17	-0.04	0.0	-0.7987	3.1325	0.0069	-0.0241	-0.0172	0.5399	0.0726	0.4673	-3.9221	
				<del></del>			<del></del>	<del></del>	<del></del>			<del></del>
_												
_												
							~					
	•											
			<del></del>								•	
			<del> </del>									
•					-							
		·			<del></del> -							
	·											
								•				
											<del></del>	<del></del>
		<del></del>									· · · · · · · · · · · · · · · · · · ·	
											· · · · · · · · · · · · · · · · · · ·	

							<del></del>				<del></del>	<del></del>
						<u></u>	·				<del></del>	
GE.	1 OF 1		Ţ.	ANGLEY RE	SEARCH C	ENTERIVAS	A)	UNITA	MY PLAN	IND TUNN	EL (UPUT)	<del></del>
EET	1 OF 1		··			787157	TOSILE IN	TE EFFEGIS	<u> </u>			
											•	
	TEST	PAPT M	ACH RX10-6	PHI	CONF	L DEL	1 DEL2	DEL3 DEL4				
	<u> </u>	37 4.	64 3.0	-90.0 B	240F31 0	<u>.0</u> 2	.00	50 0	FIXE	<u> </u>		
POINT	ALPHA	BETA	CN .	CLH	CY	CLN	CLL	CA	CAB	CAF	XCP	
1	-3.76 -1.73	0.0	-1.1974 -0.9137	3.2795	0.0128	-0.0259	-0.0141 -0.0154	0.5755 0.5327	0.0546		-2.7388 -3.2475	
3	-0.70	0.0	-0.7718	2-6110	0.0185	-0.0327	-0.0160	0.5081	0.0556		-3,6421	-
•	0.32	0.0	-0.6301	2.6457_			0.0168_	0.4837	0.0556		-4,1989	
2	1.32 2.35	0.0	-0.4804 -0.3413	2.4722		-0.0455 -0.0391		0.4589 0.4345	0.0556 0.0556	0.4033	-5.1462 -6.8009	
- <del>-</del> -	4,39	0.0	-0.0250	1.9442				0.3843	0.0554		-88.3718	
8	6.44	0.0	0.2929	1.5810		-0.0359	-0-0176	0.3463	0.0550	0.2913	5,3977	
. 9	8.49	0.0	0.6051	1.3662	0.0315		-0.0172	0.3288	0.0558	0.2730	2.2578	
10	10.54	0,0_	1.2174	1.2292		-0.0335		0.3273 0.3273	0.0561_ 0.0555	0.2712_ 0.2716	1.3379 0.9614	
_i	14.67	-0.01	1.5389	1.1030		-0.0488		0.3335	0.0543		0.7168	
13	16.74	-0.01	1.8847	0.9669		-0.0624		0.3393	0.0537	0.2856	0.5130	
15	18.79 20.87	-0.01	2.6480	0.7966		-0.0496 -0.0595		0.3468 0.3557	0.0536	0,2932	0.3566	
16	0.31	-0.01	-0.6307	2.6488			-0.0168	0.4815	0.0560		-4.1998	
			<del></del>					<del></del>				
	-											
			<del></del>		<del></del>					<del></del>		<del></del>
					<del></del>							<del></del>
								<del></del>		· · · · · · · · · · · · · · · · · · ·		
						<del></del>						
						•						
									·		····	
							<del></del>				<del></del>	
											<del></del>	

										٠.				
					55 - 96 - 9	F								
	1 of 1			ANGLEY NE	SEARCH C	MARTIN M	A) ISSILE TA	L EFFECTS	DATA	THE TURK				
SMEET	1 07 1								·					
							·							
	TEST	39 2.	BE 3.0	-90.0 B	CONF WOF32 0	O S	O D	SET3 DET4	FIXE	)				
POINT	ALPHA	BETA	CN	CLM	CY	CLN	CLL	CA	CAB	CAF	XCP			
5	-2.13	0.0	CN -1.7220 -1.4008	5.0309 4.6349	0.0198	-0.0187 -0.0189	-0.0147 -0.0120	0.8168 0.7605	0.1031 0.1050	0.7129 0.6555	-2.9215 -3.3088			
3	-1.10	-0.01	-1.2479	4.4313	0.0276	-0.0768	-0.0131 -0.0121	0.7330	0.1074	0.6256	-3.5518 -3.8654			
5	0.96	-0.01	-0.9361	3.9965	0.0279	-0.0260	-0.0111	0.6804	0.1134	0.5670	-4.2602			
- 6		_ <del>-0<u>-0</u>1</del> .	-0.7681 -0.4407	3.7650 3.3169		-0.0186	-0.0100 -0.0103	0.6542	-0.1167 0.1215		-4.9017 -7.526\$			
		0.0	-0.0517 0.3712	2.8064	0.0158	-0.0142	-0.0109	0.5487	0.1275	0.4212	-54.2618	·		
10			0.8591	1.7891	0.0186	-0.0188	-0.0087 -0.0105	0.4536	0.1255		6.1717			
11	12.50	0.0	1.3454	1.3681			-0.0111 -0.0125	0.4253	0.1213	0.3040	1.0169			
13	16.77	-0.01	2.2848	0.4288	0.0161	0.0003	-0.0158	0.4019	0.1232	0.2787	0.3627			
15		-0.01	2.7528 3.2525	0.6103	0.0194	0.0019	-0.0162	0.3865	0.1220		0.1048			
16	-0.06		-1.0905		0.0042	-0.0280	-0.0121	0.7060	0.1106		-3,8648			
							·				····			
						•								
												<del></del>	<del></del>	
						· · · · · · · · · · · · · · · · · · ·								
								•	<del></del>	<u>-</u>				
			<del></del>					<del></del> .	· · · · · · · · · · · · · · · · · · ·				<del></del>	
						<del></del>		<del></del>						
	·													
			<del></del>	<del></del>										
				<del></del>							····			
													•	

`

E :	of 1			ANGLEY R	ESEARCH C	ENTERINAS MARTIN M	A) 155ILE TA	UNITA IL EFFECTS	RY PLAN :	TIND TUNN	EL (UPHT)		
			<del> </del>					<del></del>					
	TEST	PART	MACH RX10-6	PHI	CONF	L OEL	1 DEL2	DEL3 DEL4	TRANSIT	ON			<del></del>
		40 3	.95 3.0					50 0	FIXE	<u> </u>		<del></del>	
INT	ALPHA	BETA	CN	CLH	CY	CLN	-0.0092	CA	CAB	CAF	XCP		
2	-4.13	0.01	-1.3914 -1.0946	3.5628	-0.0244 -0.0183	0.0079	-0.0072	0.6560	0.0696	0.5864			
3	-1.05	0.01	-0.9542	3.3012	-0.0250	0-0061	-0.0079	0.5874	0.0706	0.5168	-3.5435		
•	-0.03	0.01	-0.656e	3.1789	-0.0250 -0.0320 -0.0189	0.0153	-0.0100 -0.0079	0.5654 0.5411 0.5139	0.0722	0.4932	-3.9504		
5	2.03	0.01	-0.6566	2.7845	-0.0189	0-0020	-0.0079	0.5411	0.0728	0.4663	-4.5418 -5.5602		
<del>7</del>	4.07	0.01	-0.5006	2.3812	-0.0264	2400.0	-0.0040	0.4627	0.0742	0.3885	-13.1415		
8	6-14	0.0	0.1616	1.9239	-0.0187	0-0010	-0.0104 -0.0117	0.4189	0.0741	0.3448	10.5944		
9	8.20	0.0	0.5500	1.5418	-0.0151 -0.0109	0.0131	-0.0117	0.3879	0.0756	0.3123	2.0033		
0	12.36	0.0	1.2560	1.3300	-0-0054	0.0146	-0.0141	0.3741	0.0746 0.0725	0.2995	0.9610		
2	14.45	0.0	1.6008	1-1204	0.0008	0-0218	-0.0129	0.3775	0.0706	0.3069	0.6999		
	16.54	0.0	1.9676	1.0252	0.0052	0-0138	-0.0136	0.3856	0.0701	0.3155	0.5210		
5	20.74	0.0	2.3691	0.906B	0.0083	0.0069	-0.0142	0.3940	0.0710	0.3230	0,3620		
6	-0.03	0.0	2.8063 -0.8215	3.1932	0.0094	0.0020	-0.0193	0-4017	0.0707 0.0731	0.3310 0.4935	0,2582 -3,8878		
								-0.111 PM					
			<del></del>									<del></del>	<del></del>
												•	
												···	
												•	
			<del></del>				-			<del></del>		<del></del>	
		_			-								-
										<del></del>	<del></del>	<del></del>	
			•										
									· <del>· · · · · · · · · · · · · · · · · · </del>		·		
				·									
			<del> </del>						····				

	LANGLEY RESEARCH CENTER (NASA) UNITARY PLAN WIND TUNNEL (UPWT)  1 OF 1  1 OF 1												
	. OF 1											•	
			ACH RX10-			L DEL							
		<u>•1 ••</u>	64 3.0	-90.0 B	WOF32 0	•0	20 0	20	) FIXE	<u> </u>	· · · · · · · · · · · · · · · · · · ·		
NT		BETA	CN	CLM	CY	CLN	CLL_	CA	CAB	CAF	XCP		
·	-3.77 -1.73	0.0	-1.2294 -0.9397	3.3619 3.0341	0.0156	-0.0078	-0.0092	0.5895 0.5479	0.0550 0.0550	0.5345	-2.7346 -3.2288	•	
	-0.71	-0.01	-0.P001	2.8618	0.0216	0.0066	-0.0115	0.5241	0.0550	0.4691	-3,5768		
	0,31	0.0	-0.6502	2.6880	0.0150	0.0134	0.0082	0.5032	0.0550	_\$844.0_			
86	1.32	-0.01 -0.01	-0.5005 -0.3507	2.5144	0.0335	-0.0058 0.0010	-0.0090	0.4784	0.0557 0.0557		-5.0238 -6.6744		
<b>7</b> -		-0.01	-0.0413	1.9741	0.0375	-0.0107		0.4032	0.0557		-47,7979		
8	6.45	-0.01	0.2937	1-6014	0.0474	-0.0216	-0.0131	0.3680	0.0568	0,3112	5,4523		
	B.49 10.55	-0.01 -0.01	0.5965	1.4024	0.0340	-0.0096	-0.0127 -0.0150	0.3541	0.0568 0.0561	0.2973 0.2959	2.3511 1.4502		
	12.61	-0.01	1-2001	1.2567			-0.0166	0.3583	0.0555	0.3028	1.0472		
١	14.67	-0.01	1.5105	1 • 2073	0.0474		-0.0141	0.3672	0.0556	0.3116	0.7993	<del> </del>	
2	16.74	-0.01 -0.01	1.8487	1.0917	0.0328	0.0014	-0.0162 -0.0187	0.3818 0.3873	0.0536 0.0536	0.3262	0.5905		
5	20.87	-0.01	2.5935	0.7433			-0.0173	0.3954	0.0536	0.3418	0.2866		
	0.30	-0.01	-0.6603	2.6892	0,0410	-0,0131	-0.0083	0,5003	0,0561	0,4442	-4.0727		
	-		<del></del>					•					
-													
					•								
									<del></del>				
									<del></del>		•		
							<del></del>						
			<del></del>								······································	<u> </u>	
					<del></del>							<del></del>	
			•										
		•				<del></del>							
												<u></u>	
					<del></del>	· · · · · · · · ·							

	1 OF 1		· ·	ANGLEY R	ESEARCH C	ENTER(NAS MARTIN M	A) Issile ta	UNITA IL EFFECTS	RY PLAN W	IND TUNN	EL (UPWT)	
	1 07 1			<del></del>			·	•	· 			
		6.6V		Bu f			N. 05: 0	00.0	******	-		
	4	42 2	MACH RX10-6	-90,0 ы	2#0F36 0	*0 S	O O	50 8	FIXEO			
POINT	ALPHA	BETA	CN	CLH	CY	CLN	CLL	CA	CAB	CAF	XCP	
			-1.5247			-0.0379	-0.0086	0.7278	0.1200		-2,6901	
3	-2.15	0.0	-1.2281	3.7923		-0.0174		0.6696	0.1171	0.5525	-3.0880 -3.3250	
•	-0.09	0.0	-0.9323	3.4475	0.0094	-0.0277	-0.0067 -0.0071	0.6152	0.1167	0.4985	-3.6978	
5	0.94	0.0	-0.7918	3.3044	0.0029	-0.0214	-0.0071	0.5890	0.1169	0.4721	-4.1739	
- 6-	1.98	0.0	-0.6354	2-7125	-0.0046	-0.01 <u>37</u> -0.0141	0.0074_	0.5615 0.5151	_0.1158 _ 0.1174	0.3977	-4.8703 -8.7641	
8	6.14	0.0	0.0341	2.3588	0.0097	-0.0297	-0.0042	0.4721			69.1740	
•	8.24	0.0	0.4-21	1-9426		-0.01+B	-0.0056	0.4413	0.1236	0.3177		
10 . 11	10.36	0.0	1.3766	1.5253	-0.0007 -0.0047	0.0143	-0.0064	0.3994	0.1259 0.1252	0.2897	1.6689	<del></del>
iż	14.64	0.0	1.8292	1.0426	0.0061		-0.0081	0.3941	0.1257	0.2684	0,5700	
13	16.77	0.0	2.2418	0.0505	0.0021	0.0275	-0.0084	0.3890	0.1261	0.2629	0.3727	
15	21.07	0.0	2.7512 3.2532	0.3986	0.0114	0.0014	-0.0085	0.3796	0.1252	0.2544		
16	-0.09	0.0	-0.9362	3.4519		-0.0280		0.6139	0.1249		-3,4872	
7.0												
						<del></del>			<del> </del>			<del></del>
									•			
			<u> </u>			<del></del>						
——												
							<del></del>					<del></del>
											<u></u>	
											·	
	<del></del>		<del></del>					<del></del>				

E	1 OF 1		L	ANGLEY R	SEARCH C			UNITA		IND TUNA	EL (UPWT)		
	1 OF 1		· · · · · · · · · · · · · · · · · · ·		<del></del>		1331FE 14	T ELLECIS	UNIN				
	TEST	PART	ACH RX10-	PHI	CONF	L DEL	1 DEL2	DELS DELA	TRANSITI	ON			
		43 2.	36 3.0	-90.0 B	2 + OF 36 0	<u>. 0</u> 2	0 0	20 0					
INT		BETA	CN	CLM	CY .	CLN	CLL	CA	CAB	CAF	KCP		
1	-4.08	0.0	-1.7019		-0.0013	-0.0088	-0.0060	0.8016	0.1504	0.6512	-2.7990		
3	-2.00	0.0	-1.3777 -1.2410	4.3782	0.0037	-0.0355	-0.0057	0.7462	0.1471	0.5991	-3.1779 -3.4203	<del></del>	
4	0.08	0.0	-1.0798	4.0147	-0.0030	-0.0190		0.6814	0.1455	0.5359	-3.7180	•	
5	1.10	0.0	-0.9054	3.7331	0.0031	0.0088	-0.0053	0.6558	0.1461	0.5097	-4-1232		
6	2.15	0.0	-0.7512	3.5436	-0.0048		-0-0042	0-6324	0.1478	0.4846	-4.7173		
8	4.23 6.33	0.0	-0.4172 -0.0673	3-1459	0.0060	-0.0170	-0.0040 -0.0036	0.5834 0.5369	0.1494	0.4340	-7.54 <b>85</b> -40.9241		
9	8,44	0.0	0.3247	2.3689	-0.0012	-0.0006	-0.0045	0.5017	0.1556	0.3461	7.3573	<del></del>	
10	10.59	0.0	0.7992	1-9454	0.0043		-0.0049	0.4739	0.1596	0.3143	2.4966		
11	12.75	0.0	1.3127	1.6930	-0.0051	0.0088	-0.0057	0.4558	0.1625	0.2933	1.2897		
<u>                                     </u>	14,93	0.0	1.8425	1.3993	0-0010_		0.0064_	0.4425	0.1639	0.2766	0.7540		
13	17.11	0.0	2.3+61	1.2448	-0.0080		-0.0072 -0.0072	0.4383	0.1649	0.2734	0.53 <b>06</b> 0.3339		
15	21.49	-0.01	3.4486	0.6693	0.0097	0.0204	-0.0074	0.4053	0.1689	0.2364	0.1941		
16	0.07	0.0	-1.0767	4.0205	0.0106		-0.0095	0.6811	0.1457	0.5354	-3,7272		
17	0.07	0.0	-1.0904	4.0366	0.0112	-0.0224	-0.0074	0.6820	0.1452	0.5368	-3,7020		
						· · · · ·		<del></del>				· · · · · · · · · · · · · · · · · · ·	
				<u>.</u>									
									<u>-</u>				
					· · · · · · · · · · · · · · · · · · ·							· · · · · · · · · · · · · · · · · · ·	
										<del></del>			
			<del></del>								·• · · · · · · · · · · · · · · · · · ·		
							•						
		<del></del>											

			<del></del>	ANGLEY HE	SEARCH C	ENTERINAS	A3	UNITA	RY PLAM :	IND TUME	FI (UPHT)			
AGE	1 OF 1	_	<u>-</u>			MARTIN M	ISSILE T	ALL EFFECTS	DATA					
HEET	1 OF 1					-		16.0						
							· · · · · · · · · · · · · · · · · · ·	···			····			
•	19000000													
		PART	ACH RXIO-					DEL3 DEL4	TRANSIT	ION				
			.63_3.0	-90.0 64	#UF 36 U	•0 Z	0 0	50 0	FIXE					
POINT	ALPHA	BETA	CN	CLM	CY	CLN	<u>CLL</u>	CA	ÇAB	CAF	XCP			
1	-3.79	0.0	-1.1019	2.7096		-0.0654		0.5245	0.0561		-2.4590			
- 5	-1.74	-0.01	-0.A177 -0.6855	2.4520	0.0304	-0.0414	-0.0090	0.4560	0.0572	0.3982	-2,9987 -3,3908		•	
_ Ă	0.30	-0.01	-0.5436	2.1866	0.0329	0.0234_	0.0098	0.4330	0.0585	0,3745	-4.0225			
5	1,32	0.0	-0.4057	5.0655		-0.0175		0.4112	0.0585		-5.0831			
🐫	2.36 4.39	-0.01 -0.01	-0.2677 0.0178	1.6625		_0.0378_ _0.0252		0.3919 0.3487	0.0585	0.3334				
é	6.43	-0-01	0.3335	1.3542		-0.0170	-0.0120		0.0579	0.2647	4.0604	•		
9	8.49	-0.01	0.6408	1-1711	0.0309	-0.0048	-0.0154	0.3089	0.0579	0.2510	1.8275		<del></del>	
10		0. <u>01</u>	0.9466	1.0679		-0.0505		<u> </u>	0.0580_	_0.2515	1.1202_			
15	12.60	-0.01 0.0	1.2465 1.5663	1.0251	0.0316	0.0103	-0.0152	0.3159 0.3216	0.0568	0.2591	0.82 <b>24</b> 0.6148			
- i3	16.74	-0.01	1.9140	0.8260	8850.0	0.0073	-0.0151	0.3272	0.0549	0.2723	0.4326			
14	18.80	-0.01	2.2709	0.6591	0.0389	-0.0057	-0.0137	0.3359	0.0541	0,2818	0,2902			
15	20.87			0.4489		0.0037			0.0541	0.2905	0.1683			
16	0.30	-0.01	-0.5535	5-1464	0.0333	-0.0237	-0,0097	0.4300	0.05/2	0.3728	-3,9692			
							<del> </del>							
				-					*******					_
		<u> </u>												
				<del></del>								<del></del>	·	
			<del></del> -											
													•	
_							···							_
							······································							
						-								_

## APPENDIX E TEST 5

												•	
	<del></del>	<del> </del>	LA	NGLEY HES	EARCH CENT	ER (NASA)	· · · · · · · · · · · · · · · · · · ·	UNITARY	PLAN WIR	O TUNNEL	(UPUT)		
<b>39</b> /	1 OF 1				MA	RTIN MISSILE SPLITTER	TAIL EF	FECTS DA	ITA .		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
HEET	1 OF 1					SPLITTER	PLATE D	ATA .			•		
			<del></del>								···		
		PART HAC	H RX10-6	CONF TRAN	SITION								
	- 5	2 1.50	1.0	F35 F1	AED								
POINT	ALPHA	CNF	CH	CB	xcef	YCPF							
i	-6.00	-0.2429		-0.0867		0.3569							
2	-4.00	-0.1525	0.0054	-0.0499	-0.0353	0.3272							
3	-3.00	-0.1089	0.0041	-0.0338	-0.0373	0.3104							
<u>-</u> -	-2.00	-0.0636	0.0033	-0.0187	-0.0523	0.2948		<del></del>	<del></del>		·		
6	-1.00	0.0197	0.0021 0.0011	0.0125	0.0574	0.1695 0.6345							
7	1.00	0.0015	0.0003	0.0266	0.0054	0.4325		·					
103	_2.00	0.1013	-0.0007	0.0424	-0.0066	0.4186							
9	3.00	0.1525	-0.0019		-0.0122	0.3856		-					
10	6.00		-0.0033	0.0757	-0.0166	0.3785							
12	8.00	0.3026 0.3940	-0.0063		-0.0209 -0.0225	0.3658 0.3596		•					
13	10.00		-0.0117	-6.1712	-0.0238	0.3464				<del></del>	<del></del>	····	<del></del>
14	12.00		-0.0148		-0.0254	0.3425							
15	14.00		-0.0183	0.2264		0.3356							
16	16.00		-0.0209		-0.0273	0.3302							
17	16.00	0.6303	-0.0229	0.2142	-0.0269	0.3225							
						-							
													. a .
			-		,								
					<u> </u>						<del></del>		
		•											
	<del></del> ;								<del></del>			<del></del>	
-													
						<del></del>							
			<del></del>								<del></del>	<del></del>	
						<del></del>				<del></del>			<del></del>
												•	
												<del></del>	

	OF 1		LA	NGLEY RES		ER(NASA) RTIN MISSIL	E TAIL EFFE	ECT'S DATA	WIND TUNNE	L(UPUT)		
EET 1	of 1					SPLITTE	A PLATE DAT	TA				
					<del></del>						· · · · · · · · · · · · · · · · · · ·	
	TEST	PART MAC	H PX10-6	CONF TRAN	SITION							<del>.</del>
	_ 5		1-6		XED							
OINT	ALPHA	CNF	CH	Cit.	* COS	YCPF				•		=
<u> </u>	-6.00	-0.1676	0.0063		-0.0373	0.4087	•					
5	-4.00	-0.1345	0.0050	-0.0498	-0.0371	0.3703						
3	-3.00	-0.0965	0.0039	-0.0348	-0.0400	0.360b 0.3464						
5		-0.043	0.0011		-0.0466	0.2634						
6	0.0	0.0161	-0.0004	0.0065	-0.0221	6.3591						
8	1.00	0.0546	-0.0018 -0.0031	0.0198	-0.0329 -0.0343	0.3626						
9	3.00	0.1475	-0.0043	U.0480	-0.0334	0.3765	<del></del>		<del> </del>		<del></del>	
10	4.00	0.1656	-0.0053	0.0615	-0.0321	0.3709						
11	6.00	0.2464	-0.0073		-0.0294	0.3568						
13	10.00	0.3231	-0.0089		-0.0274 -0.0266	0.347 <u>6</u> 0.3391	<del></del>					
14	15.00	0.4665	-0.0121	0.1561	-0.0260	0.3346						0 8 33
15	14.00	0.5380	-0.0136	0.1753	-0.0254	0.3258						
16	16.00	0.6106	-0.0154 -0.0167	0.1935 0.2115	-0.0 <u>252</u> -0.0247	0.3169		<del></del>		<del></del>	<del></del>	
18	20.00	0.7377	-0.0150	0.2276	-0.0244	0.3085		•				
19	22.00	0.8076	-0.0207		-0.0256	0.3001	<del></del>					
20	24.00	0.8769	-0.0231	0.2583	-0.0263	0.2946						
55	28.00	1.0044	-0.0276	0.2927	-0.0275	0.2914						
23	0.0	0.0162				0.3272				<del></del>		
24	0.0	0.0163	-0.0003	0.0050	-0.0163	0.3067	<del></del>		<del></del>		<del></del>	
			_									
								<del></del>				
								•				
						<del></del>		*				
					<del></del>							
		<del></del>			<del></del> -		·		<del></del>		<del></del>	
						<del></del>						

e£	1 OF 1		LA	NGLEY RES	EARCH CENT	RTIN MISSILE	TAIL EFFEC	TS DATA	WIND TUNNEL	(UPWT)		
EET	1 OF 1					SPLITTER	PLATE DATA					
					<del></del>				****	•		
	***	DARY MAC	H RX10-6	CONE THAN	ETSYAL.							<u> </u>
	5		2.5									
					200							
DINT	-6.00		CH	-0.0483	XCPF	YCPF 0.3873		<del></del>	<del></del>	<del></del>		
ż	-4.00	-0.0001	0.0031	-0.0297		0.3371						
3	-3.00	-0.0550	0.0021	-0-0170		0.3091						
_: _	-5.00	-0.0215	0.0011	-0.0059		0.2744		<u></u>				
3.	-1.00 0.0	0.0150	0.0003 -0.0009		0.0044	0.3400 0.3898						
7	1.00	0.0749	-0.0018	0.0272	-0.0240	0.3632					<del>,</del>	<del></del> -
	5.00	0.1084	-0-0027		-0.0252	0.3589				•		
10	3.00	0.1421			-0.025 <b>6</b> -0.0254	0.3540 0.3514						
11	6.00	0.2387	-0.0059	0.0820	-0.0248	0.3435	<del></del>			<del></del>		
12	8.00	0.2993	-0.0073	0.1013	-0.0245	0.3385						
13	10.00	0.3600			-0.0251	0.3342						
15	12.00		-0.0107		-0.0268	0.3227						
16	16.00	0.5461			-0.0268	0.3120						
17	18.00	0.6032	-0.0164	0.1680	-0.0271	0.3117						
18	20.00		-0.017A	0.2024	-0.0267	0.3045						
19 20	20.00		-0.0009 -0.0150		-0.0203	0.3794	•		•			
21	22.00		-0.0201		-0.0276	0.2987						
22	24.00		-0.0216	0.2320	-0.0275	0.2954						
23	26.00		-0.0235		-0.0275	0.2909						
24	28.00	0.7148	-0.0560	0.2040	-0.0285	0.2895		<del></del>			<del></del>	
		•										
<u>.                                    </u>												
								<del></del>	<del></del>	<del></del>	<del></del>	

		•									
										47	
E	1 OF 1		LA	NGLEY RES	EARCH CENT	ER (MASA)	UNITA	RY PLAN WIN	D TUNNEL (UP #1	<b>'</b> )	
ET	i of i					SPLITT	E TAIL EFFECTS				
											,
	1651	5 1.50	H WX10-6	CONF TRAN	XED XED						
IMT	ALPHA	CNF	СН	CB		YCPF					
1	-6.00	-0.2775	-0.0056	-0.1167	0.0202	0.4205	<del></del>	<del></del>	<del></del>		
2	-4,00	-0.1579	-0.0036	-0.0652	0.0227	0.4129					
3	-3.00 -2.00	-0.1129 -0.0517	-0.0027	-0.0423 -0.0218	0.0241	0.3747					
5	-1.00	-0.0031	0.0016	0.0019	-0.5269	-0.6129			······		
6	1.00	0.0537 0.1065	0.0037	0.025 <u>3</u> 0.0+76	0.0681	0.4469					
8	2.00	0.1636	0.0076	0.0713	0.0466	0.4358					
9	3.00	0.2188	0.0086	0.0952	0.0395	0.4351					
<u>0</u>	6.00	0.2762	0.0094	0.1191	0.0341	0.431 <u>2</u> 0.4310					
2	8.00	0.5075	0.0093	0.2193	0.0182	0.4321					
3	10.00	0.6224	0.0076	0.2668	0.0122	0.4287					
5	14.00	0.8418	0.0018	0.3530	0.0021	0.4193				-	
6	16.00	0.9460	-0.0011	0.3876	-0.0012	0.4097				<del></del>	<del></del> _
									****		
					<del></del>				<del></del>		
					<del></del>						
				<del></del>			7				
									<del> </del>		
				<u> </u>							
	·										

PAGE	1 OF	1	L/	MGLEY RES	EARCH CEN	ER(NASA) RTIN MISSILE_TAIL_E	UNITARY PLAN I	WIND TUNNEL (UPUT)	
	1 OF	i				SPLITTER PLATE	DATA		
		•	<del></del> -	·· <del>···</del>			<del></del>		<del> </del>
	TES	T PART MAC			SITION				
POINT	ALPHA		CH	Cu		YCPF			
	-6.00			-0.0851		0.4524	<del></del> .		
2	-4.00		0.0011			0.3311			
3	-3.00		0.0009	-0.0356		0.2770			
	-5.00		0.0005	-0.0180	0.0065	0.2140	<del></del>		
5	-1.00		0.0004		-0.0085	0-0154	•		
	$-\frac{0.0}{1.00}$	-0.0071 0.0313	0.0002	0.0341	-0.0329	-2.76 <u>76</u> 1.0695		<del></del>	
<u>, , , , , , , , , , , , , , , , , , , </u>	5.00		-0-0002	0.0341	-0.0034	0.7529	·		
- 6	3.00		-0.0000	0.0707		0.6296			
10	4.00		-0.0009	0.0592	-0.0055	0.5766			
<del>- 11</del> -	6.00		-0.0015		-0.0061	0.5226			
12	8.00		-0.0024	0.1647	-0.0073	0.5006			
13	10.00	0.4205	-0.0036	0.2028	-0.0085	0.4823			
14	12.00		-0.0047	0.2391	-0.0092	0.4702			- <u></u>
15	14.00		-0.005B	0.2729	-0.0097	0.4580			
16	16.00		-0.0073	0.3073	-0.0107	0.4497			
17	16.00		-0.0093	0.3389	-0-0151	0.4403			
18	_ 20.00		-0-0117	0.3691	-0.0136	0.4329			
19	_ S5.00	-0.0013	-0.0151	0.3982		0.4227			
50	22.00		-0.0002		-0.1795 -0.0141	0.4075	<del></del>		
55	24.00		-0.0166	0.4206	-0.0162	0.4141			
23	26.00		-0.0184		-0.0170	0.4257	· · · · · · · · · · · · · · · · · · ·		
24	28.00		-0.0205			0.4262			
							<del></del>		
						•	•		
						<del></del>			
					<del></del>				
						-			
						<del></del>			<del></del>
									_
								<del></del>	

<del></del>			L	NGLEY RES	EARCH CENT				WIND TUNNEL	(UPWT)		
	l OF					SPLITTE	E TAIL EFFEC R PLATE DATA	IL DATA	<del></del>	· <del></del>		
	V222							<del> </del>			<del></del>	
		u societies e	- 10	Transaction	Villable							
				CONF TRAN		•						
		7_2.10		F34 F1	XED		<del></del>			<del></del>	<del></del>	
POINT	ALPHA	CNF	CH	CB		YCPF						
1 2	-6.00	-0.1484 -0.1013	0.0033	-0.0647 -0.0320	-0.0220	0.4360 0.3159						
-3-	-3.00	-0.0717	0.0016		-0.0217	0.2497						
•	-2.00	-0.0377	0.0010		-0-0560	0.0955			<del></del>	···		
5	-1.00	-0.0035 0.0307	0.0005	0.0093	-0.1333 0.0	0.7394						
— <del>ў</del> —	1.00	0.0571	-0.0005		-0.0082	0.4567			<del></del>		<del></del> -	<del></del>
	2.00	0.0942	-0.0010	0.0529	-0.0107	0.5616						
10	3.00	0.1329	-0.0015	0.0671	-0.0111 -0.0119	0.5049						
-ii	6.00	0.2360			-0.0138	0.4754	<del></del>		<del></del>		•	
_ <u>12</u>	8.00	0.3094	-0.0045		-0.0146	0.4638						
13	10.00	0.364B	-0.0054 -0.0064	0.1750	-0.0141 -0.0139	0.4548						
15	14.00	0.5344		0.2362	-0.0135	0.4420						
	16.00		-0.0084	0.2654	-0.0138	0.4349			<del> </del>	<del></del>		<del></del>
17	18.00	0.6943	-0.0102	0.2928	-0.0147 0.0023	0.4217						
19	18.00	0.6908	-0.0096	0.2942	-0.0140	0.4259		•				
50_	20.00				-0.0157	0.4294					<u> </u>	<u>:</u>
51	22.00				-0.0170 -0.0187	0.4161						
23	26.30	0.9731	-0.0191	0.4071	-0.0197	0.4184						
24	28.00	1.0477	-0.0224	0.4321	-0.0214	0.4124	<del></del>					
							•					•
						<del>-</del>						
									•			
						•		<del>.</del>				
											_	
		<del></del>		,								
					<del></del>	<del></del>			<del></del>			

	1 OF 1		LA	NGLLY RES	EARCH CENT	ER(VASA)	TAIL EFFECT	ARY PLAN W	IND TUNNEL (UPUT)		
: E T	1 OF 1					PALTITER	PLATE DATA			1	
				···					<del></del>	·	
	7567	DADT MAC	M OYIA-A	CUNF TRAN	STTION				·		
	5	8 1.50	1.8	F31 F1	xED						
ALMI	ALPHA	CNF	СН	Ca	209	F YCPF					
177		-0.1335			0.0425	0.2464	<del></del>		<del></del>		
2	-4.00	-0.079e	-0.0033	-0.0125	0.0410	0.1570					
3	-3.00	-0.0>55	0.0016	-0.0060	-0-051	0.1081			•		
		-0.0254	0.0017	0.0068	-0.0674	-0.2677	·		<del></del>		
6	0.0	-0.0093	0.0035	0.0123	-0.4098	-1.3226					
7	1.00	0.0066	0.0057	2020-0	0.8350	2.9706					
9	3.00	0.0202	0.0075	0.0288	0.3735	1.4257 0.8137					
10	4.00	0.0705	0.0105	0.0478	0.1481	0.6742					
11	6.00	0.1273	0.0122	0-0741	0.0959	0.5821					
<u> 12</u> 13	10.00	0.1695	0.0125	0.1391	0.0661	0.5493	·				
i	12.00	0.3382	0.0095	0.1681	0.0281	0.4970					
15	14.00	0.4159	0.0069	0.1988	0.0166	0.4780					
16	16.00	0.4910	0.0046	0.2281	0.0093	0.4646	<del></del>	<del></del> -		<del></del>	
iė	20.00		-0.0019	0.2655	-0.0030	0.4458					
19	22.00		-0.0077	0.3178	-0.0108	0.4441	•		· · · · · · · · · · · · · · · · · · ·		
20	24.00	0.7946		0.3443	-0.0146	0.4332					
51	26.00	0.9399		0.3673	-0.0175 -0.0195	0.4213 0.4177					
23	0.0	0.0039		0.0083	1.0171	2.1202	<del></del>		·	-	
				100941							
		<del></del>				<del></del>			·		
	<del></del>	<del></del> -					<del></del>		<del></del>		
							•				
							<del></del>				
								``			
				<del> </del>		<del></del>		<del></del> ;	<del></del>		
								· ',			

AGE	1 of 1		Ļ	MGLEY RES	EARCH CEN	TER(NASA) Artin Miss	UNITARY LE TAIL EFFECTS D	PLAN WIND TUNNEL (U)	ודשי	
HEET	1 OF 1			•		SPLIT	TER PLATE DATA		<u> </u>	
		PART MAC	H RX10-6	CONF TRAM	SITION				<del></del>	
	5	9 1.80	1:0,	F31 F1	XED				<del></del>	
POINT		-0.1174	CH	CR_	XCP					
2	-6.00 -4.00	-0.1174	-0.0037	-0.0449	0.0311	0.38 <b>25</b> 0.2722				
-3-	-3.00	-0.0756	-0.0316	-0.0476	0.0206	0,1005	······································			
	-2.00	0.0407	-0.0004	-0-0046	0.0096	0-1130		·		
2	-1.00 0.0	-0.0213 -0.0068	0.0008	0.0009	-0.0365 -0.1830	-0.0423 -1.1618				
<del>- 7</del>	1.00	0.0101	0.0020	0.0141	2005	1.3960	·			
1183	2.00	0.0293	0.0033	0.0208	0.1115	0.7099		· ·		
9	3,00	0.0485	0.0044	0.0287	0.0898	0.5910				
10	4 <u>.00</u>	0.0676	0.0051	0.0411	0.0748	0.5361				
iż	8.00	0.1797	0.0054	0.0908	0.0303	0.5053 .				
13	10.00	0.2433	0.0043	0-1176	0.0176	0.4842				
14	12.00	0.3023	0.0021	0.1460	0.0069	0.4830				
15 16	14.00	0.3670	-0.0002 -0.0026	0.1690	-0.0006	0.4605				
ijŤ.	18.00	0.4976	-0.0064	0.2100	-0,0128	0.4361			<del></del>	
_16_	50.00	0.5534	-0.0106	0.2459	-0.0191	0.4443				
19	22.00 24.00	0.6191	-0.0138	0.2685	-0.0224	0.4337 0.4272				
51	26.00	0.7504		0.3117	-0.0266	0.4154			<del></del>	
22	28.00	0.8096	-0.0233	0.3367	-0.0291	0.4206				
23	0.0	-0.0149	0.0014	0.0115	-0.0940	-0.7718				
24	0.0	-0.00%	0.0013	0.0099	-0.1377	-1.0313				
•										
							<del></del>	<del></del>		
				•			•			
						·				
					•					
	<del></del>			···-						
								····		

	<del></del>	<del>. , ;</del>				•		<del></del>	· · · · · · · · · · · · · · · · · · ·	10 1	er i segre j		٠,٠
	•	•						,	·		<del></del>		
AGE	1 of 1		LA	NGLEY RESI	LARCH CEN	TER (MASA) ARTIN_MISS	ILE TAIL EFF	ECTS DATA	WIND TUNNE				
HEET	1 OF 1					SPLIT	TER PLATE DA	ITA ·					<u>.                                    </u>
	TEST	PART MAC	H RX10-6	CONF TRANS	51110w		<del></del>			··· <u>·</u>	· 		
	5	10 2.10	2.5	F31 F1	KED			<del></del>		<del></del>		<del></del>	
<u>POINT</u>	ALPHA	CNF	CH	cg	4CP	FYCPF							
Š	-4.00	-0.0979	-0.0012	-0.0303 -0.0102	0.0134	0.3095 0.1753							
3	-3.00	-0.0+15	0.0001	-0.0039	-0.0019 -0.0375	0.0948							
5	-1.00	-0.0139	0.0012	0.0114	-0.0895	-0.8201							
7	1.00	0.0093	0.0019	0.0220	0.2007	1,5914 0,687 <b>5</b>							
8	3.00	0.0466	0.0033	0.0324	0.0701	0.6953							
10	4.00	0.0988	0.0035	0.0-20 0.0515	0.0354	0.4034 0.5213					-		
11	6.00	0.1454	0.0026	0.0756 0.0985	0.0177	0.5199							
13	10.00	0.2585	-0.0011	0.1211	-0.0042	0.4685					·		_
15	12.00		-0.0037	0.1451	-0.0120	0.4628							
16	16.00	0.4198	-0.0094	0.1890	-0.0224	0.4502							
17	18.00 20.00		-0.0128		-0.0266 -0.0302	0.4402							
20	22.00		-0.0194		-0.0325 -0.0332	0.4251							
51	26.00	0.7121	-0.0245	0.2965	-0.0344	0.4164							_
23	28.00		-0.0271 0.0019		-0.0351 0.2778	2.4714		<del></del>	<del></del>				
													_
<del></del>													
			<del></del>										
			·										
							· <del></del>						_
							· · · · · · · · · · · · · · · · · · ·						_
						•				<u>.                                    </u>			
				<u> </u>									
											<del></del>	<del></del>	

PAGE	1 OF 1		LA	NGLLY HESE		ER(NASA) ARTIN MISSILE			IND TUNNEL CUPE	T)	<del></del>
	1 00 1				<u> </u>	SPLITTER	PLATE DATA			-	
								<del></del>			
	TEST 5			CONF TRANS				,			
		11 1.50	_ 1.00	<u> </u>	TED				<del></del>		
POINT	ALPHA	CNF	CH	CR		YCPF					
1	-6.00	-0.0690 -0.0517	-0.0151 -0.0107	-0.0338 -0.0240	0.2188	0.4899					
- 5	-3.00	-0.0317	-0.0168	-0.0174	0.2194	0.5613					
•	-5.00	-0.0186	-0.0026	-0.0094	0.1398	0.5054					
5	-1.00	-0.0006		-0.0043	-2.5000	7-1667					
- 5	1.00	0.0174	0.0061	-0.0026 0.0034	0.3506	-0-1494 0-1043	<del></del>	<del></del>	<del></del>		
ė	2,00	0.0476	0.0103	0.0034	0.3160	0.2458					
	3,00	0.0652	0.0185	0.0226	0.2837	0.3466			<del></del>		
10	4.00	0.0934	0.0225	0.0303	0.2409	0.3244		<del></del>	<del></del>		
11	6.00	0.1368	0.0294	0.0541	0.2149	0.3955		•	•		
- <u>12 -</u> -	10.00	0.1990 0.2726	0.0346	0.0823	0.1739 0.1401	0.4136 0.4087				<del></del>	
14	12.00	0.3440	0.0399	0.1-66	0.1160	0.4262					
15	14.00	0.4164	0.0411	0.1771	0.0987	0.4253					
16	16.00	0.4886	0.0414	0.2143	0.0847	0.4386					· · · · · · · · · · · · · · · · · · ·
17	16.00	0.5611	0.0414	0.2491	0.0738	0.4439					
- <u>i</u> -	-22.00	0.7198	0.0397	0.3187	0.0552	0.4428					
20	24.00	0.8006	0.0387	0.3517	0.0483	0.4393		•			
51	56.00	0.8661	0.0363	0.3866	5440.0	0.4464		•			
53	28.00	0.9374	0.0378	-0.0002	0.0403	0.4403 -0.0116		<del></del>	<del></del>	<del></del>	<del></del>
23	***	0,01,5	00000	-0,000	013003	-040750					
											-
				<del> </del>		·					
	10.00										
											-
									<del></del>		
		<del></del>	·			·					

GE_	1 OF 1		LA	NGLEY RESE	ARCH CEN	ARTIN MISSI	UNITARY PLAN WIND LE TAIL EFFECTS DATA	TURNEL (UPST)	
EET	1 OF 1					SPLITT	ER PLATE DATA	•	
	1851	12 1.80	H RX10-6	CONF TRANS	ITION				
DINT	ALPHA	CNF 0.0752	CH	CH	0.1609	7CPF		<u></u>	
ż		-0.0540	-0.0096	-0.0297	0.1778	0.5500			
3	-3.00	-0.0357	-0.0067	-0.0214	0.1677	0.5994		···	
<u></u>	-2.00 00.5-	-0.0146	-0.0036	-0.0139	0.2432_ 0.2222	0.939 <u>2</u> 4.1111			
6	0.0	0.0144	0.0023	-0.0031	0.1597	-0.2153			
7	1.00	0.0301		0.0026	0.1827	0.0864			
-	4.00	0.0457	0.0090	0.0083	0.1762	0.1816	<u> </u>		
10	6.00	0.1319	0.0194	0.0474	0.1471	0.3594			
11	8.00	0.1695	0.0236	0.0709	0.1245	0.3741			
.1 <u>2</u>	10.00	0.2470	0.02 <u>71</u> 0.0299	0.1000	0.1097	0.4049			
14	14.00	0.3715	0.0318	0.1552	0.0856	0.4178			
15	16.00	0.4332	0.0326	0-1663	0.0753	0.4301			
16	18.00 20.00	0.5006	0.0328	0.2145	0.0655_ 0.0578	0.4285			
18	22.00	0.6287	0.0316	0.2715	0.0503	0.4316			
19	24.00	0.6947	0.0300	0.2999	0.0432	0.4317	•		
20	26.00	0.7611	0.0279	0.3556	0.0367	0.4312			
55	0.0	0.0141	0.0026	-0.0019	0.1544	-0.1348			
53	3.00	0.0635	0.0123	0.0166	0.1937	0.2614	•		
								· · · · · · · · · · · · · · · · · · ·	•
								-	
						<del></del>			- <del></del>
								-	
							·		

	1 07 1		LA	NGLEY RESE		ARTIN MISSI	LE TAIL EFFECTS DAT	LAN WIND TUNNEL (UPWT)	
HEET	1 0 1					SPLITT	A PLATE DATA		
							<del></del>		•
		PART HAC	H RE10-6	CONF TRANS	ITION		<del></del>		
	5	13 2.16	2.5	F32 F11	KED				
POINT	ALPHA	CNF	CH	C#		F YCPF			
5	-4.00	-0.0356	-0.0062	-0.0200	0.1152 0.1208	0.4814 0.5618			
3	-3.00	-0.0176	-0.0021	-0.0122	0.1193	0.6932	<del></del>		
<u>_</u>	-5.00	-0.0016 0.0144	0.0086	0.0065 -0.0016	-0-1875 0-1806	4.0625 -0.1111		<del></del>	
6	0.0	0.0205	0.0028	0.0047	0.1684	0.1649			
7	1.00	0.0445	0.0070	0.0113	0.1573	0.2539			
- 8	3.00	0.0406	0.0091	0.0197	0.1504	0.3256	<del></del>		<del></del>
10	4.00	0.1648	0.0122	0.0377	0.1164	0.3597			
11	6.00	0.1511	0.0147	0.0603	0.0973	0.3991			
-13 	10.00	0.2601	0.0168	0.0845	0.0826	0.4152			
14	12.00	0.3168	0.019B	0.1355	0-0625	0.4277			
15	14.00	0.3754	0.0212	0.1629	0.0565	0.4339 0.4363			
17-	18.00	0.4926	0.0241	0.2144	0.0489	0.4352			
-18	_ 50.00_	0.5480	0-05+6	0.2394	0.0454	0.4369			····
19 20	22.00	0.6052	0.0248	0.2660	0.0410	0.4395			
5)	26.00	0.7262	0.0228	0.3154	0.0314	0.4343			<del></del>
53	28.00 0.0	0.7857	0.0208	0.3391	0.1692	0.4316	<del> </del>		<del></del>
24	0.0	0.0263	0.0049	0.0063	0.1863	0.2395			
							· · · · · · · · · · · · · · · · · · ·	•	
							<del></del>		<del></del>
						<del></del>	······································		
					····		<del></del>		

	1 00 1		LA	NGLEY RES	EARCH CENT	RTIN HISSILE	TAIL EF	FECTS DATA	AN WIND TUR	MEL (UPUT)		
HEET	1 OF 1					SPLITTER	PLATE D	ATA -				
			<del></del>		<del></del>							
	TEST	PART HAC	H RX10-6	CUNF TRAN	SITION		1					
		14 1.50	1.8	F36 F1	XED					<del></del>	<del> </del>	
POINT	ALPHA	CNF	CH	CA	XCPI	YCPF						
		-0.0541	0.0051	-0.0230	-0.0937							
	-4.00	-0.0375	0.0041	-0.0189		0.5048						
4	-2.00	-0.0075	0.0023		-0.3111	1.0267						
5	-1.00	0.0009	0.0017	-0.0046	1.9259	-5.1111						
6	0.0	0-0117	0.0011	-0.0011	0.0969	-0.0940						
. 6	1.00	0.0281	0.0003	0.0041	0.0095	0.1459						
9	3.00	0.0605	-0.0015	0.0156	-0.0242	0.2579						
10	4,00	0.0741	-0.0023	0.0216		0.2915						
11	6.00	0.1141	-0.0039 -0.0064	0.0354	-0.0345 -0.0369	0.3103						
13-	10.00	0.2136			-0.0387	0.2967			· · · · · · · · · · · · · · · · · · ·			
14	12.00	0.2709			-0.0411	0.2831						
15	14.00	0.3669		0.0957 0.1118	-0.0412 -0.0398	0.2927			•			
17	18.00		-0.0174		-0.0383	0.2845			<del></del>			
18	20.00	0.5131	-0.0197	0.1462	-0.0385	0.2849						
19	20.00		-0.0199		-0.0386	0.2615						
21	27.00		-0.0255		-0.0396	0.2812				···		
55	26.00	_	-0.0283	0.1944		0.2807			•		_	
53	28.00		-0.0311		-0.0413	0.2839						
24	0.0	0.0143	0.0013	-0.0030	0.0886	-0.2098	<del></del>				<del></del>	
£ 3	•••	0.0143	0.0011	-0.0020	0.0102	~0013/5				•		
					<del></del>							
											-	
_										··		<del></del> -
											· · · · · · · · · · · · · · · · · · ·	
				•	·				·			_

ويربها ويعين يالهم الماني فالمناس والمناف والمناف والمناف والمناف والمنافي والمناف والمناف والمناف والمناف

AEDC-TR-75-125

.. ..

LANGLEY RESEARCH CENTER (NASA) UNITARY PLAN WIND TUNNEL (UPWT)

SPLITTER PLATE DATA

MARTIN MISSILE TAIL EFFECTS DATA

PAGE 1 OF 1

SHEET 1 OF 1

			LA	NGLEY RES		TER (NASA)			AN WIND TUNN	EL (UPIT)		
	1 OF 1				le,	ARTIN MISSILE	PLATE DA					
EEI .						SPLITTER	PLAIE DA	IA				
							~				·	
		****			10000		· · · · · · · · · · · · · · · · · · ·					
	1651	PART MAC	# RX10-6	CUMP THAN	SITION							
	?				nco			<del></del>		<del></del>		
INT	ALPHA	CNF	CH	CH	KCP	FYCPF						
1	-6.00	-0.0381		-0.0210		0.5512						
<u>2</u>	-4.00	-0.0238	0.0026	-0.0150	-0.1092	0.6303						
3	-3.00 -2.00	-0.0115	0.0019	-0.0101 -0.0062	-0.1681 1.4815	0.8783				•		
<del>-</del>	-1.00	0.0136	0.0005	-0.0025	0.0144	+0.1799				<del></del>		
6	0.0	0.0264	-0.0007		-0.0253	6.1212						
7	1.00	0.0366	-0.0011	0.0070	-0.0310	0.1913						
8	2.00	0.0506	-0.0017	0.0121	-0.0341	0.2382						<u>-</u>
9	3.00	0.0555	-0-0021	0.0176	-0.0319 -0.0307	0.2635						
1	6.00	0.1214	-0.0027	0.0218		0.2506			<del></del>	<del></del>		
iż	8.00	0.1020	-0.0055		-0.0327	0.2809						
13	10.00		-0.0017		-0.0373	0.2776	<del></del>					<del></del>
14	12.00	0.2517	-0.0087	0.0590	-0.0344	0.2741						
15	14.00	0.2954	-0.0098	0.0815	-0.0331	0.2754		· <del>-</del>				
<u> 1</u> 6	16.00	0.3449	-0.0117	0.0949	-0.0340	0.2752						
17 18	18.00	0.3420	-0.0138 -0.0159	0.1089	-0.0352 -0.0359	0.2778 0.2803						
19	22.00		-0.0182			0.2846	<del></del>					
20	24.00	0.5437	-0.0201	9-1557	-0-0370	0.2864						
51	26.00	0.5965		0.1705	-0.0368	0.2858					<u> </u>	
22	28.00	0.6496	-0.0238	0.1645	+0.0366	9.2840						
23 24	0.0 10.00		-0.0006 -0.0077		-0.0246	0.11 <b>89</b> 0.2764						
	10.00	0.2077	-0.0017	0.0314	-0.03/2	V 0 2 1 5 4			<del></del>			<del></del>
						<del></del>	🕶			<del> </del>	<del></del>	<del> </del>
							-					
										•		
		·				<del></del>	<del></del>					
									•	<del></del> .		
							-					
								· · · · · · · · · · · · · · · · · · ·				

. ...

AGE	1 OF 1		LA	NGLEY RESE	ARCH CENT	RTIN MISSILE	UNITARY PL	AN WIND TUNNE	(UPWT)	
HEET	1 of 1					SPLITTER	PLATE DATA			
-	TEST 5	17 1-50		CONF TRANS	SITION KED		-			
POINT	ALPHA	-0.1463	-0.0286	C9	0.1955	9.4621	<del></del>		<del></del>	
ż	-4.00	-0.0546	-0.0176	-0.0362	0.2080	0.4515	_			
3	-3.00	-0.0510	-0.0110		0.2157	0.5902	-			
4	-2.00	-D.0191	-0.0055	-0.0100	0.1152	0.5236				
5	-1.00	0.0099	0.0033	-0.0074		-0.7475				
\$	1.00	0.0424	0.0109	0.0054 0.0166	0.2571	0.1274 0.2538				
8	2.00	0.0936	0.0221	3.0261	0.2361	0.2788				
9	3.00	0.1314	0.0283	0.0417	0.2154	0.3174				
10	4.00	0.1536	0.0340	0.0597	0.2214	0.3887				
11	6.00	0.2358	0.0417	0.0886	0.1768	0.3757				
15	8.00	0.3023	0.0482	0.1245	0.1594	0.4118				
13	10.00	0.3849	0.0528	0.1597	0.1356	6.4149		•		
15	12,00	0,5452	0.0539	0.1979	0.1186	0.4354				
16	16.00	0.6308	0.0520	0.2760	0.0824	0.4375	,			
17	18.00		0.0491	0.3160	0.0687	0.4423				
18	50.00	0.7967	0.0463	0.3531	0.0581	0.4432				
19	55.00		0.0431	0.3907	0.0497	0.4502				
50	26.00	1.0181	0.0409	0-4276	0.0429	0.4487	<del></del>		<del></del>	
55	28.00	1.0996	0.0318	0.4879	0.0289	0.4437				
23	0.0	0.0432	0.0099	0.0030	5622.0	0.0694				
24	0.0	0.0463	0.0102	0.0014	0.2112	0.0290				
							•			
						<del> </del>	<del></del>			<del></del>
									<del></del>	
						. <del> </del>		····		
								-		
			-							

HEET	5 ALPHA	T PART MAC				ARTIN MISSILI SPLITTE		PECIS UALA			<del> </del>
	TES 3	T PART MAC					R PLATE D	ATA .			
P01NT	5 ALPHA	_									
PO1NT 1 2	5 ALPHA	_									-
PO1NT 1 2	5 ALPHA	_	H RX10-6	CONF TRAN	SITION				<del>-</del>		
POINT 1 2				F11 F1							
1 2		CNF	Ch	£							
<u> 2</u>	-6.00		-0-0147	C# C#	0.0987	7 YCPF 0.5165					
	-4.00		-0.0099	-0.0509	0.1159	0.5960					
3	-3.00		-0.0066	-0.0356	0.1419	0.7656					
	-2.00		0.0036	0.0247	0.1593	1.0929					
5	-1.00		-0.0007	-0.0155	-0-1061	-2.3485					
<del>-                                    </del>	0 <u>-0</u>	0.0545	0.0026 0.0055	0.0061	0.0730 0.1009	-0.177 <u>0</u> 0.1119	~		<del></del>		<del> </del>
á	2.00		0.0055	0.0178	0.1054	0.2132					
9	3.00		0.0117	0.0277	0.0993	0.2351					
10	4.00		0.0143	0.0454	0.1013	0.3215					
11	6.00		0.0190	0.0743	0.0907	0.3548					
15	8.00		0.0238	0.1055	0.0858_	0.3803					
13	10.00		0.0289	0.1368	0.0837	0.3962					
15	12.00		0.0337	0.1726	0.0816	0.4161					
16	16.00		0.0396	0.2329	0.0713	0.4195					
17	18.00		0.0407	0.2629	0.0657	0.4246		<del></del>	<del></del>		
18	20.00		0.0404	0.2951	0.0591	0.4317					
19	22.00		0.0386	0.3224	0.0515	0.4306					
20	24.00		0.0351	0.3564	0.0431	0.4377					
51	26,00		0.0308	0.3862 0.4157	0.0348	0.4364					
53	<del>-                                 </del>	0.0451	0.0044	-0.0023	0.0976	-0.0510	<del></del>	<del></del>	<del></del>		
24	0.0	0.0402	0.0036		0.0896	-0-0771					
		<del></del> -	· · · · · · ·			<del></del>					<del></del>
											······································
	•										
									<del></del>	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·

AGE	1 OF		LA	NGLEY RESI	EARCH CENTE	R(NASA) ITIN HISSILE			WIND TUNNEL (U	Pal)	
	1 OF 3						PLATE DAT				
				<del></del>		·		<del></del>	<del></del>		
				•							
		PART MAG	H RX10-6	CONF TRANS							
	5	19 2.10	2.5	F11 F1	KED			<del></del>			
THIO	ALPHA	CNF	Сн	Ce	ICPF	YCPF					
1	-6.00		-0.0054	-0.0558	0.0557	0.5759			· · · · · · · · · · · · · · · · · · ·		
2	-4.00	-0.0399	-0.0037	-0.0313	0.0927	0.7845					
3	-3.00	-0.0174	-0.0023	-0.0208	0.1322	1.1954					
	-2.00	0.0089	0.0006_ 0.0011	-0.0097	0.0353	1.0899 0.0288		<del></del>	<del></del>		
6	0.0	0.0537	0.0026	0.0097	0.0521	0.1806					
	1,00	0.0002	2400.0	0.0190	0.0524	0.2369			<del></del>		
8	2.00	0.1101	0.0059	2460.0	0.0536	0.3106					
9 -	3.00	0.1290	0.0065	0.0423	0.0504	0.3279					
10	4.00	0.1553	0.0074	0.0550	0.0476	0.3542			<del></del>		
11	6.00	0.2159	0.0091	0.0835	0.0421	0.3868 0.4087					
13-	10.00		0.0126	0.1429	0.0369	0.4184					
i÷	12.00	0.4022	0.0146	0.1678	0.0363	0.4172					
15	14.00		0.0171	0.2016	0.0370	0.4364					
16	15.00	0.5301	0.0205	0.2296	0.0387	0.4331					
17 18	18.00	0.6022	0.0262	0.2544	0.0397	0.4225					
19	22.00 00.05			0.3157	0.0391	0.4263	<del></del>				·
20	24.00		0.0257	0.3438	0.0324	0.4337					
21	26.00		0.0246	0.3713	0.0289	0.4366					
55	28.00		0.0236	0.3963	0.0256	0.4326					
23	0.0	0.0537	0.0031	0.0097	0.0577	0.1806					
		<del></del>							<del></del>	<del> </del>	_ <del></del>
		<del></del>	-								
								•			
	<del></del>		<del></del>			<del></del>	<del></del>			<del></del>	<del></del>
									<del></del>		

	1 OF 1		LA	GLEY RESI	EARCH CENT	ER (NASA)	UNITARY PLAN WIND TUNNEL (UPWT)	
	1 OF 1			•		SPLITTER (	TAIL EFFECTS DATA PLATE DATA	
						· — —		
		PART MAC 20 1.50						
POINT,	ALPHA -6.00	-0.1619	-0.0131	-0.065A	XCPF 0.0812	0.4064		
2	-4.00	-0.0929	-0.0081	-0.0385	0.0871	0.4144	· · · · · · · · · · · · · · · · · · ·	
3		-0.0641 -0.0247			0.0655	0.4119		
<u> </u>		-0.0006	0.0055	-0.0043		7.1667		<del></del>
6	0.0	0.0343	0.0055	0.0013	0.1610	6.0379		
7	2.00	0.0580	0.0089 0.0128	0.0148	0.1529	0.2552		
9	3.00	0.1263	0.0159	0.0+01	0-1256	0.3175		
10	6.00	0.1658	0.0223	0 <u>.05</u> 33_ 0.0889	0.1107 0.0911	0.3215	<del></del>	
15	8.00	0.3211	0.0239	0.1189	0.0741	0.3703		
13	10.00	0.4136	0.0239	0.1582	0.0577	0.3823		
15	14.00	0.5565	0.0226	0.1453	0.0455	0.3943	<del></del>	<del></del> -
16	16.00	0.6587	0.0162	0.2635	0.0246	0.4000		
17	18.00	0.7469	0.0124	0.2938	0.0166	0.3934		
<u> 18</u>	_ 55°00 _ 50°00	0.9082	0.006B_ 0.0019	0.3257_ 0.3560		0.3901		
20	24.00	0.9426	-0.0039	0.3781	-0.0039	0.3809		
51	26.00	1.0685	-0.0122	0.4012	-0.0112 -0.0157	0.3686		
23	0.0	0.0342	0.0055	0.0013		0.0380		<del></del>
2000	540,740	annica (	3104 1004.0	0.00	- 113974			
				<u>.</u>	······			
						· · · · · · · · · · · · · · · · · · ·		
		<del> </del>		<del></del>				

E 1 OF 1	LANGLEY RESEARCH CENTER (NA MARTIN	ASA) UNITARY PLAN WIND TUNNEL(UPWT) MISSILE TAIL EFFECTS DATA
ET 1 OF 1		SPLITTER PLATE DATA
	RX10-6 CONF TRANSITION 1.8 F15 F1XED	
INT ALPHA CNF 1 -6.00 -0.1277	CM C3 ACPF YCF	
2 -4.00 -0.0830	-0.0047 -0.0457 0.0572 0.55	506
	-0.0033 -0.0317 0.0629 0.59 -0.0011 -0.0240 0.0595 1.31	
<u> </u>	-0.001 <u>1 -0.02</u> 40 0.0595 <u>1.3</u> 1 0.0005 -0.0132 0.0907 -2.20	
6 0.0 0.0306	0.0019 -0.0024 0.0635 -0.01	784
7 1.00 0.0604 8 2.00 0.0850	0.0033 0.0068 0.0554 0.13 0.0050 0.0152 0.0586 0.13	
9 3.00 0.1145	0.0664 0.0267 0.0557 0.2	
0 4.00 0.1443	0.0072 0.0405 0.0501 0.20	
1 6.00 0.2090 2 A.00 0.2896	0.0086 0.0086 0.0413 0.3 0.0089 0.0986 0.0309 0.3	
3 10.00 0.3597	0.0085 0.1293 0.0236 0.3	595
4 12.00 0.4303 5 14.00 0.5014	0.0074 0.1576 0.0172 0.3 0.0055 0.1882 0.0110 0.3	
6 16.00 0.5730	0.0037 0.2141 0.0064 0.3	
7 18.00 0.6343	0.0015 0.2386 0.0023 0.3	
8 20.00 0.7056 9 22.00 0.7717	-0.0012	
24.00 0.8395	-0.0086 0.3137 -0.0102 0.3	737
	-0.0127 0.3339 -0.0140 0.3 -0.0173 0.3559 -0.0179 0.3	
3 0.0 0.0303	0.0022 -0.0024 0.0719 -0.0	
<del></del>		
		,
	<del></del>	

GF	1 OF 1		LA	NGLEY HES			UNIT E TAIL EFFECT	ARY PLAN WIND T	UNNEL (UPHT)		
ÆĒT	1 of 1						PLATE DATA			<del></del>	
				<del></del>					<del></del>		
	•										
		PART MAC									
	5	25 5-10	2.5	F15 F1	ED					<del></del>	
POINT	ALPHA	CNF	CH	CB	x CPF	YCPF				•	
1	-6.00	-0.0875		-0.0414	0.0204	0.4731					
<del>_{</del>	-4.00		-0.0015	-0.c316	2920-0	0.5603					
3	-3.00 -2.00	-0.0337 -0.0030	-0.0009	-0.0211	0.0254	0.6261 3.8000					
5	-1.00	0.0199	0.0005	-0.0008	0.0234	-0.0402					
- <del></del>	0.0	0.0469	0.0009	0.0085	0.0182	0.1812		······································			
	1.00	0.0695	0.0015	0.0172	0.0213	0.2475					
9	3.00	0.1239	0.0024	0.0395	0,0195	0.3188					
10	4.00	0.1506	0.0026	0.0505	0.0175	0.3349	<del></del>			- <del></del>	
11	6.00	0.2084	0.0023	0.0764	0.0108	0.3666					
<u> </u>	10.00	0.3326	-0.0002		-0.0007	0.3024					
14	12.00	0.3956	-0.0021	0.1500	-0.0053	0.3792		<del> </del>			
15 16	14.00	0.4549	-0.0040	0.1741	-0.0087 -0.0119	0.3827					
17	18.00		-0.0087		-0.0150	0.3775				· · · · · ·	
18	20.00	0.6432		26.45.0		0.3761					
20 20	22.00	0.7067		0.2658	-0.0207	0.3761 0.3649					
51	56.00	0.8381	-0.0203		-0.0242	0.3675	<del></del>				
55	28.00		-0.0234		-0.0259	0.3593					
53	0.6	0.0469	0.0009	0.0085	0.0182	0.1812				4-	
				<del></del>		<del></del>	<del></del>	· · · · · · · · · · · · · · · · · · ·			
			-				<del> </del>				
				<del></del>				<del> </del>	··		
										-	
										<del> </del>	
										•	
		<del></del>									

٠.

AGE .		•		L	ANGLE	PES	EARCH CENT	ER (NASA)	5 747: 5E	INITARY P	LAN HIND	TUNNEL (	PHT			
HEET	1 OF	1					-	RTIN MISSIL SPLITTE	R PLATE D	TA	A			<del></del>		<del></del>
								<del></del>	<del></del>				·····	·.·		
								····					,			
	TES 5	T P	ART MAC 23 1.50	H PX10-6	CONF F14		SITION RED							•		
			2 1 1 50	_ * • • •			ALU									
THIO	ALPHA		CNF	CH		CB		VCPF		<del></del>						
;	-6.00 -4.00		0.1049 0.0576	0.0059		0255	-0.0559	0.4137								
3	-3.00		0.0371	0.0033			-0.0861	0.4259						<del></del>		
Ā	-2.00		0.0221	0.0026			-0.1176	0.2036		•				•		
5	-1.00		0.0041	0.0017		0012	0.4065	0.2927								
<u> </u>	_ <u>0.0</u>		0.0247	0.0013		0086	0.0540	0.3482								
- (	2.00		0.0454	0.0007		0136 0216	0.0162 0.0	0.3047								
	3.00		0.0967	-0.0009		¥367	-0.0090	0.3795								
10	4.00		0.1232	-0.0014		0427	-0.0114	0.3466		·						
11	6.00		0.1746	-0.0029			-0.0164	0.3774								
15	8.00		0.5300	-0.0041			-0.0179	0.3681			<del></del>				<u> </u>	
13	10.00		0.2976 0.3643	-0.0059 -0.0079			-0.0199 -0.0218	0.35 <b>35</b> 0.3442				}				
15	14.00		0.4315	-0.0112		1+51	-0.0260	0.3363		-						
16	16.00		0.5126	-0.0169			-0.0329	0.3385								
17	18.00			-0.0201			-0.0341	0.3234								
18 -	20.00		0-6654	-0.023			0. <u>0.351</u> _	0+3191	<del></del> ,							
19	22.00		0.7398	-0.0273 -0.0310		2565	-0.0370 -0.0387	0.3215 0.3201	•							•
21	26.00			-0.035			-0.0404	0.3202								
22	28.00			-0.0381	0.	2970	-0.0416	0.3189								
53	0.0		0.0248	0.001	0.	2000	0.0511	0.2500				· · · · · · · · · · · · · · · · · · ·				
											<del></del>					
											•		•			
							<u></u>	·								
								•			-	•				
	- 6															
											-					
								<del></del>	<del></del>							
			·. <del></del>	····				<del></del>	<del></del>				<del></del>	<del></del>		
																•

			LA	NGLEY RES		ER (NASA)	UNITARY PLAN	A MIND TUNNEL (UPWT)	
	0f 1			<del>-</del>		SPLITTER	TAIL FFFECTS DATA		
				COAF TRAN					
	5	24 1.60	1.6	<u> F1+                                    </u>	XED	<del></del>	<del></del>		
	ALPHA	CNF	CH	Ce		YCPF			
		-0.0970		-0.0431 -0.0250	-0.0296 -0.0493	0.4443			
	-4.00	-0.0514	0.0025	-0.0176	-0.0750	0.4864		·	
	-2.00	-0.0107	0.0022	-0.0125	-0.2056_	1.1662			
•	-1.00	0.0047	0.0017	-0.0059		-1.2553			
<u> </u>	1.00	0.0200	0.0011	0.0008_ 0.0059	0.0567	0.0400		<del></del>	
1	2.00	0.0608	0.0005	0.0133	0.0099	0.2187			
	3.00	0.0761	0.0002	0.0200	0.0026	0.5658	<del></del>		
·	4.00	0.1016	-0.0001	0.0281	-0.0013	0.2766	···		
	6.00	0.1524	-0.0009	0.0466	-0.0057 -0.0095	0.3058 0.3315			
<del>-</del>	10.00	0.2596	-0.0032		-0.0123	0.3147			· · · · · · · · · · · · · · · · · · ·
	12.00	0.3114	-0.0052	0.1000	-0.0167	0.3211			
	14.00	0.3740	-0.0075	0-11-8	-0.050}	0.3070			
<del>,</del> —	16.00	0.4306	-0.0093	0.1314	-0-02 <u>17</u> -0-0237	0.3052			
	20.00	0.5492		0.1670	-0.0259	0.3041		•	
	22.00		-0.0167	0.1835	-0.0276	0.3024	•		
0.5	24.00	0.6646	-0.0201	0.2044	-0.0302 -0.0310	0.3076 0.3046		<del></del>	
5	28.00		-0.0225 -0.0253	0.2213 0.2391	-0.0325	0.3073			
3	0.0	0.0198	0.0013	0.0008	0.0640	0.0404	··-···		
		<del></del>						<del></del>	<u> </u>
	_								
		-		-					
								<del></del>	
		·				· · · · · · · · · · · · · · · · · · ·	<del>*-</del> · · · · · · · · · · · · · · · · · · ·		
							<del></del>		
		<del></del>	<u>`</u>			<del></del>	<del></del>		
								<u> </u>	
				<del>-                                    </del>				- · · · · · · · · · · · · · · · · · · ·	
		<del></del>					<del></del>	······································	<del></del>

				LA	NGLEY RES	EARCH CENT	R(NASA)	Lie	NITARY PLAN	N wIND TLINNE	LUBUTI		
	1 OF					AM	ATIN MISSIL	E TAIL EFFE	ECTS DATA	N WIND TUNNE			
EET	1 of	1				-	SPLITTE	R PLATE DAT	TA ·		•		
					<del></del>		<del></del>	·	<del></del>				
								<del> </del>					
	7E:	<b>ST</b> (	25 2.16	H RX10-6	CONF TRAM	XED ZITION							
					1000	10.1	10.000						
OINT	ALPH		CNF -0.0788	CH.	-0.0333	XCPF	YCPF			<u>.</u>			
2	-4.0		-0.0396	0.0019	-0.0157		0.3945						
3	-3.0		-0.0202	0.0017	-0.0094	-0.0A25	0.4653						
-	-2.0		-0.0004 0.0155	0.0011	-0.0033 0.0033	-2.8333 0.0258	0.1484						
6	0.0			-0.0003		-0.0076	0.2898						
7	1.0		0.0507	-0.0005	0.0177	-0.0105	0.3491						
-	3.0			-0.0009		-0.0126	0,3284						
10	4.0		0.1173	-0.0019		-0.0165	0.3478	•					
11	6.0			-0.0029	0.0560	-0.0174	0.3404						
.12. <u> </u>	10.0			-0.0043		-0.0205 -0.023Z	0.3481	<del></del>	<del></del>		<del></del>		
14	12.0		0.3034	-0.0083		-0.0272	0.3365						
15	14.0			-0.0111	0.1144	-0.0307	0.3177						
16 17	18.0		0.4080	-0.0131 -0.0157		0.03 <u>20</u> -0.0344	0 <u>.3125</u> 0.3117	<del></del>	<del></del>	<del></del>			
18	20.0		0.5120	-0.0183	0.1579		0.3084						_
19	22.0			-0.0209		-0.0370	0.3104						
<u>20</u>	24.0		0.6105	-0.0234	0.1922	-0.0389	0.3118			· · · · · · · · · · · · · · · · · · ·		<del></del>	
55	28,0		0.7324	-0.0291	0.2222	-0.0397	0.3034			-			
53	0.0	Ú)	0.0351	-0.0003	0.0102	-0.0076	9.2904		• • • • • • • • • • • • • • • • • • • •				
		_			<del></del> -								
				•				•					-
					<del></del>								
								<del></del>			• ·		
		_											
						<del></del>							<del> </del>

	1 OF 1					ER (NASA)		PERTE ALT	LAN WIND T				
	_ ~ 1		·			RTIN MISSILE	PLATE D				<del></del>	<del></del>	
						JELLIER	- FERIL U		<del></del>				
	TEST	PART HAL	H RA10-6	CONF TRANS					- 10				
	5	26 1.50	1.8	F13 FI	KED							·	
POINT	ALPHA	CNF	Сн	CH	ACPF	YCPF							
1		-0.2433		-0.1058	0.0579	0.4349							
2	-4.00	-0.1606	-0.0103	<u>-0.0696</u>	0.0644	0.4334							
3		-0.1087	-0.0067	-0.0475	0.0615	0.4370							
		-0.0615		-0.0243	0.0443_	_0.3951		<del> </del>	<del></del>		<del> </del>		
5	-1.00	-0.0094		-0-0035	-0.1737	0.3723							
<u> </u>	_0.0_	0.0-31	0.0053	0.0144	_0.1227	0-3341-						<del></del> -	
A	1.00	0.0990	0.0100	0.0384	0.1005	0.3879							
- 8	3.00	0.1514	0.0132	0.0577	0.0873	0.3811							
10	4.00	0.2428	0.0173	0.1072	0.0794	0.4209							
11	6.00	0.3486	0.0217	- 0.1460	0.0622	0.4188				<del>.</del>		<del></del>	
iż	8.00	0.4488	0.0224	0.1930	0.0499	0.4299							
13	10.00	0.5592	0.0212	0.2407	0.0370	0.4304						<del></del>	
14	12.00	0.6338	0.0196	0.2810	0.0309	0.4433					•		
15	14.00	0.7316	0.0164	0.3217	0.0224	0.4395					<del>- · · · · · · · · · · · · · · · · · · ·</del>	· ••	
-16	16.00	0.8175	0.0122	0.3559	0.0149	0.4351							
17	18.00	0.8949	0.0063	0.3863	0.0093	.0.4316				· · · · · · · · · · · · · · · · · · ·		· · · · · · ·	
18	20.00	0.9855	0.0022	0.4203	\$500.0	0.4265						· · · · · · · · · · · · · · · · · · ·	
10	22.00	1.0665	-0.0043	0.4503	-0.0040	0.4223							
20	24.00	1.1474	-0.0108	0.4774	-0.0094	0.4161			<del></del>				
51	26.00		-0.0170	0.4793	-0.0138	0.4061							
55	28.00		_0.050s	0.5180	-0.0157_	0.4033							
23	0.0	0.0474	0.0050	0.0176	0.1050	0.3713							
							<del></del>			<del></del>			
		<del></del>			·-··				-			<del></del>	
						_							
					·	<del></del>					<del> · · · · · · · · · · · · · · · · · ·</del>		
									•				
								-		<u>.</u>			
			•								•		
											•		
<del>-</del> ,													
•					•								
		· · · · · · · · · · · · · · · · · · ·		·····		<del></del>							
									• •				_
					-								_

POINT 1	5	PART MACI 27 1.60	H RX10-6	CONF TRAN		SPLITTER	PLATE DA	TA	<u> </u>	<del></del>	-	<del>-</del>
POINT	TEST 5		H RX10-6	CONF TRAN	e I e I ou							
5	5		H RX10-6	CONF TRAN	£ [ 2 ] On							
2	5		H RX10-6	CONF TRAN	£1110m							
5	5		1.0			<del></del>						
5	ALPHA	(0)		F13 F1	#ED							
5	ALPHA											
2	-6.00	CNF 0.2176	CH	-0.1037		<u>YCPF</u>		<del> </del>				
	-4.00	-0.1443	0.0001	-0.0664	-0.0004	0.4602						
3	-3.00	-0.1004	0.0005	-0.0484	-0.0023	0.4821		• • • • • • • • • • • • • • • • • • • •				
•	-2.00	-0.0562	0.0005	-0.0316	-0.0097	0.5623						
5	-1.00	-0.8170	0.0006	-0.0126	-0.0366	0.7412						
- 🐓	1.00	0.0623	0.0003	0.0049	0.0139	0.2197 0.3172		<del></del>				
Ď.	2.00	0.1061	0.0005	0.0376	0.0013	0.3563						
9	3.00	0.1455	0.0005	0.0560	0.0032	0.3904						
10	4.00	0.1645	0.0005	0.0771	0.0030	8.4179						
11	6.00	0.2673	0.0012	0.1126	0.0047	0.4212			•			
13	_ 6.00	0.3500	0.8019	0.1495	0.0056	0.4271						<del></del>
14	10.00	0.5215	0.0024 0.0028	0.1041	0.0055 0.0054	0.4203 0.4241						
15	14.00	0.6012	0.0029	0.2523	0.0050	0.4196						
16	16.00	0.6710	0.0023	0.2879	0.0034	0.4290						
17	18.00	0.7458	0.0016	0.3153	0.0022	0.4227						
18	\$0.00	0.816 <u>)</u> _ 0.8876	-0.0001 -0.0028	0.3451	0.0001	0.4228	<del></del>	-	<del></del>		<del></del>	
50	24.00	0.9553	-0.0066	0.3721 0.3987	-0.0032	0.4192 0.4174	•					
21	26.00	1.0191	-0.0105	0.4209		0.4131						
55	28.00	1.0819	-0.0144	0.4470	-0.0133	0.4132						
23	0.0	0.0268	0.0003	0.0053	0.0116	0.1978						
					-							
			<del></del>									
										<del></del>		
										<del></del>		
							- '					

			LA	NGLEY RES	EARCH CENT	ER (MASA)	UNITARY PLAN WIND TUNNEL (UPWT)
E	1 OF 1				HA	SPLITI SPLITI	LE TAIL EFFECTS DATA ER PLATE DATA
							•
	TEST	PART MAC	H #X10-6	CONF THAN	SITION	<del>:</del>	
	5	28 2.16	2.5	<u>F13</u>	XED		
DINT	ALPHA	CNF	Сн	Ca	<b>XCPF</b>	YCPF	
1	-6.00	-0.1482	0.0023	-0.0692	-0.0157	0.4669	
₹_	-4.00	-0.0/70	0.0014	-0.0413		0.5364	
•	-2.00	-0.0501 -0.0165	0.0007	-0.0259 -0.0122		0.5170 0.7394	
5	+1.00	0.0175	0.0002	0.0016	0.0133	0.0914	
•-	0.0	0.0476	-0.000 <u>1</u>	0.0151.	0.0016	0.3159	
á	1.00	0.1215	-0.0002	0.0476	-0.002 <b>0</b> -0.0051	0.3813 0.3905	
9	3.00	0.1455	-0.0009	0.0594	-0.0059	0.4082	
10	0 <u>0</u>	0.1796	-0.0013	0.0732	0.0074	0.4076	
11	6.00	0.2469 0.3177	-0.0018	0.1029	-0.0072	0.4168 0.4183	
i5—	10.00	0.3685	-0.0021	0.1640		0.4221	
14	12.00	0.4525	-0.0023	0.1935	-0.0052	0.4275	
15	14.00	0.5273	-0.0032	0.2529	-0.0043 -0.0054	0.4226	
16 17	18.00		-0.0032		-0.0074	0.4263	
18	20.03	0.7381	-0.0061	0.3068	_0.0082	0.4156	
19	27.00	0.8106	-0.0083	0.3336		0.4115	
<u>20</u>	26.00	0.8826	-0.0110 -0.0139	0.3590	-0.0125	0.4066	
55	28.00		-0.0177	0.4087		0.4018	
23	0.0	0.0509	0.0001	0.0175		0.3436	
							·
							· ·
		<del></del>	<del> </del>		<del> </del>		
					<del></del> -		
							·

					<del></del>	<del></del>	<del></del>	····	<del></del>	<del></del>	
			LA	NGLEY RESI	EAHCH CENT	ER (MASA)	UNIT	ARY PLAN WI	NO TUNNEL (UP	17)	W T
GE	1 OF 1				44	ATIN MISSILE	TAIL EFFECT	IS DATA			
	1 OF I						PLATE DATA	•			
				<del> </del>			•				
	7561	PART MAC	W EV10-4	FOUR TORK	E V T V Deu						
	5		1.8								
				<b></b>	•••						
O I MT	ALPHA	CNF -0.2252	CH	-0 -0943	0.1319	VCPF 0.4187					
2	-4.00	-0.1460	-0.0213	-0.0627	0.1439	0.4236	·				
3	-3.00	-0.0433	-0.0149		0.1597	0.4362				<del></del>	
5	-1.00	0.0052		-0.0233	0.1499 _0.0769	0.5011 -0.7308					
6	0.0	0-0516	0.0075	0.0209	0.1453	0.4050					
7	1.00	0.0484	0.0145	0.0398	0.1474 0.1502	0.4045					
9	3.00	0.2057	0.0286	0.0617	0-1390	0.3972	<del> </del>	<del></del>			
10	4,00	0.2391	0.0330	0.1063	0.1380	0.4446			·		
11	6.00	0.3347	0.0406	0.1981	0-1213	0.4425					
13 -	10.00	0.5210	0.0451	0.2373	0.1025	0.4326					<del></del>
14	12.00	0.6127	0.0509	0.2793	0.0631	0.4559 .					<u>.                                  </u>
15 16	14.00	0.7046	0.0509	0.3826	0.0722	0.4578					
17 -	18.00	0,8679	0.0520	0.3495	0.0579	0.4603	<del></del>				<del>.</del>
18_	20.00	0.9430	0.0517	0.4372	0.0548	0.4636					
50	22.00	1.0276	0.0505	0.4700	0.0491	0.4574					
21	26.00	1.1739	0.0-10	0.5365	0.0349	0.4570		· <del></del>			
SS	28.00	1.2421	0.0323	0.5612	0.0260	0.4518					
23 24	0.0	0.0655 0.0515	0.0075	0.0179	0.1145	0.2733 0.37 <b>67</b>					
			000073	000274		V 0.3, 0.1					
								•			
					<del></del>				*********	- <i>-</i> . <del></del> -	<del></del> -
							-	•	· · · · · · · · · · · · · · · · · · ·	<del></del>	
								<del></del>			

105	1 OF	,		LA	NGLEY RES	ARCH CENT	ER (NASA)	UNITARY PLAN WIND TUNNEL (UP	ut)
	1 07		<del></del>	<del></del>			SPLITTER	PLATE DATA	•
<u>-</u>									
					46			· · · · · · · · · · · · · · · · · · ·	
	1E:				CONF TRANS				
	10000		The cons		67.7	Lange de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant de la constant	T - 19 -		
POINT	_ALPH	<u></u>	CNF	CH	-0.0802	0.0343	7 YCPF		
5	-4.0		11721	-0.0045	-0.0612	0.0377	0.5126		
3	-3.0			-0.0036	-0.0428	0.0422	0.5018	<del></del>	· · · · · · · · · · · · · · · · · · ·
4	-2.0			-0.0022	-0.0263	0.0523	0.6247		
-5-	-1.0	0 -	0.0034	-0.0013	-0.0074	0.3824	2.1765		
6	0.0		0.0356	-0.0004	0.0102	-0.0112	0.2865		
7	1.0		0.0792	0.0010	0.0254	0.0126	0.3207		
8	2.0		0.1134	0.0019	0.0425	0.0168	0.3748		
9	3.0		0.1565	0.0032	0.0004	0.0204	0.3859		
10	4.0		0.1908	0.0046	0.0803	0.0241	0.4209		
11	6.0		0.2750	0.0073	0.1193	0.0263	0.4291		
12	8.0		3605	0.0113	0.1581	0.0313	0.4386	·	
13	10.0		0.4556	0.0162	0.1963	0.0356 0.0428	0.4309		
15	14.0		0.6156	0.0301	0.2769	0.0489	0.4497		
16	16.0		0.6941	0.0337	0.3109	0.0486	0.4479		
17	18.0		0.7643	0.0346	0.3440	0.0453	0.4501		
18	20.0		0.8300	0.0343	0.3779	0.0413	0.4553		
19	zz.0		0.9084	0.0326	0.4109	0.0359	0.4523		
20	24.0		0.9773	0.0318	0.4431	0.0325	0.4534		
21	26.0	0	1.0430	0.0314	0.4726	0.0301	0.4531		
22	28.0		1.1099	0.0302	0.4996	0.0272	0.4501		
23	0.0		0.0357			-0.0112	0.2465		
24	10.0	0	0.4540	0.0165	0.1971	0.0363	0.4341		
						·			
					_				
							·		
						••			
								<del></del>	

	1 OF 1		LA	NGLLY RESE	APCH CENT	ER(MASA) RTIN MISSILE SPLITTER	TAIL EF	FFECTS 01	PLAN WIN	D TUNNEL	(UPUT)		
						. 3762112-		<u></u>					
		PART MAC	H RX10-6	CONF TRANS	ITION								
	5	31 2.16	_5•2	F16 F1	KED		•		-		·		<del></del>
	ALPHA	CNF	CH	C6_		YCPF							
<u> </u>		-0.1087		-0.0528	0.0258 0.0317	0.4857				-			
<del>- {</del>	-4.00	-0.0757	-0.0024	-0.0370 -0.0234	0.0493	0.4888		-			<del></del>		
4	-2.00	-0.0093	-0.0014	-0.0085	0.1505	0.9140							
5	-1.00	90506	-0.0003	0.0040	-0.0144	0.1923	•						
·	1.00	0.0507	0.0001	0.0186 0.0320	0.0020	0.3669					<del></del>		
8:	5.00	0.1139	0.0011	0.0458	0.0097	0.4021						_	
9	1.00	0.0838	0.0008	0.0356	0.0095	0.4248							
10	3.00	0.1104	0.0012	0.0476	0.0109	0.4312 0.4196	<del></del> ,-					·	<u> </u>
iż	4.00	0.1770	0.0026	0.0773	0.0147	0.4367							
13	6.00	0.2439	0.0037	0.1082	0.0152	0.4436						-	
15	10.00	0.3140	0.0047	0.1403	0,0150 0.0168	0.4468		<del></del>		<del></del>	<del></del>		
16	12.00	0.4568	0.0082	0.2058	0.0160	0.4505							
17	14.00	0.5336	0.0103	0.2419	0.0193	0.4533			<del></del>			<del></del>	
18 19	16.00	0.6177	0.0134 0.017B	0.2745	0.0217_	0.4444	<del></del>						
50	18.00 20.00	0.7700	0.0255	0.3446	0.0256	0.444 <b>5</b> 0.4475		,					
21	22.00	0.8432	0.0235	0.3757	0.0279	0.4456		<del></del>					
22	24.00	0.9103	0.0243	0.4074	0.0267	0.4475				<del></del>	<del>-</del>		
23 24	26.00	0.9741 1.0355	0.0240 0.0230	0.4386	0.0246 0.0222	0.4505 0.4519						-	
25	0.0	0.0540	0.0004	0.0189	0.0074	0.3500				<del></del>		<del></del>	
•										•	,		
			· · · · · · · · · · · · · · · · · · ·										
· <b>_</b>					•				· · · · ·	<del></del>			
													-
										<del></del>			<del> </del>
													• • • • • • • • • • • • • • • • • • • •

Listing of Part Numbers for the Tabulated Data of Test No. 1*

							T	· .										Par	Num	ber						
CONF	L	DELI	DEL2	DEL3	DEL4	PHI	TRANSITION	R x 10 ⁻⁶	α	B	Moo	Mao	Mœ	Mao	Mœ	Mœ	MΦ	Moo	Mæ	M∞	Mæ	Mes	Moo	Wee	M _∞	Mœ
											0,20	0.40	0.50	0.60	0,80	0.85	0,92	0.94	0.95	0.96	0.98	1,00	1,05	1.10	1.20	1,30
B4WOFI2	0-	0	0	0	0	0	Unknown	2.3	Vary	0					4	5	3	9		10	(14)		15	(1)	17	18
B4WOF13	H	1		$\Box$	$\sqcap$	11	<del>                                     </del>			Ħ					(22)	24	(30)			32	(33)		34	(35)	(36)	(37)
B4WOFI6	T		$\Box$	1 1-						Ħ					(42)	43	(44)			46	(47)		48	(49)		(31)
B4WOF22				T  -	П	$\sqcap$				П					(57)	58	<b>(61)</b>				(62)			(64)	(65)	
B4W0F23	П	П		1 1						П				L	(71)	72	(73)				(74)			(3)	(76)	$(\pi)$
B4WOF21	П	П			П	П				П					(82)	83	(84)				(87)			(S)	(9)	(92)
B4WOF35	7		П												(19)	98 106	99				(00)			<b>(B)</b>	(D)	<b>®</b>
<b>B4W0F34</b>	H		1 1		☆ `	11				Ħ.	1				(II)	112	(115)				(11)			(18)	(11)	(120)
B4WOF33										П	1				(125)	126	(127)	128		129	(31)			(132)	(133)	(34)
B4WOF32										П					(39)	140	(41)			1 43	(144)			(50)	(151)	(52)
B4WOF31	$\prod$	П	П							П					(56)	157	(58)				(159)			6		(62)
B4WOFII	$\prod$	L .	-	•						$\prod$	[ - <u>-</u>				(66)	167	(68)	169		170	(171)			(12)	(13)	(74)
B2WOF0	П	OFF	OFF_	OFF	OFF					П	[				(78)	179	(80)				(181)			(182)	(183)	(184)
B5WOF0	Ш								$\Box$	П					(87)	188	(189)				(190)			(P)	(192)	(193)
B4WOF0	Ш	oxdot		$\Box$		Ш		<u> </u>	1	Ш	L			↓	(96)	197	(198)				(199)			(200)	(201)	(202)
	Ш	Ш	$\perp \perp$		L.I	$\Box$		Vary	23,5	Ш	ļ		205	<u> </u>		<u> </u>	-	<b>!</b>		L			L			
L	Щ	lacksquare	$\sqcup$	$\sqcup$	$\sqcup \sqcup$	$\sqcup$		oxdot	12.0	Ш					<u> </u>				206	<u> </u>	L		L	-		
	Щ	$\sqcup \!\!\!\!\!\!\perp$		<u> </u>	oxdot	<del>    -</del>	<b>├</b>		9.0	1		-	L		016	L	_		<u> </u>	L		010				207
	ᄔ	<b>↓</b> .↓ .	$\perp \perp$		$\sqcup \!\!\! \perp$	₩.	<del>                                     </del>	3.9	3 <u>0.0</u>	11	200	210		211	212	₩			<u> </u>			213	016	015	214	1100
	Щ	$\vdash$	<del>                                     </del>	<b>⊢</b> ↓_	Н.	₩.	<del>  </del>	2,0	1 1	₩	220	219		218	217	<b>-</b>	<u> </u>		<u> </u>	<u> </u>	l —		216	215		ļI
•	<u> </u>			⊥ '_	<u> </u>	. •	<u> </u>	3.8	Vary	Ľ	I	223	L	l _					<u>L</u>	L				L .		ш

^{*} No Tall Fin Data Presented

Listing of Part Numbers for the Tabulated Data of Test No. 2*

		Г	T				-			l ·		1		Т	7				Р	art Nu	ımber			
COP	(F	lı	Ь	ELI	DE	12	DEL	3	DEL4	PHI	TRANSITION	R x 10 ⁻⁶	α	1	3	Moo	Mœ	Moo	Mes	Mag	Mao	Mag	Mao	Mag
													-	'	1	0.59	0.80	0.85		0.98	1.10	1.20	1.29	1.30
		╁.	+	_	<u> </u>	_	_			<del> </del>			<u> </u>	+	1					<del>                                     </del>		1.20	<del>""</del>	
83W(	)FO	0	49	)FF	O	FF_	OF	F	OFF	0	Free	0.3	Vary	49	븬	7	┝	_	-			1	<u> </u>	├
		H	t	1	Н		H	٦		<del>   </del>		0.7	╁	Ħ	Н	8	<del>                                     </del>	-	-		<del>                                     </del>			┈
		П	T		П							1.1		П	Ц	9								
		₩.	╀	↓_	Н	Ţ	Н	4		ļ ļ	<b>-</b>	1.3	<b>├</b> -	44	Ц	10	<u> </u>	ļ		<u> </u>		<b>-</b>	<u> </u>	<del> </del>
		₩	╀	╀	Н	$\vdash$	₩	-		<del>                                     </del>		1.8 2.6	╀	╫	Н	12	-	-			-	<del> </del> -	<del> </del>	<del>                                     </del>
		П										3.5_		Ħ	Ħ	14_							<b></b>	
		П	L		Ц		$\Box$			Ш.		4.3		П	Ц	15			L					
83W(	FIS	₩	╀	<u>'</u>	님	<u>'</u>	ö	$\dashv$	0	<del>                                     </del>	Fixed	0.3		╫	H	16 24			<u> </u>	-		<del> </del> -	<b></b> -	├—
1	-1 13	H	t	Ť	H	_	ΙŤ		Ť	<del>                                     </del>	I	0.4	+	Н	Н	26				$\vdash$	╅	<del>                                     </del>	$\vdash$	<del>                                     </del>
		П										0.7		$\blacksquare$	П	27								
		#	↓-	_	Н	$\vdash$	${oldsymbol{arphi}}$	_	$\vdash \vdash$	<del>                                     </del>	<del>                                     </del>	1.1	⊢Ļ	4	H	31	<del> </del>		<b> </b>		₩	ļ	<u> </u>	<u> </u>
		₩	╁	1	Н	-	┝┤	-	⊢┼	<del>   </del>	<del>                                     </del>	3.4	++	+	Н	32 33	$\vdash$	<del>                                     </del>	-	<del>                                     </del>	<del>                                     </del>	+	$\vdash$	╁
		I	İ	L			ㅂ		廿	180		0,3	$\Box$	$\bot$	Ħ	36								
		П	F	F	Г	$\Box$	П	$\Box$				0.4	$\Box$	$\perp$	П	37								$\vdash$
		₩	╁	╫	H	$\vdash$	$\vdash$	-	$\vdash$	╢	<del>                                     </del>	0.7	╁┼	+	Н	_ <u>38</u> 39	_	$\vdash$	1	<del>                                     </del>	<del>                                     </del>	├──		├
$\neg$		Ħ	t	╁	H	H	H	_	H		1 1	1.3	H	$\dagger$	H	40		$\vdash$		1	<del>                                     </del>	+		一
		П	L				$\Box$					3.4	П	T	П	41				<u> </u>	L			
		H	╀	╄	Ļ	L	H		-	0	Free	0.4	┵	4	Н	47	<u> </u>	ļ	<del> </del>	<b></b>	<b>}</b>			ــــ
_		₩	╁	+-	┢	┝	╁	_	$\vdash$	+		0.7	╂═┼╴	┿	Н	48		├	<del> </del>	<del> </del> -	┼	<del> </del>	-	┢
		Ħ	t	T	T							3.4		T	Ħ	50	2111					t		匸
6000	2514	$\coprod$	L	$\perp$	L		$\Box$		Ļ	<del></del>		2.5	П	4	Н		(57)	58	(39)	(60)	<u> </u>	(2)	63	<del> </del>
B3W		₩	╁	╁	╁	┝	┨		H	+	+ + -	++	$\vdash$	+	Н		(69) (80)	70 81		(13)		(74) (85)	├	(73) (86)
B3W		Ħ	t	╁╴	T	┢	Н		$\vdash$	<del>                                      </del>	1 1	<del>                                     </del>	† †	十	Ħ		(91)	92	(B)	(%)	(93)	(%)	<del>                                     </del>	(%)
B3W(	OF32	T	Τ	ŧ		<u> </u>			1				1	Ţ	Ī		(05)	106	107	(08)	(09)			(II)
										Splitter Plate Offset				ı			-		M =55					
		L			1				L	Angle									ļ	1				1
BOW	<u> OF14</u>	F	Ŧ	_	Ŀ	=	ļΞ	=	_	0	Free	2.5	Var	7	Ш		(23)	155	962	(71)	(30)	(144)	L	(37)
	├	╁	╁	+-	╁	+	┨	_	<del>l i</del> -	30	<del>                                     </del>	<del>                                     </del>	╂┼	╬	t	-	(124)	156	180	(72)	(31)	(45)	<del> </del>	(120)
		${\dagger\dagger}$	士	$\pm$	t	t	╁┤	_	-	60	<u>                                     </u>	<del>                                     </del>	+	+	t	<u> </u>	125	157		(73)	(132)	146	$t^-$	(38) (39)
		П	I	T	Γ	Ľ				90			П	I	L		(26)	158	(167)	(74)	((33)	(47)		(40)
	-	₩	+	+	╀	╁	Н	_	╌	120	<del>                                     </del>	₩.	╀┼	<del>-</del>	H		(127) (128)	159	166	075		(148)	├	(42)
	-	╁	+	$^{+}$	t	t	H	H	++	180		<del>                                     </del>	++	+	t	-	029	161		1378	V 22)	1030	<del>                                     </del>	100
BOW	OFIL	П	I	I	Γ		П			0			$\Box$	I	I		(184)	194	(201)	(272)	(279)	(287)		(296) (295)
	<del>-</del>	H	+	+	F	Ë	$\square$		$\Box$	30		$+$ $\Gamma$	+	$\perp$	Į.		(185)	195	202	273	280	(288)	ļ	1895
	$\vdash$	╁┼	+	+-	+	╁	╁┤	-	╁┼	90	<del>                                     </del>	<del>  </del>	+	+	╁	-	(186) (187)	196	188	(274) (275)	<b>188</b>	(289) (290)	+	(296) (297)
		H	1	土	İ	İ	Ħ	╚	口	120			廿	士	T		1880	198	269	(276)	(283)	(291)	<u>L_</u>	298
		П	T						Π	150		T	$\prod$	Ţ	Γ		189	199	270	क्त		(202)		299
<u> </u>	$\vdash$	H	╁	+	+	+	Н	$\vdash$	$\vdash$	180		+	++	+	+		100	200		(270)	(285)	(202)	<del> </del>	(200
BOW	OF36	#	+	十	十	+	+	-	╁	0	<del>                                     </del>	<del>    -</del>	†-†-	╅	†		(190) (206)	215	221	(278) (230)	246	247	1	858888888
	Ĺ	ɒ	1	土	Ĺ					15			1	ユ	İ							i .		258
	ļ	Ц	1	1	L	L	П	Ĺ	$\Box$	30	<del> </del>	<del>                                     </del>	+	$\bot$	Ţ		(209) (210)	217	1224	(231)	(241)	(248)	<u> </u>	259
-	┼	₩	+	+-	╀	+	+	$\vdash$	┼┼	90	<del>                                     </del>	+ +	╁┼	+	+		(210) (211)	218 219	183	(34)	(242)	(24V)	$\vdash$	1200
	1	$\dagger \dagger$	+	+	十	+	Н	┢╌	+	120		<del>  </del>	++	+	t		(212)	220	227	236	24	(248) (249) (250) (251) (251) (253)	+-	262
		I	_	$\perp$	I	I	$\Box$		$\Box$	150			$\Box$	I	Ţ		(212) (214)	221	(228	(23)	(245)	(252)		(263)
	ŧ	1		i	L	•	1	•	_ f	180	_ •		1 •	┙	<u> </u>		(214)	222	(229	(238)	(246)	(253)	L	J (264)

^{*} After Part Number III, Only Splitter Plate Data Presented

# AEUC-1X-/5-125

Listing of Part Numbers for the Tabulated Data of Test No. 3*

												Part N	umber	
CONF	L	DELI	DEL2	DEL3	DEL4	PHI	TRANSITION	R x 10-6	α	β	Mœ	M∞	Moo	M∞
					L						2,36	2.86	3,95	4.63
BIWOF35	0	0_	0	0	0	0	Fixed	3.0	  Vary	0	(19)	(22)	(24)	25)
			•		•	45				Ц	(20)	(21)	(23)	(26)
		+	-20	•	-20	0				Ш	27	28	29	30
		20		20		45		2.5			31			
								3.0				32	33	34
BIWOF34								2.5		П	35			
201817				•		1		3.0		П		36	37	38
		0		0		. 0				П	39	40	41	42
BIWOF33		+		+		+		T-		П	43	44	45	46
1		20		20		45		2.5		П	47			
		+	1	+		+		3.0		П		48	49	50
		0	0	0	0	0		2,9		П	(51)			
		1				45		+		П	(52)			
				$\sqcap$	<del>                                     </del>	1		3.2	$\Box$	П		(53)		
				<del>                                     </del>		0		•		$\Pi$		(54)		90390.0
						45		3.0				1	(55)	(58)
						0		ī		П			(56)	(57)
BIWOF34										П	(59)	(62)	(64)	(65)
1	-					45				T	(60)	(61)	(63)	(66)
BIW1F34	15, 42					+					68	69	71	74
	1	-				0				П	(67)	(70)	(72)	(3)
		0	-20	0	-20	1	<del>                                     </del>				75	76	77	78
		20	ī	20	1	45		2,5		1	79	<del></del>		
		1		1		Ť		3.0				80	81	82
BIW IFO		OFF	OFF	OFF	OFF			1		H	84	85	89	92
1			i			0					(83)	(86)	(90)	(91)
BIWOF0	0		<b>—</b>	-	1	1	<del></del>	-	-	1	(33)	(94)	(95)	

^{*} No Tail Fin Data Presented

## Listing of Part Numbers for the Tabulated Data of Test No. 4*

												Part N	umber	
CONF	L	DELI	DEL2	DEL3	DEL4	PHI	TRANSITION	R x 10 ⁻⁶	α	β	M _∞	M∞	Mω	Mα
											2.36	2.86	3.95	4.63
B2WOF34	0	0	0	0	0	0	Fixed	3.0	Vary	0	(2)	(3)	(7)	(8)
+						-90	ī		1	I	3	4	6	9
B2WOF35						0					(12)		(13)	(0)
B2WOF33			•								(16)	(17)	(14)	(15)
B2WOF34			-20		-20						18	19	20	21
B2WOF35					ī					П	22	23	24	25
B2WOF33		1	1	Ŧ	1	•						26		
		20	0	20	0	-90						28	29	30
		1		ı	1			2.0			27	0.50		
B2WOF31								3.0		П	(34)	(35)	(36)	(37)
B2WOF32											(38)	(39)	(40)	(41)
B2WOF36	1	•	•	•		•	· ·		•	V	(43)	(42)	(44)	(45)

^{*} No Tail Fin Data Presented

AEDC-TR-75-12

Listing of Part Numbers for the Tabulated Data of Test No. 5*

,		T													Pa	art Nur	nber
CONF	L	D	ELI	DE	L2	DEL3	}	DEL4	PHI		TRANSITION	R x 10 ⁻⁶	α	ß	M _∞	M∞	M∞
															1.50	1.80	2.16
B0WOF35	-			_	_						Fixed	1.8	Vary	_	(2)	(3)	
1	ī		Ī				$\neg$			1	1	2.5					(4)
BOWOF34		T					Ī			1		1.8			(5)	(6)	
•	П	1								1		2.5					(7)
BOWOF3I	П	T					1			1		1.8			(8)	(9)	
		T	1				1			1		2.5		П			(10)
BOWOF32	П		İ				7			1		1.8				(12)	
1							1			T		2.5			54 10	1 10 A	(13)
B0W0F36	П	Ť								T		1.8			(14)	(15)	
•	П		1				1			1		2.5					(16)
B0W0F11	П									1		1.8			(17)	(18)	192
<b>↓</b>		Т					1			1		2.5		П			(19)
BOWOF15	П									1		1.8		$\prod$	(20)	(21)	
<b>+</b>	П	Τ										2,5			F20	- T	(22)
BOWOF14		Τ					7			Ī		1.8		$\prod$	(23)	(24)	
1							┪			T		2.5		П			(25)
BOWOF13							1					1.8			(26)	(27)	
1		Τ					7			Ī		2.5		П			(28)
BOWOFI6		Γ					7			1		1.8			(29)	(30)	
<b>♦</b>	1	Ĺ	V		<b>↓</b>	•		1	1		<b>.</b>	2.5		T		13/5	(31)

^{*} Only Splitter Plate Data Presented

### **NOMENCLATURE**

A Streamwise length of beveled portion of fin leading edge, in. (see Fig.

6)

ALPHA (a) Model angle of attack, deg

AR Fin aspect ratio,  $b^2/S_{\Gamma}$ 

B Streamwise length of beveled portion of fin trailing edge, in. (see Fig.

6)

BETA  $(\beta)$  Model angle of sideslip, deg

b Tail fin span, measured from the root chord to the tip, in. (see Fig.

6)

CA Axial-force coefficient, measured axial force/q_S

CAB Base axial-force coefficient,  $(p_{\infty} - p_b)/q_{\infty}$ 

CAF Forebody axial-force coefficient, CA - CAB

CB Splitter plate tail fin root bending-moment coefficient, fin bending

moment/q_S_F b

CB1, CB2, Root bending-moment coefficient of tail fins No. 1, 2, 3, and 4,

CB3, CB4 respectively, fin bending moment/q_S_F b

CH Splitter plate tail fin hinge-moment coefficient, hinge moment/q_S_FC_R

CH1, CH2, Hinge-moment coefficients of tail fins No. 1, 2, 3, and 4, respectively,

CH3, CH4 fin hinge moment/ $q_m S_F C_R$ 

CLL Rolling-moment coefficient, rolling moment/q_Sd

CLM Pitching-moment coefficient, pitching moment/q_Sd (moment

reference point located on centerline at 50 percent of model body

length)

CLN Yawing-moment coefficient, yawing moment/q_Sd

CN Normal-force coefficient, normal force/q_S

CNF Splitter plate tail fin normal-force coefficient, fin normal force/q_S_F

CNF1, CNF2, Normal-force coefficient of tail fins No. 1, 2, 3, and 4, respectively,

CNF3, CNF4 fin normal force/q_sS_F

CONF Model configuration identification

C_R Tail fin root chord, in. (see Fig. 6)

C_T Tail fin tip chord, in. (see Fig. 6)

Cy Side-force coefficient, side force/q_S

d Model body maximum diameter, in. (see Fig. 3)

DEL1, DEL2, Deflection of tail fins No. 1, 2, 3, and 4, respectively, deg

DEL3, DEL4

L Distance between model nose and the intersection of the wing leading

edge with the body (measured parallel to the body centerline), in.

MACH (M_m) Nominal free-stream Mach number

PART Data indexing number

PHI Model roll angle, deg

POINT Data indexing number per part number

pb Average static pressure at model base, psfa

p Free-stream static pressure, psfa

q Free-stream dynamic pressure, psf

R Nominal Reynolds number per foot

S Maximum body cross-sectional area, ft²

S_F Tail fin planform area, ft² (see Fig. 6)

TEST Test identification number

T_R Tail fin root thickness, in. (see Fig. 6)

TRANSITION Transition identification

X Distance from fin root chord leading edge to fin hinge line, in. (see

Fig. 6)

XCP Missile body center-of-pressure location, CLM/CN

XCPF Splitter plate fin longitudinal center-of-pressure location, CH/CNF

XCPF1, XCPF2 Longitudinal center-of-pressure location of tail fins No. 1, 2, 3, and

XCPF3, XCPF4 4, respectively, hinge moment/fin normal force

YCPF Splitter plate fin lateral center-of-pressure location, CB/CNF

YCPF1, YCPF2 Lateral center-of-pressure location of tail fins No. 1 2, 3, and 4,

YCPF3, YCPF4 respectively, root bending moment/fin normal force

Λ Tail fin leading-edge sweep angle (see Fig. 6)

 $\lambda$  Tail fin taper ratio,  $C_T/C_R$